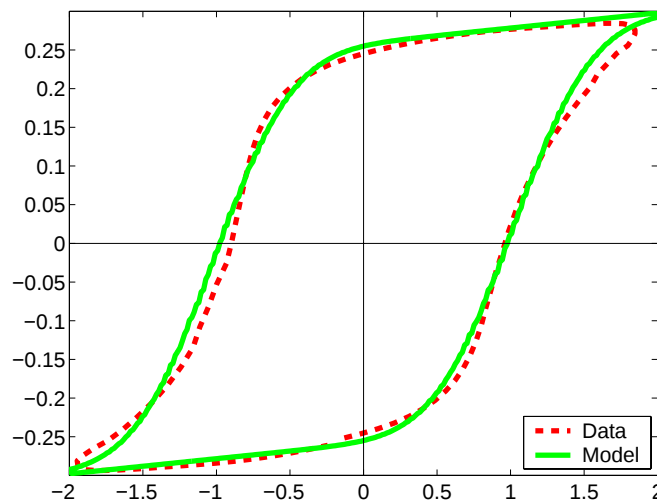


A UNIFIED MODEL FOR HYSTERESIS IN FERROIC MATERIALS

Ralph C. Smith

Department of Mathematics
North Carolina State University

- Marcelo Dapino, Ohio State University
- Zoubeida Ounaies, Virginia Commonwealth University
- Stefan Seelecke, North Carolina State University



Research Support:

Air Force grant AFOSR-F49620-01-1-0107

NASA grant NAG-1-01041

NSF grant CMS-0099764

Report Documentation Page				Form Approved OMB No. 0704-0188	
Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.					
1. REPORT DATE 00 JUN 2003		2. REPORT TYPE N/A		3. DATES COVERED -	
4. TITLE AND SUBTITLE A Unified Model For Hysteresis In Ferroic Materials				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)				5d. PROJECT NUMBER	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Department of Mathematics North Carolina State University; Ohio State University				8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)				10. SPONSOR/MONITOR'S ACRONYM(S)	
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)	
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release, distribution unlimited					
13. SUPPLEMENTARY NOTES See also ADM001697, ARO-44924.1-EG-CF, International Conference on Intelligent Materials (5th) (Smart Systems & Nanotechnology)., The original document contains color images.					
14. ABSTRACT					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT UU	18. NUMBER OF PAGES 17	19a. NAME OF RESPONSIBLE PERSON
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified			

TALK OVERVIEW

I. Smart Material Applications

- **Piezoelectrics** – Tunable lenses, nanopositioning
- **Shape Memory Alloys** – Shape modification
- **Magnetostrictives** – High force transduction

II. Modeling Hierarchies

- Develop energy relations at lattice level for single crystal, homogeneous compounds.
- Incorporate polycrystallinity and material nonhomogeneities through stochastic homogenization to obtain macroscopic constitutive relations.

III. Experimental Validation

- PZT5A – Major and biased minor loops
- Terfenol-D – Major and biased minor loops
- SMA – Thin film

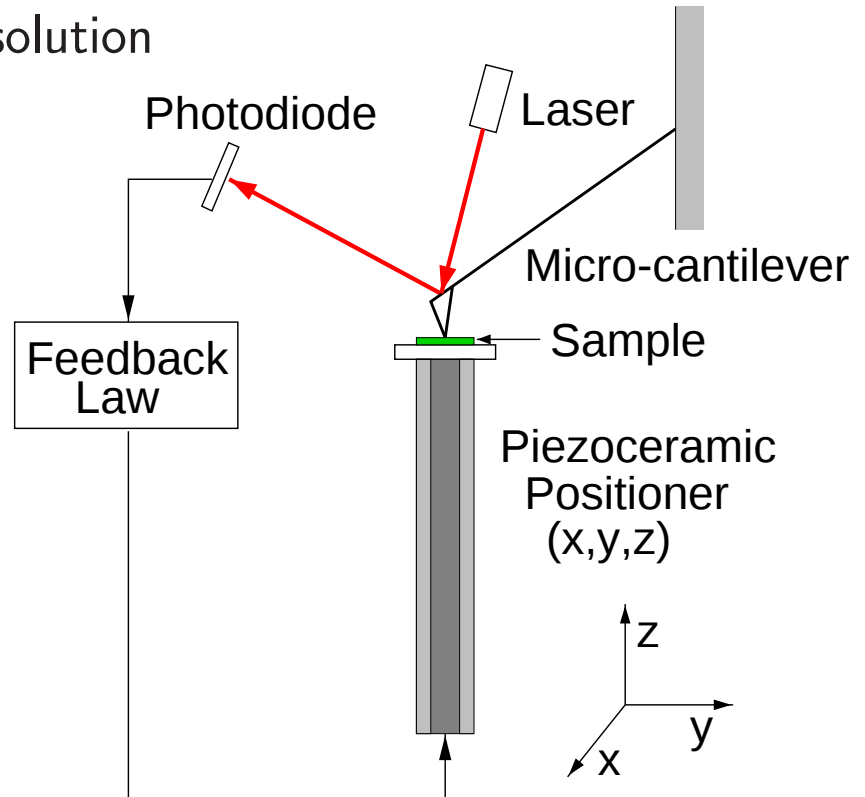
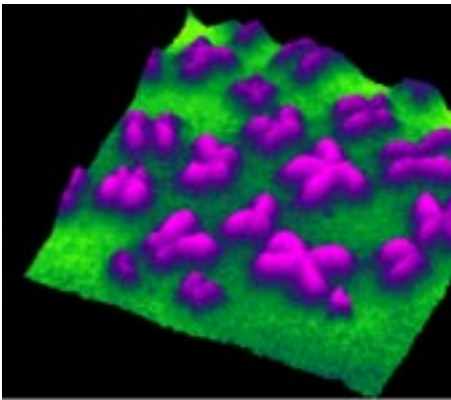
Goal:

- Develop a unified framework for model and control design for ferroic (ferromagnetic, ferroelectric and ferroelastic) materials.

I. PIEZOCERAMICS – NANOPositionING

Atomic Force Microscope:

- Can provide atomic resolution
- Human chromosomes

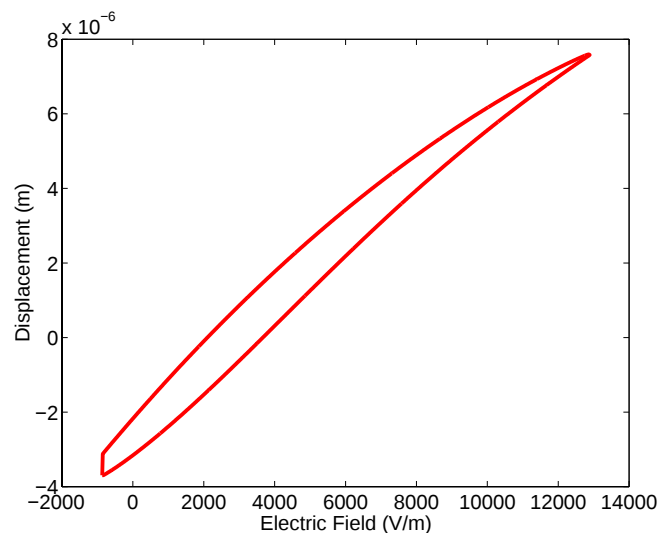


Model Development:

- Must be able to attain Angstrom-level resolution
- Must be implemented in real time

Future Capabilities:

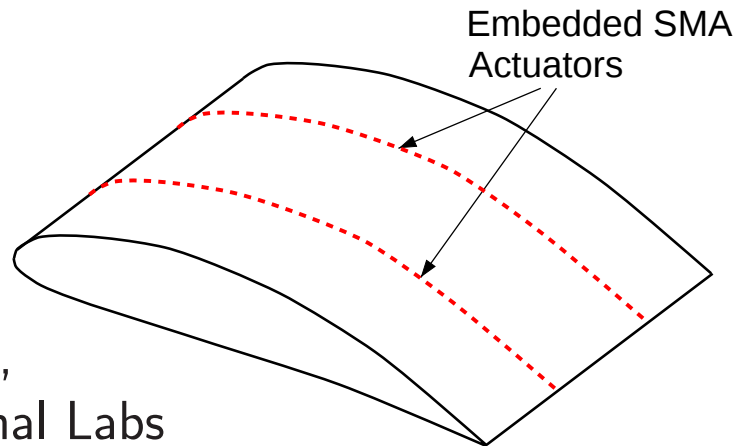
- Nanopositioning at the atomic level
- Electron spin detection: requires angstrom-level tracking



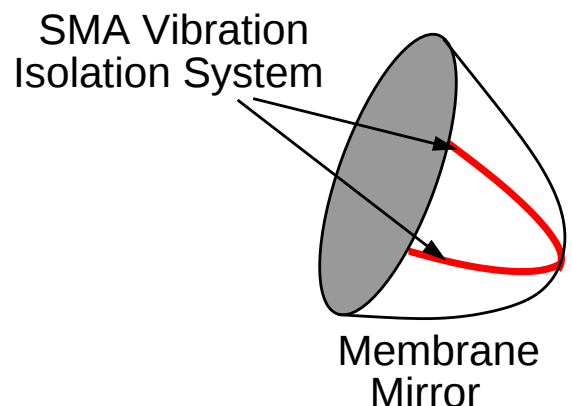
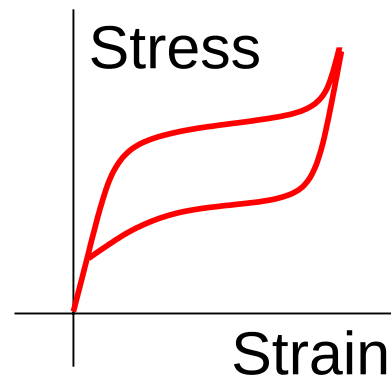
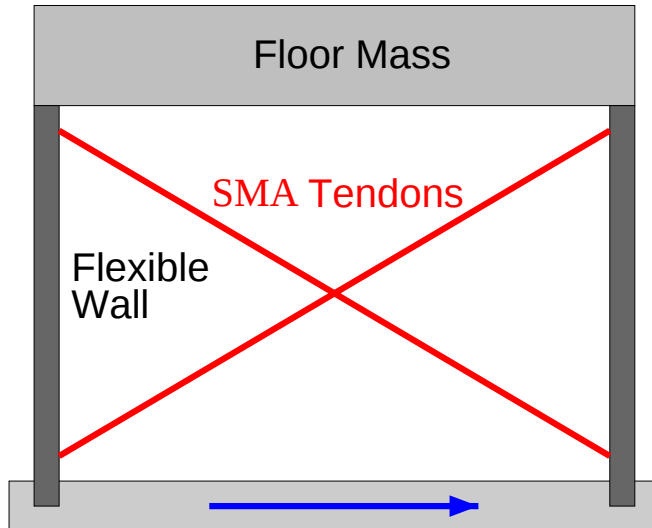
SHAPE MEMORY ALLOYS

Aerospace and Aeronautic Applications:

- Shape modification of airfoils
- Construction of modular mirrors and antennas
- Future Directions: MEM's, thin films – Sandia National Labs



Vibration Attenuation:



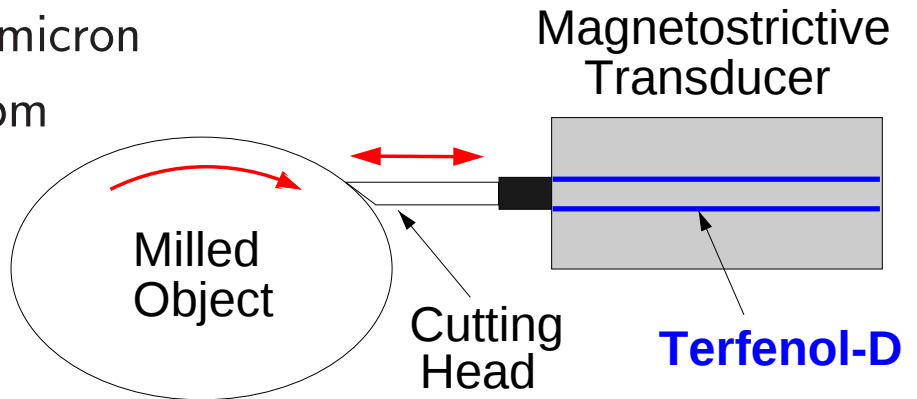
Strategy:

- Vibration attenuation in aerospace structures (e.g., mirrors)
- Operate in hysteretic regime to optimize damping

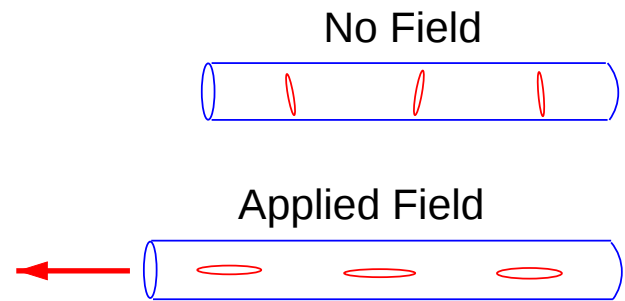
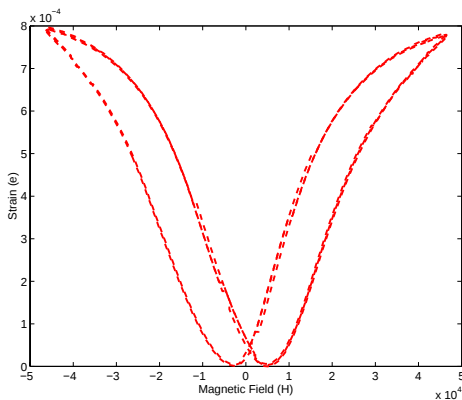
MAGNETOSTRICTIVE MATERIALS

Automotive Application: e.g., High speed milling

- Accuracy: ± 1 micron
- Speed: 3000 rpm

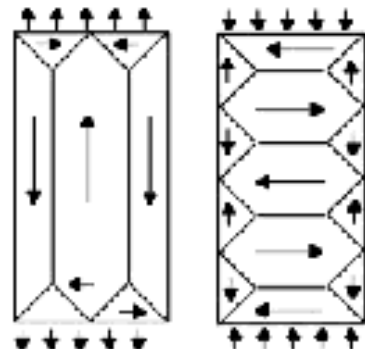
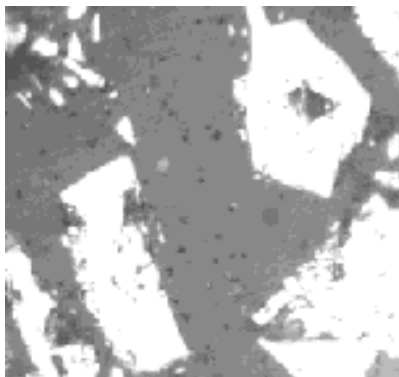


Field-Strain Relation



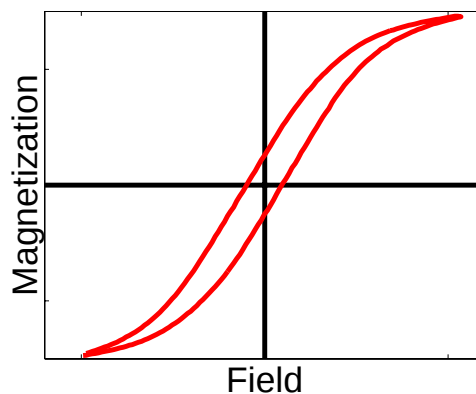
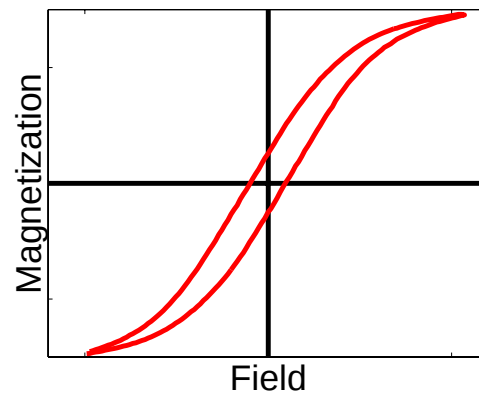
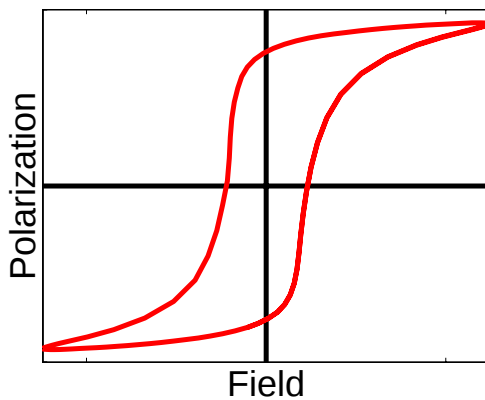
Aerospace Applications:

- Magnetostrictive composites for active structural damping



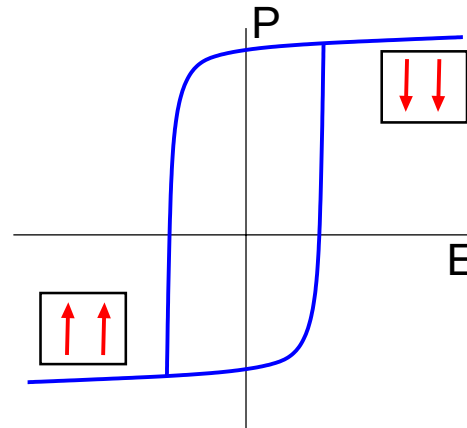
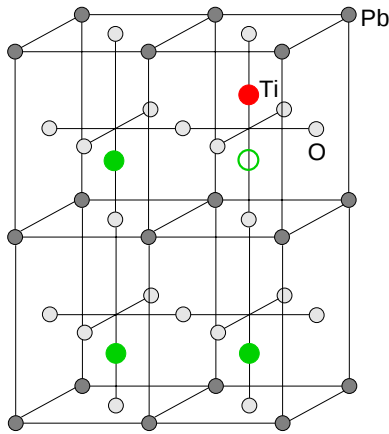
MATERIAL ANALOGIES

Ferroelectric	Ferromagnetic	Ferroelastic
Polarization	Magnetization	Strain
Electric field	Magnetic field	Stress
Paraelectric phase	Paramagnetic phase	Austenite phase
Ferroelectric phase	Ferromagnetic phase	Martensite phase
Ferroelectric domain walls	Bloch or Neel walls	Boundaries between martensite variants
Devonshire theory	Mean field (Weiss) theory	Landau theory
	Micromagnetic theory	Ginzburg-Landau theory

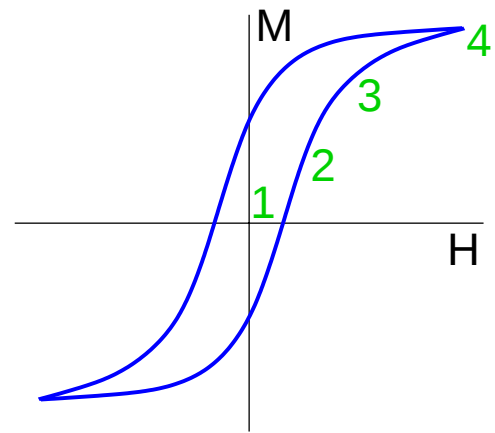
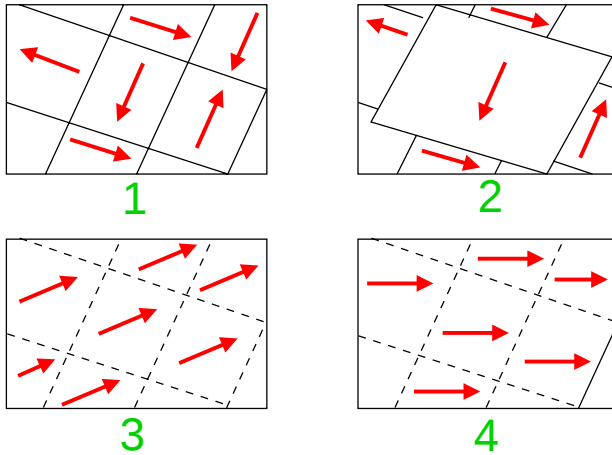


MECHANISMS WHICH PRODUCE HYSTERESIS

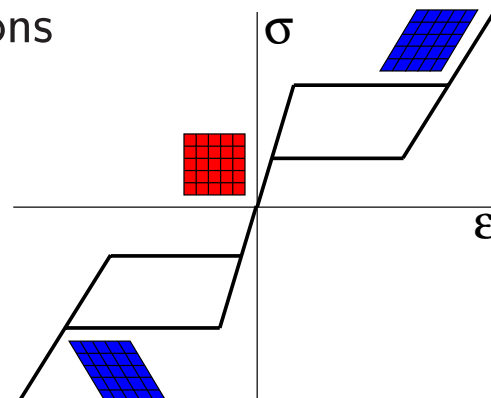
Ferroelectric: Dipole switching



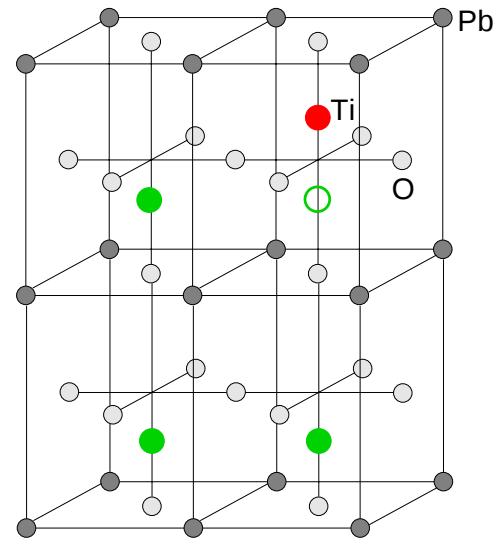
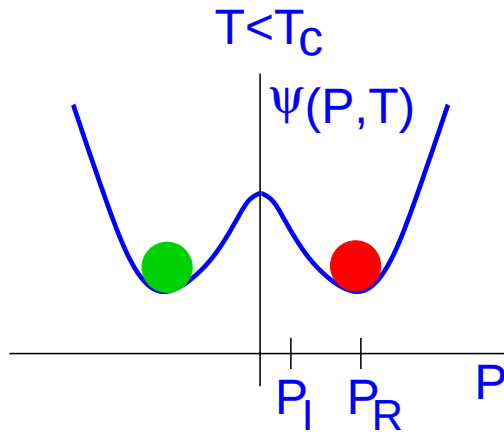
Ferromagnetic: Moment rotation, domain wall losses



Ferroelastic: Phase transitions



MESOSCOPIC MODEL – HELMHOLTZ ENERGY



Helmholtz Energy:

$$\psi(P, T) = U - ST$$

$$= \frac{\Phi_0 N}{4V} [1 - (P/P_s)^2] + \frac{TkN}{2VP_s} \left[P \ln \left(\frac{P + P_s}{P_s - P} \right) + P_s \ln(1 - (P/P_s)^2) \right]$$

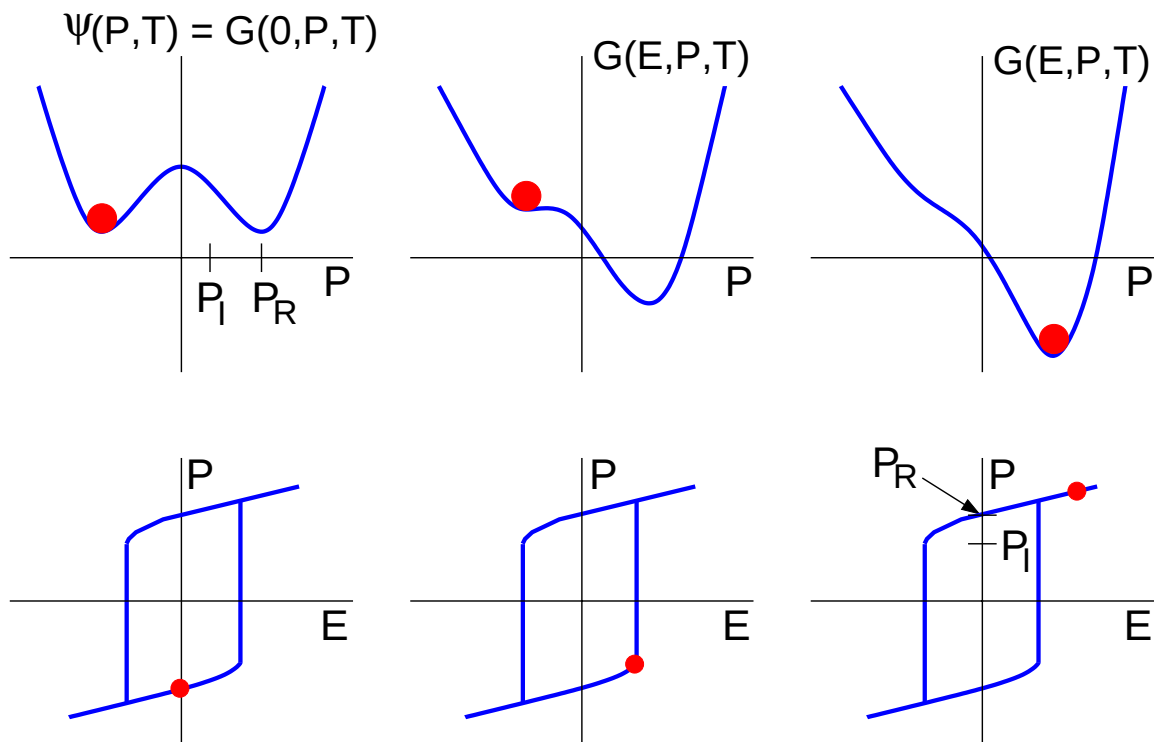
Helmholtz Energy Relations:

$$\psi(P) = \begin{cases} \frac{\eta}{2}(P \pm P_R)^2 & , |P| \geq P_I \\ \frac{\eta}{2}(P_I - P_R) \left[\frac{P^2}{P_I} - P_R \right] & , |P| < P_I \end{cases}$$

$$\psi(M) = \begin{cases} \frac{\eta}{2}(M \pm M_R)^2 & , |M| \geq M_I \\ \frac{\eta}{2}(M_I - M_R) \left[\frac{M^2}{M_I} - M_R \right] & , |M| < M_I \end{cases}$$

$$\psi(\varepsilon, T) = \begin{cases} \frac{E_M}{2}(\varepsilon \pm \varepsilon_T)^2 & , |\varepsilon| \geq \gamma_M(T) \\ -\frac{E_0(T)}{2}[\varepsilon \pm \varepsilon_0(T)]^2 + \psi_0(T) & , |\gamma_A(T)| < \varepsilon < |\gamma_M(T)| \\ \frac{E_A}{2}\varepsilon^2 + \Delta\beta(T) & , |\varepsilon| \leq \gamma_A(T) \end{cases}$$

MESOSCOPIC MODEL – GIBBS ENERGY



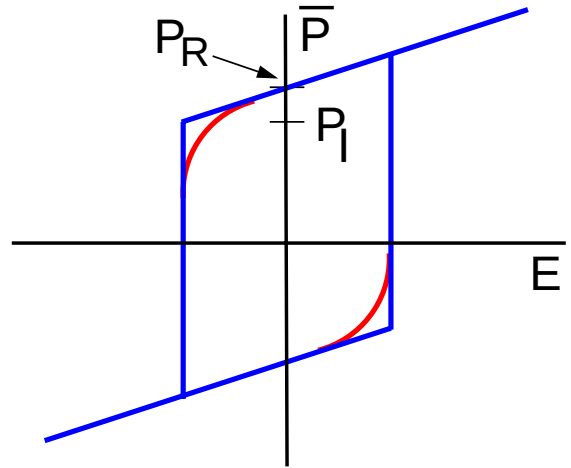
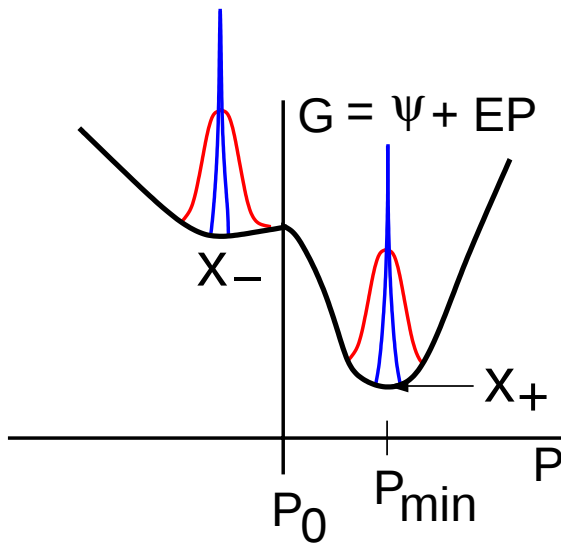
Gibbs Energy Relations:

$$G(E, P, T) = \psi(P, T) - EP \quad (\text{Ferroelectric})$$

$$G(H, M, T) = \psi(M, T) - \mu_0 H M \quad (\text{Ferromagnetic})$$

$$G(\sigma, \varepsilon, T) = \psi(\varepsilon, T) - \sigma \varepsilon \quad (\text{Ferroelastic})$$

MESOSCOPIC MODELS – UNIFORM LATTICE



Boltzmann Probability:

$$\mu(G) = C e^{-GV/kT} \Rightarrow p_{+-} = \sqrt{\frac{kT}{2\pi m V^{2/3}}} \cdot \frac{e^{-G(E, P_0(T), T)V/kT}}{\int_{P_0}^{\infty} e^{-G(E, P, T)V/kT} dP}$$

Evolution Relations:

$$\frac{dx_+}{dt} = -p_{+-}x_+ + p_{-+}x_-$$

$$\frac{dx_-}{dt} = -p_{-+}x_- + p_{+-}x_+$$

Ferroelastic: Analogous

Polarization:

$$\bar{P} = x_+ \langle P_+ \rangle + x_- \langle P_- \rangle$$

where

$$\langle P_+ \rangle = \int_{P_0}^{\infty} P \mu(G) dP$$

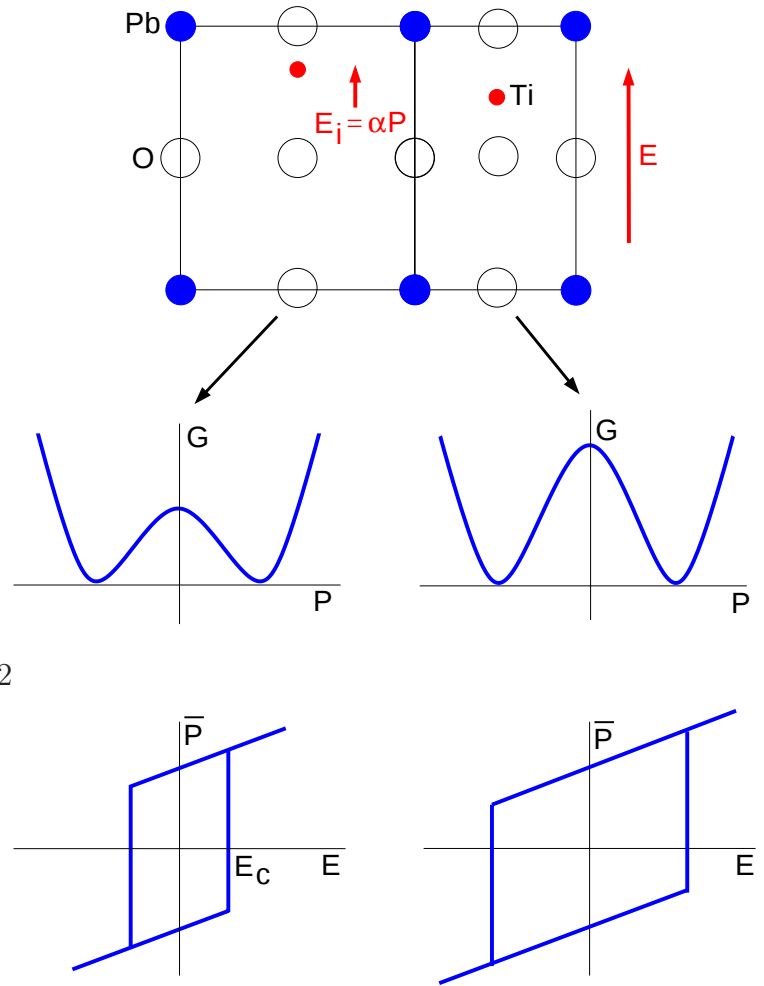
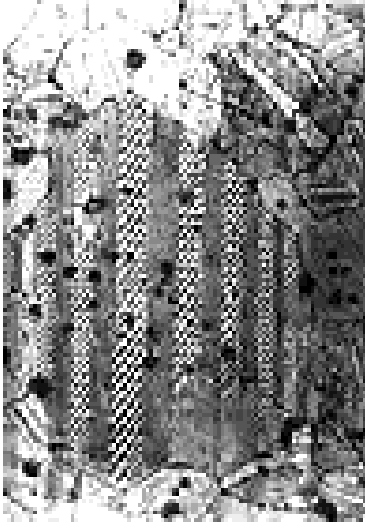
Magnetization:

$$\bar{M} = x_+ \langle M_+ \rangle + x_- \langle M_- \rangle$$

where

$$\langle M_+ \rangle = \int_{M_0}^{\infty} M \mu(G) dM$$

MACROSCOPIC MODELS



Nonuniform Lattice:

$$f(E_c) = C_1 e^{-[\ln(E_c/\bar{E}_c)/2b]^2}$$

Variable Effective Fields:

$$\hat{f}(\mathcal{E}) = C_2 e^{-(\mathcal{E}-E)^2/\bar{b}}$$

Macroscopic Models:

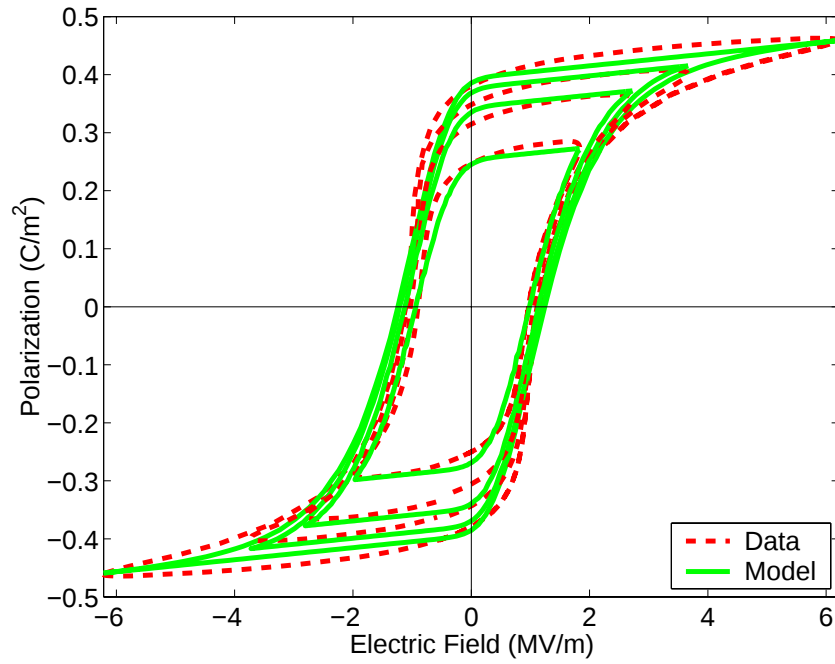
$$[P(E, T)](t) = C \int_0^\infty \int_{-\infty}^\infty f(E_c) \hat{f}(\mathcal{E}) [\bar{P}(\mathcal{E} + E, T)](t) d\mathcal{E} dE_c$$

$$[M(H, T)](t) = C \int_0^\infty \int_{-\infty}^\infty f(H_c) \hat{f}(\mathcal{H}) [\bar{M}(\mathcal{H} + H, T)](t) d\mathcal{H} dH_c$$

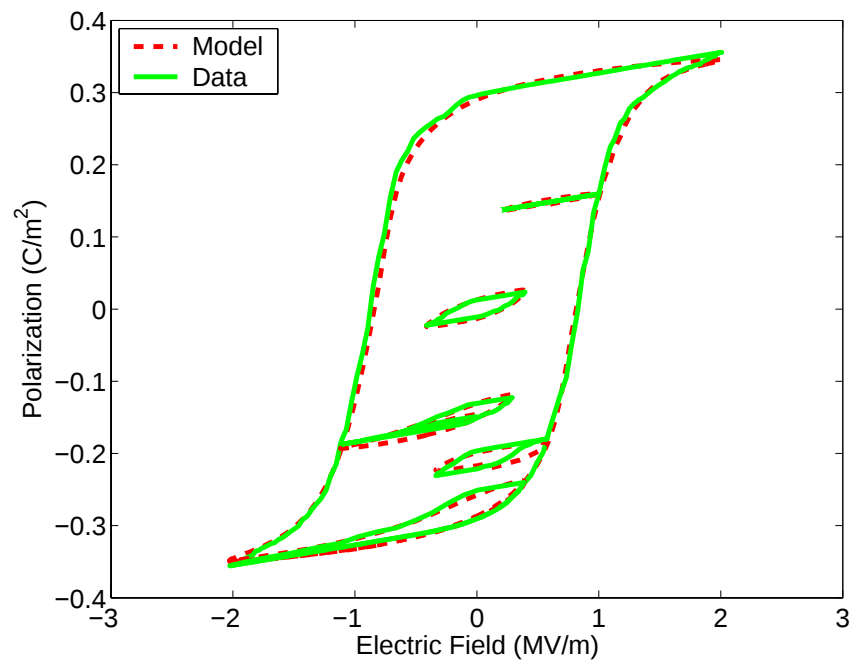
$$[\varepsilon(\sigma, T)](t) = C \int_0^\infty \int_{-\infty}^\infty f(\delta) \hat{f}(\sigma_E) [\bar{\varepsilon}(\sigma_E + \sigma, T)](t) d\sigma_E d\delta$$

III. EXPERIMENTAL VALIDATION

PZT5A: Lognormal/normal densities

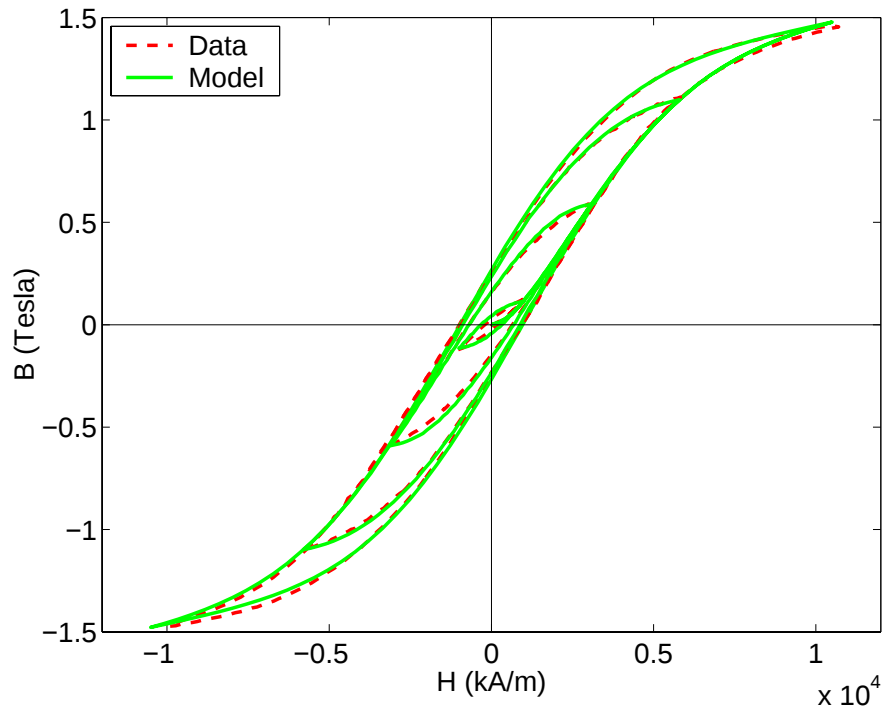


PZT5A: ID of general densities [B. Mukherjee, S-F. Liu - Data]

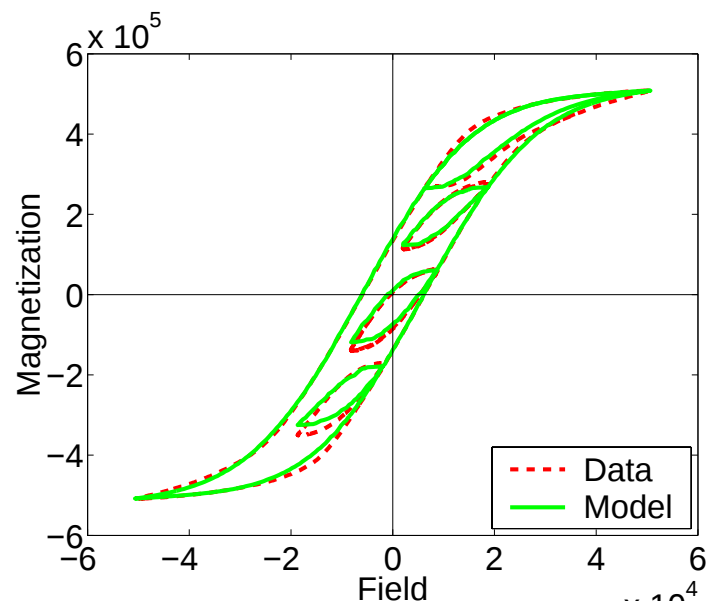
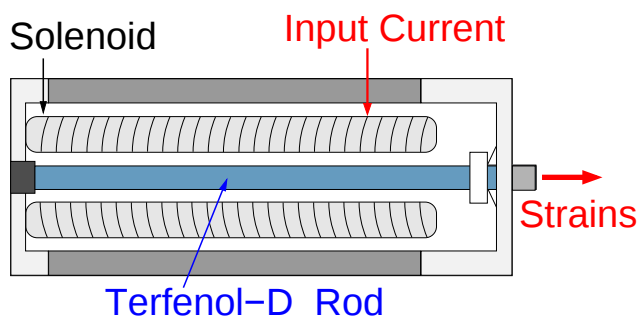


VALIDATION – FERROMAGNETIC MATERIALS

Example 1: Steel data from [Jiles and Atherton; 1984]

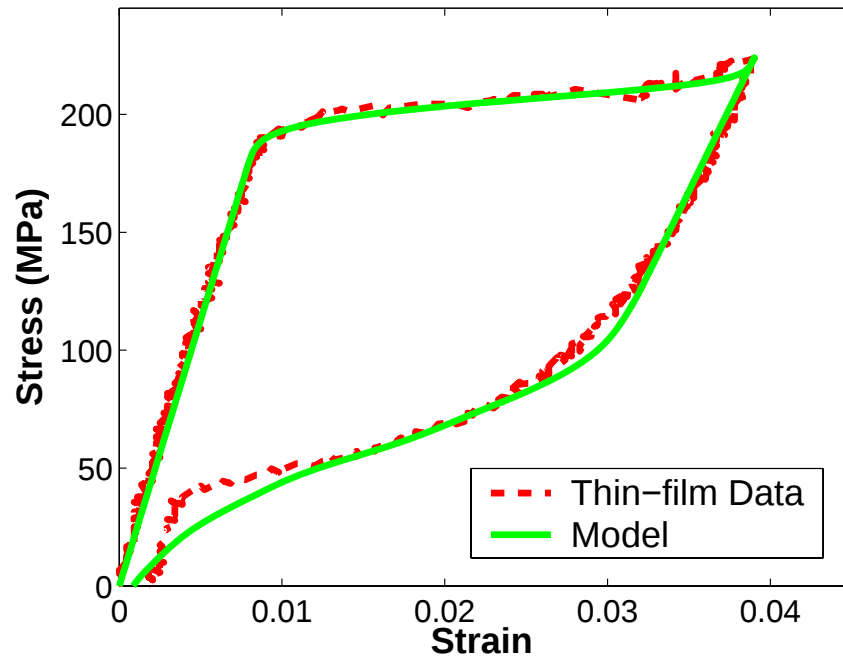


Example 2: Terfenol-D Transducer



EXPERIMENTAL VALIDATION – SMA

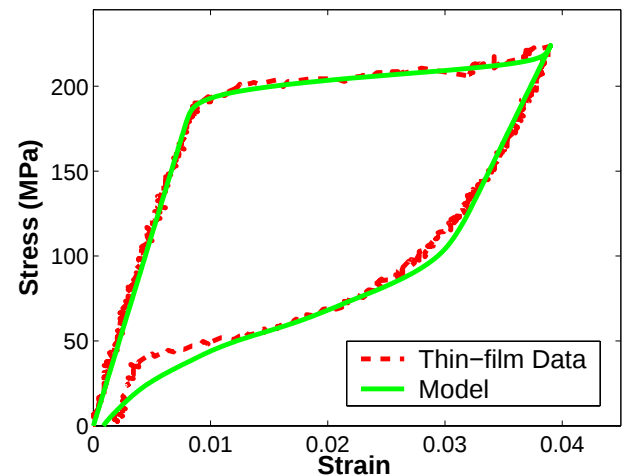
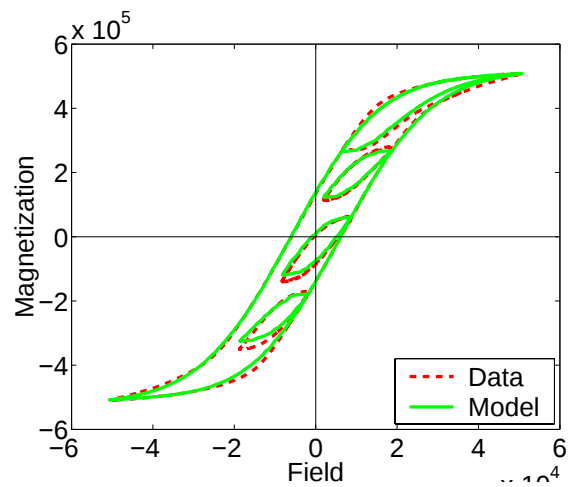
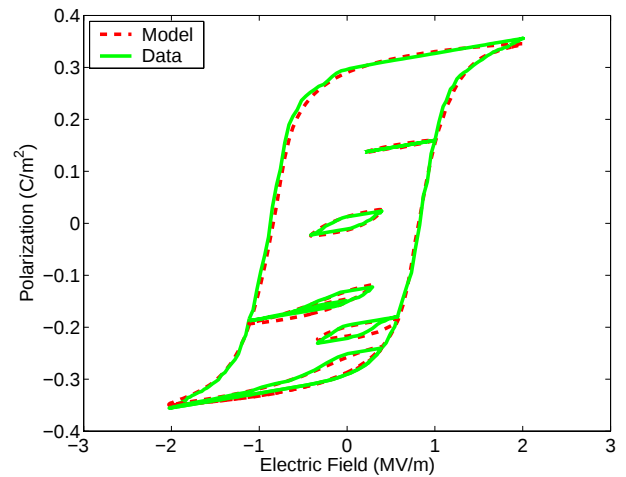
Thin Films:



CONCLUDING REMARKS

Model Attributes:

- (1) Technique provides unified framework for modeling hysteresis in ferroelectric, ferromagnetic and ferroelastic materials.
- (2) Low number (5-10) and physical nature of parameters facilitates parameter estimation and control implementation.
- (3) Model guarantees closure of biased minor loops.
- (4) Model is amenable to inversion which facilitates linear control design.
- (5) Method provides energy basis for Preisach models.



References

- [1] H.T. Banks, A.J. Kurdila G. and G. Webb, "Identification of hysteretic control influence operators representing smart actuators Part I: Formulation," *Mathematical Problems in Engineering*, 3, pp. 287-328, 1997.
- [2] M. Brokate and J. Sprekels, *Hysteresis and Phase Transitions*, Springer-Verlag, New York, 1996.
- [3] M.J. Dapino, R.C. Smith, L.E. Faidley and A.B. Flatau, "A coupled structural-magnetic strain and stress model for magnetostrictive transducers," *Journal of Intelligent Material Systems and Structures*, 11(2), pp. 134-152, 2000.
- [4] P. Ge and M. Jouaneh, "Modeling hysteresis in piezoceramic actuators," *Precision Engineering*, 17, pp. 211-221, 1995.
- [5] J.E. Massad, R.C. Smith and G.P. Carman, "A free energy model for thin-film shape memory alloys," CRSC Technical Report CRSC-TR03-03; Proceedings of the SPIE, Smart Structures and Materials 2003, to appear.
- [6] I.D. Mayergoyz, *Mathematical Models of Hysteresis*, Springer-Verlag, New York, 1991.
- [7] N. Papenfuß and S. Seelecke, "Simulation and control of SMA actuators," Proceedings of the SPIE, Smart Structures and Materials 1999, Volume 3667, pp. 586-595, 1999.
- [8] S. Seelecke and I. Müller, "Shape memory alloy actuators in smart structures – Modeling and simulation," *ASME Applied Mechanics Reviews*, to appear.
- [9] R.C. Smith, M.J. Dapino and S. Seelecke, "A free energy model for hysteresis in magnetostrictive transducers," *Journal of Applied Physics*, 93(1), pp. 458-466, 2003.
- [10] R.C. Smith and J.E. Massad, "A unified methodology for modeling hysteresis in ferroic materials," Proceedings of the 18th ASME Biennial Conference on Mechanical Vibration and Noise, 2001.
- [11] R.C. Smith and Z. Ounaies, "A domain wall model for hysteresis in piezoelectric materials," *Journal of Intelligent Material Systems and Structures*, 11(1), pp. 62-79, 2000.
- [12] R.C. Smith, M.V. Salapaka, A. Hatch, J. Smith and T. De, "Model development and inverse compensator design for high speed nanopositioning," Proc. 41st IEEE Conf. Dec. and Control, 2002, Las Vegas, NV.
- [13] R.C. Smith and S. Seelecke, "An energy formulation for Preisach models," Proceedings of the SPIE, Smart Structures and Materials 2002, Volume 4693, pp. 173-182, 2002.
- [14] R.C. Smith, S. Seelecke and Z. Ounaies, "A free energy model for piezoceramic materials," Proceedings of the SPIE, Smart Structures and Materials 2002, Volume 4693, pp. 183-190, 2002.
- [15] R.C. Smith, S. Seelecke, Z. Ounaies and J. Smith, "A free energy model for hysteresis in ferroelectric materials," CRSC Technical Report CRSC-TR03-01; *Journal of Intelligent Material Systems and Structures*, to appear.

- [16] A.N. Soukhojak and Y.-M. Chiang "Generalized rheology of active materials," *Journal of Applied Physics*, 88(11), pp. 6902-6909, 2000.
- [17] J. Woolman, "Effect of atomic composition on the mechanical properties of thin film pseudoelastic nickel titanium," Master's Thesis, Mechanical and Aerospace Engineering Department, UCLA, in preparation.