

MODELISATION OF PROBE FEED EXCITATION USING ITERATIVE METHOD

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ABSTRACT

This paper presents an implementation of an iterative method based on the waves concept for analyzing patch antennas fed by coaxial probes. This method includes a two-dimensional fast Fourier transform (FFT-2D) in a wave guide environment. The method has the advantage of simplicity in that it does not involve basis functions and inversion of matrices, as used in other calculation methods. Therefore, it is capable of analyzing larger bodies than other classical techniques. An implementation of the iterative calculation is shown for the extraction of S parameters of microwave components and antennas. The good agreement between simulation results and experimental published data justifies the design procedure and validates the present analysis approach.

INDEX TERMS : Iterative method, fast Fourier transform in waveguide environment, probe feed.

I- INTRODUCTION

Microstrip patch antennas are widely used in wireless communication because of their advantages, such as being low profile, light weight, and conformal. Different numerical electromagnetic analysis techniques such as the method of moments [1], the finite elements method [2], and the finite difference time domain method can be used to accurately simulate the microstrip antenna [3]. In most cases those numerical techniques are not practical to use

directly in CAD software for design and optimisation purposes, due to the enormous amount of computer time required. Circuit simulators on the other hand are very fast. However, models of microwave integrated circuits used in circuit simulators are often inaccurate or even invariable. To overcome these difficulties, the use of the iterative method, which is based on the concept of waves, has been proposed. It consists of generating a recursive relationship between incident waves and reflected waves at the interface containing the circuit which is divided into cells [4]. A high computational speed has been achieved by using 2D fast Fourier Transform in wave-guide environment [5].

In this paper, a general implementation of the iterative method is proposed to treat microstrip patch antennas. The theory as well as its procedure implementation is described. The numerical results are compared to measured data [8] to establish the validity and usefulness of the iterative method given in this study.

II- GENERAL FORMULATION OF ITERATIVE METHOD

We consider the shielded microstrip circuit, assumed to be loss-less, presented in Fig. 1.

The air-dielectric interface π is divided into cells denoted by three sub-domains corresponding to metal, source and dielectric.

Report Documentation Page				Form Approved OMB No. 0704-0188	
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1. REPORT DATE 02 JUL 2004		2. REPORT TYPE N/A		3. DATES COVERED -	
4. TITLE AND SUBTITLE Modelisation Of Probe Feed Excitation Using Iterative Method				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)				5d. PROJECT NUMBER	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Department of Physics, Faculty of Sciences of Tunis 2092 El Manar Tunisia				8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)				10. SPONSOR/MONITOR'S ACRONYM(S)	
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)	
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release, distribution unlimited					
13. SUPPLEMENTARY NOTES See also ADM001760, Applied Computational Electromagnetics Society 2004 Archive., The original document contains color images.					
14. ABSTRACT					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT UU	18. NUMBER OF PAGES 8	19a. NAME OF RESPONSIBLE PERSON
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified			

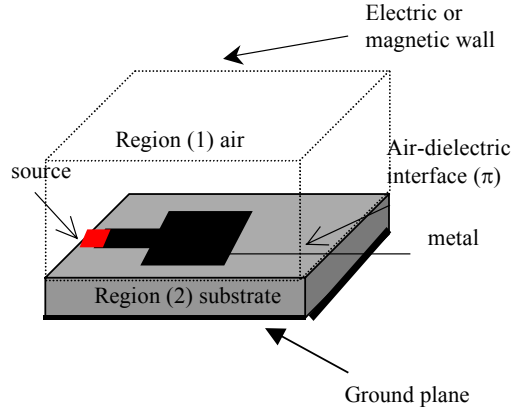


Figure 1. Typical planar circuit.

The wave concept is introduced by writing the transverse (plane π) electric field E_i and current density J_i in terms of incident and reflected waves [5]. It leads to the following set of equations:

$$\begin{cases} A_i = \frac{1}{2\sqrt{Z_{0i}}}(E_i + Z_{0i}J_i) \\ B_i = \frac{1}{2\sqrt{Z_{0i}}}(E_i - Z_{0i}J_i) \end{cases} \quad (1)$$

J_i is defined as follows:

$J_i = H_i \times n$, n is oriented as the incident waves A_i .

Z_{0i} is the characteristic impedance of the medium i ($i = 1, 2$). It is equal to:

$$Z_{0i} = \sqrt{\frac{\mu_0}{\epsilon_0 \epsilon_{ri}}}.$$

In order to generate two waves, B_{ix} and B_{iy} , in the space domain, the structure is excited by an electric planar source. The model of the source is an electric field E_{oi} equivalent to a magnetic current density.

The Fast Fourier Transform (FFT-2D) in waveguide environment is then used to obtain two spectral waves B_i^{TE} and B_i^{TM} in each region. Then, these spectral waves are reflected in the spectral domain of the Region(1) and Region(2) as described in Fig. 2.

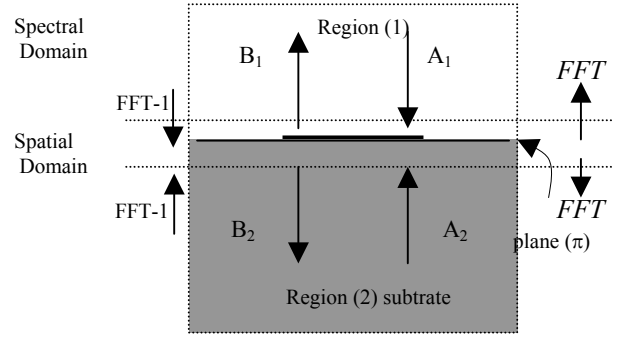


Figure 2. Definition of incident and diffracted waves.

The travelling part of these waves is then stored in memory, whereas the evanescent part constitutes the incident waves for the second iteration. The implementation of the iterative process consists of establishing a recursive relationship between waves (incident and reflected) at the q and $q-1$ iteration.

Initially, the interface circuit (plane (π)) on which the boundary conditions have to be satisfied (spatial domain) must be meshed.

Let us note H_d and H_m the indicator functions of respectively the dielectric and metal. These are equal to one in the considered domain and zero elsewhere. Due to the continuity relationship ($E_{t1}=E_{t2}$ and $J_1+J_2=0$ on the dielectric, $E_{t1}=E_{t2}=0$ on the metal) in each point of the discontinuity plane, it is easy to deduce from the equation (1) and (2) the following system:

$$\begin{bmatrix} B_1 \\ B_2 \end{bmatrix} = \begin{bmatrix} -H_m \frac{1-N_2}{1+N_2} H_d & \frac{2N}{1+N_2} H_d \\ \frac{2N}{1+N_2} H_d & -H_m \frac{1-N_2}{1+N_2} H_d \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix}. \quad (3)$$

Then the scattering matrix corresponding to the metal and dielectric domains can be expressed as follows:

$$\Gamma\pi = \begin{bmatrix} -Hm - \frac{1-N2}{1+N2} Hd & \frac{2N}{1+N2} Hd \\ \frac{2N}{1+N2} Hd & -Hm - \frac{1-N2}{1+N2} Hd \end{bmatrix}$$

$H_m=1$ on the source and 0 elsewhere.

$H_d=1$ on the source and 0 elsewhere.

$$N = \sqrt{\frac{Z_{o1}}{Z_{o2}}}$$

- Sub-domain of the source

There are numerous possibilities for choosing the source. The most simple consist in a realistic description of the excitation by a microstrip line (Fig.1).

This source generates two waves on both sides of the interface. The boundary condition on the source can be written as follows:

$$\begin{bmatrix} B_1 \\ B_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} + \begin{bmatrix} \frac{E_0}{\sqrt{Z_{o1}}} \\ \frac{E_0}{\sqrt{Z_{o2}}} \end{bmatrix}.$$

$$E_1 = E_2 = E_0 - Z_0(J_1 + J_2).$$

Then the scattering matrix on the sub-domain source is expressed as

The drawback of this source is that we must use a box with electric walls to connect the source to the ground plane.

Another technique of spatial excitation is described in Section (III).

The waves B_i^α are reflected on the upper and lower parts of the structure. Consequently, in spectral domain the relation between waves become:

$$\begin{bmatrix} A_i^{TE} \\ A_i^{TM} \end{bmatrix} = \begin{bmatrix} \rho_i^{TE} & 0 \\ 0 & \rho_i^{TM} \end{bmatrix} \begin{bmatrix} B_i^{TE} \\ B_i^{TM} \end{bmatrix} \quad (4)$$

where the reflection coefficient in the dielectric substrate is:

$$\rho_i^\alpha = \frac{1 - Z_{oi}^\alpha Y_{mn,i}^\alpha \coth(\gamma_{m,n,i} h_i)}{1 + Z_{oi}^\alpha Y_{mn,i}^\alpha \coth(\gamma_{m,n,i} h_i)} \quad (i=2)$$

and the reflection coefficient in the free space (region 1) is:

$$(\alpha \text{ is TE or TM mode}) \text{ with} \quad (i=1)$$

$$Y^{TE} = \frac{\gamma_{mn,i}}{j\omega\mu_0}; \quad Y^{TM} = \frac{j\omega\epsilon_0\epsilon_r}{\gamma_{mn,i}}$$

where k_0 is the space wave number.

$$\gamma_{mn,i}^2 = \left[\frac{m\pi}{a} \right]^2 + \left[\frac{n\pi}{b} \right]^2 - k_0^2 \epsilon_r$$

III- MODELISATION OF PROBE FEED

The coaxial current probe offers a more realistic method to excite currents on a patch antenna [9]-[10]. The coaxial probe is connected through the ground plane with the centre conductor embedded vertically and terminated on the patch surface, where the outer conductor of the coax is connected to the ground plane. Figure 3 shows the attachment of the coaxial probe to the patch antenna surface.

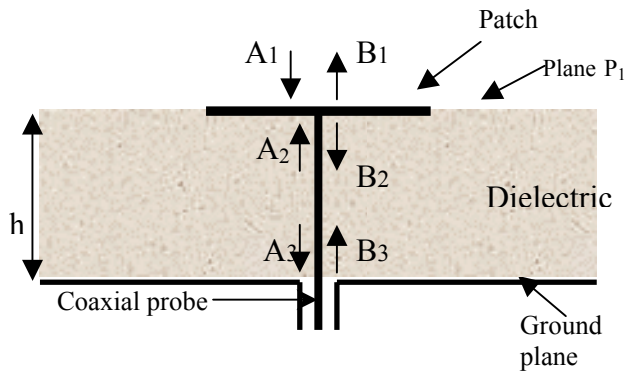


Figure 3. Microstrip patch antenna excited by coaxial probe feed.

The purpose is to determine the relationship between B_1 , B_2 and A_1 , A_2 on the sub-domain source.

We suppose that there are four metallic cells on the discontinuity plane (P_1) which are connected to the via hole. In this case the current density distribution is illustrated in Fig.4.

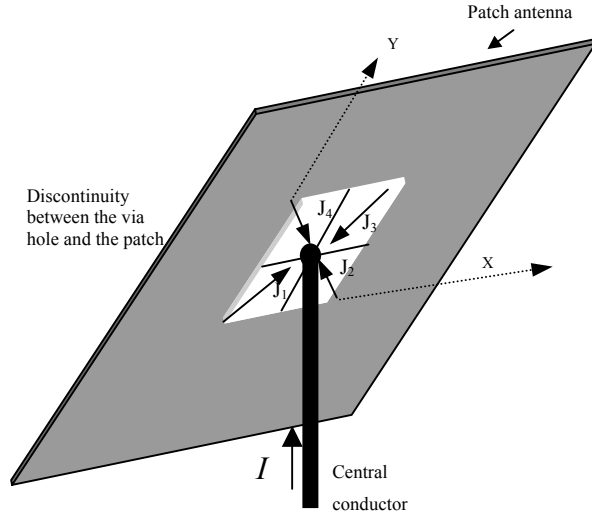


Figure 4. Bottom view of the patch antenna: Distribution of magnetic field on the discontinuity patch-via hole.

Let us note that I is the current excitation that verifies the following relationship:

$$J \times h = I \quad (5)$$

According to Fig.4, it is possible to establish the following relationship:

$$J_1 + J_2 + J_3 + J_4 = J \quad (6)$$

The vector J which characterizes the current distribution on the pixels of the discontinuity (via hole-patch) is given by:

$$J = \frac{1}{\sqrt{8}}(1, 1, -1, 1, -1, -1, 1, -1)_{(x,y)}^T \quad (7)$$

In order to modelize the discontinuity (via hole –plane P_1), we assume that only fundamental mode can be propagated in the via hole and the other modes are evanescent. The passage from four cells characterizing the current density J to modes and vice versa can be considered as multi-port network depicted in Fig. 5.

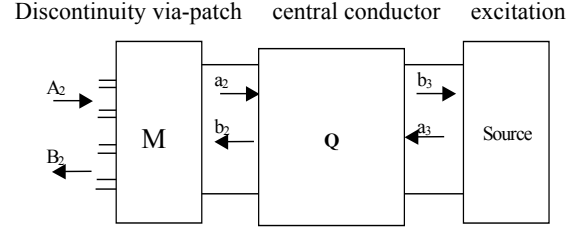


Figure 5. Coupling of Cells-Modes, Modes-Cells in the discontinuities between the via hole and the planes P_1, P_2 .

Q is a two-port network which characterizes the via hole, using the theory of transmission lines. The scattering matrix of this two-port network is given by:

$$[S] = \begin{bmatrix} 0 & e_{j\theta} \\ e_{j\theta} & 0 \end{bmatrix}, \theta = k_0 h; \quad k_0 = \frac{2\pi}{\lambda_0} \quad .$$

λ_0 : length wave in the free space.

Consequently, the relationship between waves a_2, a_3, b_2 , and b_3 , can be deduced:

$$\begin{bmatrix} b_2 \\ b_3 \end{bmatrix} = [S] \begin{bmatrix} a_2 \\ a_3 \end{bmatrix} \quad (8)$$

The expression of the matrix M characterizing the multi-port network is demonstrated in reference [6]. It is given by the following equation:

$$[M] = \begin{bmatrix} JJ^T & J \\ J^T & 0 \end{bmatrix}.$$

Therefore, the relationship between incident and reflected waves is:

$$\begin{bmatrix} B_2 \\ a_2 \end{bmatrix} = \begin{bmatrix} JJ^T - 1 & J \\ J^T & 0 \end{bmatrix} \begin{bmatrix} A_2 \\ b_2 \end{bmatrix} \quad (9)$$

The source can be modeled by the equivalent circuit illustrated in Fig. 6.

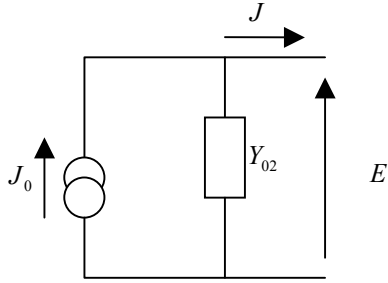


Figure 6. Equivalent circuit of the source.

As is known from the equivalent circuit given in fig.6, it is possible to deduce:

$$J = J_0 - Y_{02}E, \quad (10)$$

where Y_{02} is the admittance of Region (2),

$$Z_{02} = Y_{02}^{-1}.$$

Let us assume that the source excites the mode a_3 . However the magnitude of $b_3 = 0$. Using the equations (5) and (6) we deduce:

$$B_2 = (JJ^T - 1)A_2 + e^{j\theta}Ja_3. \quad (11)$$

According to equations (7) and (11) we deduce:

$$a_3 = \frac{1}{2h} \sqrt{Z_{02}} I_0. \quad (12)$$

In the region (1), if we suppose that we have a metal domain, it is possible to establish: $B_1 = -A_1$.

According to the equations (11) and (12), we can deduce the relationship between incident and diffracted waves on the sub-domain source:

$$\begin{bmatrix} B_1 \\ B_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & JJ^T - 1 \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{2} \sqrt{Z_{02}} J_0 e^{j\theta} J \end{bmatrix}. \quad (13)$$

The complete scattering matrix can be expressed as follows

$$\begin{cases} \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} = \begin{bmatrix} -Hm - \frac{1-N2}{1+N2} Hd & \frac{2N}{1+N2} Hd \\ \frac{2N}{1+N2} Hd & -Hm - \frac{1-N2}{1+N2} Hd \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} & \text{On sub-domains metal and dielectric} \\ \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & JJ^T - 1 \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{2} \sqrt{Z_{02}} J_0 e^{j\theta} J \end{bmatrix} & \text{On sub-domain source} \end{cases}$$

At K^{th} iteration, it is possible to calculate the electric field and current density at interface plane:

$$J_i^k = \frac{1}{\sqrt{Z_{0i}}} (A_i^k - B_i^k) \quad (15)$$

$$E_i^k = \sqrt{Z_{0i}} (A_i^k + B_i^k). \quad (16)$$

IV- RESULTS AND DESIGN EXAMPLES

As an application, we are interested in characterizing two different shapes of patch antennas. We have developed a program to calculate the input impedance and the reflection coefficient of each antenna.

1. Rectangular patch antenna:

The first example is a rectangular patch antenna deposited on substrate with relative dielectric constant $\epsilon_r = 2.2$. The coaxial probe is attached to the patch antenna at (x_c, y_c) .

In this case, the circuit plane is meshed with 64x64 square cells.

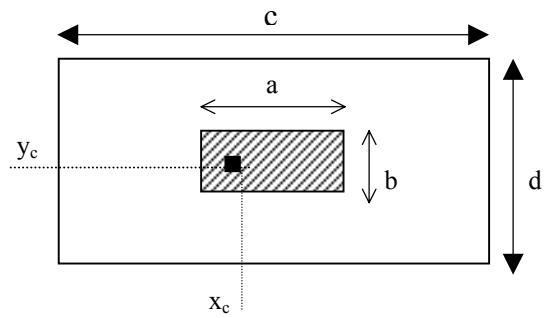


Figure 7. Rectangular patch antenna structure $c=100\text{mm}$, $d=76\text{mm}$, $a=25\text{mm}$, $b=19\text{mm}$, $x_c=45,5\text{mm}$, $y_c=34,5\text{mm}$, $\epsilon_r=2.2$.

First, the convergence of parameters is tested.

In Fig. 8, The real part of Z_{in} is illustrated as function of the iteration number. It is seen that convergence is achieved for 160 iterations.

The iterative process is terminated when the convergence is reached.

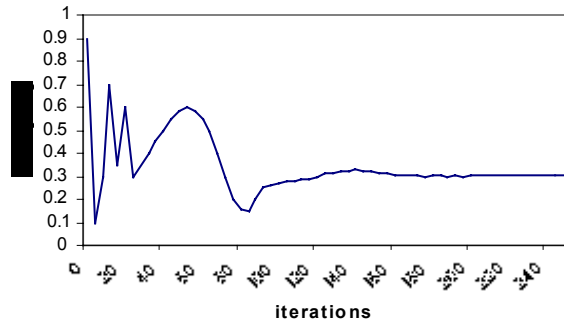


Figure 8: Real part of Z_{in} as function of the iteration number.

Figure 9. show the comparison between simulation and measured data reference [7]. It is seen that the error between them is 5 to 7%. The error can be minimized by meshing the structure with high resolution (128x128 pixels).

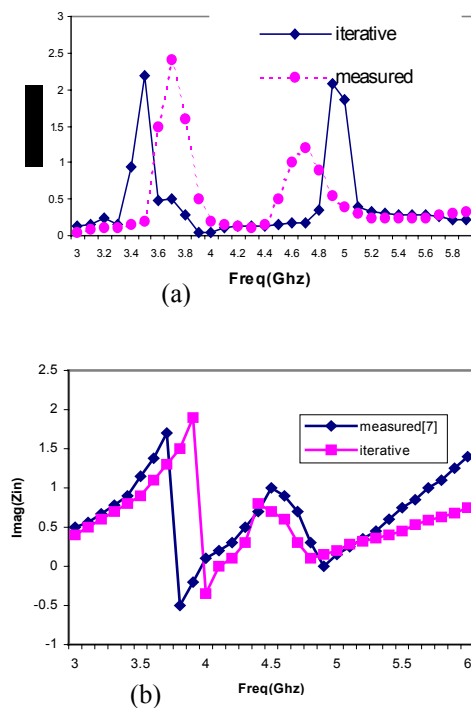


Figure 9. Input impedance of a rectangular patch antenna as a function of frequency, (a) real part and (b) imaginary part.

Figure 10 shows that the second resonance frequency is eliminated when the position of probe feed excitation is at the center of the patch antenna

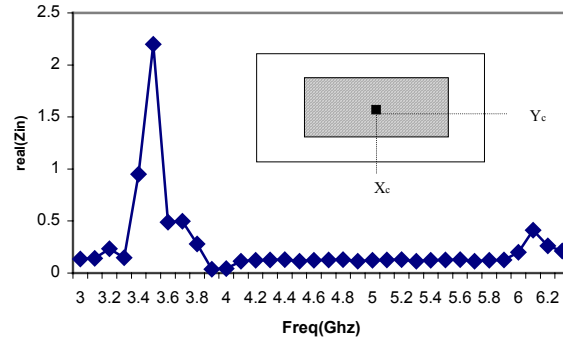


Figure 10. Input impedance of rectangular patch antenna $c=100\text{mm}$, $d=76\text{mm}$, $a=25\text{mm}$, $b=19\text{mm}$, $x_c=0$, $y_c=0$, $\epsilon_r=2.2$.

2. Patch Inverted-F Antenna (PIFA):

The antenna was printed on a thin, flexible Mylar substrate. The end of the ground plane is wrapped around the former, reducing the overall length of the antenna by the height without affecting the antenna performance.

Figure 11 shows the geometries and dimensions of the studied structure.

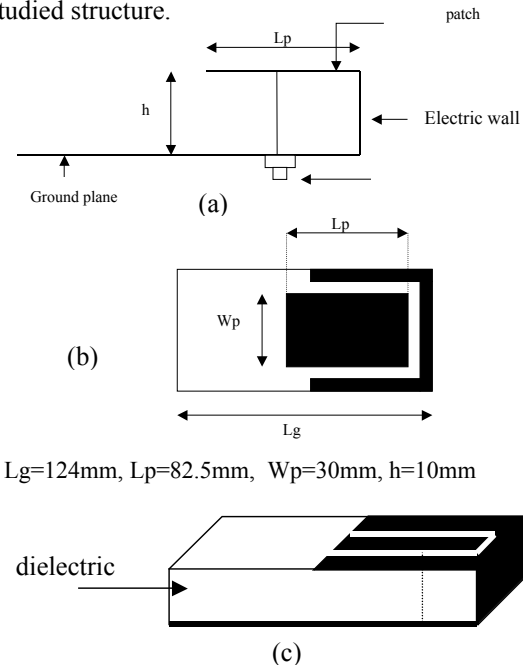


Figure 11. (a) Side view of the antenna (b) top view of the antenna (c) schematic view on the antenna.

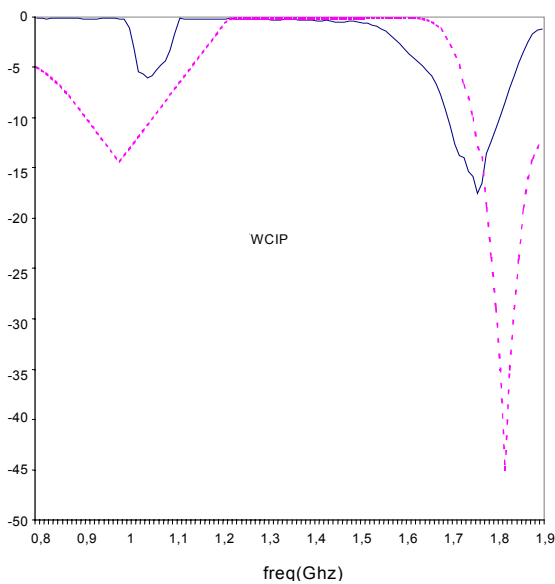


Figure 12. Reflection coefficient against frequency for the pifa antenna WCIP [8].

Finally the reflection coefficient is extracted and compared in Fig. 12 to the measured response given in reference [8], an agreement between them is observed.

IV- CONCLUSION

An iterative technique based on the concept of waves has been used for the simulation of the input impedance of rectangular patch antenna and the reflection coefficient of PIFA antenna. Thanks to its simplicity, the presented method does not involve bases functions and inversion of matrix. The good agreement between computed and published results justifies the design procedure and validates the present analysis approach. Consequently, the present approach will be investigated for further new applications such as air bridges, diodes, active elements.

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- Optimisation des circuits non linéaires
- Calcul des circuits microondes par les schémas équivalents-exercices CEPADUES Editions). He co-signed over 100 publications in journals and 250 communication in international conferences.
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