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14. ABSTRACT Time-resolved force sensing and intensified charge-coupled device (ICCD) imaging techniques were applied to the study of the force generation mechanism for laser ablation of liquids. A Transversely Excited at Atmospheric pressure (TEA) CO ₂ laser operated at 10.6 μm, 300 ns pulse width, and 9 J pulse energy was used to ablate liquids contained in various aluminum and glass vessels. Net imparted impulse and coupling coefficient were derived from the force sensor data and relevant results will be presented for various container designs and liquids used. ICCD imaging was used in conjunction with the dynamic force techniques to examine dependencies on absorption depth, irradiance, surface curvature, and container geometry. ICCD imaging was also used to determine whether surface or volume absorption should be preferable for laser propulsion using liquid propellants. Finally, ballistic experiments were conducted in order to verify the dynamic force data and lend additional evidence as to the predominant methods of force generation.					
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Ablation of Liquids for Laser Propulsion with TEA CO₂ Laser (Preprint)

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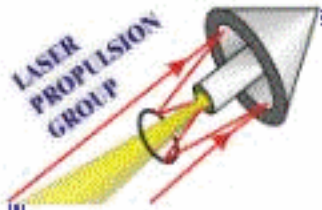
Gene Nelson

UAH Glassblower

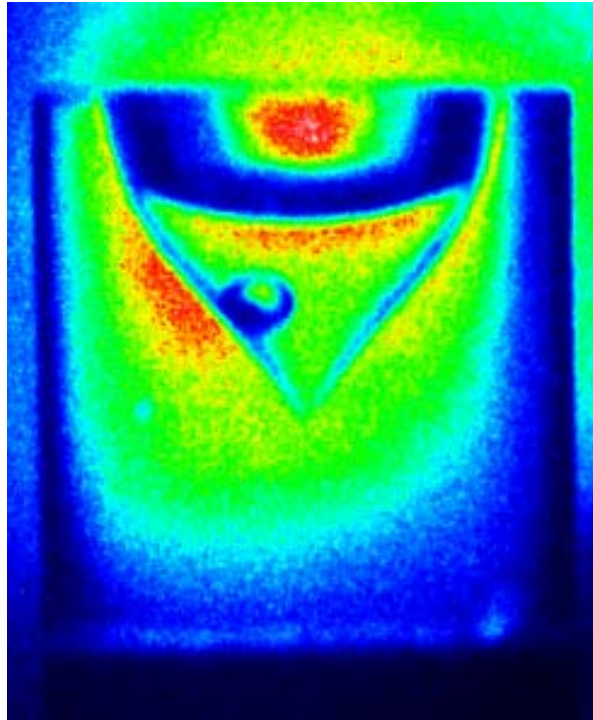
Scott Anderson

Audio Arrangement

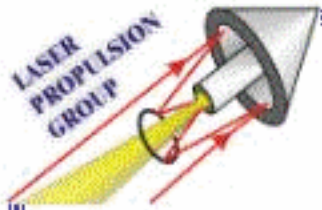




Outline

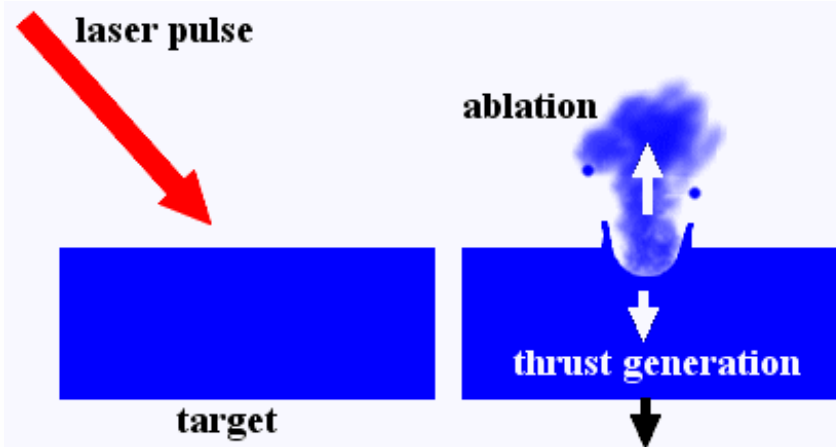


1. Introduction
2. Force
3. ICCD Ballistics
4. ICCD Imaging
5. Results and Discussion
6. Conclusions



Laser Ablation

- Laser Ablation: removal of material by any physical process under laser irradiation



- Laser Ablation of Liquids
 - C_m up to 350 dyne/W
 - Irradiance: 10^7 - 10^8 W/cm²
 - I_{sp} up to 50 s



Motivation

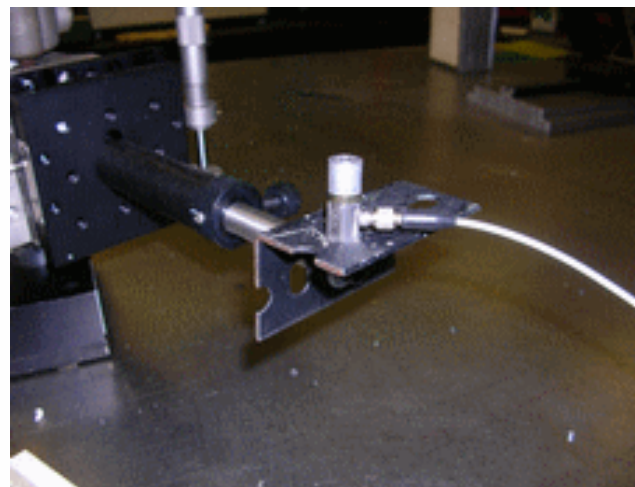
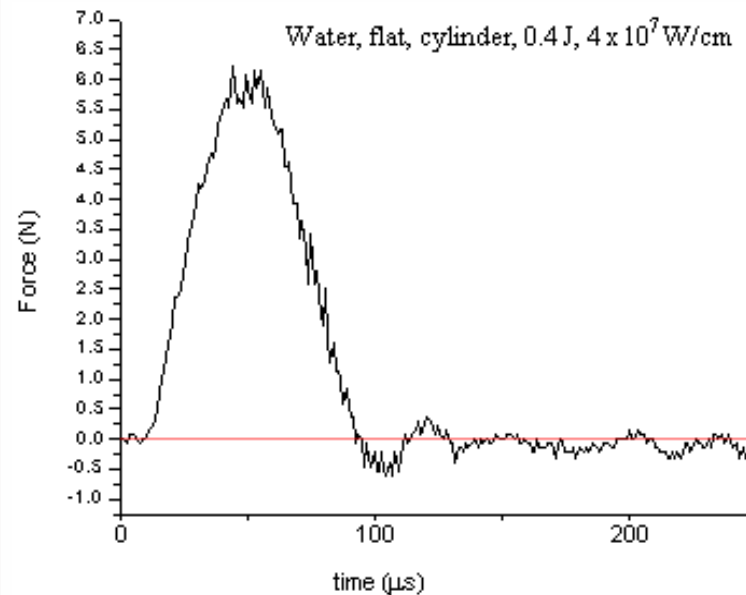
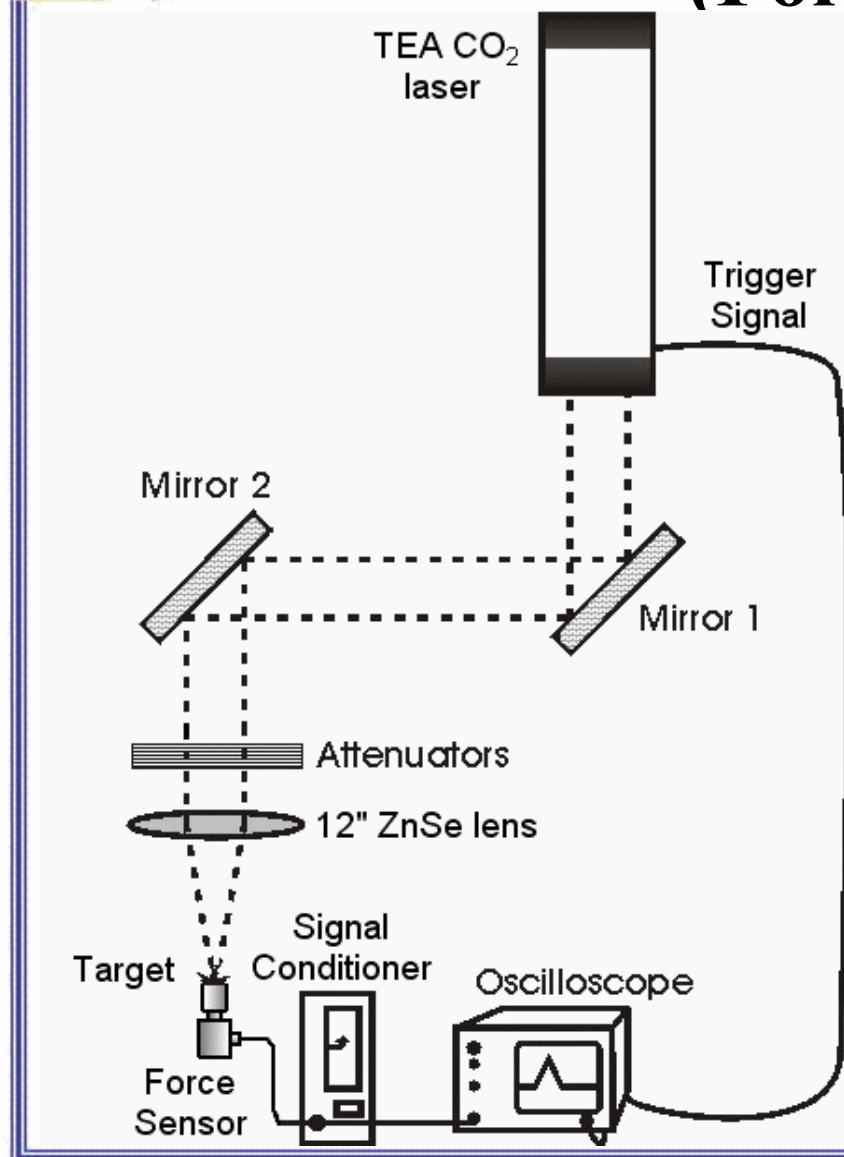
- (1) What is the physical mechanism generating thrust during the laser ablation of a liquid?
 - Plasma formation
 - Vaporization
 - Explosive boiling / Phase explosion
 - Cavity collapse / splashing
- (2) How do the ablation mechanisms for surface and volume-absorbing liquids differ?
- (3) How does C_m depend on:
 - Container geometry
 - Liquid surface curvature
 - Absorption depth



Force Experiments



Experimental Setup (Force Sensors)





Piezoelectric Force Sensors

Small Force Sensor

- **Maximum Force: 9.786 N**
- Linearity: $< 1\%$
- Sensitivity: 526.6 mV/N
- Discharge time constant: > 1.0 s
- Rise Time: 5 μ s
- Resolution: 10^{-4} N



PCB-209C01

Large Force Sensor

- **Maximum Force: 444.8 N**
- Linearity: $< 0.4\%$
- Sensitivity: 11.96 mV/N
- Discharge time constant: > 500 s
- Rise Time: 8 μ s
- Resolution: 10^{-3} N

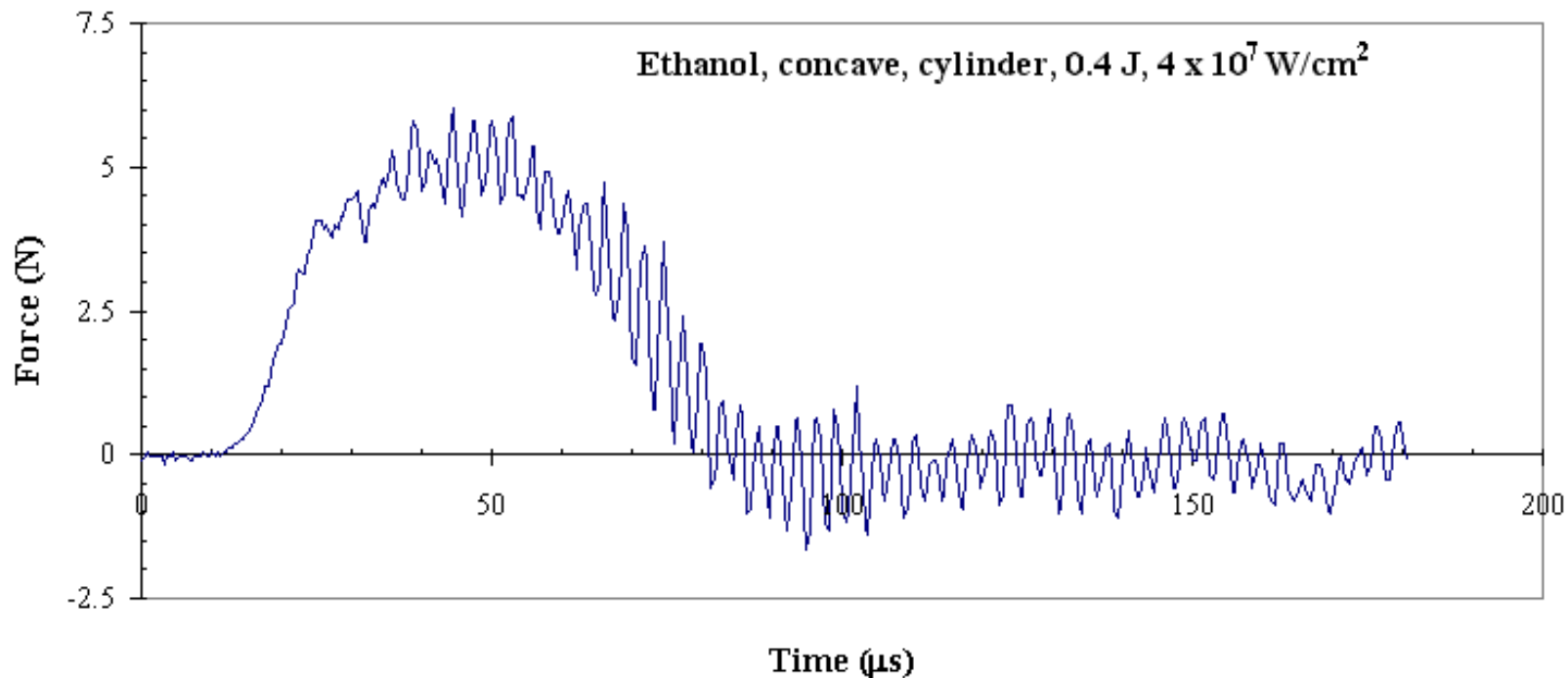


PCB-200B02



Force-Time Curve

- Measurements are as follows:
 - Single laser shot
 - Force vs. time
 - Large force peak observed (10-90 μs , centered 40-50 μs)



- Integrate to find I, then derive C_m

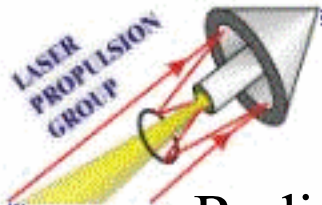


Coupling Coefficients and Peak Force

Peak Force (N)		Hexane	Ethanol	Water
Cylinder	Flat	3.4 ± 0.4	5.2 ± 0.6	4.1 ± 0.4
	Concave	3.1 ± 0.2	6.0 ± 0.1	5.7 ± 0.5
Cone	Flat	3.6 ± 0.3	5 ± 1	4.1 ± 0.4
	Concave	3.7 ± 0.3	5.8 ± 0.4	5.3 ± 0.4

C_m (dyne/W)		Hexane	Ethanol	Water
Cylinder	Flat	22 ± 3	50 ± 3	43 ± 4
	Concave	22 ± 3	56 ± 4	60 ± 6
Cone	Flat	23 ± 1	49 ± 6	47 ± 5
	Concave	24 ± 3	56 ± 3	56 ± 6

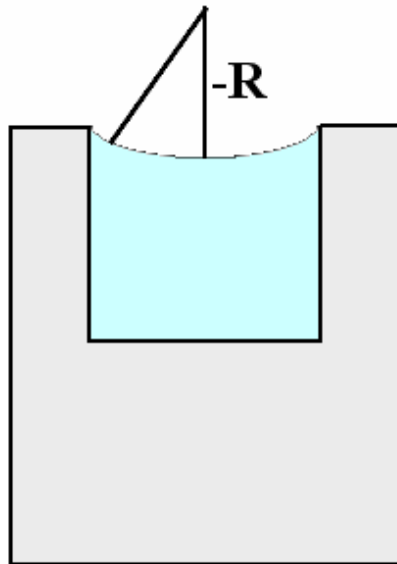
$(1.6 \times 10^7 \text{ W/cm}^2, 0.4 \text{ J, Force Sensor})$



Surface Curvature

- Radius of Curvature R

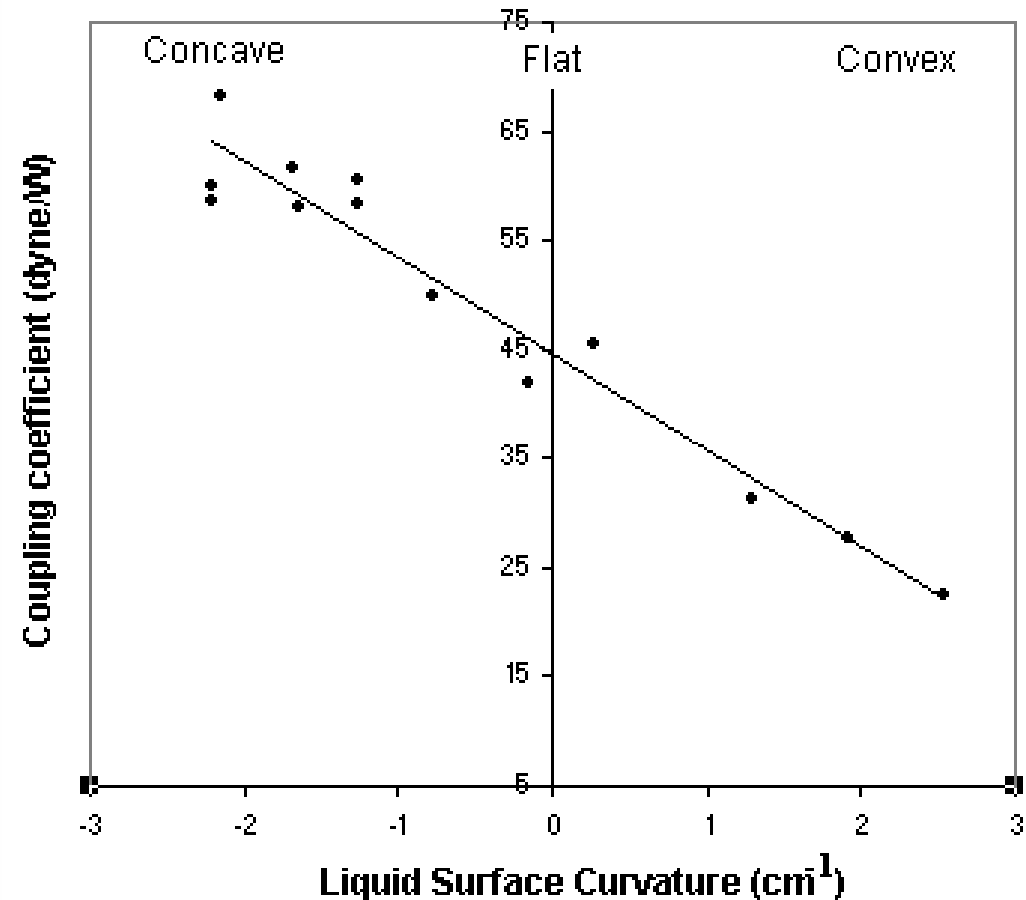
Water, flat, cylinder, 0.4 J, $2 \times 10^7 \text{ W/cm}^2$



- Curvature $\kappa \text{ (cm}^{-1}\text{)}$

$$\kappa \equiv \frac{1}{R}$$

- C_m directly dependent on κ





Imaging Experiments



ICCD Imaging

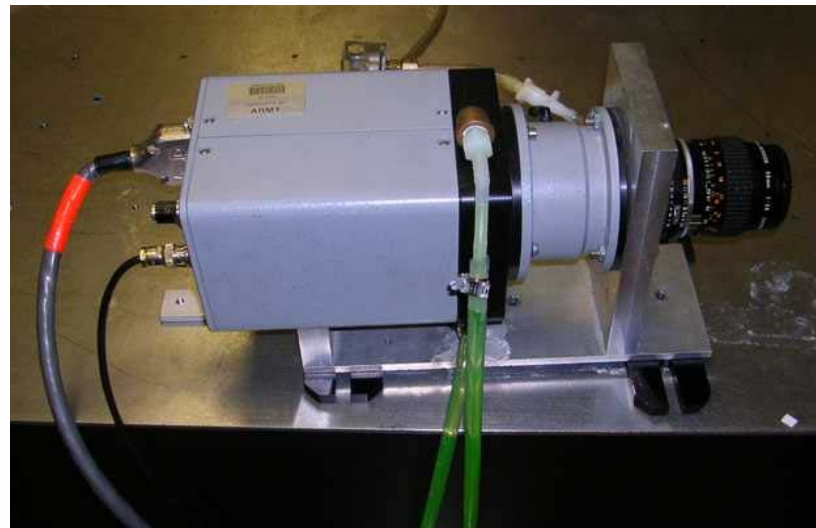
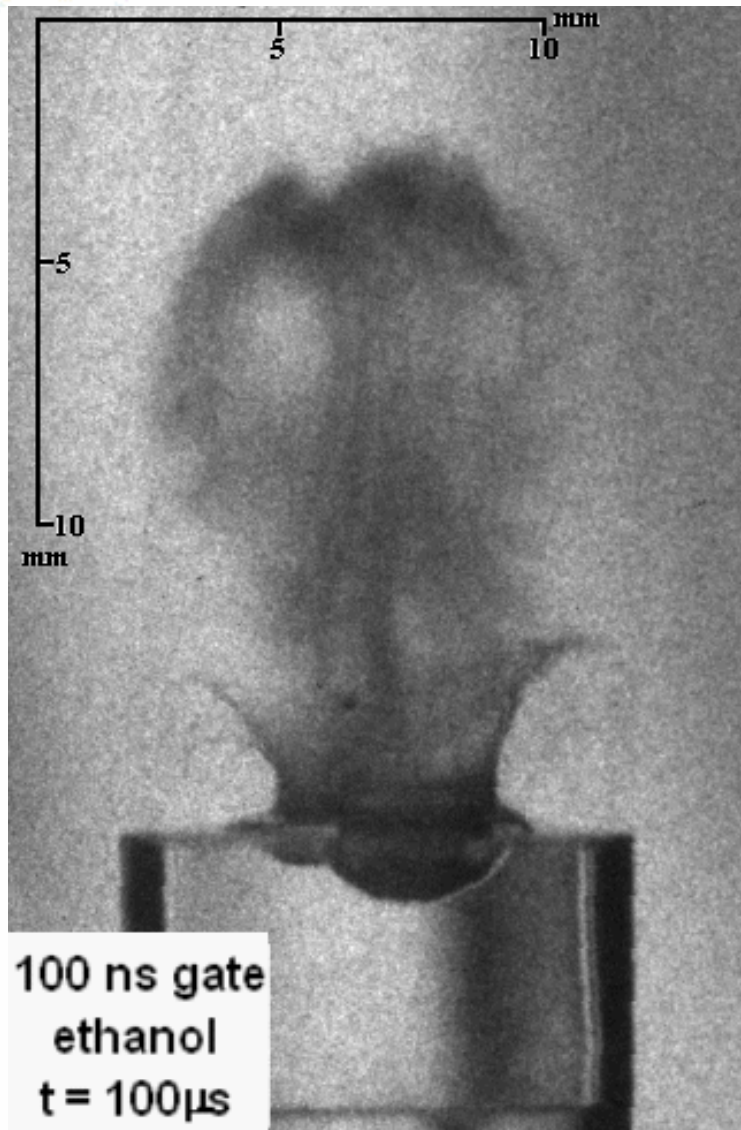
Information on:

Initial plume velocities

Cavity growth rates

Characteristic physical processes

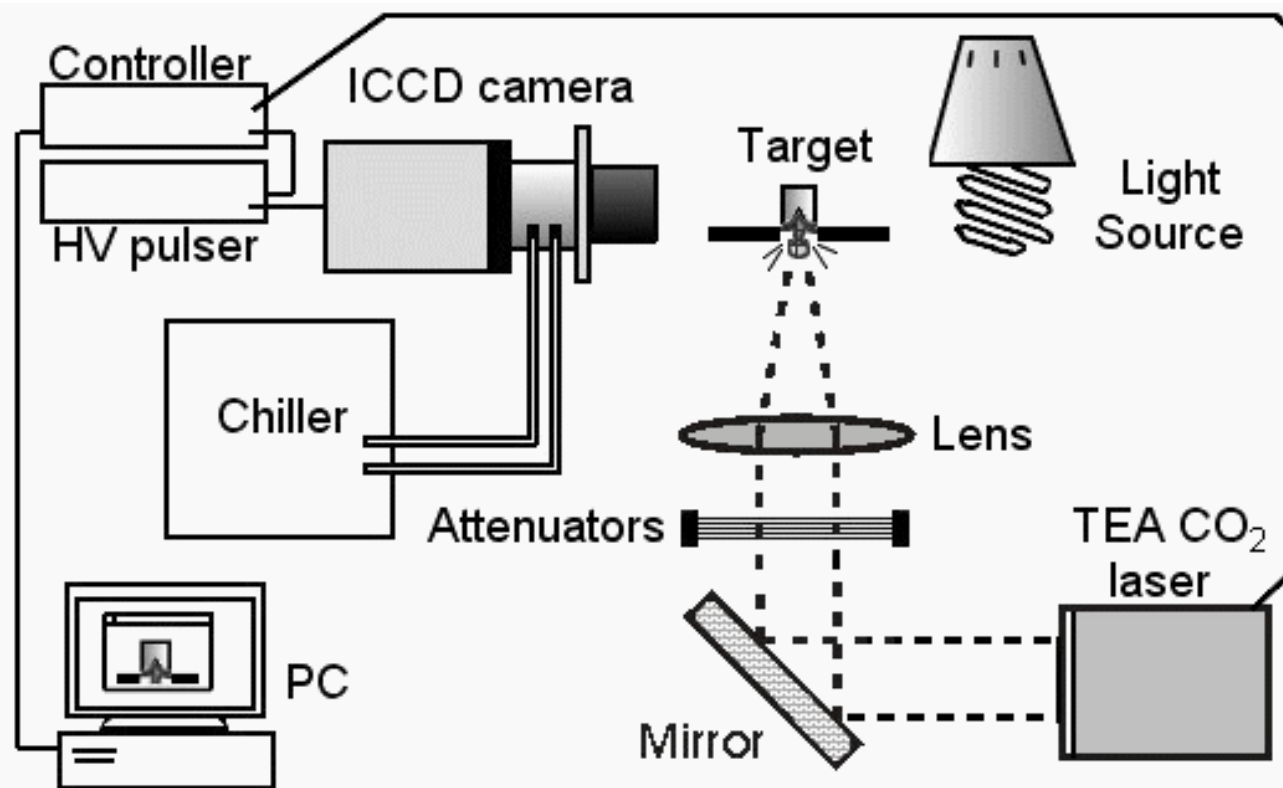
Timeline of processes





ICCD Ballistics Setup

- Gated CCD technique
- Single laser shot per image
- Highly repeatable
- Composite sequences
- 382 x 574 pixel images
- >5 ns gate width (exposure)
- 5 ns - 83 ms delay





Coupling Coefficients, dyne/W

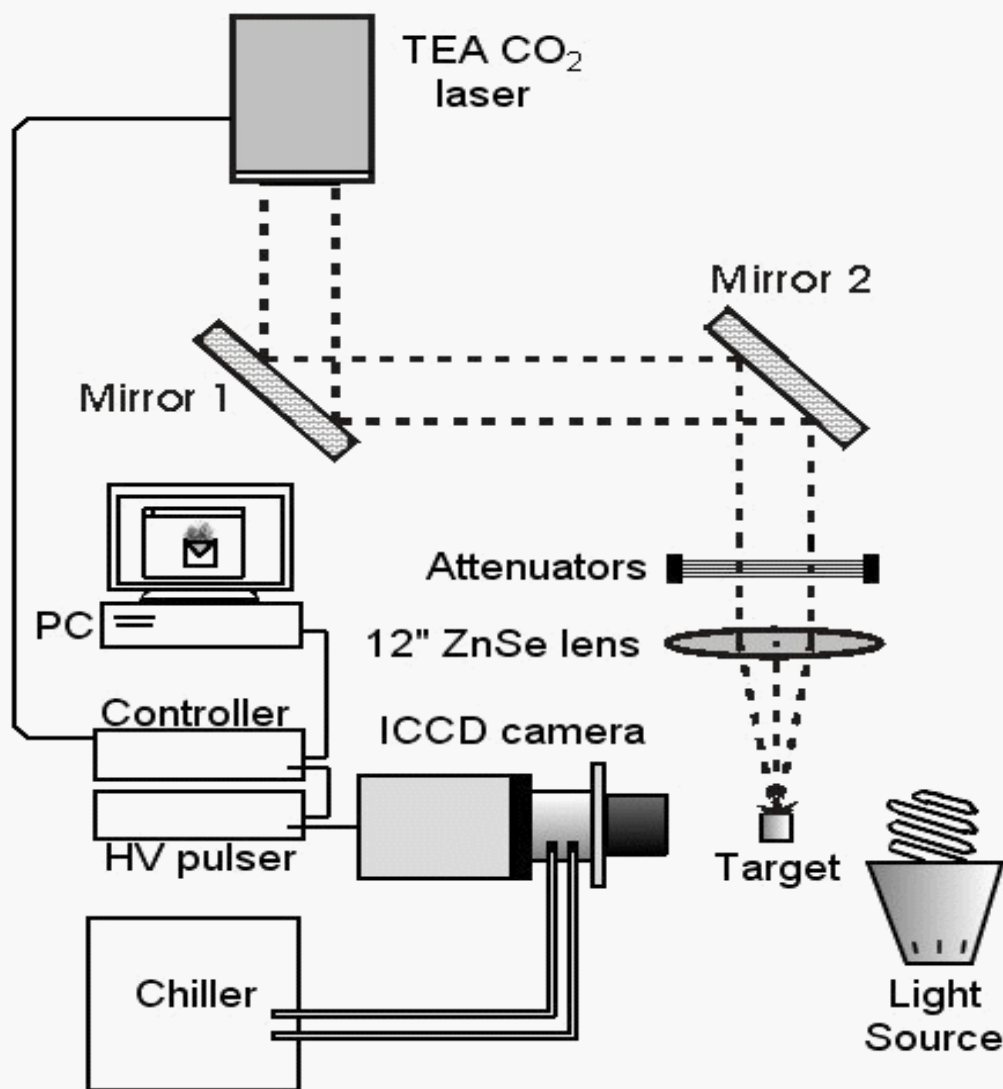
(Water, 3 mm² spot size)

Energy (J)	Irradiance (W/cm ²)	Small Force Sensor	Large Force Sensor	Ballistics
0.4	4 x 10 ⁷	110 ± 14	-	98 ± 9
1.2	1 x 10 ⁸	44 ± 24	53 ± 21	37 ± 5
3.6	5 x 10 ⁸	-	14 ± 3	14 ± 2

$$C_m = \frac{I}{E_{\text{pulse}}} = \frac{m}{E_{\text{pulse}}} \sqrt{2 g h_{\text{max}}}$$

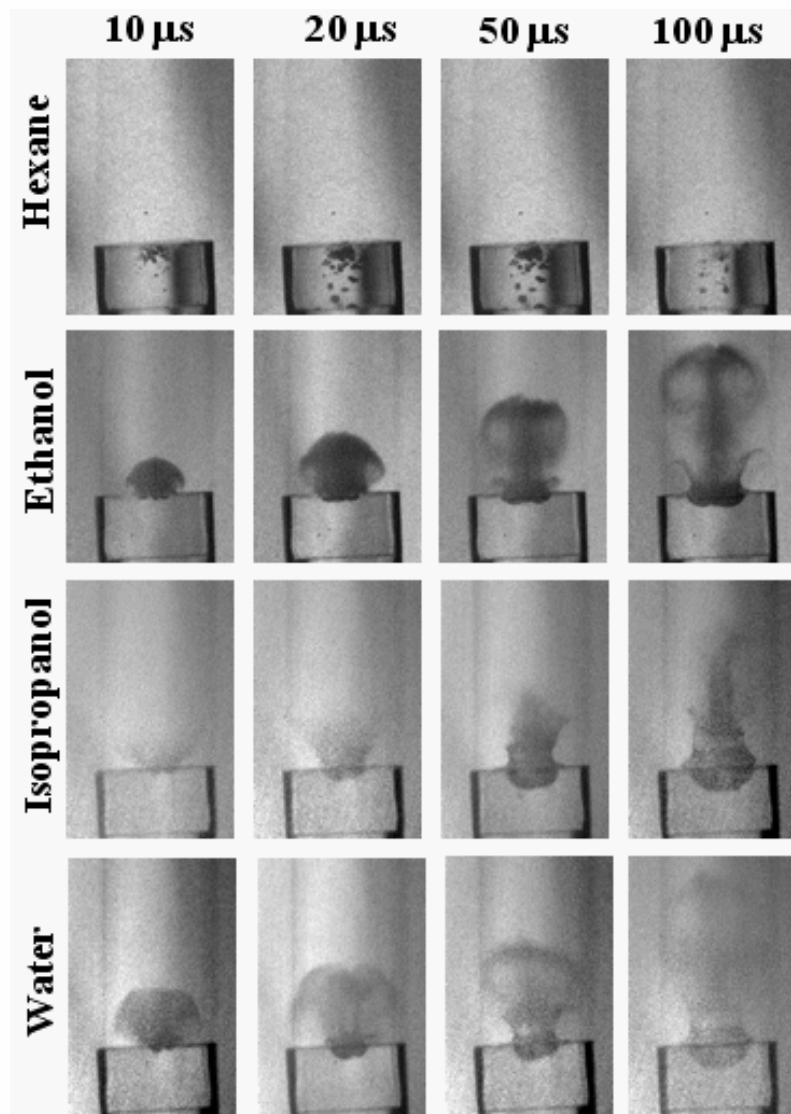


Imaging Setup





ICCD Images



Volume-absorbing

(hexane)

- No observed plume
- No cavity formation
- Boiling

Surface-absorbing

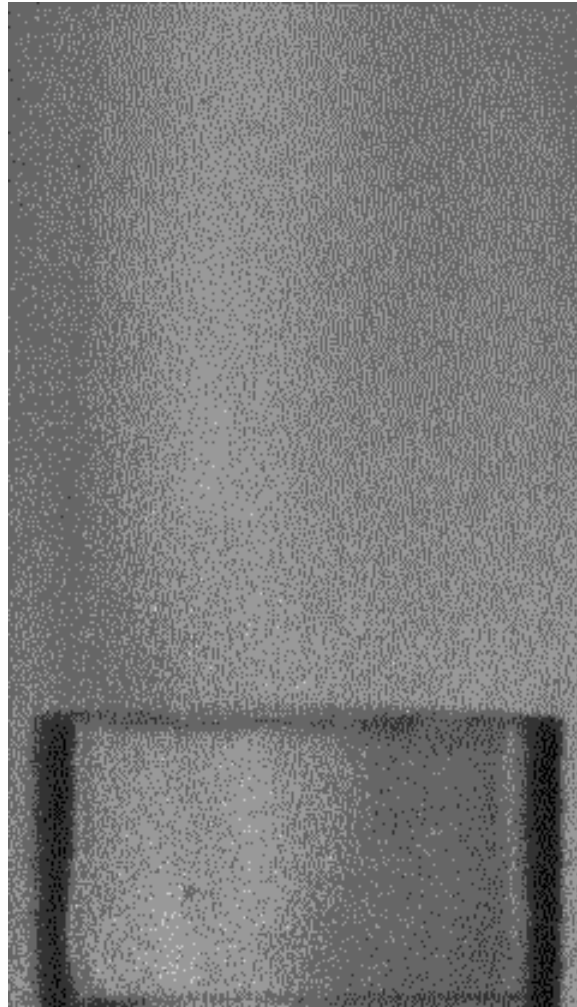
(ethanol, isopropanol, water)

- Vapor plume
- Cavity formation



Surface Absorption

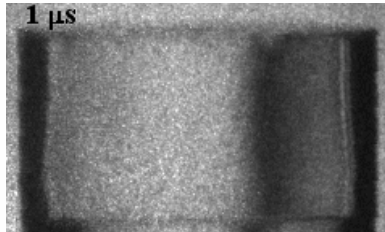
Ethanol, 0.4 J, 4×10^7 W/cm²



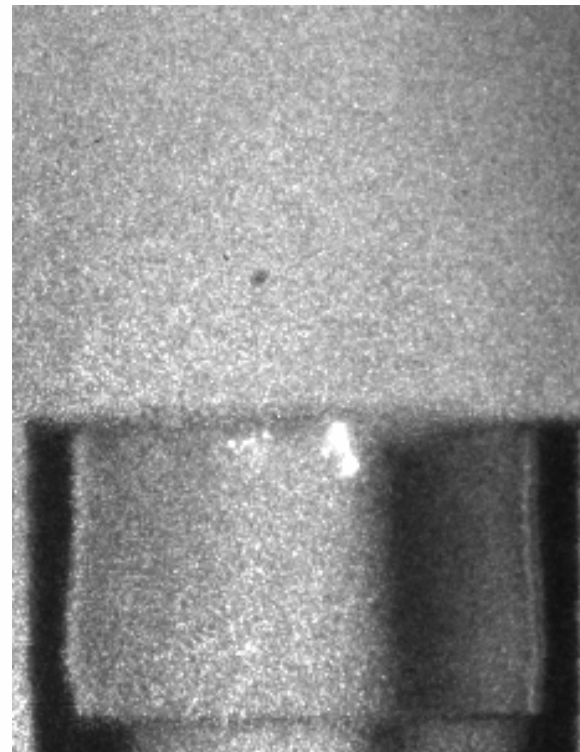
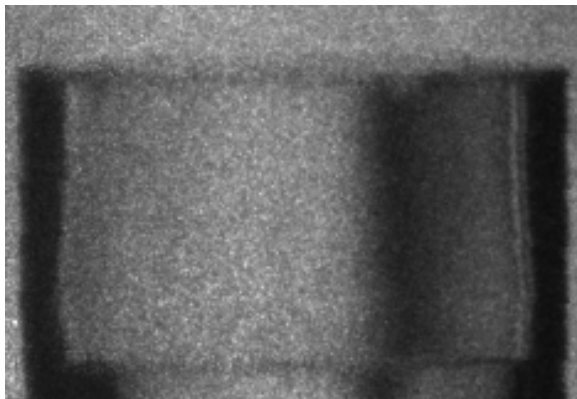
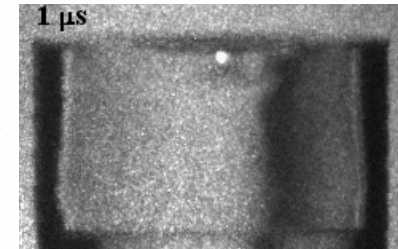


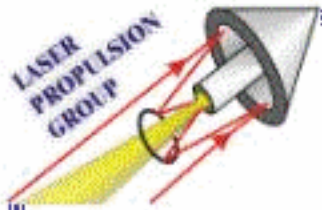
Volume Absorption (Hexane)

- 0.4 J
- $4 \times 10^7 \text{ W/cm}^2$
- No plasma
- No cavity
- No plume
- Boiling



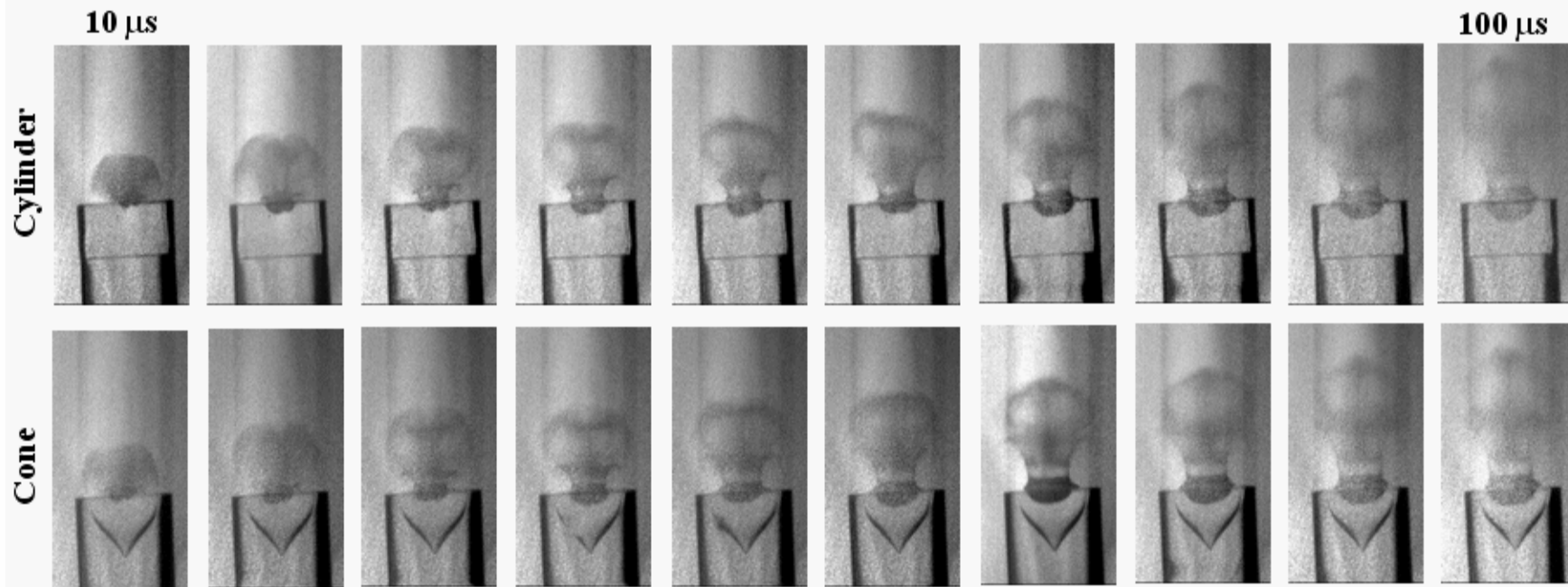
- 1.1 J
- $1 \times 10^8 \text{ W/cm}^2$
- Plasma
- Surface cavity
- Vapor plume





Containers: Cylinder vs. Cone

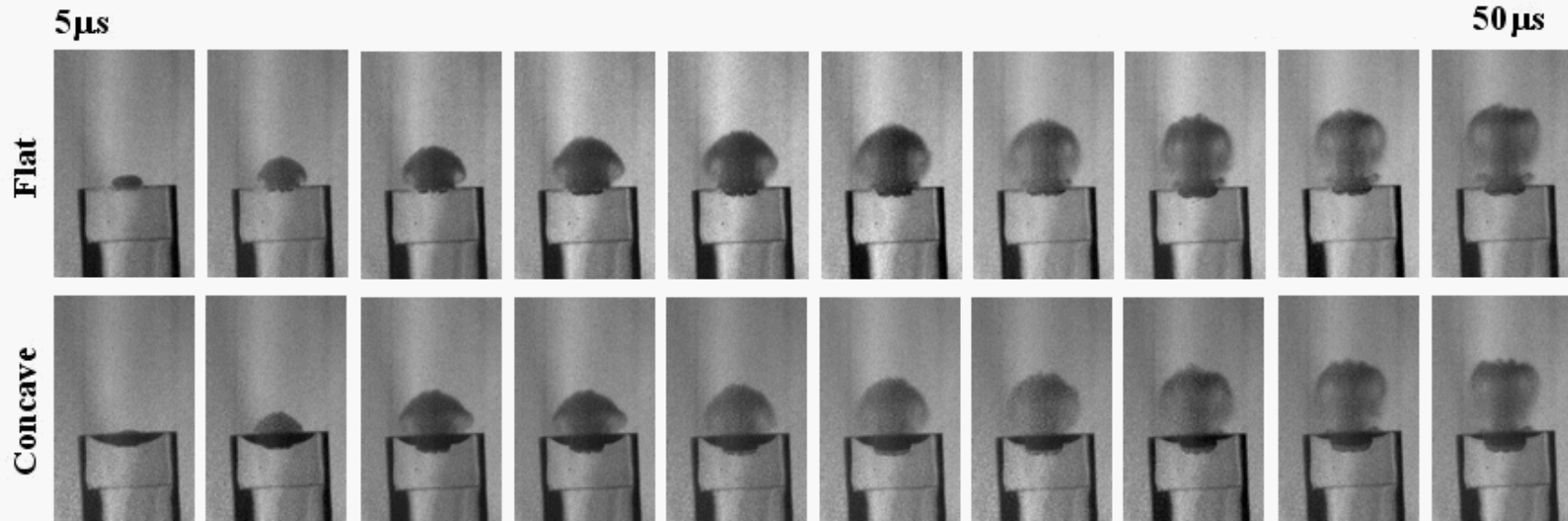
- Water, 10-100 μs
- Virtually no difference observed





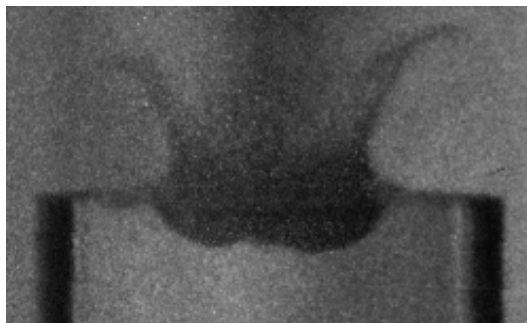
Surfaces: Flat vs. Concave

- Ethanol, 5-50 μs :

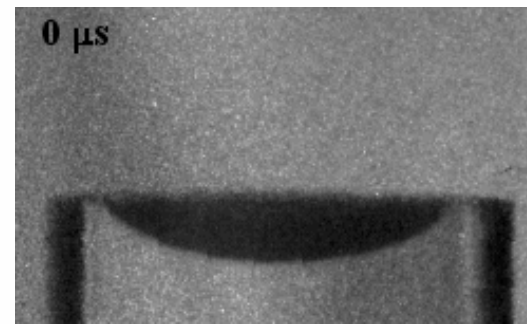


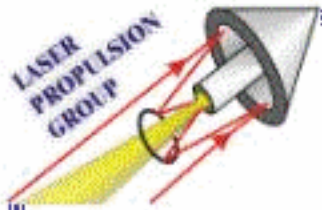
Effect of Initial Curvature (100 μs)

Flat:



Concave:



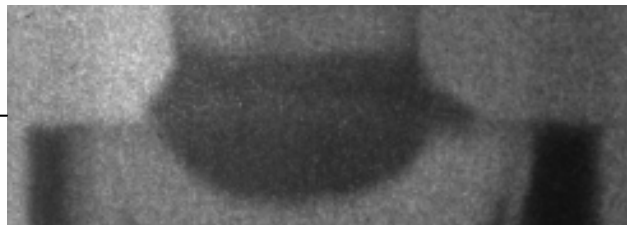
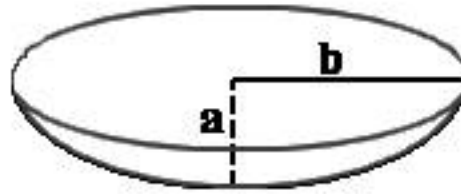


Analysis of Mass Loss and Cavity Growth

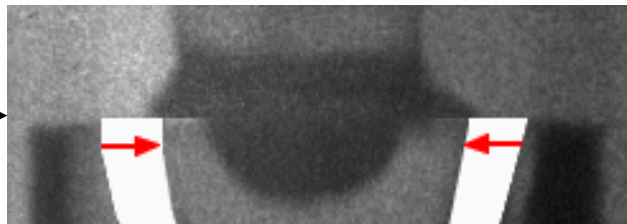


Model as oblate spheroid

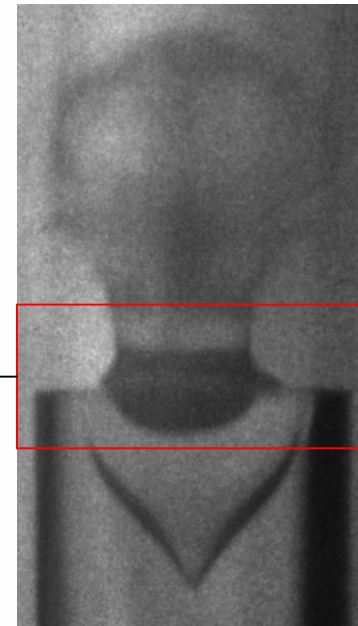
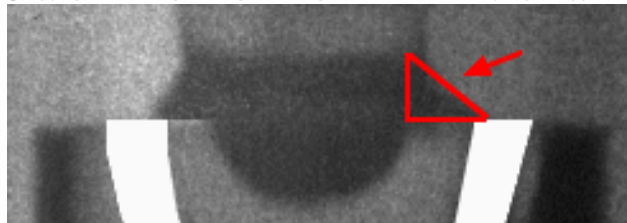
$$\left(V = \frac{2}{3} \pi a b^2 \right)$$



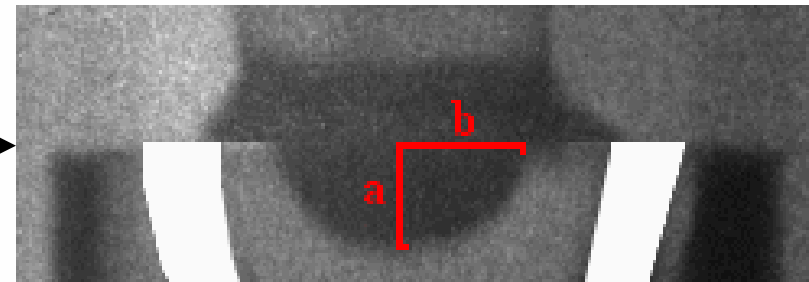
Correction for distortion



Subtraction of rim volume



Cavity measurement





Liquid Mass Loss

- All data using cylinder, flat surface, 0.4 J, 7×10^7 W/cm²
- Increased cavity growth during initial 100 μ s
- ICCD imaging: Mass (mg) removed during initial 100 μ s
- Scientific Balance: Total mass (mg) removed in entire process

Mass Loss (mg)

Liquid	Hexane	Ethanol	Isopropanol	Water
0-100 μ s	0	2 ± 1	1 ± 1	1 ± 1
Total Process	4 ± 1	51 ± 6	51 ± 2	51 ± 5
Ratio	0 %	4 %	2 %	2 %



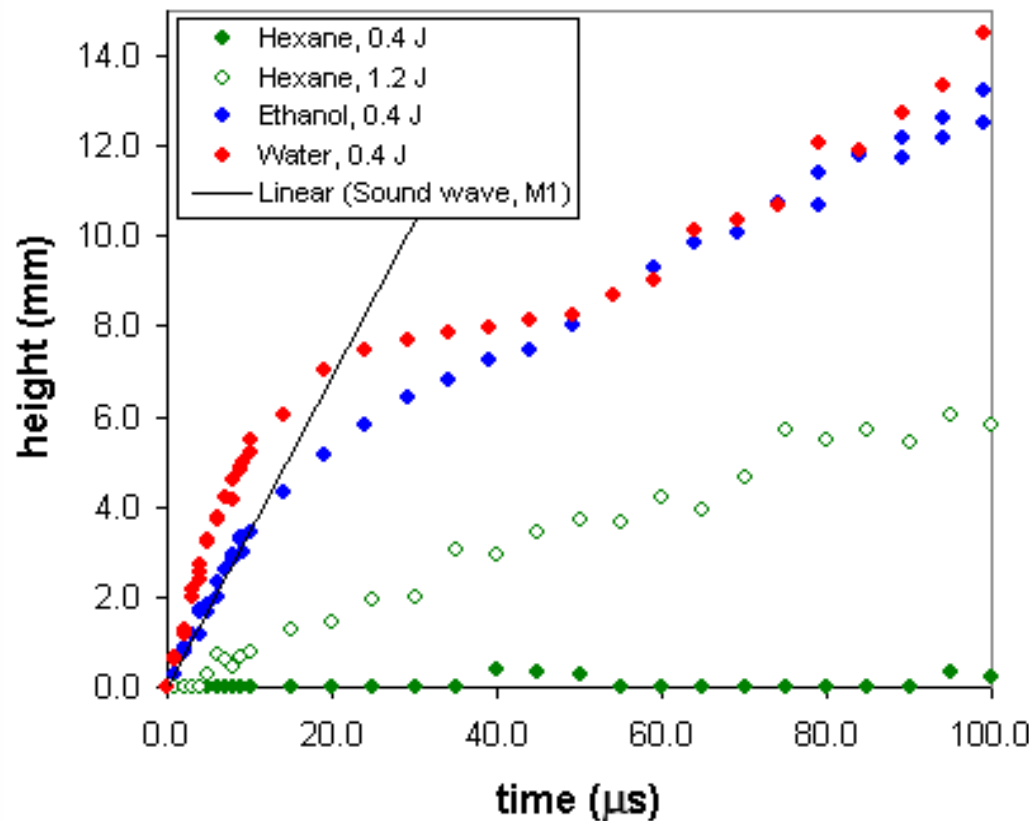
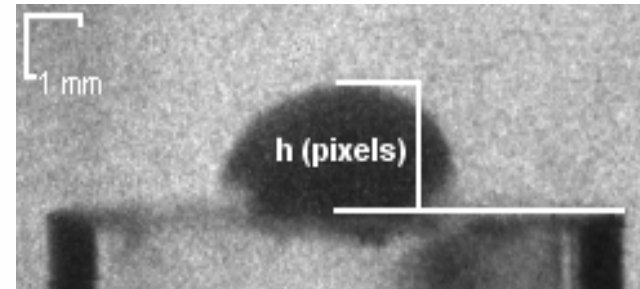
Analysis of Initial Velocities



Center plume front height h

Δh paired with known Δt

$$\lim_{t \rightarrow 0} \frac{\Delta h}{\Delta t} = v_0$$



Surface absorbing liquids
transonic – supersonic
initial velocities observed

Volume absorbing liquids:
subsonic to transonic
velocities observed



Specific Impulse and Internal Efficiency

$$I_{sp} \equiv \frac{I}{W} \approx \frac{u_e}{g}$$

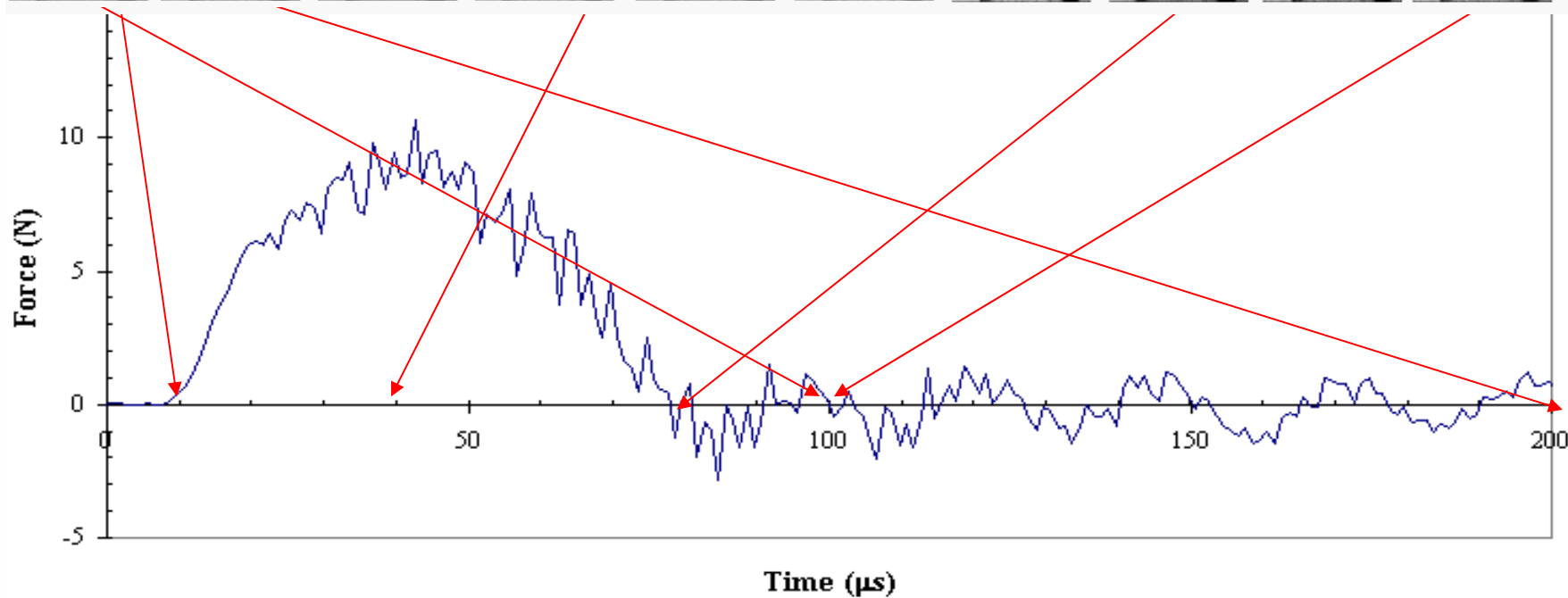
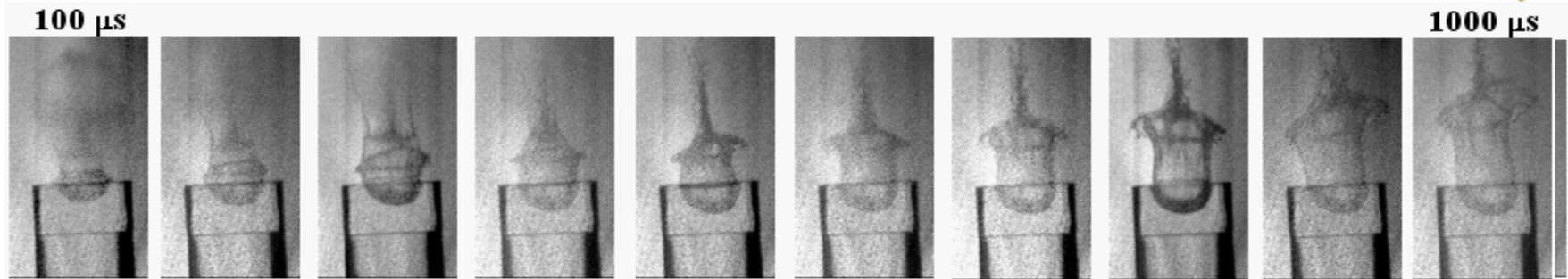
(1.6×10^7 W/cm², 0.4 J)

Specific Impulse (s)	Hexane	Ethanol	Water
from v_0/g	-	42 ± 1	84 ± 3
1 st 100 μ s	-	10 ± 5	20 ± 10
Total process	2.3 ± 0.6	0.40 ± 0.05	0.34 ± 0.05

Internal Efficiency (%)	Hexane	Ethanol	Water
from v_0/g	-	10.3 ± 0.7	18 ± 2
1 st 100 μ s	-	3 ± 1	4 ± 2
Total process	0.24 ± 0.08	0.10 ± 0.01	0.07 ± 0.01



Force Data with ICCD Imaging



(Water, cylinder, concave, 0.4 J, 4×10^7 W/cm²)



Conclusions



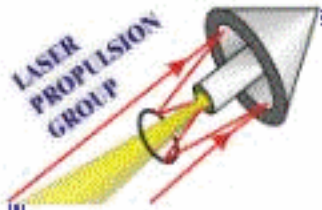
Conclusions

- 1) A series of experiments with time-resolved force sensors and ICCD imaging were conducted on liquids.
- 2) 2 major physical ablation processes are observed: vaporization and splashing. In some cases plasma formation was also achieved.
- 3) The major source of thrust generation in the laser ablation of liquids is vaporization.
- 4) ICCD imaging shows vaporization occurs from 0 to 100 μs after the laser pulse. Splashing is initiated after about 100 μs .
- 5) Force generation occurs during the vaporization regime.
- 6) The peak force was observed $\sim 40\text{-}50$ μs after the laser pulse.
- 7) Ballistics experiments corroborate the impulse measurements with force sensors.
- 8) Surface absorbing liquids show higher C_m ($\sim 50\text{-}150$ dyne/W) than volume absorbing liquids ($\sim 10\text{-}50$ dyne/W).



Conclusions (continued)

- 9) C_m is dependent on surface geometry for surface absorbing liquids.
Changing geometry does not affect C_m for volume absorbing liquids.
- 10) C_m is dependent on container geometry for volume absorbing liquids.
Changing container geometry does not affect C_m for surface absorbing liquids.
- 11) The majority of mass loss occurs due to splashing (>95%) rather than vaporization (<5%).
- 12) Momentum coupling was observed to be about 3 times more sensitive to changes in the surface curvature for surface absorbing liquids than to changes in the container geometry for volume absorbing liquids.
This is additional evidence in favor of a dominant vaporization mechanism.



THANK YOU



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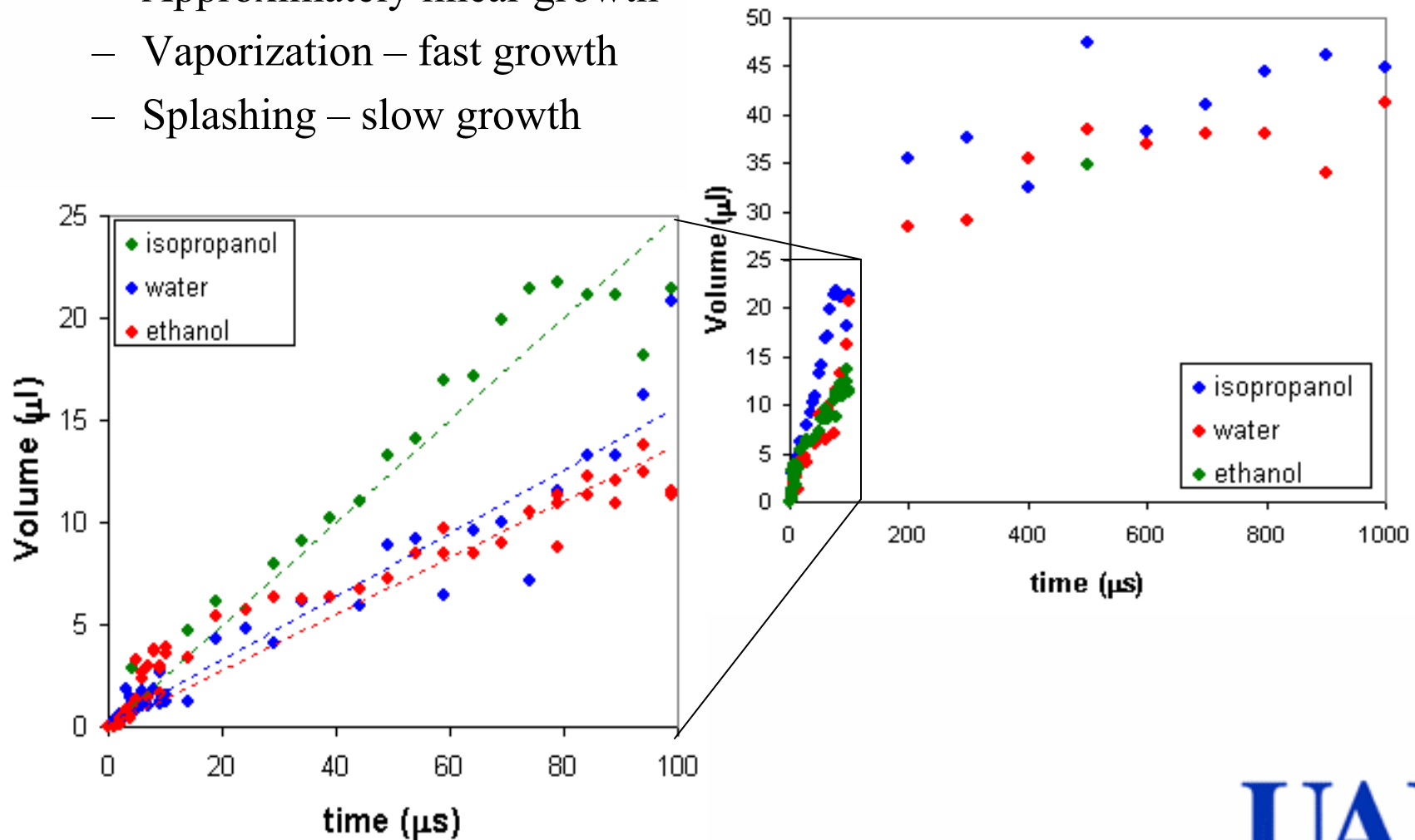
UAH
The University of Alabama in Huntsville





Cavity Growth

- 2 Regimes:
 - Approximately linear growth
 - Vaporization – fast growth
 - Splashing – slow growth





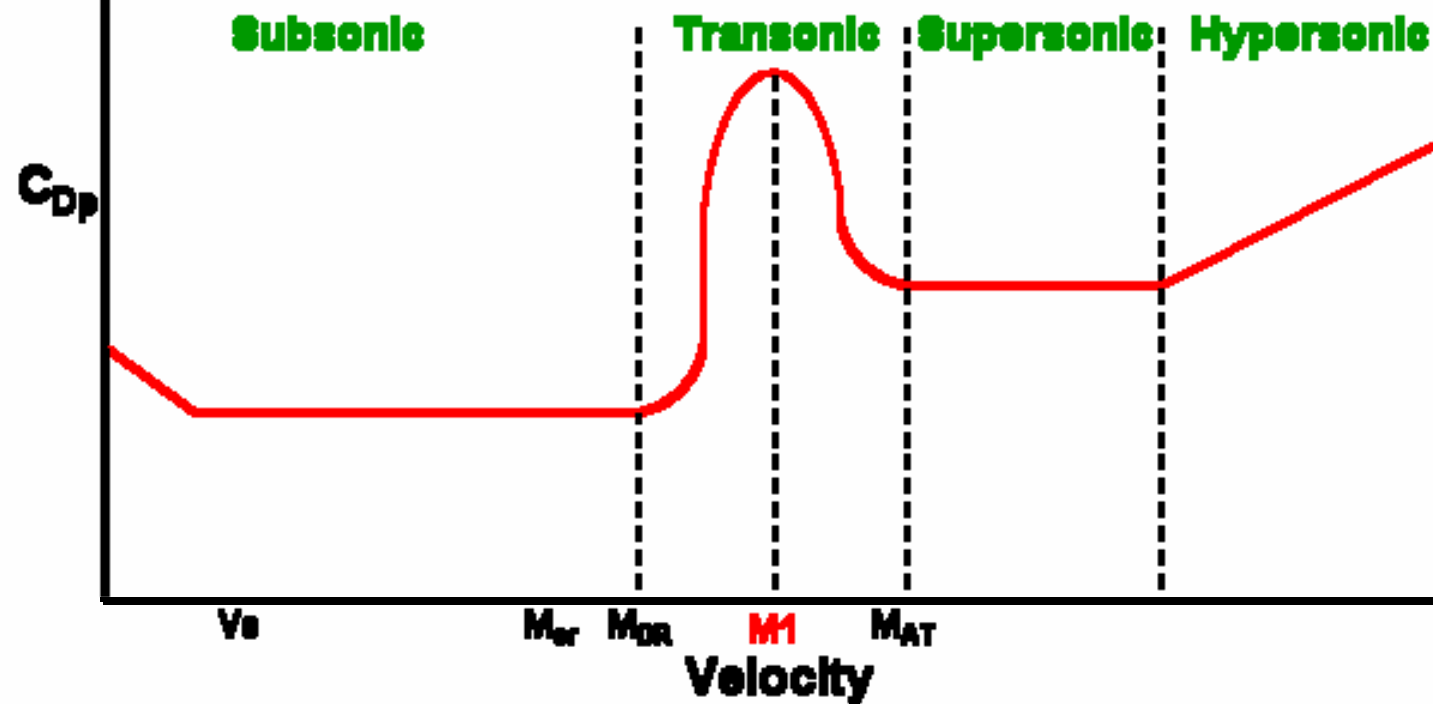
Challenges of Using Piezoelectric Force Sensors

- Measurements in an accelerating frame
 - Distortion*
 - Solution: Sensor at rest
- Rise time limits detection speed
 - Plasma processes $\sim 1 \mu\text{s}$
 - Liquid vaporization $\sim 100 \mu\text{s}$
 - Cavity Collapse $\sim 1 \text{ ms}$
 - Liquid splashing $\sim 10 \text{ ms}$
 - (Force sensors: $5 \mu\text{s}$ rise time)
- Natural frequencies
 - Solution: Fourier analysis



Drag vs. Velocity

Coefficient of Parasite Drag Vs. Velocity

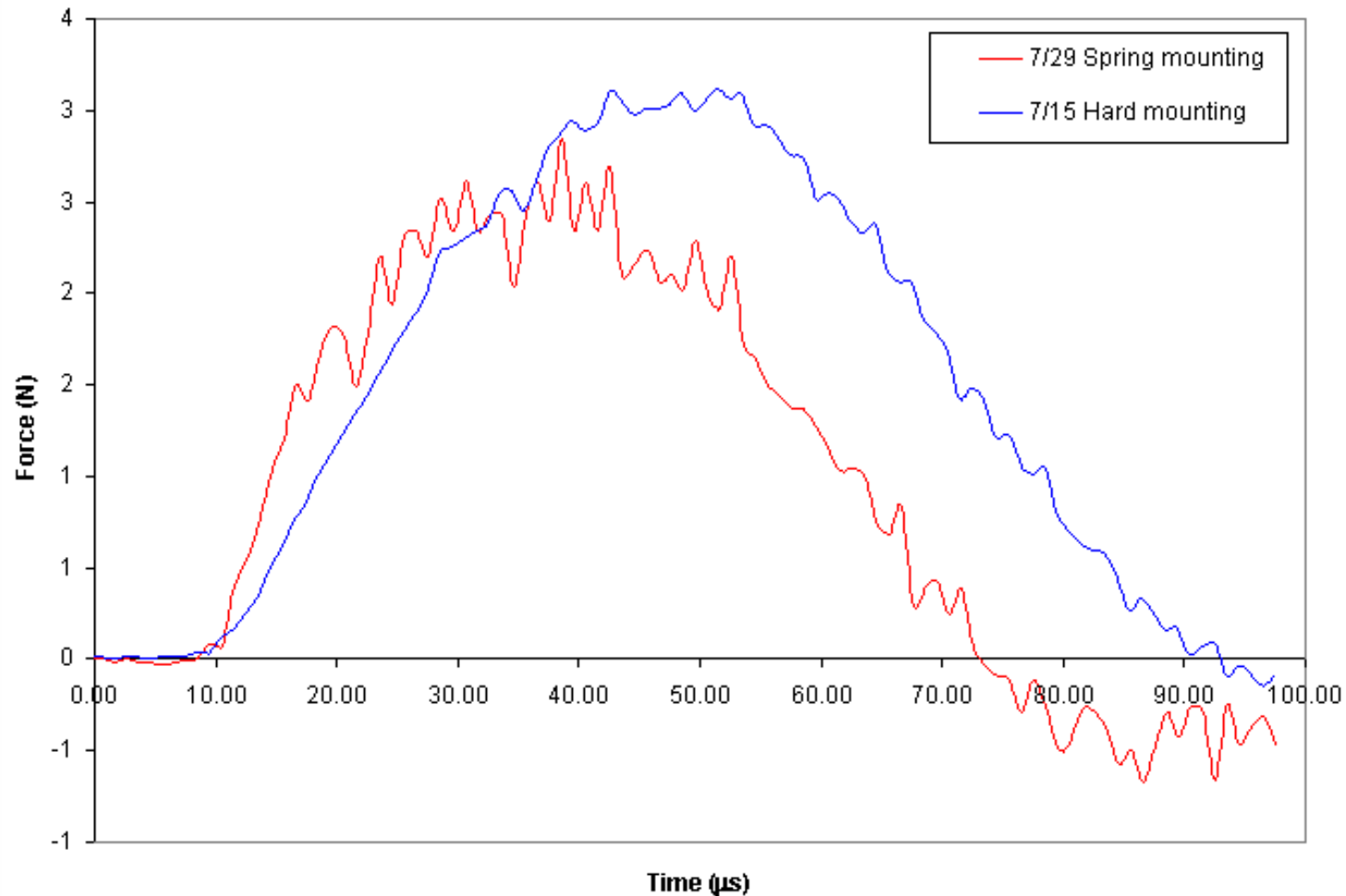




Force Sensor Distortion

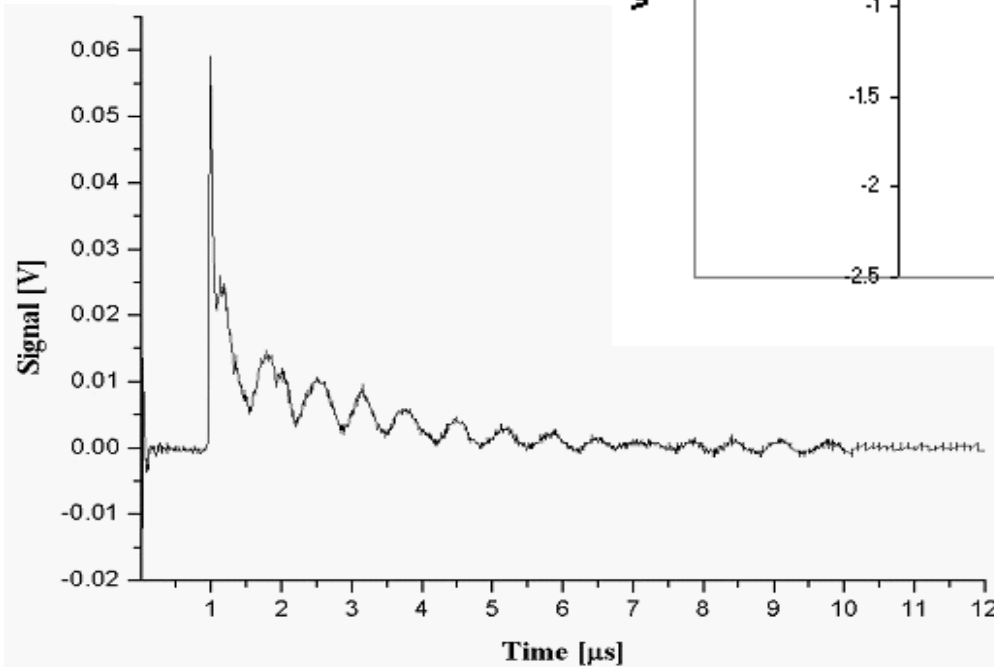
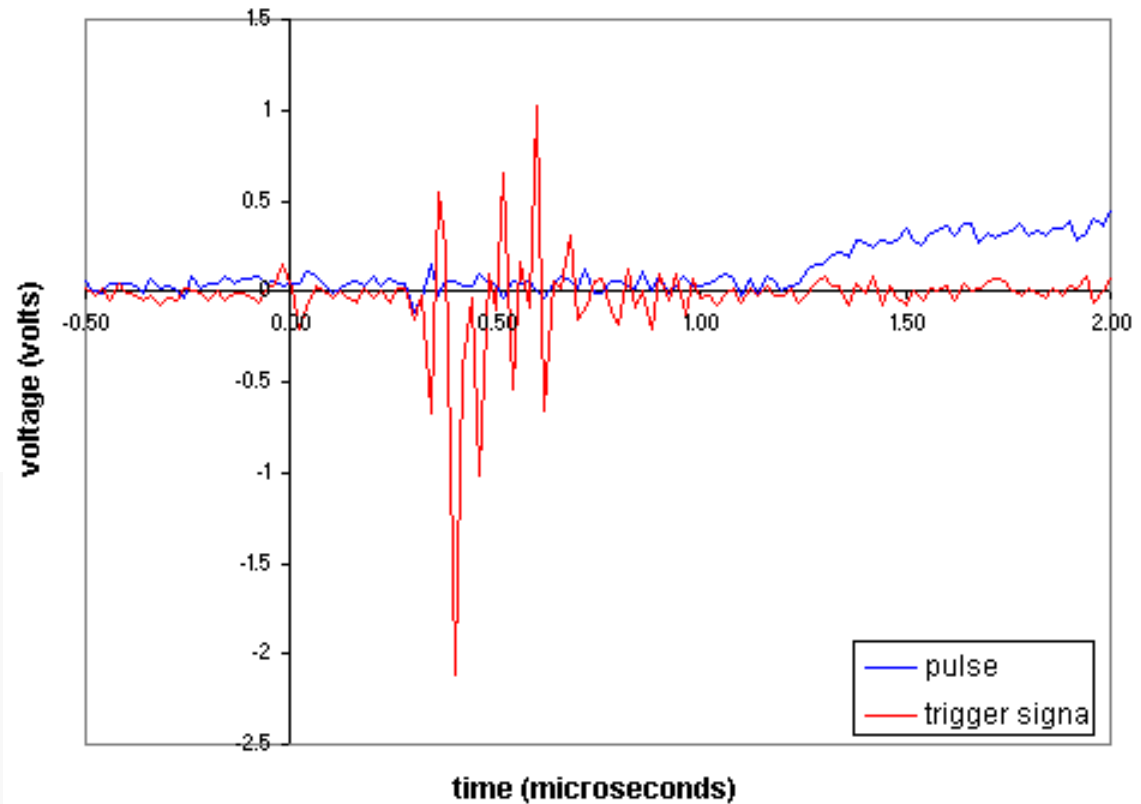
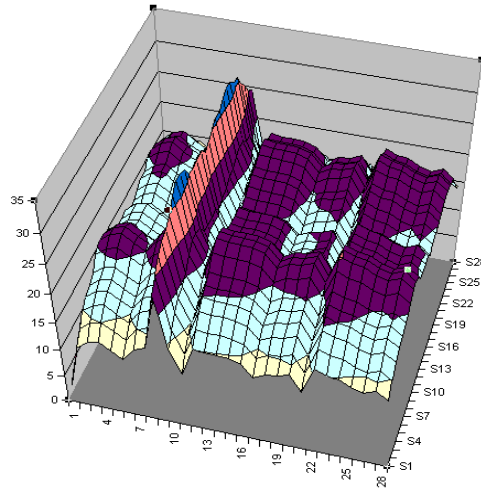
- Spring mounted vs. Hard mounted sensor

[back](#)





Laser Properties





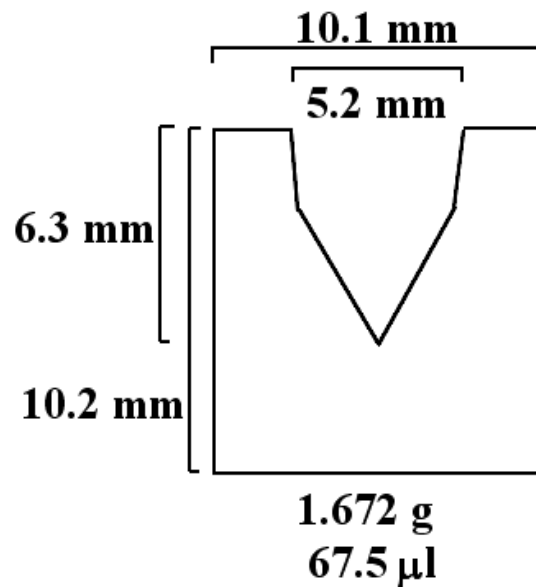
Liquids

	Hexane	Ethanol	Isopropanol	Acetone	Water
Chemical Formula	C_6H_{14}	C_2H_5OH	C_3H_7OH	C_3H_6O	H_2O
Absorption Coefficient (cm^{-1})	~ 0	17	67	~ 100	~ 3300
Absorption Depth (μm)	large	574	149	78	3
Density (g/ml)	0.66	0.79	0.785	0.790	1.0
Molecular Weight (g/mol)	86.18	46.07	60.10	58.08	18.02
Enthalpy of Vaporization (kJ/mol)	28.85	38.6	39.85	29.1	43.99
Surface Tension (dyne/cm)	18	22.3	21.7	23.7	73.05
Viscosity (mPa-s)	0.3	1.07	2	0.306	1.002

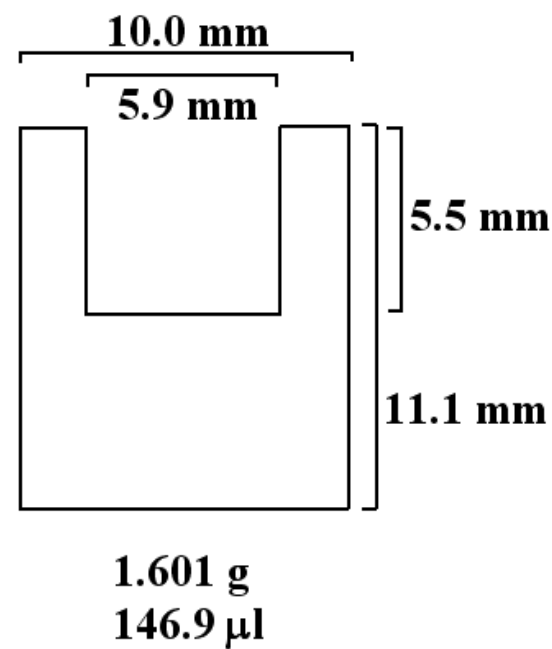


Quartz Target Containers

Cone



Cylinder





Surface Distortion

