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MINI-ROCKET USER GUIDE

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System Simulation and Development Directorate
Aviation and Missile Research, Development, and
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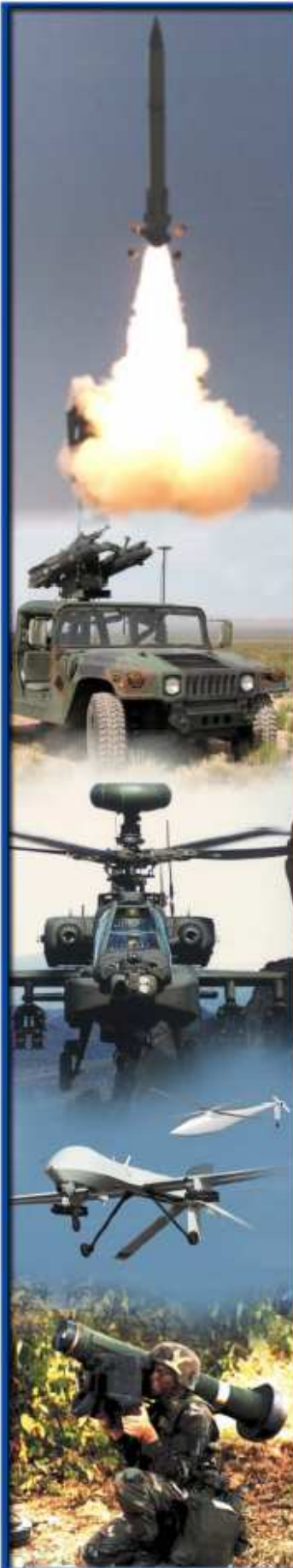
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13. ABSTRACT (Maximum 200 Words) This document describes the use of a missile/rocket fly-out model that represents a significant advance in efficiency for these type of simulations given its modest requirements for complexity and runtime efficiency. The model is useful for generating trajectories and associated flight parameters for multi-stage powered missiles flying over a rotating, spherical earth. The model uses a unique osculating plane formulation that preserves relatively high fidelity while maintaining run-time efficiency and simplicity of input. This formulation provides for user-specified flight guidance options including ballistic flight and profiles for acceleration, flight path angle rate, and flight path angle. This model was designed to expedite many of the same analyses conducted with the old industry-standard ROCKET code – hence the name “Mini-Rocket.” See page ii				
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ABSTRACT (CONTINUED)

While this manual documents the use of a standalone, executable version of Mini-Rocket, it also provides enough information to configure the Mini-Rocket source code as an embedded model and/or to modify it for a specific application.

Mini-Rocket was built with C++ Model Developer (CMD). CMD is a highly-refined C++ source code environment for building missile simulations such as this one. CMD provides a common platform for building a wide range of missile simulations ranging from simple fly-out models to high-fidelity six Degree-of-Freedom (DOF) simulations. The benefit is a clearly structured architecture that makes it easy to maintain and discern model source code. However, no C++ knowledge is needed to use Mini-Rocket.

EXECUTIVE SUMMARY

Mini-Rocket is a very easy-to-configure, multiple Degree-of-Freedom (DOF) missile and rocket fly-out model that accurately generates trajectories in three-dimensional space, including maneuver characteristics. It features an advanced algorithm that accurately models missile dynamics at a fraction of the computational cost of conventional 6-DOF simulations while maintaining a significant amount of the fidelity. The program is ideal for those analyses requiring trajectory modeling without the necessity of detailed modeling of the onboard missile subsystems.

Program features include quick generation of trajectories and associated flight parameters for multi-staged rockets and missiles flying over a spherical, rotating earth. In addition to simple ballistic flight, user-selectable guidance options include user-specified profiles for acceleration, flight path angle rate, and flight path angle.

For maximum flexibility, the program is configured as a simple console application that retrieves data from an input data file at runtime. The program is written in standard C++ so that it can be readily compiled and ran on a wide range of computer operating systems. Mini-Rocket provides a viable alternative to 6-DOF simulation for many cases where 3-DOF simulation is inadequate and represents a significant advance in utility for these type of simulations given its modest requirements for complexity and runtime efficiency.

PREFACE

The Advanced Experimentation Branch of the System Simulation and Development Directorate (SSDD-AE), Aviation and Missile Research, Development, and Engineering Center (AMRDEC) has as one of its missions the task of developing and/or discovering resources that specifically aid the simulation design and analysis process. The technology initiative that is primarily responsible for this effort is the Aviation and Missile Collaborative Design Environment (AMCODE). The AMCODE is a toolbox that contains resources specifically tailored to optimize the work flow process associated with the digital simulation task. One of the cornerstone resources in the AMCODE tool box is the Mini-Rocket simulation. This tool is uniquely suited for a majority of simulation tasks performed by the SSDD and other AMRDEC directorates. It can be easily coupled with other AMCODE resources, such as a genetic algorithm, to provide powerful and fast turnaround analyses of Army systems. The Mini-Rocket simulation has evolved over the past 20 years and, as this report shows, has been extensively proven effective and accurate by numerous users on a wide variety of missile and rocket programs. The Mini-Rocket is a logical choice for AMCODE. It currently supports the design trade studies for Advanced Technology Objective (ATO) programs within the AMRDEC and other Army labs. It is also the backbone architecture for effectors (guns, missiles, lasers) in the AMRDEC Missile Server Executable Code (ICD Version 2.3).

George A. Sanders, III

“Don’t put another ‘*six-dof*’ into our ‘*six-dof*’,” our lead simulationist said (or really *commanded*) as I was given instructions to upgrade the target model in our interceptor missile 6 Degree-of-Freedom (6-DOF) simulation. The modeling requirement was somewhat unique: we needed to model the sudden in-and-out-of-plane, “jinking” motion of a postulated maneuvering re-entry vehicle. This new target was beyond the capability of the existing point-mass target model (3-DOF) that heretofore had served us well. On the other hand, the complexity of upgrading the model to a full 6-DOF representation was clearly overkill given the fidelity required for this target. The timeframe was 1985. Little did I know at the time that my response to this model requirement would begin an over 20-year model legacy whose wide range of application I could then never have imagined.

A simple, but powerful, equations-of-motion formulation was arrived at after seemingly endless trials and explorations into the arcane aspects of rigid body dynamics modeling. The search ended with the discovery of a unique way to apply an *osculating* plane to describe the motion. This resulted in a computationally efficient, intuitive algorithm that was first mechanized in a FORTRAN subroutine. It allowed the modeling of a wide variety of trajectory motions in three-dimensional space, but at much less the cost and complexity of a full 6-DOF representation. The subroutine quickly proved itself capable of simulating a wide variety of target trajectory behaviors for objects flying in the atmosphere. But was the model only confined to unpowered flight trajectories? What if a longitudinal force was added to emulate an axial thrust component?

With the addition of an axial force, the subroutine rapidly evolved into a standalone rocket and missile model where the trajectory could begin from a stationary launch point. This efficient trajectory generator quickly found application for a number of modeling tasks. Depending on analysis needs and the advance of programming language maturity (mine as well as advance in state-of-the-art), it was coded in many dialects of Basic, Pascal, C, Ada, and many others. It was

used by myself and a growing list of users from things as simple as the motion of a piece of debris, to endo- and exo- interceptor missiles, to intercontinental ballistic missiles, to theater and tactical missiles and targets, and even to ground-test, sled-launched test articles. Versions of the model were also coded to be embedded as missile model representations in larger battlefield simulations¹. There are doubtless many other applications that I am unaware of. Every now-and-then, someone unexpectedly informs me that they are using the model or they have seen it used (in many cases, they had no indication of the origin but saw my name in the source code!). The model representations have proved their worthiness by providing efficient analysis results in the many cases where the overhead and resources of a full-up 6-DOF were not required. Over time, the domain for requiring trajectory modeling above that of a 3-DOF but not needing those of a 6-DOF proved to be vast and the model fit. It fit very well.

Its widening use dictated that it be called something, so the name Mini-Rocket was adopted and seemed to “stick.” Many users had previously used the industry-standard ROCKET² code that was very capable, but had become somewhat antiquated by the advance of programming language technology. “Mini” implied that tools developed from the algorithms had much of the functionality of ROCKET but that the code was more streamlined and easier to use. Using “ROCKET” in the name conveyed functionality to a community that was already aware of the very successful legacy of ROCKET (but recognizing that Mini-Rocket was developed completely independently from ROCKET).

The formulation and publication of the C++ Model Developer³ (CMD) provided an ideal medium for a formalized mechanization of the Mini-Rocket model. CMD was expressly designed for building simulations of dynamical systems and has a well-defined and mature architecture. CMD’s concise architecture was a natural complement for the simple but powerful algorithms in the Mini-Rocket equations of motion. The CMD-implementation of Mini-Rocket continues and expands on the successful original Mini-Rocket legacy of a powerful tool for trajectory analysis. The CMD-based Mini-Rocket is currently being used for a wide variety of missile modeling applications by a diverse community within the U.S. Army’s AMRDEC and elsewhere.

What began as a FORTRAN subroutine has grown into a versatile and widely-used tool for trajectory modeling and will certainly continue to proliferate. The malleability and simplicity of the algorithms makes it easily tailorable for many applications. This guide aims to continue and encourage this proliferation by undergirding the tool with formalized implementation and documentation.

Ray Sells
May 24, 2007

¹ *Extended Air Defense Simulation (EADSIM) Methodology Manual*, Section 5.9, “Interceptor Missile Flight.” Teledyne Brown Engineering, Huntsville, AL, 1995.

² Boehm, Barry W. *Rocket: Rand's Omnibus Calculator of the Kinematics of Earth Trajectories*. Prentice Hall, (1964).

³ Sells, H.R., Sanders, G.A., Snyder, G., Hester, J.W., and Painter, L. 2005. “C++ Model Developer (CMD) User Guide.” U.S. Army Technical Report AMR-SG-05-12, April 2005.

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1 INTRODUCTION

Mini-Rocket provides the capability to model realistic trajectories associated with the boost and fly-out of a multi-stage missile flying over a rotating, spherical earth. Multi-stage missiles are modeled using flight sections to represent the missile's properties. Each flight section consists of a separate specification for the aerodynamic, propulsion, and guidance parameters. Within a flight section, any combination or sequence of guidance modes can be selected including ballistic, prescribed acceleration, prescribed flight path angle rate or prescribed flight path angle. This flexible combination of guidance options makes it possible to replicate virtually any missile steering behavior, both in-plane and out-of-plane in three-dimensional coordinate space. A unique osculating plane representation keeps prescribed maneuvers clearly discernable in either pure pitch or yaw even though the missile motion itself may be complex.

The flight trajectories during boost and fly-out are realistically constrained with aerodynamic and structural capabilities. Lateral acceleration for steering is aerodynamically limited according to a user-specified angle-of-attack. Also a "hard" limit is placed on lateral steering acceleration representing maximum g-loading structural capabilities.

This missile model was formulated with particular attention to the speed of execution. A unique point-mass model with wind-axes is used to include the variation of drag with angle-of-attack as the missile maneuvers without resorting to the computational burden associated with a full 6 Degree-of-Freedom (DOF) rigid body for the missile. Trajectories generated with this modified point-mass model have been shown to closely match those generated by a very high fidelity 6-DOF simulation (within the resolution of time-history plots).

Mini-Rocket was built with C++ Model Developer (CMD)[1]. CMD is a highly-refined C++ source code environment for building missile simulations such as this one. CMD provides a common platform for building a wide range of missile simulations ranging from simple fly-out models to high-fidelity 6-DOF simulations. The benefit is a clearly structured architecture that makes it easy to maintain and discern model source code. However, no C++ knowledge is needed to use Mini-Rocket.

This manual is organized to equip the user to get Mini-Rocket "up and running" as quickly as possible. Following this objective, the following section describes installation which is easily accomplished since Mini-Rocket runs from a command-line interface. The contents of the input data file are then described in a narrative tied to an example set of input parameters. Although not required for operation, an in-depth mathematical description is then presented to give additional insight into the model and how it can be extended. Perhaps the most important question about any modeling tool is how well it represents what is being simulated. Mini-Rocket has been rigorously compared to other accepted models and has obtained the confidence of a wide variety of users for its ability to accurately model trajectories. A variety of example cases supporting this claim are shown in Section 5. Section 6 gives a brief description of Mini-Rocket's implementation in code using the aforementioned CMD. This section is a starting point for consulting the source code and CMD documentation [1] to understand the code mechanization behind Mini-Rocket. Appendix 1 describes operation of a convenient plotting tool (included with Mini-Rocket) for visualizing output. Appendix 2 builds on the input data

description in Section 3 showing a step-by-step example of using Mini-Rocket to generate a trajectory.

While a standalone, executable version of Mini-Rocket is documented in this manual, the underlying code that comprises Mini-Rocket is far more flexible than a simple standalone program. Due to its modular, object-oriented coding structure, the source code is easily configured for a broad range of applications including use as an embedded model in more broadly-scoped simulations or modifications to add additional functionality. Thus, this manual also serves the dual purpose as an introduction and starting point to configure the Mini-Rocket source code for custom-tailored applications.

2 INSTALLATION

Mini-Rocket is a single executable Windows file that is compatible with any MS Windows machine that has a DOS prompt¹. In addition to the single executable file, a data file is also required. Make sure the data file is in the same directory as the executable.

The program is most conveniently executed by typing `minirock` at the DOS prompt in a console window followed by a file name with the input data.

For example:

```
C:>minirock rocket.dat
```

If you do not include a file name with the `minirock` command, you are prompted for a filename:

```
Mini-Rocket v1.01  
by Ray Sells, DESE Research, Inc.
```

```
Input file: _
```

Output is printed directly to the screen after the data file is entered. Normal DOS file commands can be used to redirect output for storage, as needed. Mini-Rocket also automatically pipes data to an output file for post-processing (plotting, for instance). Instructions for this automatic output are in the following section.

¹ While the instructions for installing and running Mini-Rocket in this guide are directed at the Windows operating system, installation and running the program will proceed similarly for Unix/Linux operating systems since the program is operated from a command line interface.

3 INPUT DATA FILE

This section illustrates by example how to configure an input data file to be used by the Mini-Rocket missile fly-out model. The model can be used very effectively by making changes only to the input data file. The input data file specifies the missile's properties, its flight guidance instructions, and data reporting.

The missile fly-out is described by the use of multiple flight sections. Each flight section consists of a separate specification of aerodynamic, propulsion, and mass properties as well as guidance steering commands. Describing the missile as a series of flight sections provides the capability to model virtually any missile. Normally the flight section will correspond to a stage but this does not necessarily have to be the case. The mathematical formulation for each section is identical. Each section consists of specification for

- vacuum thrust profile
- specific impulse
- nozzle exit area
- initial mass
- aerodynamic reference area
- aerodynamic tables for lift and drag
- guidance instructions

Within a section, guidance instructions consist of a table specifying periods of operation (by means of sequentially listed start times) for any combination of four guidance phases:

- ballistic
- follow a commanded acceleration profile in the y and z channels
- follow a commanded flight path angle rate profile
- follow a commanded flight path angle profile

3.1 Data Formatting

Owing to CMD's input/output system, format restrictions on the input data are very relaxed since all numeric parameters are tagged to an identifier. The only rule on input is that the parameter name must appear followed by its value on a single line. An optional equals sign can be used between the name and value. The data can be specified in any order and there are no spacing or column restrictions on how or where the data can appear. Comments can be freely interspersed throughout the input data file.

Example:

The data in the input file can appear as:

```
tmax = 50.  
v0 = 100.  
h0 = 200.
```

The model also uses one- and two-dimensional tables in the data file. CMD also provides a very flexible format for specifying tables. The exact format is apparent in the table descriptions that follow.

3.2 *Scenario and Control Data*

Input data is divided into two sets. The first set (Scenario and Control Data) describes the fly-out scenario and initial conditions as well as execution model options. The second set describes the physical characteristics of each stage including aerodynamics, mass properties, and propulsion. This section describes the first set of data for the scenario and initial conditions.

The following parameters describe the fly-out scenario and model execution instructions.

```
**** rocket ****
tmax = 100.
echo = 1
lon0_d = 45.
lat0_d = 38.708
v0 = 0.01
h0 = 0.0
az0_d = -70.
el0_d = 90.0
xrail=1000.0
nstages = 3
rotating_earth = 1
```

These parameters are described in Table .

The tag `**** rocket ****` must appear in the data file before any of the parameters. This provides maximum flexibility to place the parameters anywhere in the file.

Table 1. Scenario and Control Data Descriptions

Name	Description
tmax	Simulation termination time. Missile launch is at time = 0. The simulation will also terminate if the missile's altitude is less than zero.
echo	echo = 1 to echo contents of data file to screen as they are read. echo = 0 for no printout. It is good practice to echo output while configuring the data file. That way, if the simulation crashes for some reason while reading the input data, you can see the last data item successfully read.
lon0_d	Launch point longitude on a spherical earth (deg).
lat0_d	Launch point latitude on a spherical earth (deg).
v0	The velocity of the missile when it is launched relative to the earth's surface (m/sec). This parameter provides the flexibility of starting the simulation at some time after the missile is actually launched or simulating an object with an initial impulse applied (such as a bullet or an air-launched missile).
h0	Launch point altitude above the spherical earth's surface (m).
az0_d	Launch direction azimuth (deg).
el0_d	Launch elevation (deg).
xrail	The distance from the launch point over which the missile's gravity turn (or pitchover) is constrained to zero (m). As its name implies, this parameter can be used to include the effect of a launch rail if the missile is launched non-vertically. The majority of missiles fail to build up enough instantaneous axial acceleration at launch to prevent excessive pitching over (due to gravity) when launched at an angle. Thus a launch rail is used to point the missile immediately after launch, giving it time to accelerate to sufficient velocity to develop lift. This parameter does not necessarily have to correspond to the launch rail's length (if one is used). As an alternative to formulating the guidance commands to make the missile travel a straight line after launch, much larger values of this length can be used (on the order of hundreds of meters or more) to prevent the missile from pitching over due to gravity.
nstages	Number of stages. The missile fly-out sequence is divided into discrete stages. Stages are numbered sequentially 1..nstages. Independent properties are specified for each stage. As a special case, two or more stages in this model can be used to describe a single physical stage on the missile whose properties change during flight for some reason. For example, the homing stage may have a protective shroud covering its seeker window in which case its aerodynamic properties would be different for the shrouded versus the unshrouded vehicle. In this case, two stages in this model could be used to describe the two sets of aerodynamic (and mass) properties for this single stage.
rotating_earth	A boolean parameter indicating whether or not earth rotation is turned on. rotating_earth = 1 sets the earth rotation rate to $7.292115(10)^{-5}$ rad/sec. rotating_earth = 0 sets the earth rotation rate to zero.

The following parameters specify output instructions to a data file and the screen.

```
Output
fname = OutputRun0.dat
pt = 0.01
pt_console = 1.0
```

These parameters are provided to designate output to the screen and to the output file designated with `fname`. The tag `Output` must precede these parameters and designates where in the file for the CMD parser to start looking for the parameters. The output data to the screen and file output are identical. `pt` and `pt_console` are the output time increments for the output file and console, respectively.

The parameters specified for output are as they appear in the source code with a `p_` prefix. `0` or `1` designates whether or not the variable is output (0-no, 1-yes). For convenience, a description of each parameter is included in the input data owing to the flexible nature of the CMD file parser.

```
p_range      = 1 Ground range over spherical earth surface (m).
p_h          = 1 Altitude above spherical earth (m).
p_vel       = 1 Velocity (m/sec).
p_mach      = 0 Mach number.
p_q         = 0 Dynamic pressure (N/m2).
p_p         = 0 Local atmospheric pressure (N/m2).
p_vs        = 0 Local velocity of sound (m/sec).
p_rho       = 0 Local atmospheric density (kg/m3).
p_gamma_d   = 1 Flight path angle, with respect to horizontal (deg).
p_alph      = 1 Total angle-of-attack (deg).
p_mass      = 0 Mass (kg).
p_xstage    = 0 Identifier for current stage.
p_t xv      = 0 Vacuum thrust (N).
p_tx        = 0 Delivered thrust (N).
p_amax_alph = 0 Max. acceleration at max.-specified angle-of-attack (m/sec2).
p_range_slant = 0 Slant range (m).
p_ay        = 0 y-acceleration, in velocity axes coordinate system (m/sec2)
p_az        = 0 z-acceleration, in velocity axes coordinate system (m/sec2)
p_ax        = 0 x-acceleration, in velocity axes coordinate system (m/sec2)
p_xmode     = 0 Current guidance mode.
p_ay_cmd    = 0 Commanded y-acceleration (m/sec2).
p_az_cmd    = 0 Commanded z-acceleration (m/sec2).
p_lat_d     = 0 Current latitude (deg).
p_lon_d     = 0 Current longitude (deg).
p_azimuth_d = 0 Current azimuth of velocity vector (deg).
p_ca        = 0 Axial force coefficient.
p_cd        = 0 Equivalent drag coefficient.
p_cna       = 0 Linearized normal force coefficient (/deg).
p_cla       = 0 Linearized equivalent lift coefficient (/deg).
```

These parameters may appear anywhere in the file; they need not be preceded by a tag.

3.3 Stage Section Data

The stage section parameters characterize the properties of each stage. The following data is identically specified for all stages on the missile, `1...nstage`. The data for each stage is tagged to a text identifier `**** stage n ****` where *n* is the number of the stage. The stages do not have to be specified in order (that is, stage 2 data may appear in the data file before stage 1 data). All data for each stage is associated with the most recent identifier that preceded it. Within the block of data for each stage, the parameters may be specified in any order.

Scalar parameters for each stage are specified as:

```
**** stage 1 ****
dt = 0.01
tstage=40.
sref=0.6206
anoz=0.
alphmax=20.
amax=100.
isp=261.865
m0=2499.895
```

These parameters are described in Table 2.

Table 2. Stage Section Data Descriptions

Name	Description
dt	Integrating time step (sec). 4 th order Runge-Kutta is used for integration. Note that you can use multiple time steps per stage by simply having two flight sections with identical properties, but with different time steps.
tstage	Time to transition to next stage (sec). This time is referenced from the starting time of the current stage (and NOT the current time).
sref	Aerodynamic reference area (m ²). This parameter is used in conjunction with aerodynamic coefficients to compute lift and drag.
anoz	The exit area of the nozzle used for axial propulsion (m ²). This exit area is used to adjust the vacuum thrust for atmospheric pressure. The local atmospheric pressure reduces the delivered thrust by the product of the exit area and the local ambient pressure.
alphmax	The maximum total allowable angle-of-attack for maneuvering (deg). To enforce realistic aerodynamic maneuvering, the lateral acceleration of a section is limited using the angle-of-attack. The lateral force acting on the vehicle is constrained using the product of the angle-of-attack, the linearized normal force coefficient, the aerodynamic reference area, and the local dynamic pressure. The maximum angle-of-attack for missiles is normally around 20 deg, beyond which the aerodynamics become highly nonlinear and less predictable.
amax	An absolute hard limit on how much acceleration the missile can generate for steering (m/sec ²). This constraint is intended to reflect the structural limits of the missile. This parameter typically varies 10 - 30 g's for long, slender and short, stubby missiles, respectively. Homing stages or kill vehicles can sometimes tolerate 50 or more g's. The acceleration is also constrained by maximum angle-of-attack depending on the atmospheric regime the missile is operating in.
isp	Boost propulsion parameter describing the unit thrust per rate of expenditure of propellant (fuel and oxidizer) (sec) in a vacuum. The thrust per unit rate of propellant expenditure is this parameter multiplied by gravity, g, which yields units of N per kg/sec. This quantity is typically in the range of 250 sec for solid rocket motors at sea level.
m0	The initial mass for each section (kg). Mass is reduced during missile section operation by propellant usage (if any) according to the specific impulse.

Tabular parameters for each stage are specified as follows. The tables can appear in any order; the only caveat is that they should appear after the appropriate stage tag identifier (the CMD parser first finds the stage tag identifier and then looks for the table tag).

The `txv_table` specifies the axial thrust profile.

```
txv_table
4
t txv
0.0 119484.02
40.0 119484.02
40.01 0.0
100. 0.0
```

This table is the vacuum propulsive thrust acting along the vehicle's longitudinal axis (N). Normally this is the thrust profile during boost. The thrust at any time is linearly interpolated from this table. The delivered thrust is the vacuum thrust minus the product of the nozzle exit area and the local ambient pressure.

The first entry is the table tag which must be `txv_table`. The number of table entries, 4, follows. The column labels, `t` and `txv`, are followed by their entries.

These `ca_off` and `ca_on` tables specify the axial-force coefficient data when the axial thrust is off and on, respectively.

```
ca_off
10 2
amach
.2 .9 1.0 1.5 2. 3. 5. 7. 9. 10.
alpha
0. 10.
ca
.223 .223
.415 .409
.466 .460
.369 .383
.304 .307
.233 .261
.188 .214
.177 .201
.177 .200
.178 .200

ca_on
10 2
amach
.2 .9 1.0 1.5 2. 3. 5. 7. 9. 10.
alpha
0. 10.
ca
.201 .201
.374 .368
.419 .414
.332 .345
.274 .276
.210 .235
.169 .193
.159 .181
.159 .180
.160 .180
```

This coefficient is used to calculate the missile's drag along the velocity vector. The drag force is the product of this coefficient converted to wind-axes, the aerodynamic reference area, and the local dynamic pressure. A linear two-dimensional interpolation is used to compute this coefficient as a function of angle-of-attack and Mach number. Two sets of data are provided for the drag coefficient since the drag varies significantly depending on whether the section's axial propulsion is on or off. The exiting plume of the motor's exhaust reduces the drag.

The first entry is the table identifier. The next row of data is the number of Mach # entries and angle-of-attack entries. The specific Mach #'s (rows of data that follow) and angles-of-attack (column of data that follow) are specified as shown. The `ca` data itself follows.

This `cna_table` specifies the normal force coefficient data.

```
cna_table
10
amach cna
.2 .0344
.9 .0381
1.0 .0444
1.5 .0459
2. .0490
3. .0565
5. .0563
7. .0562
9. .0560
10. .0559
```

`cna` is the linearized normal force coefficient as a function of Mach number (/deg). The force turning the missile's velocity vector for steering is calculated as the product of dynamic pressure, aerodynamic reference area, this coefficient, and angle-of-attack. This coefficient describes the linearization of the variation of the normal force coefficient with angle-of-attack. Typically, the normal force coefficient versus the angle-of-attack is a parabolic-like curve, but it can be approximated as a straight line for small angles-of-attack. The slope of this line is the linearized coefficient. The normal force coefficient slope is linearly interpolated from this table. The coefficient is typically on the order of 0.05/deg although it can be much larger if the missile has significant wing area.

This coefficient is used in tandem with the maximum angle-of-attack input to limit the missile's lateral acceleration for steering.

The first entry is the table identifier. The next row of data is the number of `cna` entries. The `cna` data itself follows.

The `guide_mode_table` is used to specify the type of guidance used for steering in this stage.

```
guide_mode_table
6
t mode
0. 0
20. 3
25. 1
30. 0
40. 3
100. 3
```

Four modes of steering can be independently specified: 0) ballistic, 1) follow a commanded acceleration profile in the y and z channels, 2) follow a commanded flight path angle rate profile, and 3) follow a commanded flight path angle profile. This table specifies the mode profile for each stage. The guidance mode stays constant between table inputs (that is, table is step-wise constant).

This method of guidance selection provides maximum flexibility in specifying how the missile flies. Any order or sequence of flight modes can be prescribed using a mode or modes more than once, if desired. Note that the commanded flight path mode, when active, always follows the commands in the associated table at that time. Thus only one commanded flight path angle table is needed even though this mode may be specified multiple times at different times in the flight.

Ballistic (`mode = 0`) is flight with no steering. The forces acting on the missile are only drag, gravity, and axial thrust, if any.

Depending on the flight modes selected, the following tables may be used. They must appear for each stage whether used or not. Linear interpolation is used on all the tables. The last value is used if the current time (independent variable) is greater than the last entry.

The missile can be commanded to follow a pre-specified lateral acceleration steering profile using `ay_table` and `az_table` (`mode 1`).

```
ay_table
3
t ay
0.  0.0
10. 9.0
40. 9.0

az_table
3
t az
0.  -999.0
10. -999.0
100. -999.0
```

The units are m/sec^2 . Mini-Rocket uses an *osculating plane* formulation which greatly simplifies this process. As shown in Figure 1, an orthogonal triad is composed of the missile's velocity axis (x), an axis perpendicular to the x-axis and tangent to the earth's surface (y), and a final axis that is the cross-product of the x and y axes (z). Thus the x-z plane is always the pitch plane (up-down) and the x-y plane is the yaw plane (right-left). This makes it very intuitive to prescribe the missile's motion since +/- z is always up/down and +/- y is always left/right. In other words, the `az_table` controls pitch and `ay_table` controls yaw. Contrast this simplicity with having to ascertain what these directions are if a missile body coordinate frame (which rolls) was used to describe the motion.

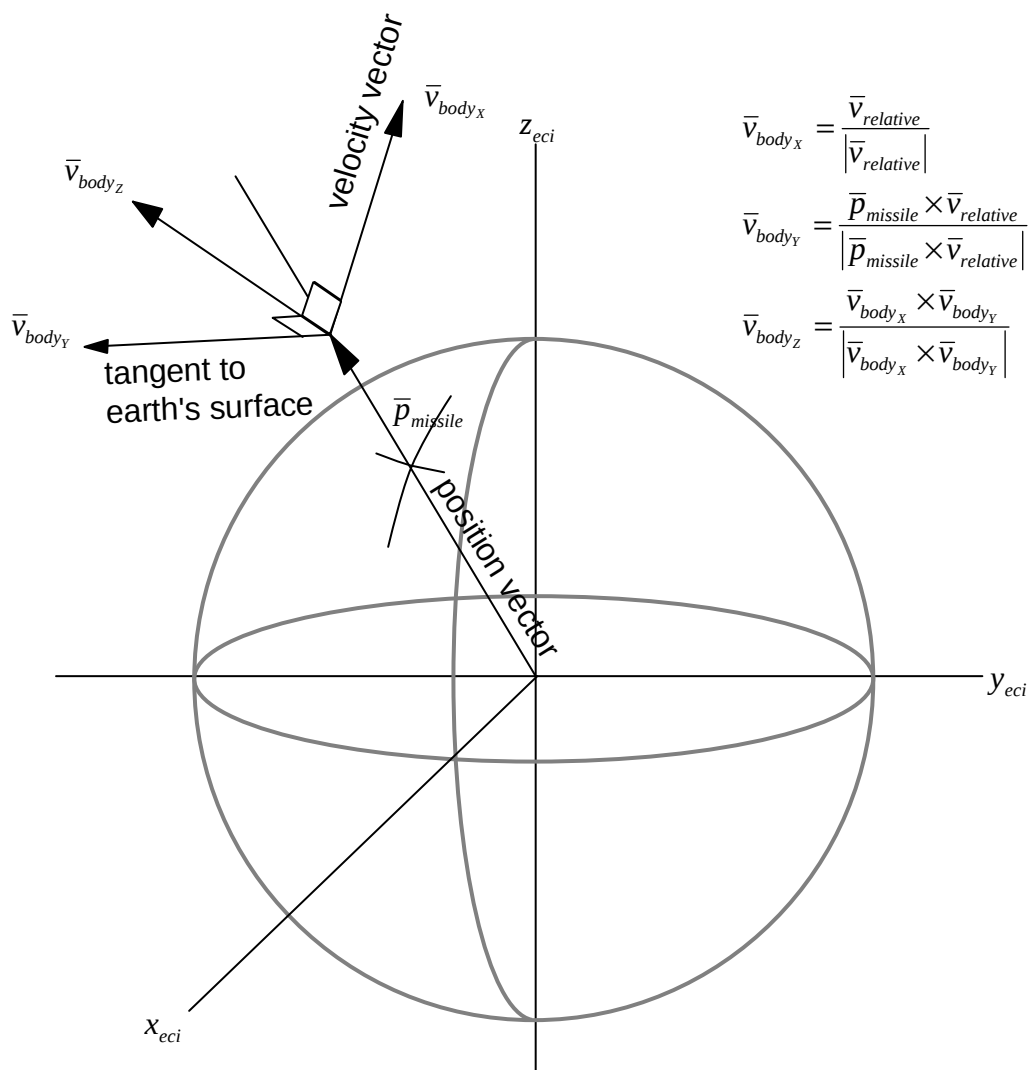


Figure 1. Mini-Rocket Coordinate Frame Definition

The missile can be commanded to follow a pre-specified flight path angle rate steering profile in the pitch channel using the `gammad_table (mode = 2)`.

```
gammad_table
3
t gammad
0.    0.0
10.   0.1
100.  0.1
```

Units for this table are degree/second. The flight path angle is the angle between the missile's velocity vector and the local earth's surface. In this guidance mode, steering occurs only in the missile's pitch channel; the acceleration to change the heading is zero. Positive `gamma_d` pitches the missile up.

The missile can be commanded to follow a pre-specified flight path angle steering profile in the pitch channel with the `gamma_table (mode = 3)`.

```
gamma_table
3
t gamma
0.    0.0
10.   80.0
100.  80.0
```

Units for this table are degrees. A simple feedback controller is used to command a pitch acceleration based on the difference between the commanded flight path angle and the current flight path angle. The dynamics of this feedback process, along with the gain of the feedback loop, result in a lag corresponding to a first order system with a 1.0 second time constant. In this guidance mode, steering occurs only in the missile's pitch channel; the acceleration to change the heading is zero.

Data for succeeding stages is input in an identical manner. Simply precede the data with `**** stage 2 ****`, `**** stage 3 ****`, and so forth.

4 MATHEMATICAL DESCRIPTION

This section describes the mathematical formulation of the missile fly-out model and is intended to give more insight into operation of the program. The following calculations are updated each integrating time step starting at launch. The equations are the same for each stage on a multiple stage missile; stages are defined by specifying different properties for each stage.

The vector magnitude of the missile's position vector is calculated in Earth-Centered Inertial (ECI) coordinates:

$$|\bar{p}_{missile}| = \sqrt{p_{missile_x}^2 + p_{missile_y}^2 + p_{missile_z}^2} \quad (1)$$

where

$$\bar{p}_{missile} = \begin{bmatrix} p_{missile_x} \\ p_{missile_y} \\ p_{missile_z} \end{bmatrix} = \text{missile position vector, ECI}$$

The ECI position vector of the missile's launch point is calculated by

$$\bar{p}_{launch} = \begin{bmatrix} (r_e + h_0) \cos(\theta_{lat_0}) \cos(\theta_{lon_0} + \omega_e t) \\ (r_e + h_0) \cos(\theta_{lat_0}) \sin(\theta_{lon_0} + \omega_e t) \\ (r_e + h_0) \sin(\theta_{lat_0}) \end{bmatrix} \quad (2)$$

where

$\bar{p}_{launch}$ = launch point position vector, ECI coordinates

r_e = earth's radius, 6371008.7714 m (mean radius of semi-axes in WGS84 Ellipsoid)

h_0 = launch point altitude above spherical earth's surface

θ_{lat_0} = launch point latitude

θ_{lon_0} = launch point longitude

ω_e = earth's rotation rate, $7.292115(10)^{-5}$ rad/sec

t = elapsed time since missile launch

The earth's rotation rate can optionally be set to zero.

The component of the missile's velocity (in the ECI) frame due to the earth's rotation is calculated as

$$\bar{v}_{earth} = \bar{\omega}_{earth} \times \bar{p}_{missile} = \begin{bmatrix} \omega_y p_{missile_z} - \omega_z p_{missile_y} \\ \omega_z p_{missile_x} - \omega_x p_{missile_z} \\ \omega_x p_{missile_y} - \omega_y p_{missile_x} \end{bmatrix} = \begin{bmatrix} -\omega_e p_{missile_y} \\ \omega_e p_{missile_x} \\ 0 \end{bmatrix} \quad (3)$$

where

$$\begin{aligned} \bar{v}_{earth} &= \text{local velocity due to earth's rotation} \\ \bar{\omega}_{earth} &= \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \omega_e \end{bmatrix} = \text{earth rotation rate vector, ECI} \end{aligned}$$

The missile's velocity relative to the earth at the current missile's position is

$$\begin{aligned} \bar{v}_{relative} &= \bar{v}_{missile} - \bar{v}_{earth} \\ |\bar{v}_{relative}| &= \sqrt{v_{relative_x}^2 + v_{relative_y}^2 + v_{relative_z}^2} \end{aligned} \tag{4}$$

where

$$\begin{aligned} \bar{v}_{relative} &= \text{missile's velocity relative to earth} \\ \bar{v}_{missile} &= \text{missile's velocity referenced to fixed ECI coordinates} \end{aligned}$$

Unit vectors for a missile “body” coordinate frame are defined in Figure 2.

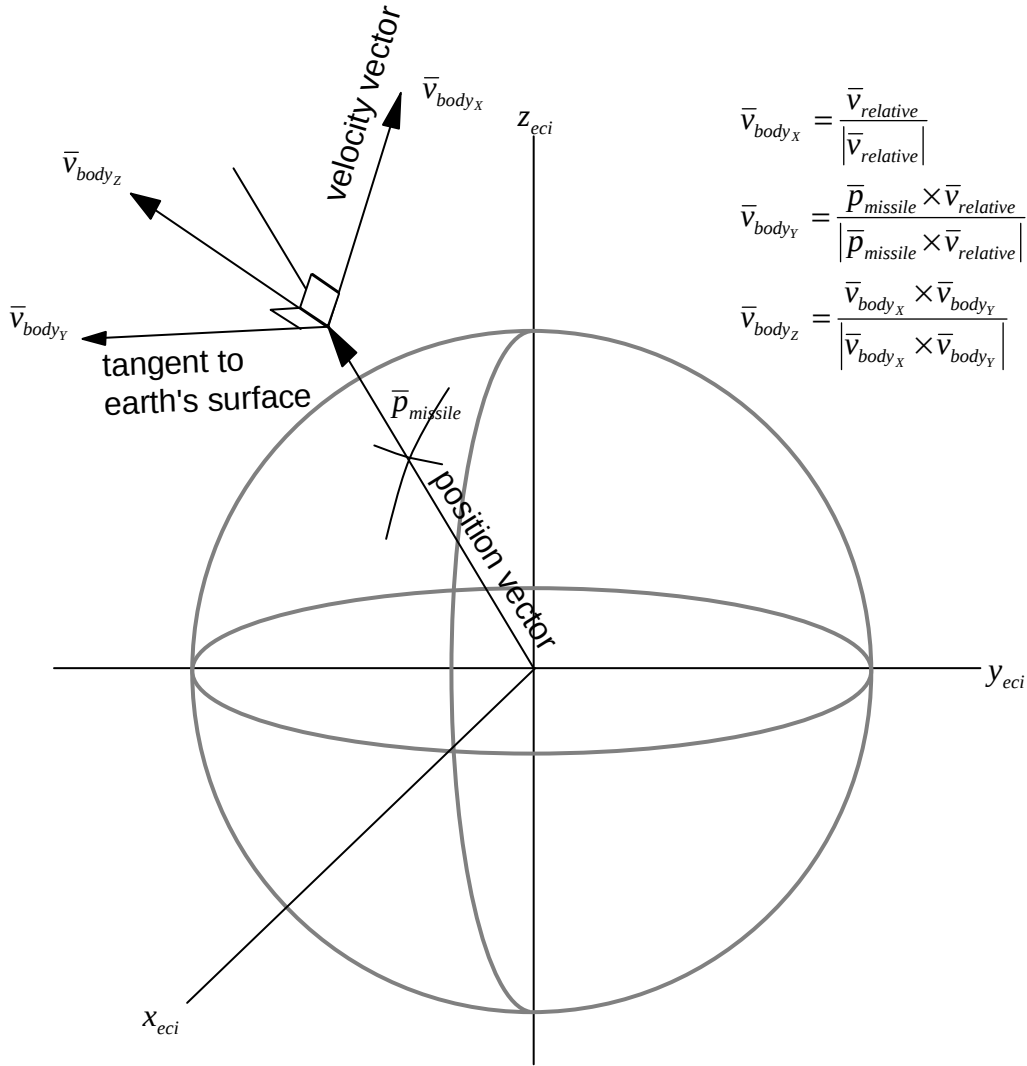


Figure 2. Missile Body Coordinate Frame

The cross product $\bar{p}_{missile} \times \bar{v}_{relative}$ is 0 for a vertical launch leaving the axis $\bar{v}_{body_y}$ undefined. In this special case, the launch elevation angle is adjusted to $\frac{\pi}{2} - \varepsilon$, $\varepsilon \ll 1$ so that the cross product is nonzero.

The flight path angle is calculated

$$\gamma = \frac{\pi}{2} - \cos^{-1} \left(\frac{\bar{p}_{missile} \cdot \bar{v}_{relative}}{|\bar{p}_{missile}| |\bar{v}_{relative}|} \right) \quad (5)$$

The altitude above the spherical earth's surface is

$$h = |\bar{p}_{missile}| - r_e \quad (6)$$

The dynamic pressure and Mach number are

$$q = \frac{1}{2} \rho |\bar{v}_{relative}|^2$$

$$M = \frac{|\bar{v}_{relative}|}{v_{sound}} \quad (7)$$

where

ρ = atmospheric density at current altitude, h

v_{sound} = speed of sound at current altitude, h

A 1962 standard atmosphere model is used to define the atmospheric properties.

The vacuum thrust, T_{vacuum} , is linearly interpolated from a table of T_{vacuum} vs. time.

The delivered thrust, $T_{delivered}$, is calculated:

$$T_{delivered} = T_{vacuum} - a_{nozzle} P \quad (8)$$

where

a_{nozzle} = Nozzle exit area

P = atmospheric pressure at current altitude, h

The delivered thrust, $T_{delivered}$, is zero if $T_{vacuum} - a_{nozzle} P < 0$.

The change in mass with propellant consumption is calculated:

$$\dot{m} = -\int \frac{T_{vacuum}}{I_{sp}} dt \quad (9)$$

where

I_{sp} = Motor specific impulse

Guidance steering is accomplished by defining components of lateral acceleration along the body y and z axes as shown in Figure 3.

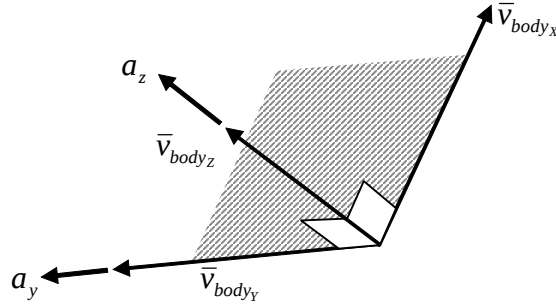


Figure 3. Guidance Steering Reference Frame

The applied lateral accelerations, a_y and a_z , turn the velocity vector, $\bar{v}_{body_x}$. Each lateral acceleration vector, normal to $\bar{v}_{body_x}$, forms an *osculating* plane where the turning of $\bar{v}_{body_x}$ is described by

$$a = v\dot{\gamma} \quad (10)$$

where

a = applied acceleration normal to v (these two vectors comprise an osculating plane)
 $\dot{\gamma}$ = turning rate of v

The velocity, v , is tangent to the instantaneous direction of flight and the acceleration, a , is normal to the flight path. Two osculating planes are formed in the y- and z- channels to independently maneuver in each direction. These vectors for the two channels are defined as described earlier ($\bar{v}_{body_y}$ and $\bar{v}_{body_z}$). This maneuver axis convention (z is up/down and y is left/right), in tandem with the osculating plane formulation, provide a very intuitive basis for specifying the steering commands. Thus, a wide variety of maneuvers in three-dimensional space can be programmed by manipulating a_y and a_z .

Based on this osculating plane formulation, four guidance options are provided to specify a_y and a_z and, hence, turn $\bar{v}_{body_x}$:

- 0) Coast (ballistic)
- 1) Follow commanded acceleration profile
- 2) Follow commanded flight path angle rate profile
- 3) Follow commanded flight path angle profile

These can be used in any combination and sequence during the flight.

For ballistic flight, the commanded accelerations are

$$\begin{aligned} a_{cmd_y} &= 0 \\ a_{cmd_z} &= 0 \end{aligned} \quad (11)$$

To follow a commanded acceleration profile, the acceleration commands are linearly interpolated as a function of time from a one-dimensional table

$$\begin{aligned} a_{cmd_y} &= a_{cmd_y}(t) \\ a_{cmd_z} &= a_{cmd_z}(t) \end{aligned} \quad (12)$$

To follow a commanded flight path angle rate profile, the flight path angle rate command in the z-direction (which controls pitch) is first linearly interpolated as a function of time from a one-dimensional table

$$\begin{aligned} \dot{\gamma}_{cmd_y} &= 0 \\ \dot{\gamma}_{cmd_z} &= \dot{\gamma}_{cmd_z}(t) \end{aligned} \quad (13)$$

The acceleration commands are then calculated

$$a_{cmd_z} = |\bar{v}_{relative}| \dot{\gamma}_{cmd_z} + g \cos \gamma \quad (14)$$

where

g = local acceleration of gravity at missile's altitude

Local gravity is added to the command to compensate for the missile's natural gravity turn downward. The local gravity is calculated as

$$g = \frac{\mu}{|\bar{p}_{missile}|^2} \quad (15)$$

where

$$\mu = \text{earth gravitational constant} = 3986005.0e8 \frac{m^3}{sec^2}$$

A simple feedback loop is implemented to emulate closed-loop airframe response to follow a flight path angle as shown in Figure 4.

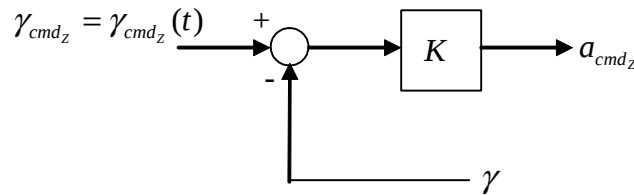


Figure 4. Airframe Response Feedback Loop

The commanded flight path angle, γ_{cmd_z} , is linearly interpolated as a function of time from a one-dimensional table. The commanded flight path angle is compared to the current flight path angle, γ , and multiplied by a gain, K , to compute the commanded acceleration in the z-direction, a_{cmd_z} . The gain, K , is calculated

$$K = \frac{|\bar{v}_{relative}|}{\tau} \quad (16)$$

where

τ = time constant for a closed-loop first-order system = 1.0 sec.

The commanded acceleration is compensated for the missile's natural gravity turn downward:

$$a_{cmd_z} = a_{cmd_z} + g \cos \gamma \quad (17)$$

The commanded acceleration in the y-direction, a_{cmd_y} , is set to zero.

The commanded acceleration is subject to a number of constraints reflecting actual flight conditions and hardware limits as illustrated in Figure 5.

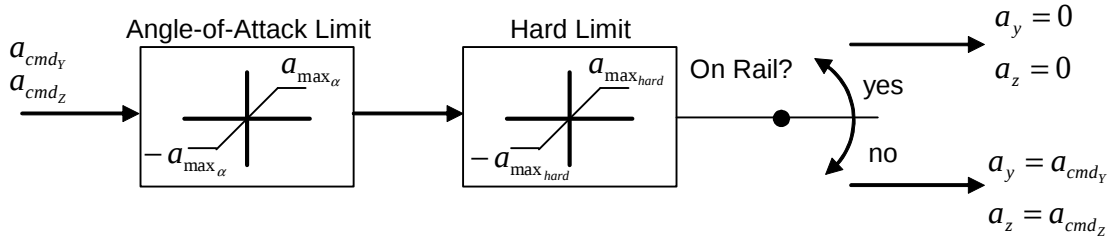


Figure 5. Commanded Acceleration Constraints

The acceleration is first constrained by a user-specified angle-of-attack limit. The angle-of-attack limit is based upon the free-body diagram in Figure 6.

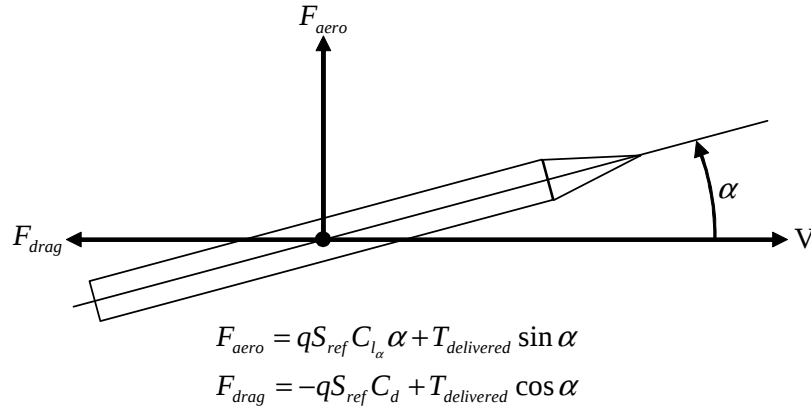


Figure 6. Missile Free-Body Diagram

where

F_{aero} = aerodynamic lift force
 F_{drag} = aerodynamic drag force
 S_{ref} = aerodynamic reference area
 C_{l_α} = linearized lift force coefficient
 α = angle-of-attack
 C_d = drag coefficient

The equation for lift can be simplified with the approximation

$$F_{aero} = qS_{ref}C_{l_\alpha}\alpha + T_{delivered}\sin\alpha = (qS_{ref}C_{l_\alpha} + T_{delivered})\alpha \quad (18)$$

where

$$\sin\alpha \approx \alpha$$

From this, a maximum lift force, $F_{aero_{max}}$, and corresponding maximum acceleration, a_{max} , can be defined based on the maximum angle-of-attack, α_{max}

$$\begin{aligned}
 F_{aero_{max}} &= (qS_{ref}C_{l_\alpha} + T_{delivered})\alpha_{max} \\
 a_{max} &= \frac{F_{aero_{max}}}{m}
 \end{aligned} \quad (19)$$

The linearized force lift coefficient is linearly interpolated as a function of Mach number from a one-dimensional table.

The commanded accelerations are also subject to hard limits which might reflect the missile's structural limit, for instance. Finally, just after launch, the acceleration is subject to a "launch rail" constraint. In this case, the steering accelerations, a_y and a_z , are simply set to zero so that the missile is not allowed to turn. This constraint is imposed as long as the magnitude of the vector, $\bar{p}_{missile} - \bar{p}_{launch}$, is less than a user-specified limit (that is, the missile is still on the "rail"). This option is useful for simulating non-vertical launches where time must be allowed for the missile to generate enough lift to avoid pitching down and falling into the ground.

The total angle-of-attack can now be calculated subject to the steering acceleration limits by rearranging the equation for lift:

$$\alpha = \frac{m\sqrt{a_y^2 + a_z^2}}{qS_{ref}C_{l_\alpha} + T_{delivered}} \quad (20)$$

The acceleration due to drag is calculated using the expression for F_{drag} in the free-body diagram (Figure 6) and including gravity

$$a_x = \frac{-qS_{ref}C_d + T_{delivered} \cos \alpha}{m} - g \sin \gamma \quad (21)$$

The drag force coefficient is linearly interpolated as a function of Mach number, angle-of-attack, and power on/off from a three-dimensional table. Power is defined as on if $T_{delivered} > 0$.

The missile accelerations, in the missile body frame, are converted to ECI coordinates with the previously defined unit vectors that define the body frame

$$a'_{ECI} = \begin{bmatrix} a_{ECI_x} \\ a_{ECI_y} \\ a_{ECI_z} \end{bmatrix} = [\bar{v}_{body_x} \mid \bar{v}_{body_y} \mid \bar{v}_{body_z}] \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix} \quad (22)$$

Centripetal and coriolis accelerations must be added since a'_{ECI} is in a rotating frame:

$$a_{ECI} = a'_{ECI} + a_{centripetal} + a_{coriolis} \quad (23)$$

where

$$\begin{aligned} a_{centripetal} &= \omega_e \times (\omega_e \times \bar{p}_{missile}) \\ a_{coriolis} &= 2\omega_e \times \bar{v}_{missile} \end{aligned}$$

The acceleration of the missile is successively integrated in the ECI frame to velocity, then to position

$$\begin{aligned} \bar{v}_{missile} &= \int \bar{a}_{ECI} dt \\ \bar{p}_{missile} &= \int \bar{v}_{missile} dt \end{aligned} \quad (24)$$

The missile's surface range from the launch point is calculated

$$r = r_e \cos^{-1} \left(\frac{\bar{p}_{missile} \cdot \bar{p}_{launch}}{|\bar{p}_{missile}| |\bar{p}_{launch}|} \right) \quad (25)$$

The missile's longitude and latitude are calculated

$$\begin{aligned}\theta_{lon} &= \tan^{-1} \frac{p_{missile_y} - \omega_e t}{p_{missile_x}} \\ \theta_{lat} &= \tan^{-1} \frac{p_{missile_z}}{\sqrt{p_{missile_x}^2 + p_{missile_y}^2}}\end{aligned}\tag{26}$$

where θ_{lon} is calculated in the correct quadrant depending on the signs of $p_{missile_x}$ and $p_{missile_y}$.

5 REAL-WORLD COMPARISON

Perhaps the most important question about any modeling tool is how well it represents what is being simulated. This is certainly a pertinent question that should be addressed for Mini-Rocket since it has been, and will continue to be, used for predictions that have significant impact on the tasks and programs where it is applied.

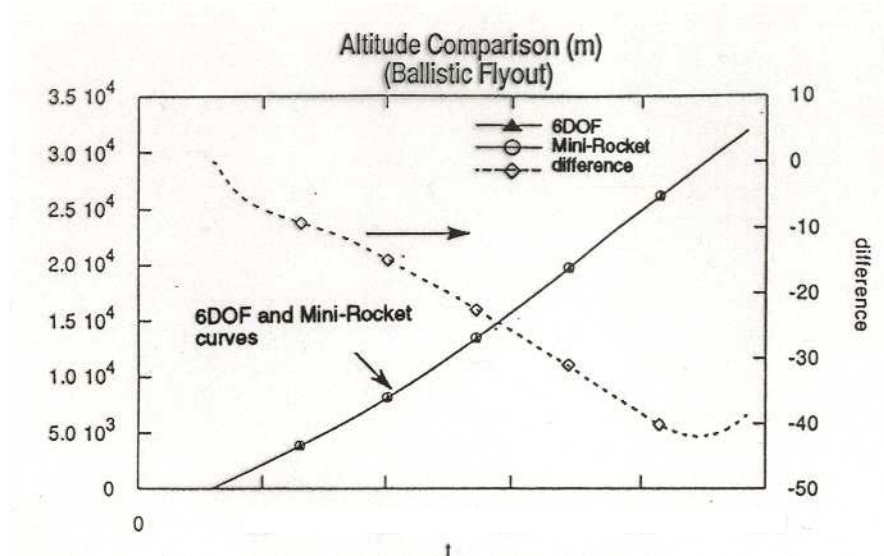
Mini-Rocket has been rigorously compared to other accepted models and has obtained the confidence of a wide variety of users for its ability to accurately model trajectories. Conventionally, a formal Independent Verification and Validation (IV&V) process is used to certify the accuracy of a tool. In this vein, Mini-Rocket has not been through a formal IV&V process and, as such, the words “verification” and “validation” are not used in this section (nor the title) since the authors recognize that the term IV&V conveys a specific meaning in the formal software engineering terminology. More significantly, Mini-Rocket has been subjected to perhaps *more* extensive external scrutiny (than a formal IV&V) by its widespread application over a large number of tasks and users. In the end, the process used to establish accuracy is not the central aim but, instead, how well the simulation represents the real-world process that is being studied. The number of users and applications, which in a sense reflects confidence in the tool’s accuracy, is a good metric for measuring a tool’s credibility. Most analysts are skeptics by nature and will not use a tool until they convince themselves that it is accurate subject to their own internal tests and processes.

This section provides a brief summary and illustration of cases where Mini-Rocket performance predictions have been compared to other models and data over a period of the last 15 years. The initial benchmark comparison to another simulation demonstrated that Mini-Rocket could be a surrogate for higher-fidelity simulation. The Mini-Rocket credibility trail-of-record is then extended with discussion of its application to more complex modeling tasks than the initial benchmark. The section concludes with a discussion of recent and on-going Mini-Rocket application where traceability to trusted external models is critical.

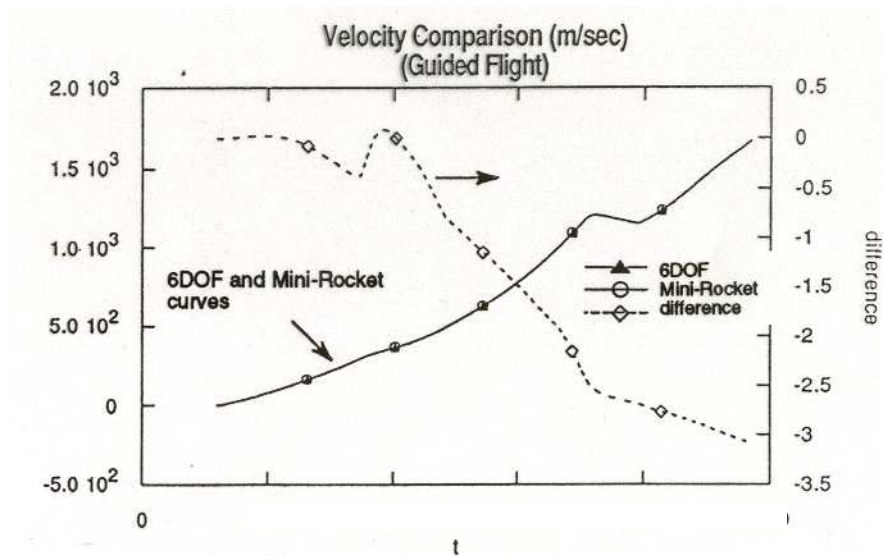
5.1 *Initial Benchmark Comparison for Accuracy (1993)*

The Aries is a ballistic missile defense testing target vehicle derived from the Minuteman. It was used or planned to support ERIS, GBI, LEAP, and Brilliant Pebbles tests. An accredited 6-DOF model was built for the Kinetic Energy Weapon Digital Emulation Center (KDEC) that was successfully benchmarked to flight telemetry. An Aries representation was constructed in Mini-Rocket to demonstrate that simpler models (than 6-DOF) could be an effective surrogate when only the trajectory characteristics themselves are desired. Trajectory kinematic predictions from the KDEC simulation were successfully compared for two cases: 1) Ballistic flight from a non-vertical launch and 2) Guided flight with a pitchover maneuver after vertical launch [2].

Results from the comparison are shown in Figure 7.

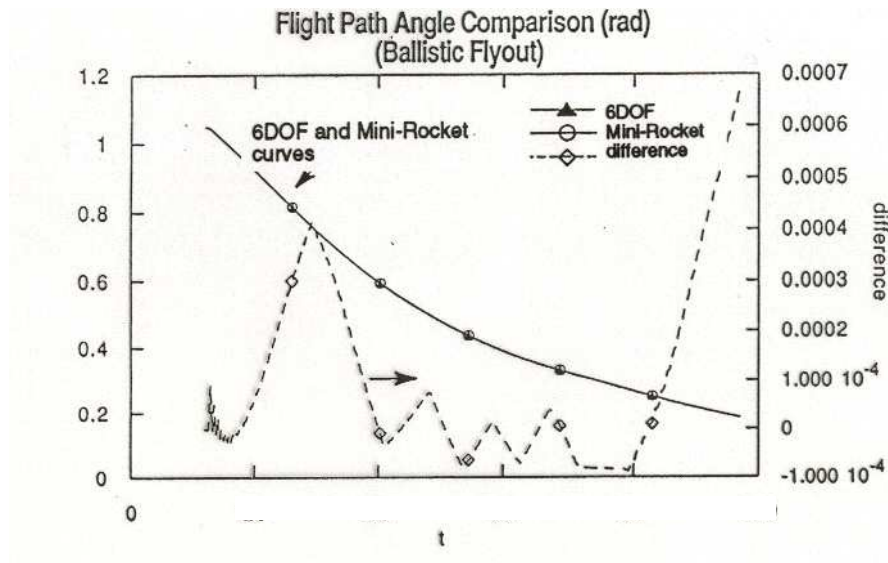


a. Altitude Comparison

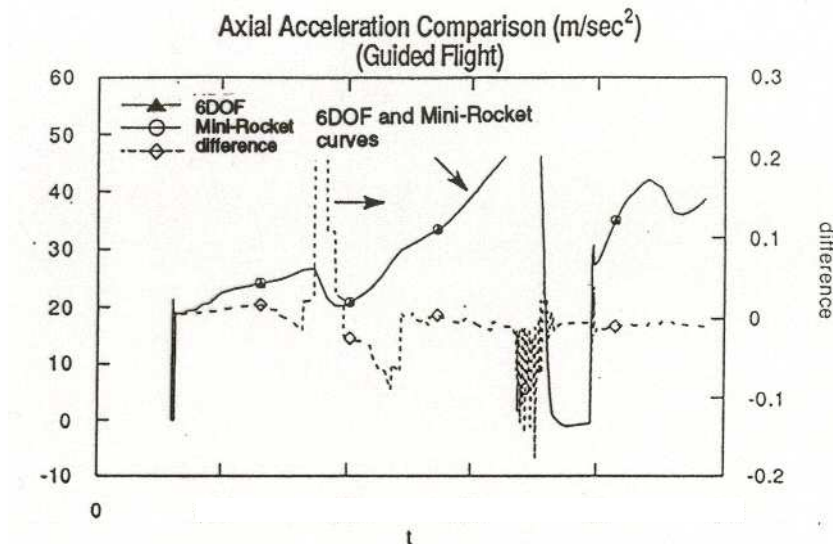


b. Velocity Comparison

Figure 7. Aries Simulation Comparisons



c. Flight Path Angle Comparison



d. Axial Acceleration Comparison

Figure 7. Aries Simulation Comparisons (Concluded)

A significant, but fortuitous, difficulty was encountered in the course of the comparison. The Mini-Rocket results so closely matched those from the 6-DOF that they were virtually indistinguishable from each other when plotted together! To overcome this, the difference between the two curves are also plotted and read from the right scale. As is clearly seen, the Mini-Rocket predictions very closely match the 6-DOF predictions. As a result of this comparison, Mini-Rocket was successfully used to supply trajectory parameter data requests and, in the process, satisfy those data requests much more quickly than could be accomplished using the 6-DOF simulation.

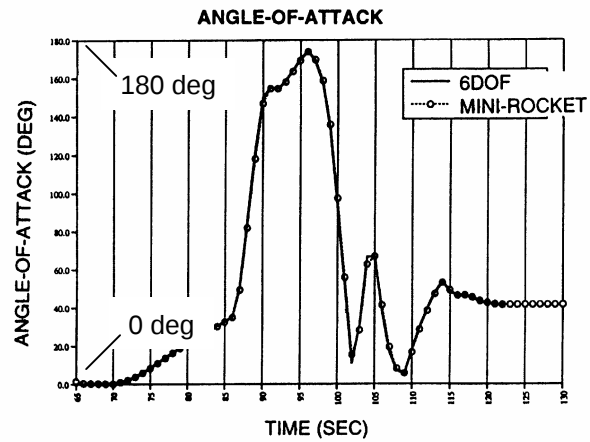
5.2 *A Trail of Successful Comparisons*

The initial Aries representation and comparison set the stage for widespread Mini-Rocket application. Some of the more prominent programs are summarized here.

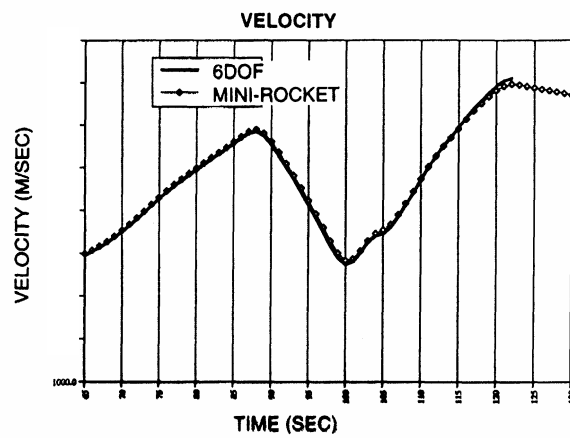
5.2.1 Integrated System Test Capability

The Integrated System Test Capability was a key hardware-in-the-loop component of the system-of-systems testing conducted by the then U.S. Army Space and Strategic Defense Command. A trajectory model for an exoatmospheric interceptor was needed to “stimulate” other models, including radar, for a key experiment. The model was complicated by the feature that the interceptor performed a Generalized Energy Management Steering (GEMS) maneuver during fly-out to meet intercept point geometry requirements. The GEMS maneuver could require attitude changes up to nearly 180-degree angle-of-attack during boost — a complicated phenomenon to simulate, even in a 6-DOF simulation.

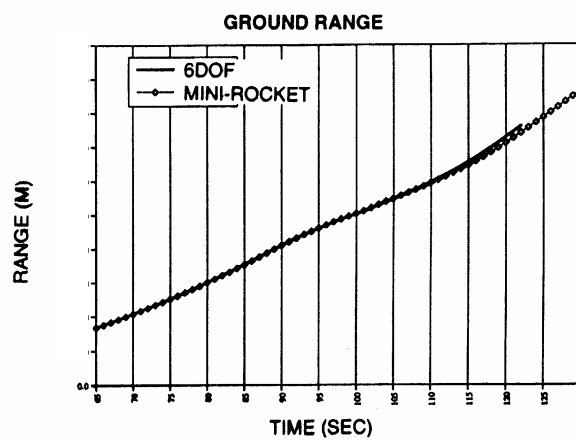
The GEMS maneuver was implemented in Mini-Rocket and the trajectories were successfully anchored to those generated by the engineering-level 6-DOF simulation used by the missile developer [3]. A comparison of simulation results is shown in Figure 8.



a. Angle-of-Attack Comparison



b. Velocity Comparison



c. Ground Range Comparison

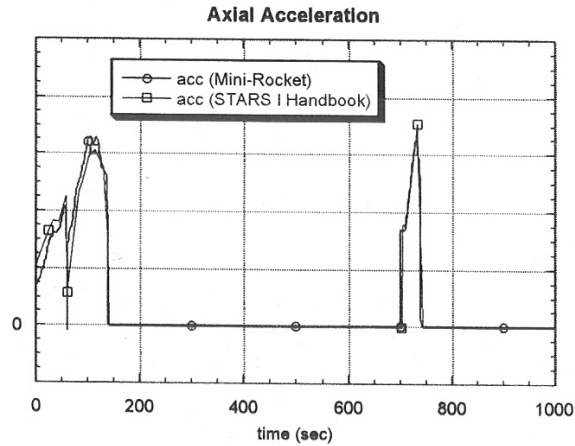
Figure 8. ISTC Simulation Comparisons

In particular, note the very high angle-of-attack, which in effect, produced a negative thrust vector. This effective reverse thrust “wastes” energy to minimize and shape the velocity for this particular intercept. The agreement between Mini-Rocket and the 6-DOF simulation is remarkable for this complex maneuver, even though Mini-Rocket does not directly model the missile rigid body dynamics.

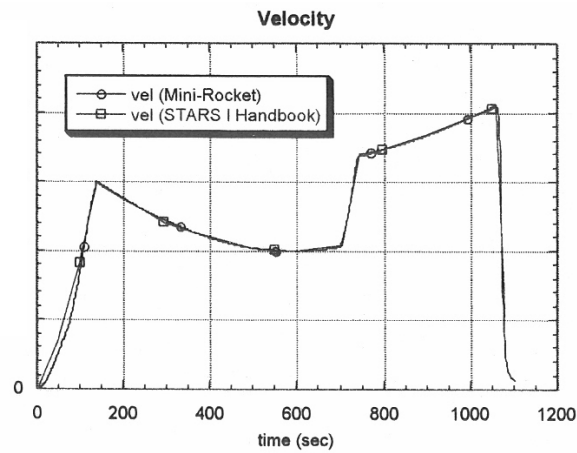
The ISTC subsequently used Mini-Rocket as a driver to stimulate other models and as a risk-reduction until a contractor-developed model was delivered.

5.2.2 Anti-Satellite Mission Scenario Analysis

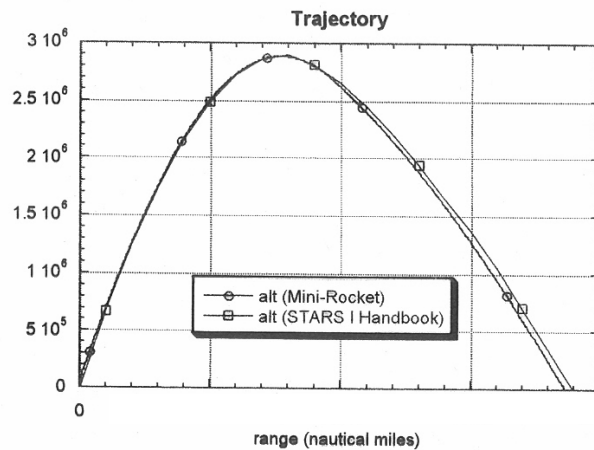
The Strategic Target System (STARS) was selected as the carrier vehicle for kinetic energy anti-satellite (ASAT) interceptor testing. In addition to being the simulation used to screen different candidate booster systems, Mini-Rocket was used to study and establish test flight scenarios. A number of constraints made configuring the scenario somewhat complicated. The ASAT kill vehicle was to be launched from the Pacific Missile Range (Hawaii) for intercepts in the vicinity of the Kwajalein Missile Range. A dog-leg maneuver had to be performed just after launch to satisfy range safety requirements. A pitch-up maneuver, late into boost, had to be performed to replicate geometry aspects of a satellite intercept. Although, Sandia National Laboratories, the STARS developer, had overall simulation responsibility with their in-house 6-DOF simulation, another simulation was needed to perform the large number of trajectory trades that were required to fully develop mission scenarios. As a first step in establishing Mini-Rocket credibility to satisfy this need, a Mini-Rocket STARS characterization was developed and compared to trajectory data in the STARS Payload Designer Handbook [4]. Results of the comparison are shown in Figure 9.



a. Axial Acceleration Comparison



b. Velocity Comparison



c. Trajectory Comparison

Figure 9. STARS Simulation Comparisons

The successful comparison demonstrated Mini-Rocket's viability to rapidly screen large sets of potential trajectories that could be explored in more detail with the Sandia National Laboratory 6-DOF simulation. In addition to being successfully used for the ASAT mission trajectory studies, Mini-Rocket came to be used as a trusted simulation to address other ASAT studies, including trajectory dispersion and preliminary range safety studies.

5.2.3 EADSIM

Early versions of Extended Air Defense Simulation (EADSIM) (version 4.0 and before) did not have a simulation-based missile model per se; instead, interceptor missile trajectories were represented by table look-ups. The data in the tables were generated by external simulations. User requests for increased fidelity dictated that a missile flight model be directly incorporated into EADSIM. Speed-of-execution was a key requirement and thus precluded use of a 6-DOF representation. An embedded version of Mini-Rocket fit the requirement perfectly and was integrated into EADSIM [5]. The Mini-Rocket model augmented EADSIM with the capability to directly characterize the trajectory dynamics of interceptor missiles homing and engaging a target. In essence, each new incorporation of a missile into the EADSIM fly-out model represents another successful comparison since the performance of the Mini-Rocket-based EADSIM model is checked against external trajectory predictions in the normal course of confirming successful model installation.

5.3 *A Legacy of Successful Comparisons Continues*

Mini-Rocket builds on a successful legacy of accurately depicting trajectories for diverse rocket and missile applications and has established itself within the AMRDEC as the tool of choice for characterizing missile systems. As of the time of writing for this report, Mini-Rocket is being actively exploited on two key programs within the AMRDEC.

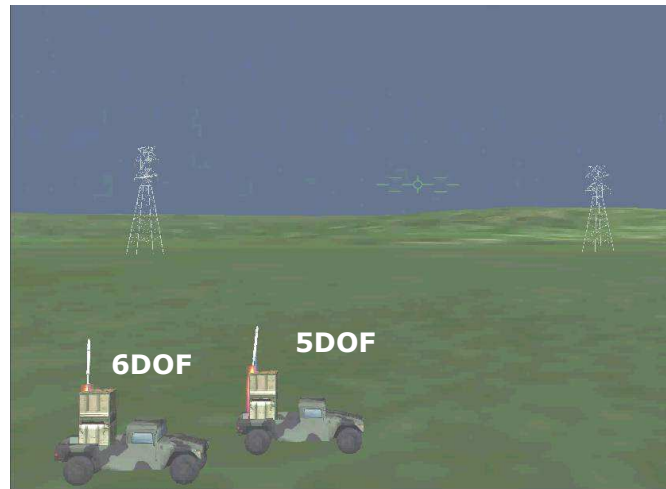
5.3.1 Extended Air Protection and Survivability Program (EAPS)

The EAPS program is developing a missile concept to protect against short-range rockets, artillery, and mortars. A key feature of the development, conducted in-house by the AMRDEC, was to prototype a design based on simulation collaboration by the missile subject matter experts. An evolving simulation, whose fidelity was consistent with the maturity of the design, was used as the central collaboration tool to document the design. The strategy was to begin the top-level aspects of the design with a reduced fidelity simulation and then mature it to a full 6-DOF as design of the missile's subsystems progressed.

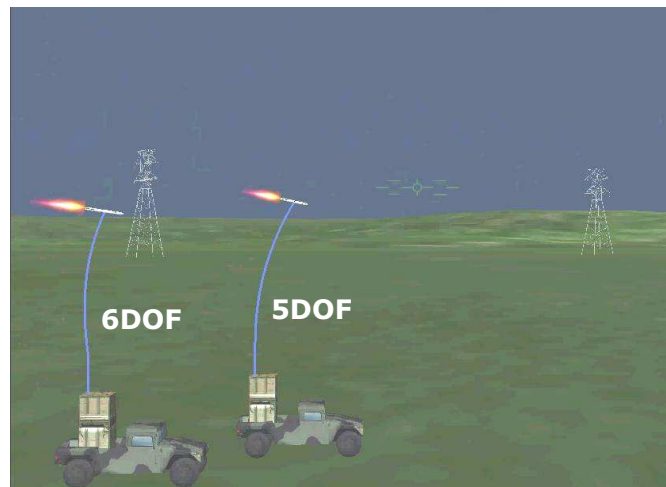
The object-oriented architecture of the CMD (described in a later section in this manual) was selected as the ideal coding platform to execute the simulation development process. Mini-Rocket, which is hosted in the CMD architecture, was used to study and assess candidate designs due to its unique combination of relatively high-fidelity (compared to conventional 3-DOF) and modest coding complexity and runtime efficiency (compared to 6-DOF). A baseline design was arrived at after extensive trade studies with Mini-Rocket and the resulting design was remodeled from a Mini-Rocket implementation to a full-up 6-DOF representation (all within the same CMD code kernel). This presented the *unique opportunity to simultaneously run the Mini-Rocket-*

based EAPS missile in the same physical simulation as the 6-DOF-based EAPS missile (that is, they are launched at the same time and fly out simultaneously) [6].

Figure 10 shows excerpts from an animation constructed from the simultaneous simulations. Both a Mini-Rocket-based EAPS and a 6-DOF EAPS are shown flying out side-by-side, starting from launchers that are slightly offset from each other.

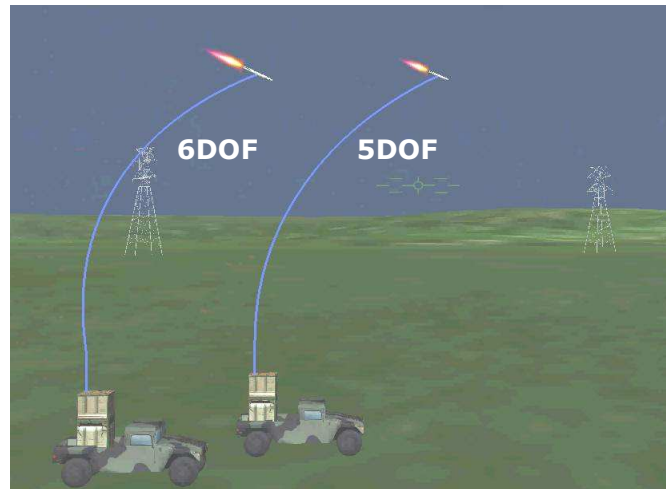


a. Just After Launch

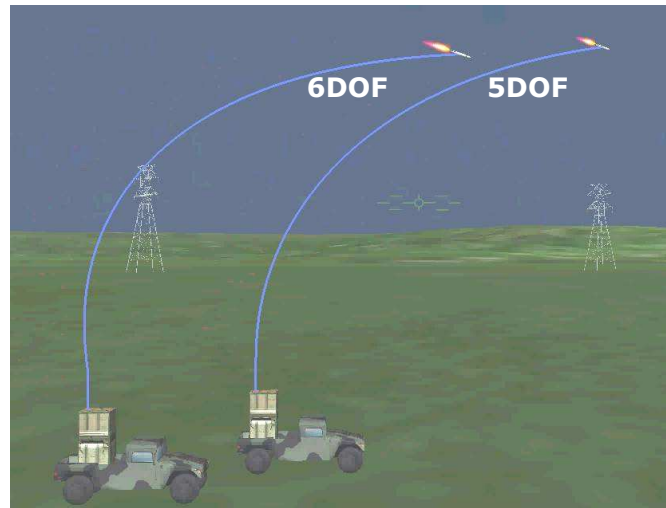


b) Initial Pitchover

*Figure 10. EAPS Side-by-Side Simulation Comparisons
(6-DOF and Mini Rocket)*



c. Initial Pitchover Complete



d. Downrange Flight

*Figure 10. EAPS Side-by-Side Simulation Comparison
(6-DOF and Mini-Rocket) (Concluded)*

The similarity between the trajectories and the missiles' attitudes is remarkable knowing that the underlying physics model characterizations (Mini-Rocket and 6-DOF) are completely different. As documented in the Mathematical Description, Mini-Rocket does not directly model the rigid body attitude of the missile, but instead the angle-of-attack. For Mini-Rocket, it was a simple matter to “back-out” the attitude for the animation knowing the angle-of-attack (angle between missile body and the velocity vector).

In addition to again confirming the accuracy of the Mini-Rocket equations-of-motion (mathematical formulation), this incremental simulation evolution process implemented on EAPS successfully demonstrated how simulation can be the central apparatus to coordinate the missile design as opposed to its conventional role as a supporting analysis tool.

5.3.2 Interactive Distributed Engineering Evaluation and Analysis Simulation (IDEAAS)

IDEAAS is a tactical missile constructive simulation that incorporates interactive models of all the tactical battlefield elements including shooters (missiles), surveillance and fire control radar, and battle management. A key component of IDEAAS is a *missile server* that generates, on-demand, tactical missile representations. It was not important for this missile-server to simulate the onboard missile subsystems; the key IDEAAS requirement for a missile model is to accurately depict trajectories that, in turn, stimulate or drive the other battlefield elements. Mini-Rocket's level of fidelity was ideal for this requirement, providing runtime efficiency without undue complexity. In addition, Mini-Rocket, with its underlying CMD object-oriented kernel could be readily embedded into IDEAAS. Because IDEAAS is Java-based, the Mini-Rocket model algorithms were refactored in Java, with an identical architecture as the C++ model. The object-oriented simulation kernel in CMD is programming language independent and was already coded in Java (as well as other languages) so it was a straightforward exercise to convert the model to Java. The Java-based Mini-Rocket was easily wrapped with a simple, but powerful, interface that could be called by the IDEAAS executive to instantiate (create) a missile object [7]. The exact missile being simulated is specified via the conventional Mini-Rocket input file described in this manual.

A Mini-Rocket-based missile model must have traceability to the original design before its missile server representation can be used in IDEAAS. One of the more challenging models successfully implemented in IDEAAS was a vertically-launched ground-to-ground missile. For long-range intercepts, the trajectory is "lofted" so that lift can sustain a relatively long flight. Successful comparison to the originating design activity's 6-DOF simulation is shown in Figure 11 for this scenario.

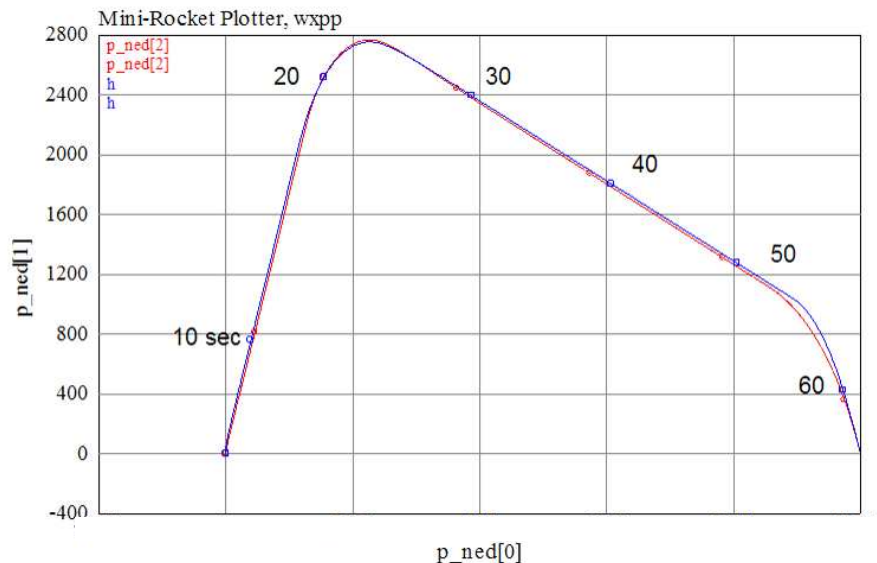


Figure 11. Ground-to-Ground Missile Simulation Comparison

Much more stressing from a modeling view are short-range trajectories. The missile is capable of accomplishing very short range intercepts by flying out and “looping” back. A simulation-generated example from the prime contractor developer is shown in Figure 12. Normally, this would be very difficult to simulate given the complexity of the commands to execute the maneuver.

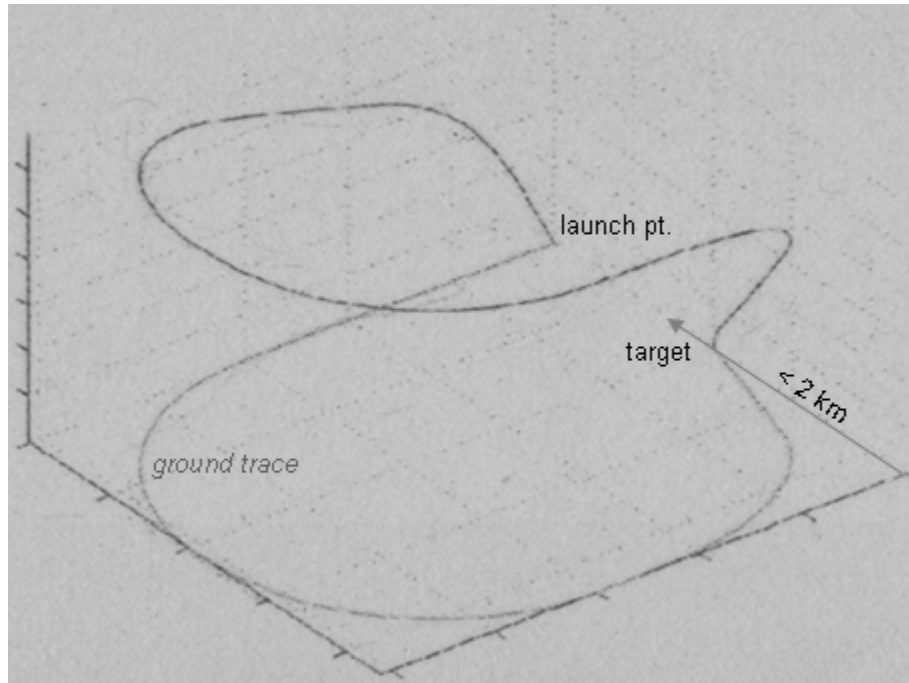


Figure 12. Prime Contractor Simulation Depiction of Complex “Loop-Back” Maneuver

The unique osculating plane formulation behind Mini-Rocket made it relatively simple to replicate the trajectory since a left/right and up/down frame-of-reference is used to specify steering in the input data. Example Mini-Rocket-generated results are shown in Figure 13 which very closely replicated the missile’s performance.

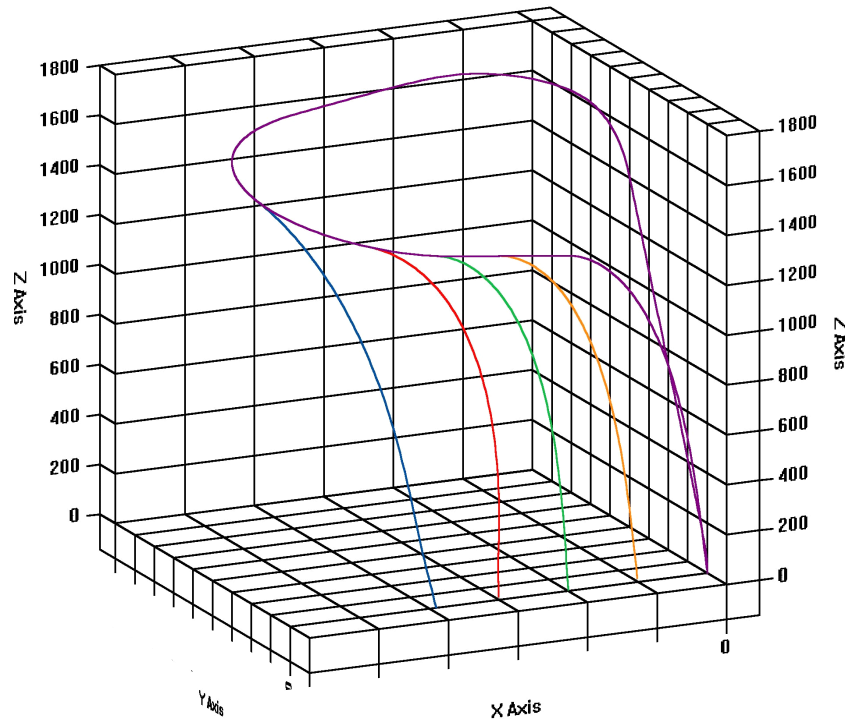


Figure 13. Mini-Rocket Replication of “Loop-Back” Maneuver

Several other missile-server representations have been developed within IDEEAS using the same embedded Mini-Rocket engine.

5.4 Conclusion

A long, traceable heritage of comparisons exists to establish the accuracy of the Mini-Rocket model and coding mechanizations. The comparisons to independently-developed data and models shown in this section support the accuracy of Mini-Rocket predictions. Equally significant to the plotted comparisons shown here is the fact that Mini-Rocket was subjected to intense independent scrutiny before it was accepted and selected as a simulation tool for the each of the applications described in this section.

6 HOW MINI-ROCKET WAS BUILT

Mini-Rocket was built with C++ Model Developer . CMD is an open-source C++ source code based environment for building simulations of systems described by time-based differential equations. The principal design objective behind CMD is to provide a tool to go from mathematical representation to working, extensible C++ code with a minimum amount of effort.

The heart of CMD is a powerful Object-Oriented Simulation Kernel (OSK) that represents significant technology advances in the application of object-oriented principles to simulation development and design [8]. The OSK architecture is language-independent and can serve as the basis for recreating Mini-Rocket in other computer languages as shown in Figure . In fact, Mini-Rocket as described in this User Guide has been replicated in Java and Python. Standalone programs in these languages use the same identical input data file as the CMD-based executable version.

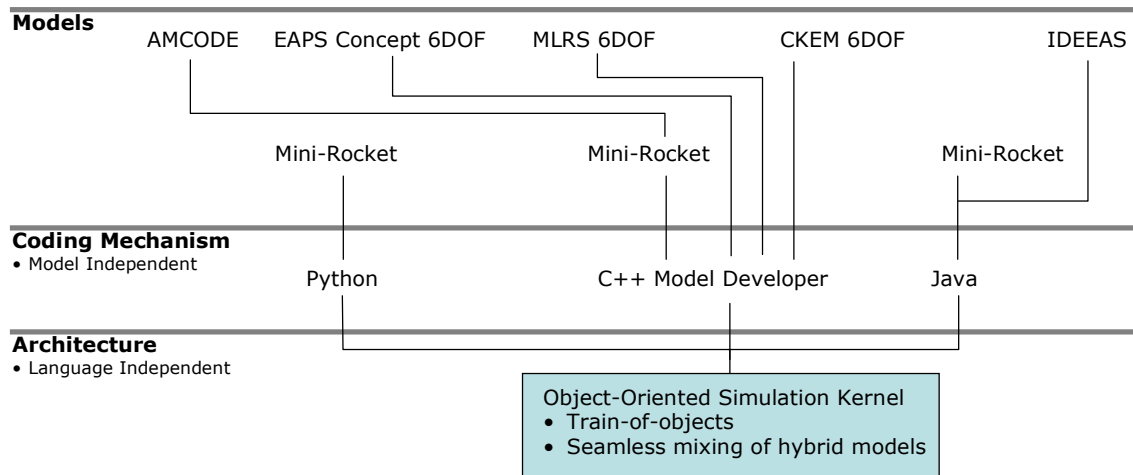


Figure 14. Object-Oriented Simulation Architecture and Simulation Construction Hierarchy

A key feature and state-of-the art advance of the OSK is the *train-of-objects* architecture depicted in Figure . The OSK's unique train-of-objects architecture is well suited for the multiple stage modeling required by Mini-Rocket. The organization of the entities used by the kernel is shown in Figure . At a micro-level, each state (that is each individual integrator) is a C++ object (STATE in the figure). One or more states are combined, connected by algorithms for their derivatives, into a block (or model). Several models are combined into a stage. Finally, a series of stages are combined in a list. A simulation class in the kernel then decomposes this "list-of-lists-of-lists" to execute the models in the desired order (specified by their order in the lists) and, within each model, the appropriate methods described in the previous section.

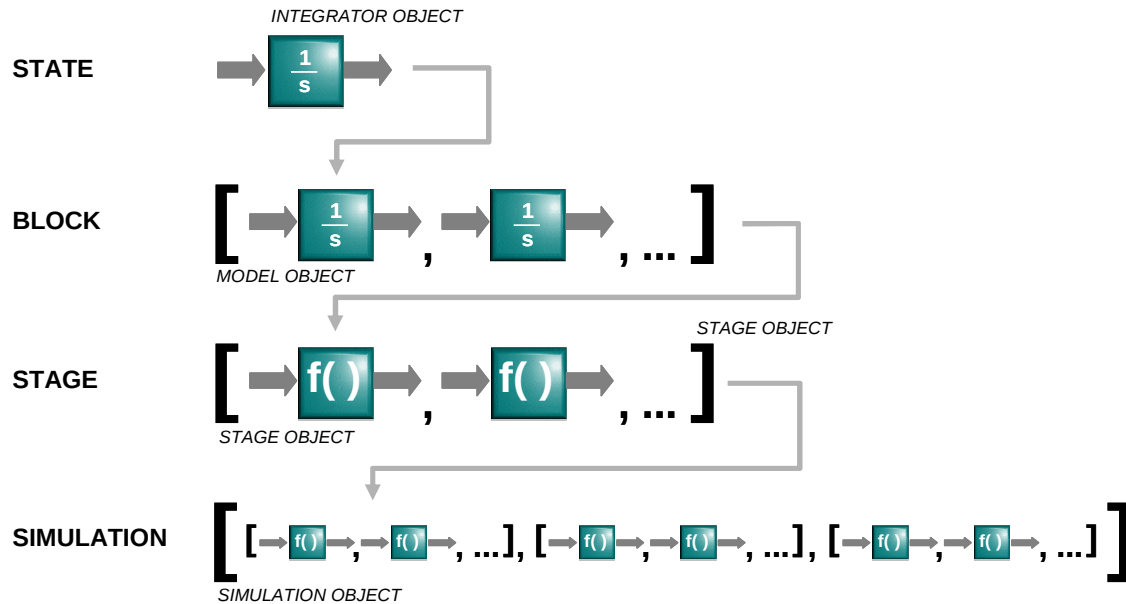


Figure 15. OSK Train-of-Objects

Thus the kernel implements the object-oriented paradigm at all levels: dynamic states are objects, models themselves are objects, stages are objects, and the aggregate simulation is an object. The key feature is that staging is provided for in the simulation architecture itself and the Mini-Rocket math models are not burdened with logic controlling the sequence of stages.

The first (and very successful application) of CMD was the U.S. Army Compact Kinetic Energy Missile Program. This program funded CMD's documentation in a U.S. Army Technical Report [1] as a technology transfer to offer it to a much larger simulation domain and audience.

7 SUMMARY

Mini-Rocket fills an important simulation niche as shown by the vast number of applications and tasks where it has been utilized over a number of years. In these analyses, the fidelity requirements are not satisfied with a 3-DOF simulation, but the complexity, and associated resource requirements, of a 6-DOF far exceed what is required to satisfy analysis needs. With the progressive advent of faster and faster computing power, the difficulty with using a 6-DOF (over a 3-DOF) is not any longer computer runtime but, instead, the far greater complexity of configuring input for the 6-DOF owing to the detail of its underlying subsystem models. Mini-Rocket resolves this issue, effectively having a broad subset of the fidelity of a 6-DOF simulation, but with the resource requirements (runtime and input complexity) of a 3-DOF.

An integral part of the Mini-Rocket application success story is its malleability to be easily modified and augmented. This report documents a packaged, standalone version of the algorithms that comprise Mini-Rocket and this packaged tool has been, and will continue to be, used by a wide audience. But, perhaps more importantly, a broader application arena for Mini-Rocket is its flexibility to be molded and configured to address specific analysis and modeling situations. The algorithm code is relatively short, concise, and readily understood, which makes it very easy to modify for a broad domain of needs. The inherent modular nature of the object-oriented simulation kernel behind CMD was a great medium for exploiting the power of the algorithms behind Mini-Rocket. It is anticipated that Mini-Rocket will continue to morph into even more application areas and coding mediums in the future.

In summary, Mini-Rocket is a versatile tool having the distinguishing characteristics of a high degree of fidelity given its very modest complexity (the unique mathematical formulation), a long legacy of successful application to establish credibility, and a flexible code structure that enables it to be rapidly configured or modified for a wide variety of custom applications.

REFERENCES

1. Sells, H.R., Sanders, G.A., Snyder, G., Hester, J.W., and Painter, L. 2005. "C++ Model Developer (CMD) User Guide." U.S. Army Technical Report AMR-SG-05-12, April 2005.
2. Sells, H.R., "Comparison of KDEC Aries Test Article Trajectories to Off-Line Model," Teledyne Brown Engineering technical letter SSDCSY-93-61AB01-1533100801-0573 to Ms. Jackie Steele, U.S. Army Space and Strategic Defense Command, 10 August 1993.
3. Sells, H.R., "Mini-Rocket GEMS Implementation," report delivered to Mr. Dan Bowman, Teledyne Brown Engineering, 1995.
4. Sells, H.R., and Cupples, M., "ASAT Test Mission Scenario Analysis – Trajectory Studies," report for U.S. Army Space and Strategic Defense Command, contract DASG60-97-C-0054, 21 January 1998.
5. Extended Air Defense Simulation (EADSIM) Methodology Manual, Section 5.9, "Interceptor Missile Flight." Teledyne Brown Engineering, Huntsville, AL, 1995.
6. Sells, H.R., and Leopard, P., "EAPS Simulation Build 6 – 6-DOF Simulation Description and Delivery," report delivered at EAPS Simulation Working Group #27 to Mr. George Sanders, AMRDEC, 1 March 2007.
7. Sells, H.R., "Java Mini-Rocket Live Code Demo," report and model delivery to Mr. Ron Saylor, AMRDEC, 9 December 2005.
8. Sells, H.R., Sanders, G., and Saylor, R., "An Object-Oriented Simulation Kernel for a Large Spectrum of Simulations," Summer Computer Simulation Conference, Society for Computer Simulation, 2006, Calgary, Alberta.

ACRONYMS

3-DOF	3 Degree-of-Freedom
6-DOF	6 Degree-of-Freedom
AMCODE	Aviation and Missile Collaborative Design Environment
AMRDEC	Aviation and Missile Research, Development, and Engineering Center
ASAT	Anti-Satellite Program
CKEM	Compact Kinetic Energy Missile
CMD	C++ MODEL DEVELOPER
DOF	Degree-of-Freedom
IDEEAS	Interactive Distributed Engineering Evaluation and Analysis Simulation
ISTC	Integrated System Test Capability
IV&V	Independent Verification and Validation
KDEC	Kinetic Energy Weapon Digital Emulation Center
EAPS	Extended Air Protection and Survivability
EADSIM	Extended Air Defense Simulation
ECI	Earth Centered Inertial
GEMS	Generalized Energy Management Steering
OSK	Object-Oriented Simulation Kernel
ROCKET	Rand's Omnibus Calculator of the Kinematics of Earth Trajectories
STARS	Strategic Target System

APPENDIX 1 MAKING PLOTS

APPENDIX 1 – MAKING PLOTS

Although not a part of Mini-Rocket itself, a simple-to-use plotter is provided that is compatible with the output files generated at runtime. The name of the plotter is *wxpp*. *wxpp* is a quick-and-easy interactive, scriptable 2-d x-y plotting tool. It is primarily designed to expedite the rapid visualization of simulation results as quickly as possible without the necessity of navigating selection menus or other options. *wxpp* is fully scriptable since it is command-line driven with options specified in an ASCII-text configuration file. Plots can be totally configured and generated from simple scripts.

wxpp produces production-quality, high-resolution plots suitable for direct incorporation into reports or briefings. Some of its most basic capabilities are briefly described here and should be adequate for use with Mini-Rocket.

1.1 *Installing the Plotter*

wxpp is a single standalone Windows “.exe” file so it can easily be installed and used. Make sure the file “wxpp.txt” is also in the same directory.

1.2 *Basic Usage*

The most fundamental way to use *wxpp* is from the command line to generate plots lightening fast.

The environmental variable `DATAFILE` specifies the filename of the data to be plotted. This can be set from the command line as:

```
C:> set DATAFILE=OutputRun0.dat
```

Within the data file, data to be plotted is formatted as

```
0
t rng h mach gammad v tx alph
0.000 0.00 0.00 0.00 40.00 0.01 0.0 0.00
0.770 450.99 372.96 5.40 39.50 1828.42 0.0 0.00
1.000 775.35 640.11 5.41 39.45 1828.69 1259.0 0.00
```

The contents of the first line is ignored and can contain any text (maybe some information about the file’s contents for instance). The second line contains the names of the fields that can be plotted. Each name corresponds to a column of data in the subsequent line. The remaining lines of the file contain rows of data for each field.

The available fields for plotting can be queried by

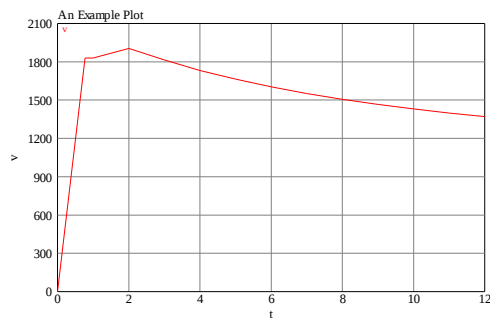
```
C:> wxpp
```

which results in

```
0 t
1 rng
2 h
3 mach
4 gammad
5 v
6 tx
7 alph
```

A simple one line plot is created:

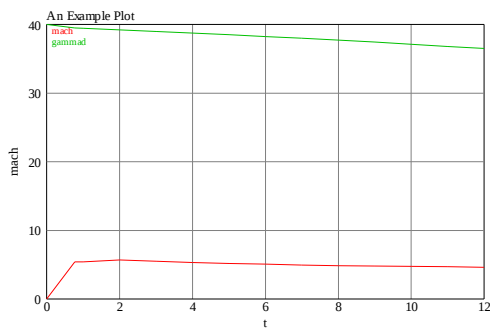
```
C:> wxpp 0 5
```



The arguments 0 and 5 are the x-value and y-value.

More than one parameter can be plotted

```
C:> wxpp 0 3 4
```



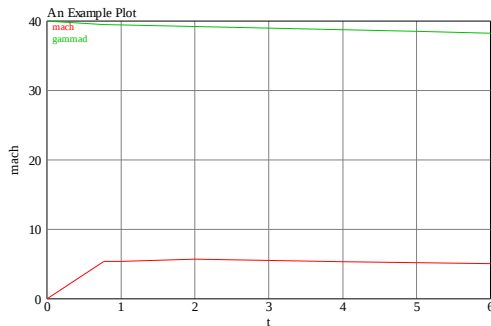
The arguments 3 and 4 identify the fields to be plotted against field 0.

The plot can be dismissed (that is, closed) by selecting Exit from the File menu, selecting the window close button, or, most expediently, simply hitting any key on the keyboard.

1.3 Scaling

Normally, the scales are auto-adjusted. The scale can be manually specified with a `-s` option

```
C:> wxpp -s "0,6,1,0,40,10" 0 3 4
```



The `-s` option requires a 6-element, comma-delimited list. The first three arguments are for the x scale and the last three are for the y scale. For each, the arguments are starting value, ending value, and increment. The 6-element, comma-delimited list must be enclosed by quotes as shown.

The scale can be specified in one axis and auto-adjusted in the other. To preserve auto-scaling, simply enter all 0's. For example,

```
C:> wxpp -s "0,0,0,0,40,10" 0 3 4
```

Here, the plot is auto-scaled in x and specified in y.

1.4 Exporting Plots for Publication

A Windows metafile named "plot.wmf" is created each time a plot is made. This option provides the powerful capability to generate publication-quality graphs for later inclusion in documents. These type of files are easily imported into word processing and presentation software. To preserve the plots between runs, manually change the name of the existing "plot.wmf" file.

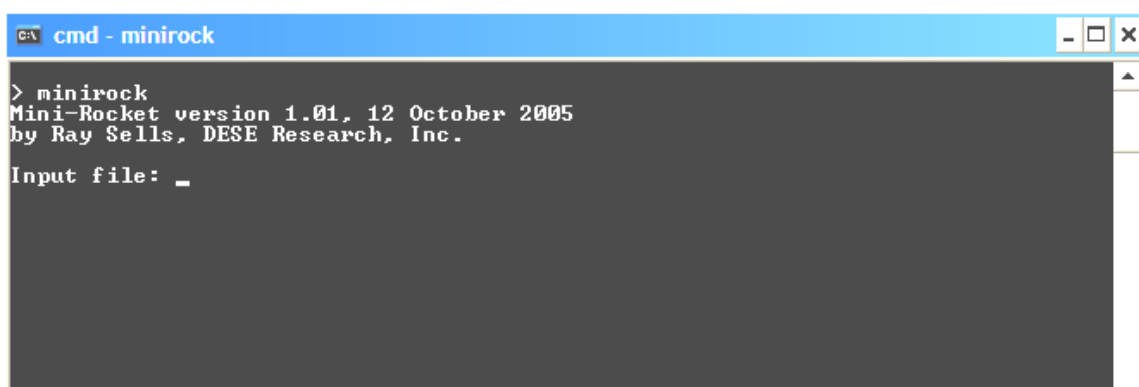
**APPENDIX 2
EXAMPLE CASE**

APPENDIX 2 - EXAMPLE CASE

An example case is shown here to acquaint the user with typical output and to illustrate Mini-Rocket functionality.

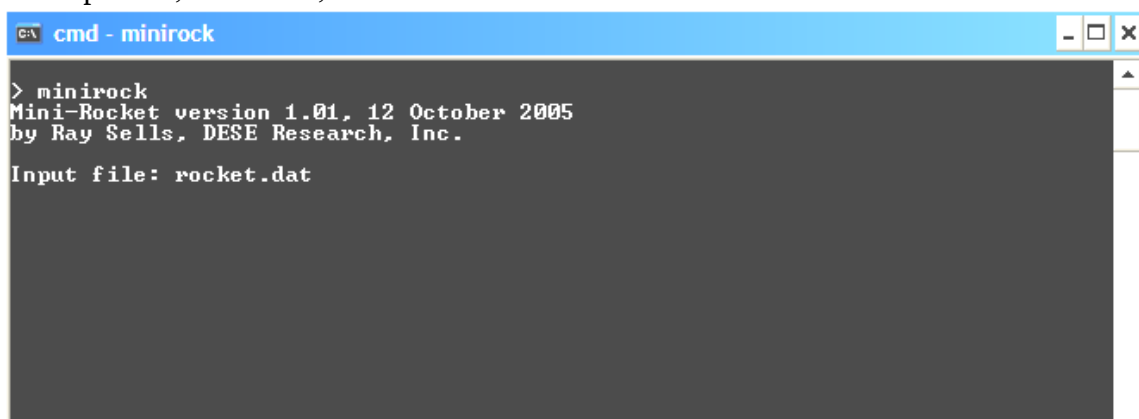
The input for this example is exactly that used to describe the input in the previous “Input Data File” section of this report. The missile being simulated is a hypothetical three-stage exo-atmospheric missile vertically launched from the ground. Program operation in a Windows environment is shown here. Of course, Mini-Rocket is cross-platform since it is written in standard C++ and is operated from a simple console interface.

Operation proceeds as described in section “Installation.”



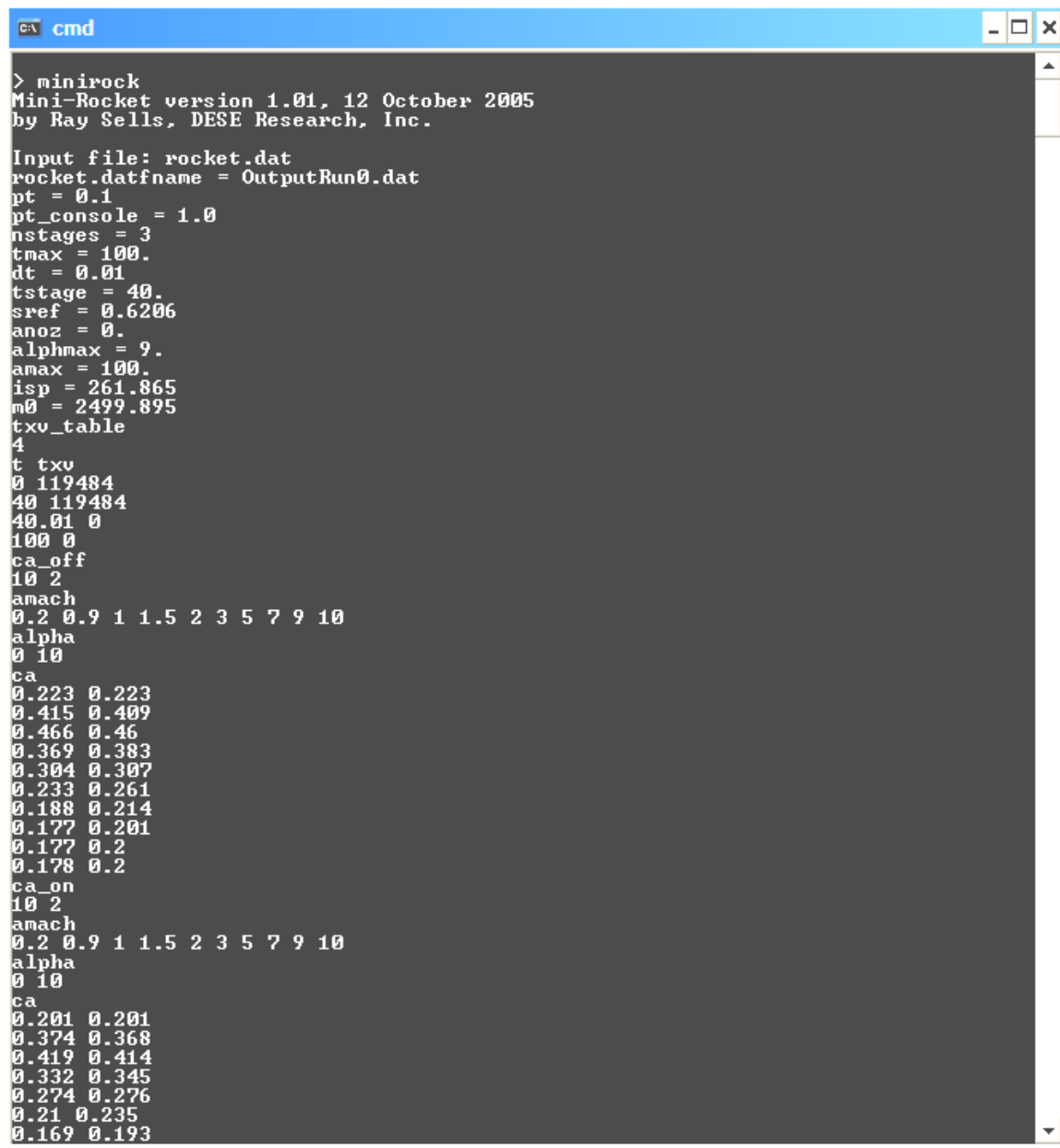
```
C:\> minirock
Mini-Rocket version 1.01, 12 October 2005
by Ray Sells, DESE Research, Inc.
Input file: _
```

The input file, rocket.dat, is the same as described earlier.



```
C:\> minirock
Mini-Rocket version 1.01, 12 October 2005
by Ray Sells, DESE Research, Inc.
Input file: rocket.dat
```

First, the contents of the input data file are echoed (after the standard program output banner).



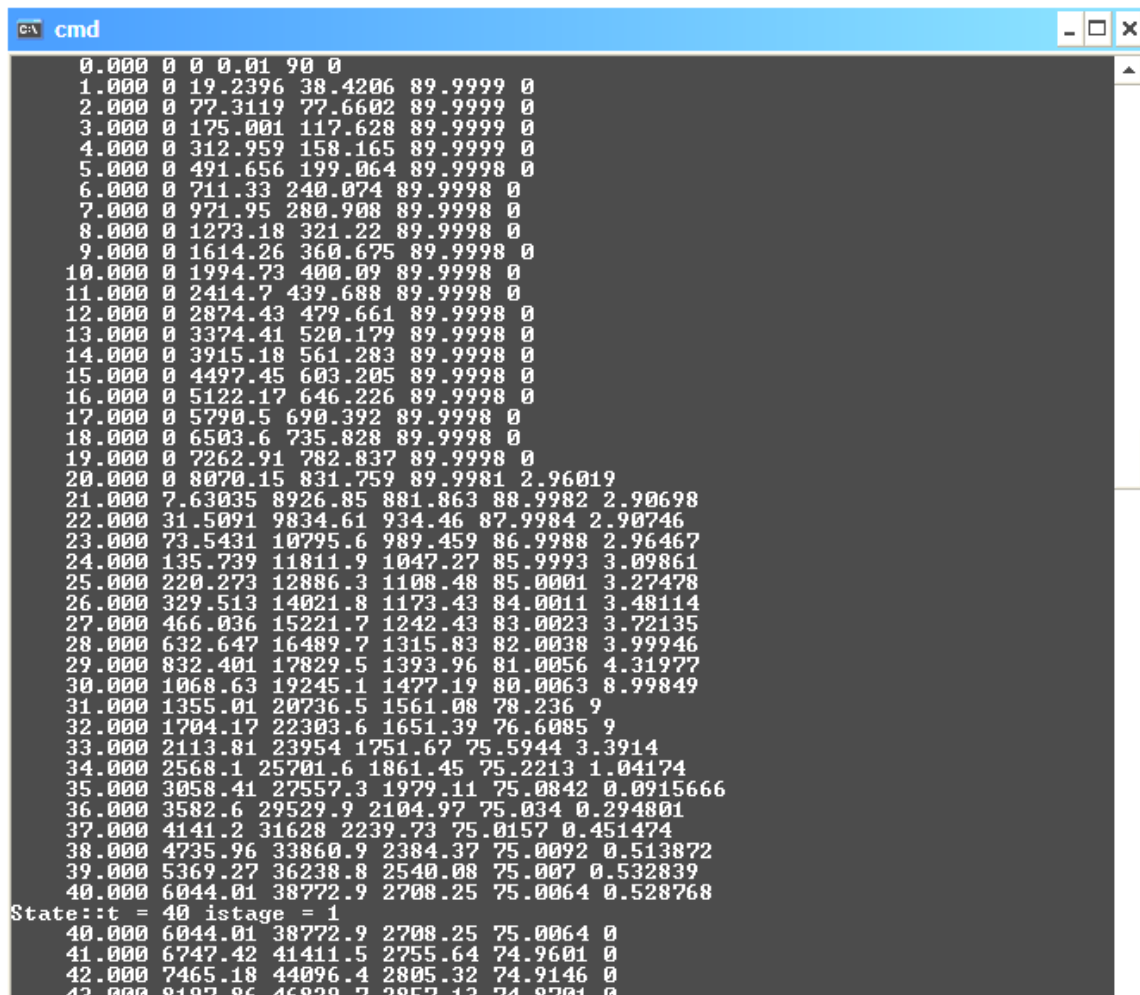
```

> minirock
Mini-Rocket version 1.01, 12 October 2005
by Ray Sells, DESE Research, Inc.

Input file: rocket.dat
rocket.datfname = OutputRun0.dat
pt = 0.1
pt_console = 1.0
nstages = 3
tmax = 100.
dt = 0.01
tstage = 40.
sref = 0.6206
anoz = 0.
alphamax = 9.
amax = 100.
isp = 261.865
m0 = 2499.895
txv_table
4
t txv
0 119484
40 119484
40.01 0
100 0
ca_off
10 2
amach
0.2 0.9 1 1.5 2 3 5 7 9 10
alpha
0 10
ca
0.223 0.223
0.415 0.409
0.466 0.46
0.369 0.383
0.304 0.307
0.233 0.261
0.188 0.214
0.177 0.201
0.177 0.2
0.178 0.2
ca_on
10 2
amach
0.2 0.9 1 1.5 2 3 5 7 9 10
alpha
0 10
ca
0.201 0.201
0.374 0.368
0.419 0.414
0.332 0.345
0.274 0.276
0.21 0.235
0.169 0.193

```

Computed program output to the console consists of those parameters specified for output in the input data file in columnar format. Each row begins with the time followed by parameter values at that time.



```

0.000 0 0 0.01 90 0
1.000 0 19.2396 38.4206 89.9999 0
2.000 0 77.3119 77.6602 89.9999 0
3.000 0 175.001 117.628 89.9999 0
4.000 0 312.959 158.165 89.9999 0
5.000 0 491.656 199.064 89.9998 0
6.000 0 711.33 240.074 89.9998 0
7.000 0 971.95 280.908 89.9998 0
8.000 0 1273.18 321.22 89.9998 0
9.000 0 1614.26 360.675 89.9998 0
10.000 0 1994.73 400.09 89.9998 0
11.000 0 2414.7 439.688 89.9998 0
12.000 0 2874.43 479.661 89.9998 0
13.000 0 3374.41 520.179 89.9998 0
14.000 0 3915.18 561.283 89.9998 0
15.000 0 4497.45 603.205 89.9998 0
16.000 0 5122.17 646.226 89.9998 0
17.000 0 5790.5 690.392 89.9998 0
18.000 0 6503.6 735.828 89.9998 0
19.000 0 7262.91 782.837 89.9998 0
20.000 0 8070.15 831.759 89.9981 2.96019
21.000 7.63035 8926.85 881.863 88.9982 2.90698
22.000 31.5091 9834.61 934.46 87.9984 2.90746
23.000 73.5431 10795.6 989.459 86.9988 2.96467
24.000 135.739 11811.9 1047.27 85.9993 3.09861
25.000 220.273 12886.3 1108.48 85.0001 3.27478
26.000 329.513 14021.8 1173.43 84.0011 3.48114
27.000 466.036 15221.7 1242.43 83.0023 3.72135
28.000 632.647 16489.7 1315.83 82.0038 3.99946
29.000 832.401 17829.5 1393.96 81.0056 4.31977
30.000 1068.63 19245.1 1477.19 80.0063 8.99849
31.000 1355.01 20736.5 1561.08 78.236 9
32.000 1704.17 22303.6 1651.39 76.6085 9
33.000 2113.81 23954 1751.67 75.5944 3.3914
34.000 2568.1 25701.6 1861.45 75.2213 1.04174
35.000 3058.41 27557.3 1979.11 75.0842 0.0915666
36.000 3582.6 29529.9 2104.97 75.034 0.294801
37.000 4141.2 31628 2239.73 75.0157 0.451474
38.000 4735.96 33860.9 2384.37 75.0092 0.513872
39.000 5369.27 36238.8 2540.08 75.007 0.532839
40.000 6044.01 38772.9 2708.25 75.0064 0.528768
State::t = 40 istage = 1
40.000 6044.01 38772.9 2708.25 75.0064 0
41.000 6747.42 41411.5 2755.64 74.9601 0
42.000 7465.18 44096.4 2805.32 74.9146 0
43.000 8197.86 46929.7 2857.13 74.8781 0

```

In this case, time is followed by range, altitude, velocity, flight path angle, and angle-of-attack. A message is printed at stage separation (section change) events.

Console output is merely a convenience to see that the program ran and to quickly observe, in a coarse sense, key flight parameters. Beyond that, it is difficult to discern much more from the console output. The primary output record is constrained in a separate output text file. This file is ASCII-text and can be opened with any simple text editor. The name of the file is that specified with the identifier `fname` in the input data file.

An excerpt from the data file is as shown.

```
n = 6
time range h vel gamma_d alph
0 0 0 0.01 90 0
0.1 0 0.200525 3.81198 90 0
0.2 0 0.781713 7.6228 89.9999 0
0.3 0 1.74444 11.4424 89.9999 0
0.4 0 3.08959 15.2707 89.9999 0
0.5 0 4.81803 19.1077 89.9999 0
0.6 0 6.93062 22.9533 89.9999 0
0.7 0 9.42822 26.8075 89.9999 0
0.8 0 12.3117 30.6701 89.9999 0
0.9 0 15.5819 34.5412 89.9999 0
1 0 19.2396 38.4206 89.9999 0
1.1 0 23.2857 42.3084 89.9999 0
1.2 0 27.721 46.2044 89.9999 0
1.3 0 32.5463 50.1085 89.9999 0
1.4 0 37.7625 54.0208 89.9999 0
1.5 0 43.3703 57.9411 89.9999 0
```

The parameters output here are identical to those sent to the console (parameter output for both are specified with the single output specification list in the input data file). By virtue of being a simple data file, this output is easily accessed by any external post-processing or data visualization tool.

The *wxpp* plotting tool included with the Mini-Rocket distribution provides a convenient means to quickly visualize the data in the form of two-dimensional plots. The program is invoked:

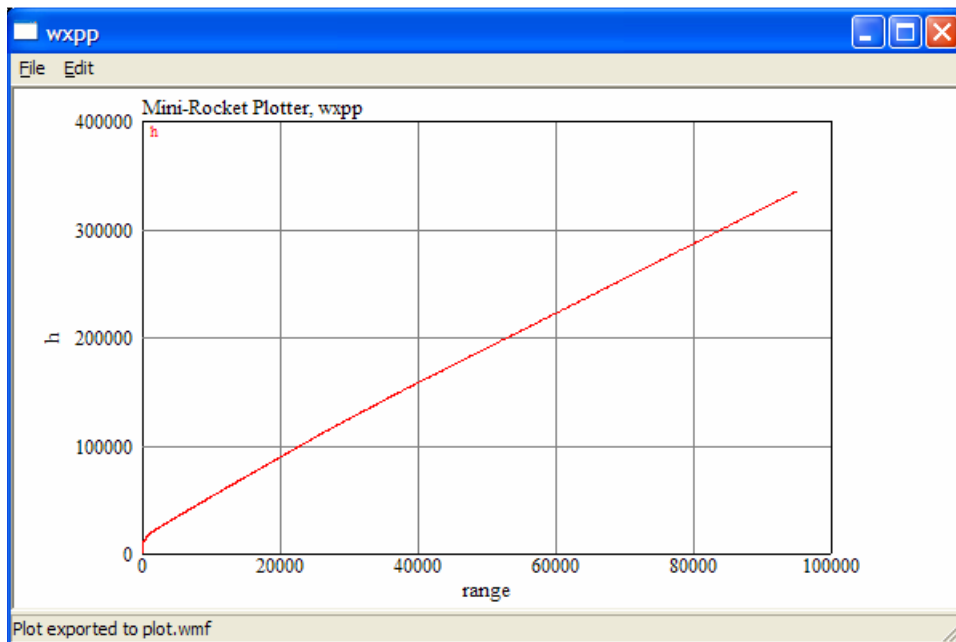
```
cmd
> wxpp
wxpp by Ray Sells, DESE Research, Inc., v51012
0 time
1 range
2 h
3 vel
4 gamma_d
5 alph
>
```

As explained in Appendix 1, five parameters are available for plotting (from the output data file, OutputRun0.dat) with the first field of output being time. The trajectory can be plotted using range (1 [range](#)) and altitude (2 [h](#)):

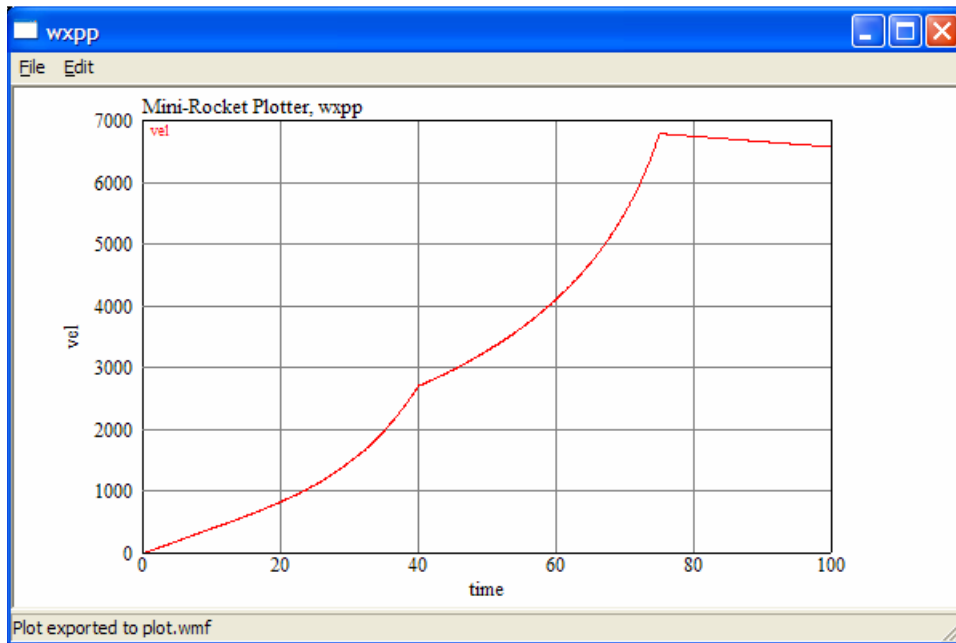
```
cmd - wxpp 1 2
> wxpp
wxpp by Ray Sells, DESE Research, Inc., v51012
0 time
1 range
2 h
3 vel
4 gamma_d
5 alph

> wxpp 1 2
wxpp by Ray Sells, DESE Research, Inc., v51012
-
```

The resulting plot is:

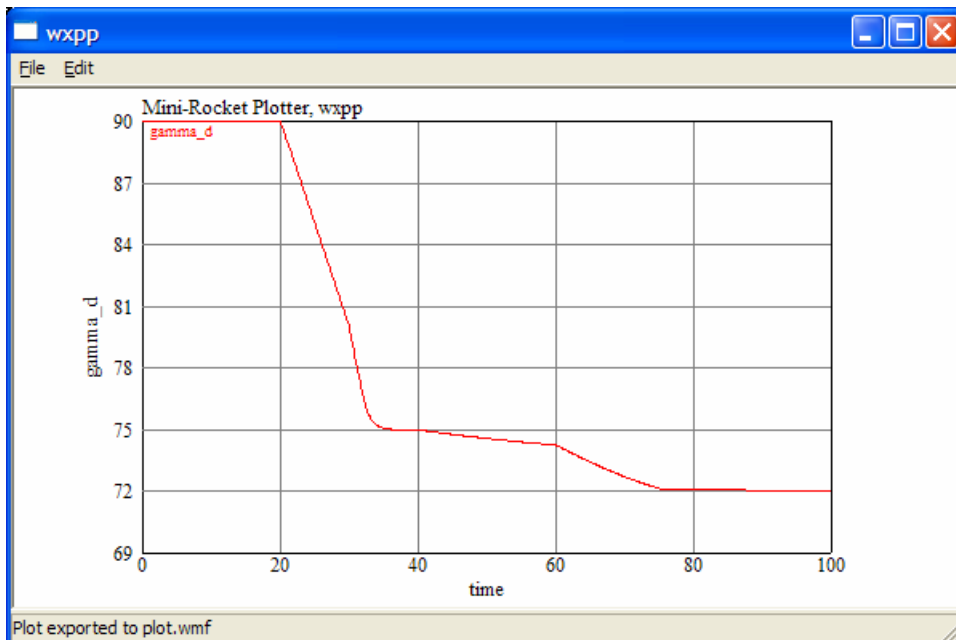


The action of the three stages can easily be discerned in the velocity vs. time plot ([wxpp 0 3](#)):



The discontinuity in velocity (sudden change in slope or acceleration) at 40 seconds indicates the transition to the second stage. Likewise, the discontinuity at 75 seconds clearly shows second stage burnout and the transition to the third stage, where velocity is lost due to ballistic flight.

The guidance flight modes can be seen by plotting the flight path angle vs. time (wxpp 0 4):

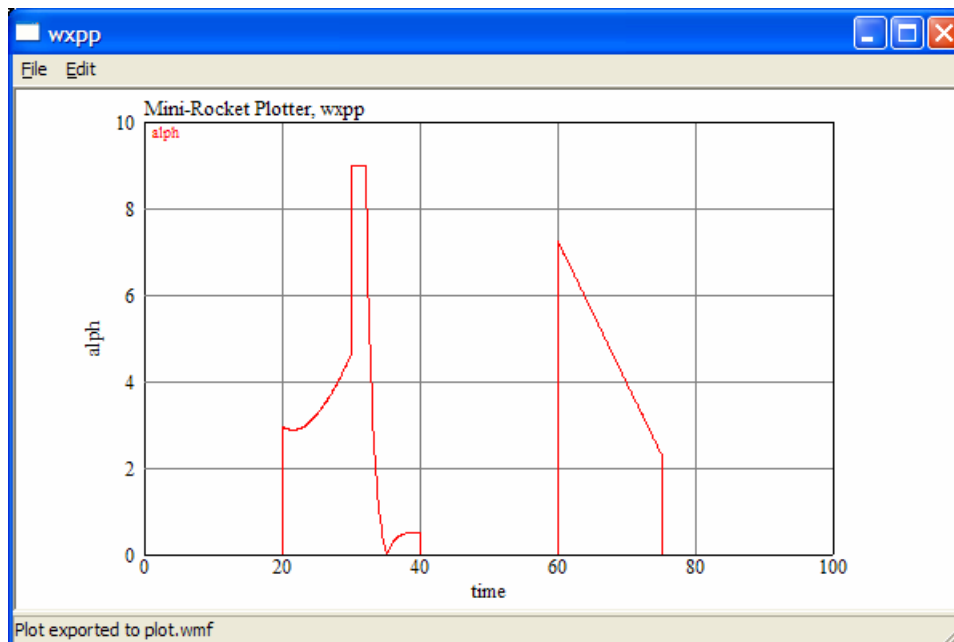


The slope of the curve confirms execution of the guidance modes specified in the input data. The guidance command tables in the input data can be summarized as follows:

time (sec)	stage	guidance mode
0-20	1	vertical launch, ballistic flight
20-30	1	pitch over at 1 deg/sec
30-40	1	pitch over to 75 deg flight path angle
40-60	2	fly ballistically
60-75	2	accelerate down (-z direction) at 11 m/sec^2
75-100	3	fly ballistically

The maneuvers are verified by reconciling the entries in the table to the behavior of the plot. The flight path stays constant at 90 degrees from vertical launch (0 to 20 seconds). The 1 degree/second pitch down is clearly seen as the flight angle goes from 90 to 80 degrees (change of 10 degrees) in 10 seconds (20 to 30 seconds). Consistent with an equivalent time constant of 1 second, the flight path angle quickly changes to 75 and holds there (30 to 40 seconds). The flight path angle slowly decreases as the missile flies ballistically and slowly pitches down due to gravity (40 to 60 seconds). A downward acceleration is clearly observed in response to the acceleration guidance command (60 to 75 seconds). Again, the downward pull of gravity is seen by the slowly decreasing flight angle during the final ballistic flight segment (75 to 100 seconds).

It is usually a good “sanity” check to confirm that the vehicle’s motion was “well-behaved” – that is, the vehicle was not tumbling! An easy way to check this is to plot the Angle-of-Attack (AOA):



It is quickly seen that the AOA stayed within a reasonable limit for the entire flight. Again, the behavior in the table can be reconciled to the plot. The AOA was zero after launch until the missile began to pitch over (0 to 20 seconds). The AOA becomes non-zero for the 1 degree/second pitchover (20 to 30 seconds). Notably, the AOA saturates (that is, reaches its

specified maximum limit of 9 degrees, $\alpha_{\max}$ in the data file) to fully accomplish the 75-degree flight path angle (30 to 40 seconds). Again the AOA is zero while the missile flies ballistically (40 to 60 seconds). The AOA becomes non-zero for the downward acceleration maneuver (60 to 75 seconds). Finally, the AOA is zero for the ballistic duration of the flight (75 to 100 seconds).

Of course, the parameters that can be plotted are not limited to those shown here; a full range of other parameters can be specified for plotting via selection in the input data. As shown by this example, Mini-Rocket in tandem with quick turnaround plotting tool (like *wxpp*) form a potent analysis tool to quickly determine missile performance and play “what-ifs” by perturbing the parameters that characterize the missile. A myriad of analyses can be performed using the cycle of steps shown in this example.

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