

ESTIMATING THE INSTABILITY OF A COMPOSITE CLOCK

C. A. Greenhall¹

Jet Propulsion Laboratory, California Institute of Technology
4800 Oak Grove Dr., MS 298-100, Pasadena, CA 91109, USA

E-mail: cgreen@mail.jpl.nasa.gov

Abstract

A composite clock created from a local clock ensemble is known by its time offsets from the ensemble clocks. By a geometrical argument, estimates for the instability of the composite clock are calculated from the instabilities of the ensemble clocks, individually and against the composite clock. The method is illustrated by examples using simulated and real ensembles.

1 INTRODUCTION

Suppose that we have a local ensemble of uncorrelated clocks $A_1, \dots, A_n$, called the base clocks. Their instabilities are assumed to be known, where instability is defined by any of the deviations (Allan, modified Allan, Hadamard) customarily used for clocks. In addition, there is another clock X whose offset from each A_i is known as a function of time. In particular, X could be a composite clock that is formed from some timescale algorithm operating on measurements of the differences $A_i - A_j$ of the base clocks; the measurement errors are assumed to be negligible. Having estimated the instabilities of the base clocks A_i and of the offsets $X - A_i$, how much can we find out about the instability of X itself? There has to be some information about it, but is it good enough to be useful?

By a geometrical argument, we will show how to compute the range of possible instabilities of X without using any outside comparisons and without knowing anything about the algorithm that produces X . For one or two clocks, the geometry can be shown by a simple diagram; for any number of clocks, the argument is carried out by algebra, and the results are given by simple formulas. There is a minimum instability, a maximum instability, and an intermediate “mid” estimate.

After developing the formulas we show three examples, two from simulations and one from real clocks, and discuss the limitations of the method that are inherent in our imperfect knowledge of the required data.

¹This work was performed by the Jet Propulsion Laboratory, California Institute of Technology, under a contract with the National Aeronautics and Space Administration.

Report Documentation Page				Form Approved OMB No. 0704-0188	
Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.					
1. REPORT DATE DEC 2004		2. REPORT TYPE		3. DATES COVERED 00-00-2004 to 00-00-2004	
4. TITLE AND SUBTITLE Estimating the Instability of a Composite Clock				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)				5d. PROJECT NUMBER	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) California Institute of Technology, Jet Propulsion Laboratory, 4800 Oak Grove Dr, Pasadena, CA, 91109				8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)				10. SPONSOR/MONITOR'S ACRONYM(S)	
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)	
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited					
13. SUPPLEMENTARY NOTES See also ADM001784. 36th Annual Precise Time and Time Interval (PTTI) Systems and Applications Meeting, Washington, DC on 7-9 Dec 2004					
14. ABSTRACT see report					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT Same as Report (SAR)	18. NUMBER OF PAGES 10	19a. NAME OF RESPONSIBLE PERSON
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified			

2 A GEOMETRICAL ARGUMENT

Any RMS instability measure, for a single averaging time, can be regarded as a norm generated by an inner product on a vector space of random phase residuals. To be specific, consider Allan deviation $\sigma_y(\tau)$, where τ is fixed in this discussion. If A and B are two clocks with phase deviations $x_A(t)$ and $x_B(t)$, define the inner product

$$\langle A, B \rangle_\tau = \frac{1}{2\tau^2} \mathbb{E} [\Delta_\tau^2 x_A(t)] [\Delta_\tau^2 x_B(t)], \quad (1)$$

where it is assumed that the expectation does not depend on t . Then $\sigma_y(\tau)$ for clock A is the norm $\|A\|_\tau$ generated by this inner product:

$$\sigma_y(\tau) = \|A\|_\tau = \sqrt{\langle A, A \rangle_\tau}. \quad (2)$$

Each τ determines a different norm², or metric. The instability of A and B relative to each other is $\|A - B\|_\tau$, the distance between the two points in this metric space. The clocks are orthogonal in this inner product, $\langle A, B \rangle_\tau = 0$, if the clocks are uncorrelated and $[\mathbb{E} \Delta_\tau^2 x_A(t)] [\mathbb{E} \Delta_\tau^2 x_B(t)] = 0$.

We may now use the algebraic machinery of inner product spaces to find our way about. Because we are dealing with a finite number of “vectors,” this algebra is the same as the algebra of Euclidean spaces and can be interpreted geometrically. In the following arguments, the base subspace is defined as the space of linear combinations of the base clocks, which are assumed to be orthogonal.

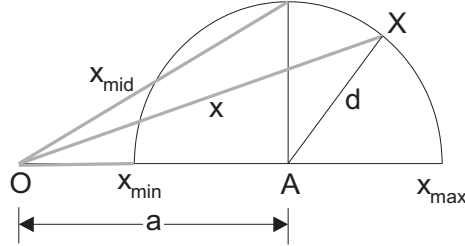


Figure 1: One base clock.

2.1 One Base Clock

We can begin with just one base clock A and the other clock X . Let $a = \|A\|_\tau$, $x = \|X\|_\tau$, $d = \|X - A\|_\tau$. We know a and d , and we want to estimate x . In Figure 1, the point X is somewhere on a circle with radius d and center at a on the baseline, and x is the length of OX . The maximum and minimum of x are $a + d$ and $|a - d|$ (whether or not $a \geq d$). The intermediate

²Strictly speaking, this is a seminorm because $\|A\| = 0$ if the clock has constant frequency. Or we can identify clocks that differ only by a constant frequency.

estimate of x comes from the assumption that clock X equals clock A plus a vector orthogonal to A . Thus, for one base clock we express the results as

$$x_{\max} = a + d, \quad x_{\min} = |a - d|, \quad x_{\text{mid}} = \sqrt{a^2 + d^2}. \quad (3)$$

2.2 Two Base Clocks

For two base clocks, three dimensions are needed. Figure 2 shows the geometry without the third dimension. The orthogonal base clocks A_1 and A_2 have norms a_1 and a_2 . We also know the distances d_1 and d_2 of X from A_1 and A_2 . The possible values of $x = \|X\|_\tau$ are realized by rotating X out of the plane about the axis A_1A_2 , keeping the distances d_1 and d_2 fixed. The picture shows $x_{\min}$ and $x_{\max}$, which are the values of x when X is in the plane, that is, in the base subspace. (In the picture, X is at the max position.) When X is directly above a point on A_1A_2 , then X is as far from the plane as it can be, and X is a weighted average of the base clocks plus a vector $X_\perp$ orthogonal to the base subspace. We define x_{mid} to be the length of this X . (In an extreme case, one of the two weights can be negative, though their sum is 1.) The author feels intuitively that this solution has special value for estimating the norm of a composite clock, simply because timescale algorithms express the increment of the composite clock as a weighted average of the increments of the detrended base clocks. The author has no further argument to support this intuition, however.

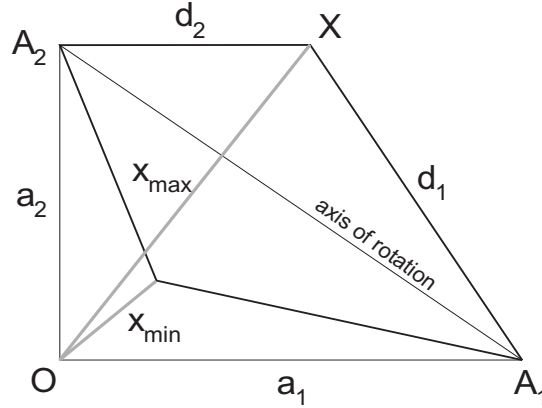


Figure 2: Two base clocks. The point X is rotated out of the plane.

2.3 Any Number of Base Clocks

For n base clocks the argument can be carried out algebraically. The clocks A_i are assumed to be orthogonal. Given $a_i = \|A_i\|_\tau > 0$ and $d_i = \|X - A_i\|_\tau$ for all i , we wish to estimate $x = \|X\|_\tau$. We can represent X by the orthogonal expansion

$$X = \left(\sum_{i=1}^n x_i \frac{A_i}{a_i} \right) + X_\perp, \quad (4)$$

where

$$x_i = \frac{\langle X, A_i \rangle_\tau}{a_i}, \quad (5)$$

and $X_\perp$ is a vector that is orthogonal to the base subspace. Let $x_\perp = \|X_\perp\|_\tau$. Then

$$x^2 = \left(\sum_{i=1}^n x_i^2 \right) + x_\perp^2. \quad (6)$$

Now

$$\begin{aligned} d_i^2 &= \|X - A_i\|_\tau^2 = x^2 - 2 \langle X, A_i \rangle_\tau + a_i^2 = x^2 - 2a_i x_i + a_i^2, \\ 2x_i &= \frac{x^2 + a_i^2 - d_i^2}{a_i}. \end{aligned} \quad (7)$$

Square both sides of (7) and sum over i . By (6),

$$4(x^2 - x_\perp^2) = \sum_{i=1}^n \frac{(x^2 + a_i^2 - d_i^2)^2}{a_i^2}.$$

Expand the terms in this sum and collect powers of x . Setting

$$\varepsilon_i = 1 - \frac{d_i^2}{a_i^2} \quad (8)$$

we get

$$x^4 \sum a_i^{-2} - 2x^2 (2 - \sum \varepsilon_i) + \sum a_i^2 \varepsilon_i^2 + 4x_\perp^2 = 0.$$

To simplify this equation further, set

$$y = x^2 \sum a_i^{-2}, \quad (9)$$

$$y_\perp = x_\perp^2 \sum a_i^{-2}. \quad (10)$$

Then

$$y^2 - 2By + C + 4y_\perp = 0, \quad (11)$$

where

$$B = 2 - \sum \varepsilon_i, \quad (12)$$

$$C = \left(\sum a_i^{-2} \right) \left(\sum a_i^2 \varepsilon_i^2 \right). \quad (13)$$

The solutions of (11) are

$$y = B \pm \sqrt{B^2 - C - 4y_\perp}, \quad (14)$$

with corresponding solutions for x according to (9).

A necessary and sufficient condition for meaningful solutions to exist is

$$B \geq \sqrt{C}. \quad (15)$$

If (15) holds and $0 \leq y_{\perp} \leq \frac{1}{4}(B^2 - C)$, then there are nonnegative y solutions corresponding to the points X that are the same distance $x_{\perp}$ above and below the base subspace. When $y_{\perp} = 0$ we have the extremal solutions

$$y_{\max} = B + \sqrt{B^2 - C}, \quad y_{\min} = B - \sqrt{B^2 - C}, \quad (16)$$

for which X is in the base subspace. When $y_{\perp}$ takes its maximum value $\frac{1}{4}(B^2 - C)$, we have the intermediate estimate

$$y_{\text{mid}} = B. \quad (17)$$

For this special solution, $\sum \frac{x_i}{a_i} = 1$. In fact, if $y = B$ then $x^2 = B / \sum a_j^{-2}$. By (7) and (8),

$$\frac{x_i}{a_i} = \frac{B}{2a_i^2 \sum a_j^{-2}} + \frac{\varepsilon_i}{2},$$

and $\sum \frac{x_i}{a_i} = 1$ follows from (12). Then (4) says that X is a weighted average of the A_i plus a vector orthogonal to the base subspace. (Again, some of the weights can be negative.)

If $B < \sqrt{C}$ there are no meaningful solutions: there is no point X at the given distances d_i from orthogonal vectors A_i having given lengths a_i . In Figure 2, the two pivoting rods fastened to A_1 and A_2 are too short or too mismatched for their free ends to meet at a common point X .

The reader is reminded that this calculation has to be carried out anew for each averaging time τ .

3 EXAMPLES

The first example (Figure 3) is from an eight-clock simulation [1]. The duration of the simulated run is 1.44×10^8 s. The clocks are all simulated with white FM plus random walk FM. The odd-numbered clocks are statistically identical to clock 1, the even-numbered clocks to clock 2. The dotted curves show the measured Allan deviation (Adev) of clocks 1 and 2. The black curve with the asterisks is the measured Adev of the actual composite clock (CC) phase, which was produced with a modified Kalman filter algorithm. Not shown are the Adevs of the base clocks against the CC, d_i in the previous section. The blue curves with the plus signs, labeled “True,” show the min, mid, and max CC estimates using the measured Adev of the true simulated clocks for a_i . These curves end when the condition (15) is violated. Because stability measurements of the individual base clocks would not be directly available in reality, Barnes’s n -cornered-hat formulas [2,3] were also used to generate values for a_i from the measured Adevs of all base clock pairs. The resulting CC estimates are shown by the green curves with the open circles, labeled “NCH.” These curves end when some of the variance estimates from the n -cornered hat are negative. The NCH mid and max estimates agree well with the True estimates where they both exist. The mid estimate is at most 1.25 times the actual CC Adev; the max estimates are less than 1.8 times the actual CC Adev. The min estimates are too low and variable to be useful.

The second example (Figure 4) is from a four-clock simulation [4], in which the CC phase was also generated by a modified Kalman algorithm. The simulated duration is 10^6 s. The ratio of mid estimate to actual CC Adev is between 0.95 and 1.12.

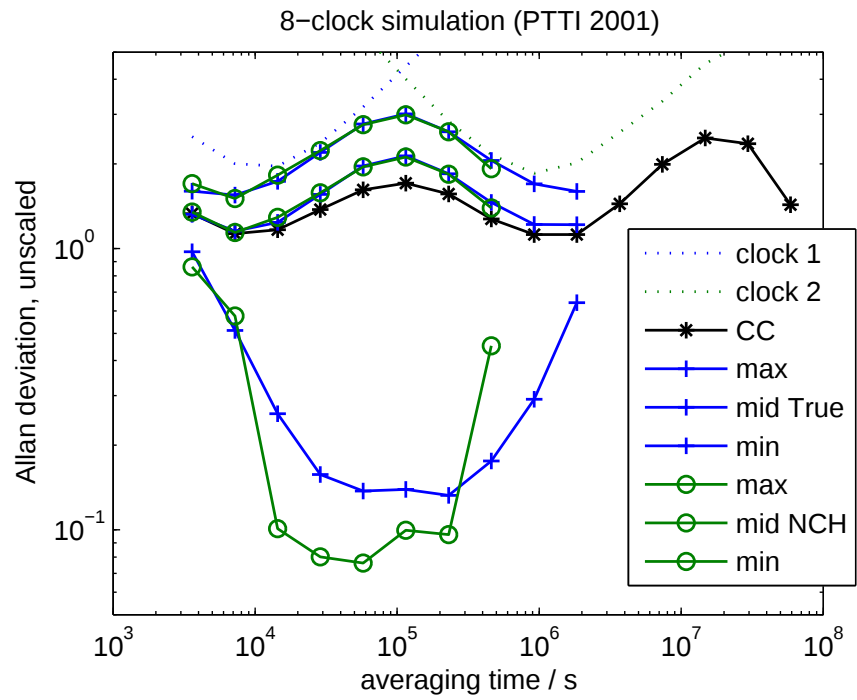


Figure 3: An eight-clock simulation

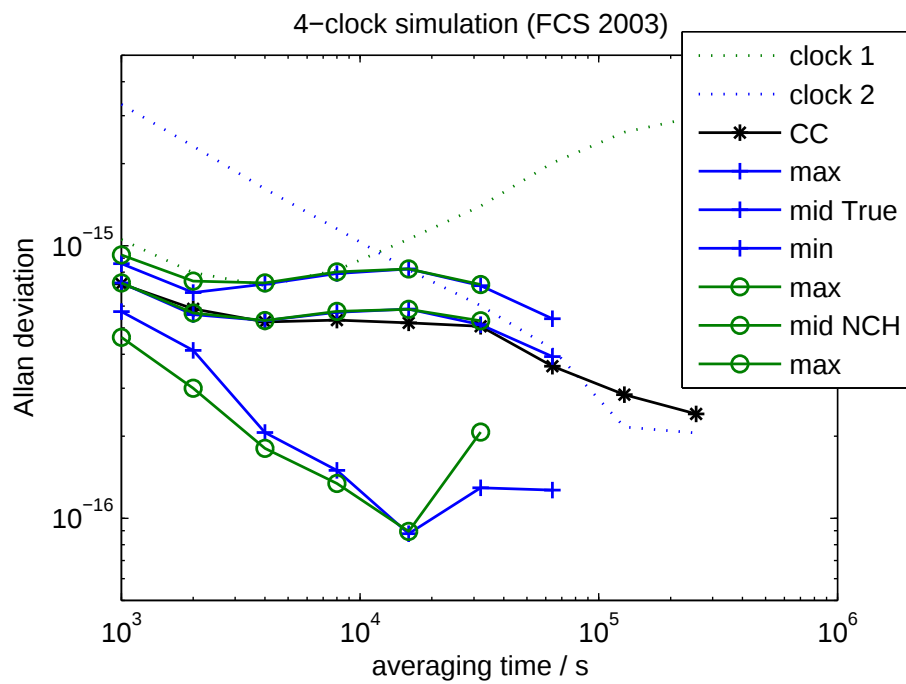


Figure 4: A four-clock simulation

The third example (Figure 5) uses actual data from a comparison of three hydrogen masers at the National Physical Laboratory between MJD 53005 and MJD 53160 [5]. To eliminate the effect of linear frequency drift, Hadamard deviation (Hdev) is used for the instability measure. The dotted curves are the three-cornered hat Hdev estimates of the base clocks. The CC phase (relative to the base clocks) is generated by a novel Kalman algorithm, in which the frequency state of each clock is represented as the sum of independent stationary Markov processes. Here we do not know the actual CC Hdev, but the black curve shows a theoretical computation of its Hdev, obtained from an auxiliary Kalman filter calculation [5]. The mid estimate agrees remarkably well with the theoretical CC Hdev. Furthermore, the min and max estimates are relatively tight. Geometrically, the point X has to stay close to the plane of weighted averages of the three clocks. For two clocks (Figure 2), X would be close to the line A_1A_2 ; this would happen if $d_1 + d_2$ were only slightly greater than $\sqrt{a_1^2 + a_2^2}$.

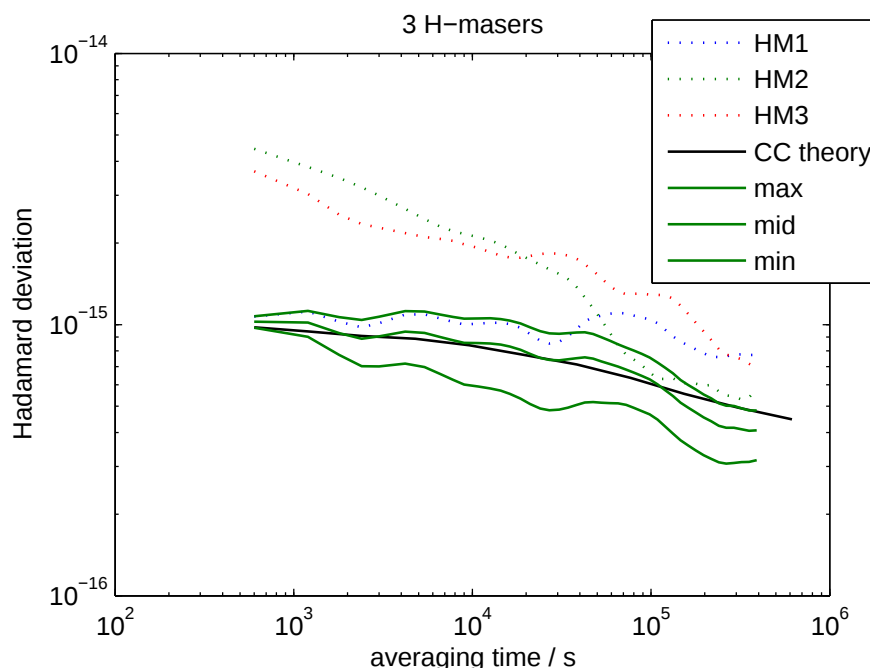


Figure 5: An ensemble of three hydrogen masers.

4 DISCUSSION

We have shown a method for calculating estimates for the instability of a composite clock from knowledge of the instability of the base clocks and of their offsets from the composite clock. Like the n -cornered hat, this method needs a long data interval for a given averaging time to give useful results. The theory behind the calculation assumes that we know the exact expected values of the required instabilities, and that the base clocks are uncorrelated stochastic processes. Of course, the values have to be estimated from finite data; moreover, the base clock instabilities a_i themselves often come from an n -cornered hat calculation. The base clocks may also be physically correlated. (In any case, their finite samples almost always have nonzero correlations.) Nevertheless, in the

examples that were tried, the method gives practical max and mid estimates whenever they can be calculated at all.

The author's experience with this method is limited to a few examples in which the composite clock was generated by a modified Kalman algorithm. Users of other timescale algorithms should try the method on simulated data before trusting it to give useful results for real clocks.

5 REFERENCES

- [1] C. Greenhall, 2003, "*Kalman plus weights: a time scale algorithm*," in Proceedings of the 33rd Precise Time and Time Interval (PTTI) Systems and Applications Meeting, 27-29 November 2002, Long Beach, California, USA (U.S. Naval Observatory, Washington, D.C.), pp. 445–454.
- [2] J. Barnes, 1982, Notes from NBS 2nd Symposium Atomic Time Scale Algorithms (National Bureau of Standards, Boulder, Colorado).
- [3] J. Barnes, 1992, **The Analysis of Frequency and Time Data** (Austron, Inc.).
- [4] C. Greenhall, 2003, "*An optimal modification of a Kalman filter for time scales*," in Proceedings of the 2003 IEEE International Frequency Control Symposium & PDA Exhibition Jointly with the 17th European Frequency & Time Forum (EFTF), 5-8 May 2003, Tampa, Florida, USA (IEEE 03CH37409C), pp. 228–232.
- [5] J. Davis, C. Greenhall, and P. Stacey, 2005, "*A Kalman filter clock algorithm for use in the presence of flicker frequency modulation noise*," **Metrologia**, **42**, 1-10.

Questions and Answers

DEMETRIOS MATSAKIS (U.S. Naval Observatory): Brown wrote a paper which I believe was published in 1981 in the Institute of Navigation, and he did the Composite Clock of GPS as his example; it was Kalman-based. I am sure he came up with a formula, and I believe it was something as simple as a weight squared times the Allan variance equals a composite Allan variance. Have you compared your results to whatever he had in there?

CHUCK GREENHALL: I think that was for a special example where all the clocks had the same phase spectrum except at different levels, if I remember correctly.

MARC WEISS (National Institute of Standards and Technology): I have always thought that the case for a clock independence results in – well, if the algorithm is optimal, you get the resistance-in-parallel law; that is, one over the variance of the composite clock should be equal to one over the variance of the clocks. And I guess you can throw the weight over the variance of the clock. Maybe it is times, but something like that. Is that what you have done here? Is that consistent with that idea?

GREENHALL: I have had a little time to think now. This method doesn't even know what kind of algorithm is used for the Composite Clock. So I think just using the method you say would be sort of equivalent to saying that the Composite Clock is close to the origin as you can get – on this line here.

Yes, you see, and in other words d_1 plus d_2 would be equal the length of this line. I think that is what would happen. But I am just guessing, you know.

