



AFRL-RZ-WP-TM-2012-0192

TURBINE AEROTHERMAL RESEARCH

Rolf Sondergaard, Shichuan Ou, and Richard Rivir

Turbomachinery Branch

Turbine Engine Division

MAY 2012

Final Report

Approved for public release; distribution unlimited.

See additional restrictions described on inside pages

STINFO COPY

**AIR FORCE RESEARCH LABORATORY
AEROSPACE SYSTEMS DIRECTORATE
WRIGHT-PATTERSON AIR FORCE BASE, OH 45433-7542
AIR FORCE MATERIEL COMMAND
UNITED STATES AIR FORCE**

NOTICE AND SIGNATURE PAGE

Using Government drawings, specifications, or other data included in this document for any purpose other than Government procurement does not in any way obligate the U.S. Government. The fact that the Government formulated or supplied the drawings, specifications, or other data does not license the holder or any other person or corporation; or convey any rights or permission to manufacture, use, or sell any patented invention that may relate to them.

This report was cleared for public release by the USAF 88th Air Base Wing (88 ABW) Public Affairs Office (PAO) and is available to the general public, including foreign nationals. Copies may be obtained from the Defense Technical Information Center (DTIC) (<http://www.dtic.mil>).

AFRL-RZ-WP-TM-2012-0192 HAS BEEN REVIEWED AND IS APPROVED FOR PUBLICATION IN ACCORDANCE WITH THE ASSIGNED DISTRIBUTION STATEMENT.

*//Signature//

ROLF SONDERGAARD
Project Engineer
Turbomachinery Branch
Turbine Engine Division

//Signature//

CHARLES W. STEVENS
Branch Chief
Turbomachinery Branch
Turbine Engine Division

//Signature//

ROBERT D. HANCOCK
Principal Scientist
Turbine Engine Division
Aerospace Systems Directorate

This report is published in the interest of scientific and technical information exchange, and its publication does not constitute the Government's approval or disapproval of its ideas or findings.

*Disseminated copies will show “//Signature//” stamped or typed above the signature blocks.

REPORT DOCUMENTATION PAGE				Form Approved OMB No. 0704-0188	
The public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.					
1. REPORT DATE (DD-MM-YY) May 2012		2. REPORT TYPE Final		3. DATES COVERED (From - To) 01 May 2005 – 31 June 2009	
4. TITLE AND SUBTITLE TURBINE AEROTHERMAL RESEARCH				5a. CONTRACT NUMBER In-house	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER 61102F	
6. AUTHOR(S) Rolf Sondergaard, Shichuan Ou, and Richard Rivir				5d. PROJECT NUMBER 2307	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER Q0EE	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Turbomachinery Branch (AFRL/RQTT) Turbine Engine Division Air Force Research Laboratory Aerospace Systems Directorate (formerly Propulsion Directorate) Wright-Patterson Air Force Base, OH 45433-7542 Air Force Materiel Command, United States Air Force				8. PERFORMING ORGANIZATION REPORT NUMBER AFRL-RZ-WP-TM-2012-0192	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) Air Force Research Laboratory Aerospace Systems Directorate (formerly Propulsion Directorate) Wright-Patterson Air Force Base, OH 45433-7542 Air Force Materiel Command United States Air Force				10. SPONSORING/MONITORING AGENCY ACRONYM(S) AFRL/RQTT (formerly AFRL/RZTT)	
				11. SPONSORING/MONITORING AGENCY REPORT NUMBER(S) AFRL-RZ-WP-TM-2012-0192	
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited.					
13. SUPPLEMENTARY NOTES PA Case Number: 88ABW-2012-3444; Clearance Date: 13 Jun 2012. Report contains color.					
14. ABSTRACT This in-house task was funded under AFOSR ILIR grants 92PR07COR and 02PR02COR. This task and its predecessors have been in continual operation since 1985 and have covered a broad range of topics relating to the aerodynamics and thermodynamics of the turbine module of gas turbine engines. The work initially focused on the effects of very high turbulence freestream flows on the development of the boundary layers of the turbine component, with particular attention to the effect on heat transfer. It has also pursued techniques for the control of airfoil boundary layers and cooling flows and the development of advanced techniques for the measurement and study of these flows.					
15. SUBJECT TERMS turbine heat transfer, turbine aerodynamics, film cooling, turbine flow control					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT: SAR	18. NUMBER OF PAGES 22	19a. NAME OF RESPONSIBLE PERSON (Monitor) Rolf Sondergaard 19b. TELEPHONE NUMBER (Include Area Code) N/A
a. REPORT Unclassified	b. ABSTRACT Unclassified	c. THIS PAGE Unclassified			

Table of Contents

<u>Section</u>	<u>Page</u>
LIST OF FIGURES	ii
1.0 SUMMARY	1
2.0 RESEARCH RESULTS	2
2.1. Heat Transfer and Film Cooling Research	2
2.2. Turbulence Model Development:.....	5
2.3. Aerodynamic Flow Control	5
2.3.1. Passive Boundary Layer Control.....	5
2.3.2. Active Boundary Layer Control: Vortex Generator Jets	6
2.3.3. Active Boundary Layer Control: Atmospheric Plasmas:.....	7
2.4. Engine LPT application	8
3.0 CONCLUSIONS.....	11
APPENDIX: LIST OF PUBLICATIONS	12
LIST OF ACRONYMS	14

List of Figures

<u>Figure</u>	<u>Page</u>
Figure 1: Infrared Images from Transient Pulsed Heat Transfer Test	4
Figure 2: Pulsed Cooling Flow Reduced Data.....	4
Figure 3: Computed Flow Over Spherical Dimples	6
Figure 4: Effect of Vortex Generator Jet (VGJ) Blowing on Loss	7
Figure 5: Boundary Layer Velocity Profiles.....	8
Figure 6: Engine LPT Cascade Blades	9
Figure 7: Dimpled HPT Vanes for Turbine Research Facility	9
Figure 8: TRF Wake Traverse of Dimples on Roughened Vanes	9

1.0 SUMMARY

The objectives of this task are to increase turbine engine performance and lifetime by improving reliability, reducing cooling flows, increasing turbine efficiencies, increasing thrust to weight ratio, and reducing turbine engine design cycle time.

To that end, the program seeks to:

- Establish fundamental understanding of heat transfer and cooling mechanisms in gas turbine engines; provide an understanding of the effects of unsteady and free stream turbulence on turbine blade heat transfer; improve the accuracy of heat transfer predictions and computations; and develop concepts and strategies for the control of turbulent heat transfer.
- Investigate turbine flow control for reduction of secondary flow losses; reduction of losses associated with low Reynolds number separated flows; control of flow areas, flow direction, and airfoil circulation. Investigate technologies for turbine flow control, including passive and active fluidic, mechanical, and electromagnetic actuation.
- Transition basic research results to the gas turbine industry and to Improved High Performance Turbine Engine Technology (IHPTET) and Versatile Affordable Adaptive Turbine Engines (VAATE) Technology Demonstrations.

2.0 RESEARCH RESULTS

2.1. Heat Transfer and Film Cooling Research

The primary source of error in the prediction of heat transfer and film cooling effectiveness in the turbine engine hot section is the inability to accurately model the effect of the highly unsteady environment found inside the turbine engine. Unsteadiness affecting the turbine section ranges from large scale, high amplitude, coherent unsteadiness due to shocks and wakes from upstream components down to fine scale isotropic turbulence. Unsteadiness across this wide range of amplitudes, scales, and frequencies significantly affect the development of the boundary layers on the hot section components, often in very complex ways. Understanding these complex interactions, and validating computational models of them, requires carefully executed precision measurements of heat transfer and film cooling under well defined unsteady forcing.

Initial experiments under this program were performed using a wall jet facility (essentially a long, instrumented flat plate with a high speed rectangular jet blown along it) in order to produce a boundary layer with very high levels of unsteadiness outside the boundary layer. Hot wire anemometers and pitot-static pressure instrumentation were used to quantify the boundary layer and external flow fluid mechanical properties. Fast response thermocouples were used to quantify the flow temperatures and measure the response of the wall temperature to rapid changes in the external temperature. The wall temperature response, combined with knowledge of the thermodynamic properties of both the boundary layer flow and the wall, were used to extract the heat transfer coefficient under various flow conditions at various points under the boundary layer. The major findings of these experiments were that the levels of turbulence that exist in high pressure turbines from wakes, upstream disturbances, film cooling, horseshoe vortices and secondary flows results in levels of 10-20%. The initial wall jet experiments showed augmentation of heat transfer by factors of 2 to 4. Previous experiments on the effects of turbulence on heat transfer showed only marginal effects for levels of 1-6% and this is because the near wall shear layer of a "fully turbulent" boundary layer already has a peak in turbulence of typically 8-10% so these free stream levels of 1-6% had little effect - but the wall jet, with increased levels of 10-20%, had significant increases in heat transfer. Correlations of the wall heat flux from high response series thermopiles with the free stream fluctuations showed correlations of 50 to 60% indicating new physics for computations. The turbulent Prandtl Number now required significant modification and these measurements and calculations were also accomplished in this facility for these conditions. These initial experiments were initiated to explain engine measurements which showed increases of engine heat transfer by factors of three - 4 over that expected for a fully turbulent boundary layer as this was the highest value thought possible. Detailed results from these experiments are available in publications listed in the appendix.

After the effects of high freestream unsteadiness were quantified in the wall jet facility, model film cooling holes were introduced to study the interaction of film cooling with the turbulently driven boundary layer. Of primary interest were the influence of the cooling film injection on the wall heat transfer in the vicinity of the holes and the effect of unsteadiness, both in the holes

and outside the boundary layer on the film cooling effectiveness (essentially a measure of how well the cooling flow is working).

The extraction of both heat transfer and film cooling effectiveness required development of a three-temperature testing technique. By setting the freestream, cooling flow, and wall to one set of three initial temperatures, running the test, and then repeating the same with another set of three initial temperatures while holding all the fluidic conditions constant, it is possible to solve a pair of coupled non-linear equations for both the heat transfer coefficient and the film cooling effectiveness coefficient. The usefulness of these measurements was increased greatly by the introduction of first Thermochromic Liquid Crystals (a surface coating which changes color with temperature) and then accurate infrared temperature measurements which allowed simultaneous measurement of temperature over the entire surface, instead of just the few dozen points measurable with thermocouples. One of the major findings of these experiments was that it is not sufficient to simply increase film cooling effectiveness. Because of the complex coupling between film cooling and heat transfer, it is possible to increase film effectiveness, but at the same time increase heat transfer to such an extent that your overall heat transfer situation actually degrades. Detailed results from these experiments are available in publications listed in the appendix.

Later experiments sought to increase the realism of the flows studied. Large scale coherent unsteadiness was added to try to emulate the sorts of aerodynamic forcing the turbine components see due to upstream wakes. External pressure gradients were imposed in order to emulate the effects of pressure variations on the suction and pressure sides of turbine airfoils. A facility was designed and built to study the influence of the high curvature and saddle-type flow kinematics on and near the leading edge of turbine blades. Detailed results from these experiments are available in publications listed in the appendix.

Most recently, experiments have been conducted to try to demonstrate how unsteadiness might be used to improve the performance of the cooling system. By pulsing the film cooling flow it has been demonstrated that a significant reduction in film cooling mass flow (75%) at the same effectiveness is possible without a corresponding increase in heat transfer coefficient. Pulsed film cooling has been applied to both straight, cylindrical, holes and shaped holes.

A transient IR measurement was used to obtain the film effectiveness and heat transfer on a representative turbine leading edge with pulsed film cooling. The transient IR technique allows the measurement of both film effectiveness and heat transfer coefficient using wall temperatures from a single transient test run. Temperature data from two different times in the run, instead of two separate runs as is traditionally required for accurate transient thermochromic liquid crystal measurements, are used to solve the pair of coupled equations describing the evolution of the wall temperature. This same technique could also be used with thermochromic liquid crystals but because the temperature range of available liquid crystals is so limited, accurate measurements are not possible. The transient IR technique has been shown to be more accurate than transient LC in a direct comparison using matching flow conditions. This is due to the single run, the availability of the initial temperature distribution, and the wide temperature range over which accurate IR measurements can be made.

Figure 1 shows typical transient IR measurements of the surface temperature on the cylindrical leading edge of a turbine blade model with pulsed injection at 10 Hz. Measurements are shown for three times during a single test run. Figure 2 shows the resulting heat transfer coefficient and film cooling effectiveness distributions that are obtained from processing of the IR temperature measurements.

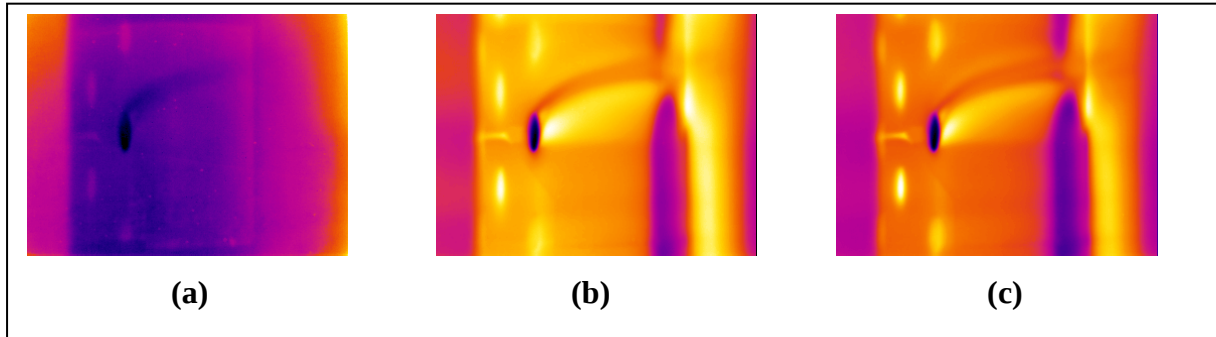


Figure 1: Infrared Images from Transient Pulsed Heat Transfer Test
(a): Start of test, $t = 0$; (b) $t = 25$ sec; (c) $t = 70$ sec.

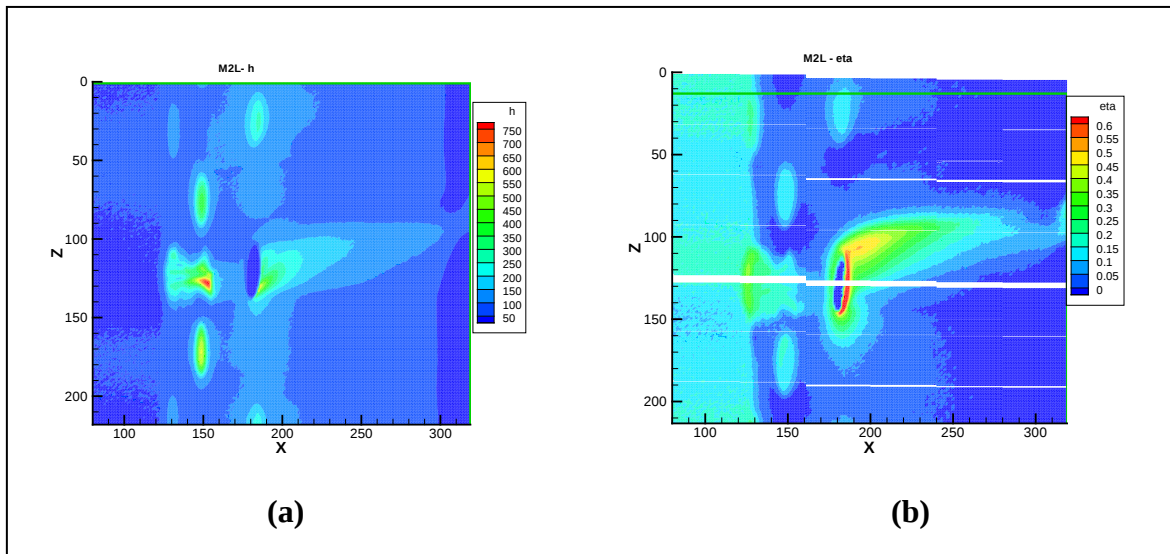


Figure 2: Pulsed Cooling Flow Reduced Data
(a). Heat transfer coefficient (h) distribution. (b) Cooling effectiveness (η) distribution.

Reduction of the duty cycle of the pulsing (ratio of the flow on time to the total cycle time), at a given pulse rate, reduces the mean coolant mass flow. Current measurements have shown that the duty cycle can be reduced to 25% (flow on only one quarter of the time) without losing cooling effectiveness. The ability to reduce film cooling flow directly translates into a proportional increase in turbine engine thrust. For more details see list of publications.

2.2. Turbulence Model Development:

The primary focus of this task was to obtain detailed experimental measurements of the aerothermodynamics of turbine related flows under highly unsteady conditions for use by researchers outside of the organization to develop models. There was some successful model development under this task however. Edward Michaels, while working on his Doctoral Dissertation, developed a very accurate two-scale turbulence model for the prediction of heat transfer and skin friction under high freestream turbulence conditions. He was able to predict these parameters to within 2%, an accuracy not provided by any other current models. Outside organizations have picked up this model and are working on extending and applying it.

2.3. Aerodynamic Flow Control

The aerodynamic loading and efficiency of the turbine components play a large role in the overall efficiency and power output of the the gas turbine engine. The low pressure turbine presents significant opportunities for improvements in this regard. A typical commercial aircraft turbine engine or ground power unit can have anywhere between five and twelve low pressure turbine stages. Low bypass engines used in high performance military engines will typically have two to four stages. Increasing blade loading allows for significant reduction in part count, and has the potential to allow the removal of whole stages of the low pressure turbine module, which translates into significant weight, performance, and cost savings.

The primary obstacle to increasing loading is maintaining efficiency. For the low pressure turbine a major cause of loss of efficiency is flow separation on the rear of the turbine airfoil, where there is a strong adverse pressure gradient.. Controlling this separation requires reenergizing the boundary layer flow in order to make it more separation resistant. There are many techniques for accomplishing this, but they can be separated into two broad categories: active techniques, which rely an the application of external energy; and passive techniques, which rely on making fixed surface or profile modifications to the airfoil in order to influence the boundary layer. Both passive and active separation control techniques were studied under this work unit, in cooperation with work performed under work units 2302NP01 and 2307NP01.

2.3.1. Passive Boundary Layer Control

Passive separation control techniques studied include suction side v-grooves, slots, trips, turbulators, and spherical and asymmetric dimples. Of the passive techniques studied, the dimples proved to be the most effective at flow separation while cause a minimum of adverse affects on the airfoil loss characteristics. Figures 3a and 3b show a computation of the flow over a single row and a double row of spherical dimples respectively. The effect of the dimples is to generate a streamwise vortex pair in the boundary layer near the wall. This vortex pair serves to pump high energy fluid from outside the boundary layer down into the boundary layer near the wall, energizing the boundary layer. It also serves to trip a laminary boundary layer, speeding transition to turbulence, which again increases the boundary layer's resistance to separation.

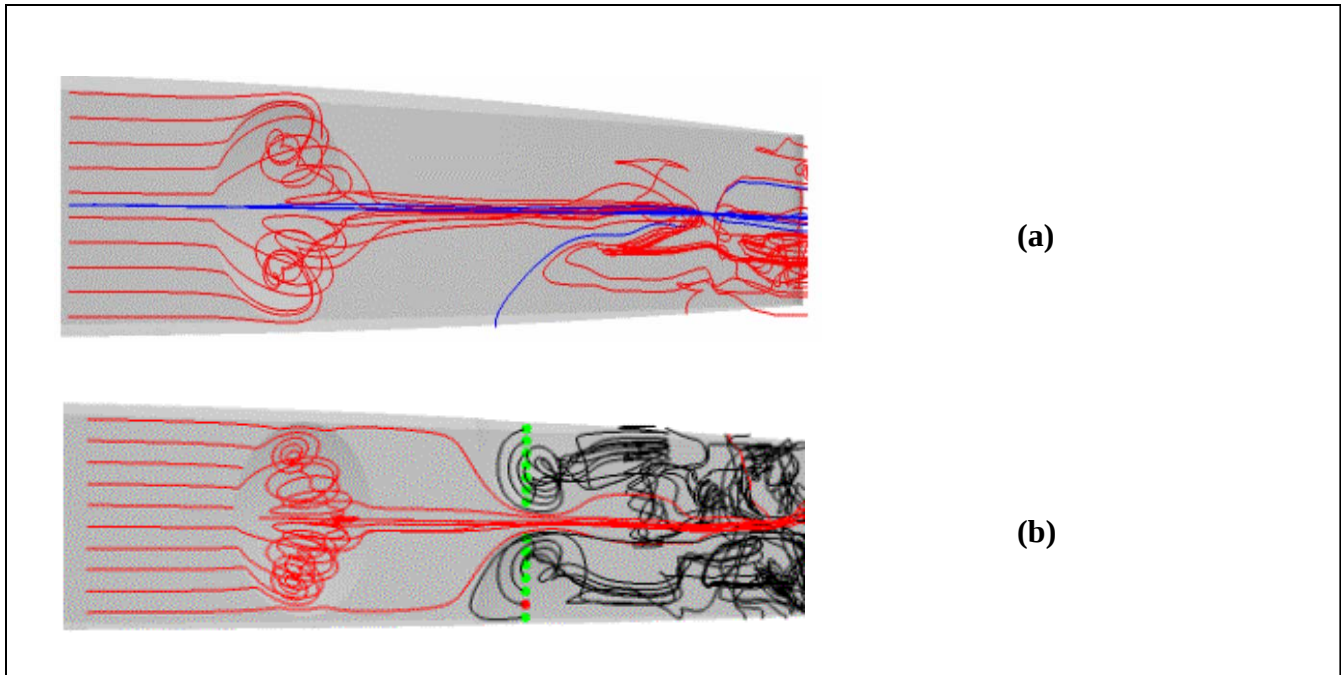


Figure 3: Computed Flow Over Spherical Dimples
Suction side of a low pressure turbine airfoil with spanwise periodic boundary conditions. (a) Single row of dimples. (b) Double row of dimples.

2.3.2. Active Boundary Layer Control: Vortex Generator Jets

A number of active boundary layer control actuators were considered for study, including Helmholtz resonators, micro-electro-mechanical devices (MEMS), thermal actuators, plasma actuators, and Vortex Generator Jets (VGJs). The last, VGJs, were chosen to be the focus of study because of their proven effectiveness in external flows, and because of their physical similarity to the film cooling technologies already found in gas turbine engines. More recent work has examined the use of plasmas for forcing. That work will be discussed in the next section.

Vortex Generator Jets are small jets that are injected through the airfoil surface into the boundary layer. VGJs are typically configured with a low pitch angle (30-45 degrees) and aggressive skew angle (45-90 degrees) to the local freestream flow direction. Here pitch angle is defined as the angle the jet makes with the local surface and skew angle is defined as the angle of the projection of the jet onto the surface relative to the local freestream direction. In this skew configuration, the VGJ creates a horseshoe vortex pair with one very strong leg accompanied by a weak leg of opposite sign. The result is a single, dominant, slowly-decaying streamwise vortex downstream rather than the two weaker counter-rotating horseshoe vortices generated by a jet with 0 degrees skew or a symmetric passive boundary-layer obstruction. It has been shown that this single-sign vortex energizes the separating boundary-layer by effectively bringing high momentum freestream fluid down to the wall.

Figure 4 shows the effect of VGJ blowing on the pressure loss through low pressure turbine cascade at low Reynolds number. The blowing ratio is the ratio of the momentum flux per unit

area exiting the VGJ to the momentum flux per unit area of mid-channel flow outside the hole. At a blowing ratio of 0 (no flow through the VGJs) the flow over the LPT is separated and the loss coefficient (a normalized measure of the energy lost going through the cascade) is large. Once the blowing ratio is increased above a certain critical value, here approximately $B=1.0$ for steady blowing, the flow separation is greatly reduced and the loss is cut by approximately 60%.

Also shown on Figure 4 are the results for pulsed VGJs. Here the jet flow is turned on periodically for only a fraction of the total cycle time. The effect is to greatly reduce the required mass flow from the VGJs. As can be seen in Figure 4, a pulsed VGJ with an effective average blowing ratio of $B=0.02$ still effectively suppresses the separation and drives the losses down by 60%. Detailed results from these experiments are available in publications listed in appendix A.

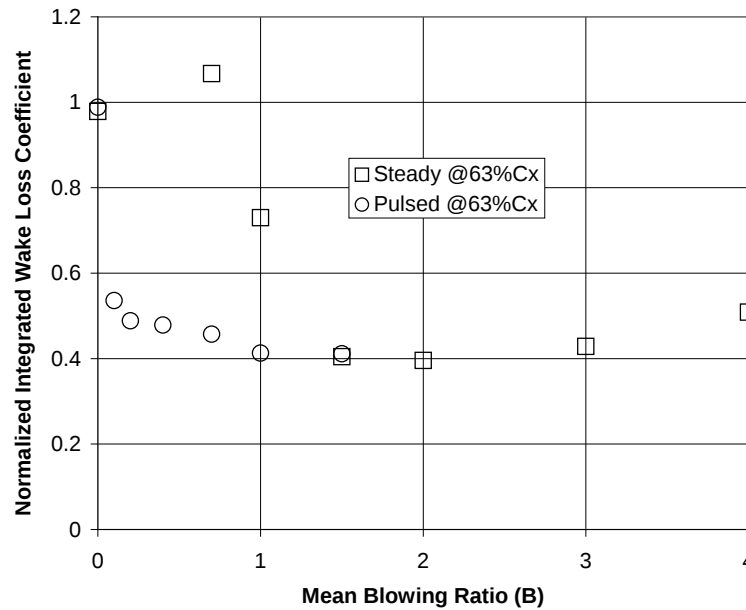


Figure 4: Effect of Vortex Generator Jet (VGJ) Blowing on Loss
Low pressure turbine blade pressure loss coefficient, steady and unsteady VGJ flow.

2.3.3. Active Boundary Layer Control: Atmospheric Plasmas:

Work on flow control using plasma discharges has recently begun and has demonstrated a significant ability to modify the velocity profiles near the wall. Multi-kilohertz double pulsed lasers and cameras have been acquired and used to obtain velocity measurements that resolve the non steady flows occurring in the high frequency pulsed plasma applications.

The control of the voltage current characteristics for atmospheric glow discharges for control of subsonic flows has been investigated for high frequency AC and pulsed DC sources of excitation. Uniform atmospheric AC glow discharges were obtained from 1 kHz to 10 kHz for various electrode lengths of ~26 cm, 56 cm and 78 cm. Uniform Pulsed DC glow discharges were obtained with pulse widths from 22 nanoseconds to 2 micro seconds at a pulse rate of 100 pulses/second, for electrode lengths of ~ 26 cm, 56 cm and 78 cm. Calculated pulsed discharge

peak power levels exceed 20-50KW. The discharge impedance was inductively and frequency matched for high frequency AC excitation and resistively matched for the pulsed DC case. The glow discharge with various electrode configurations has been installed in the 2D boundary layer tunnel and boundary layer and PIV measurements initiated. Figure 5 shows PIV boundary layer profiles with and without plasma at low freestream velocities with an augmentation of the wall velocity to ~ 3.3 m/s. Boundary layer traverses with freestream velocities of 2.5, 4, 5.8, 18.5m/s, indicate a decreasing % augmentation of the wall $\delta P/P$. The PIV laser and camera were upgraded to provide kHz double pulse capability for resolution of the plasma discharges and the pulsed vortex generator jets. Shown below are the u and v velocity profiles averaged correlations from hundreds of PIV individual images with plasma on (dashed) plasma off (solid). The v component shows a very large component just downstream of the electrodes. The capability to extend these averages to several thousand frames and perform phase locked PIV with discharge voltages / currents can now be accomplished.

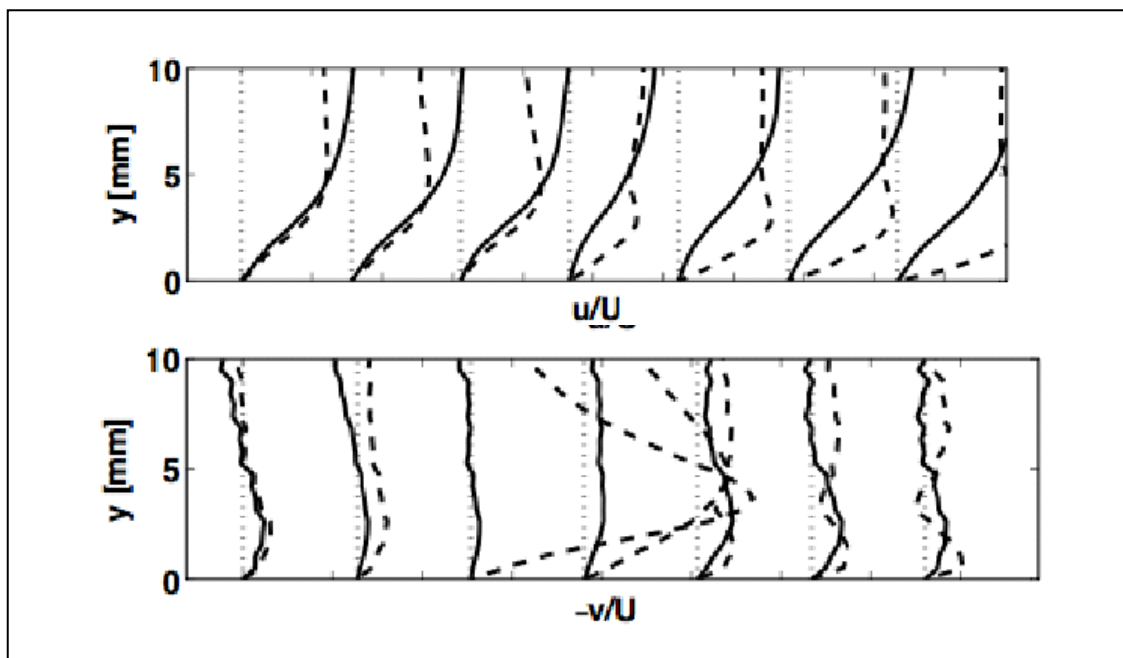


Figure 5: Boundary Layer Velocity Profiles
Profiles of u (streamwise) and v (wall normal) boundary layer velocity without (solid) and with (dashed) plasma discharge forcing, $U_{\infty} = 1.0$ m/s

2.4. Engine LPT application

The Low Reynolds number low pressure Turbine work is progressing to investigation of application of Dimples to the low pressure turbine of an existing turbine engine, to correct for losses incurred at altitude. Three sets of scaled up cascade blades were fabricated: first vane, first rotor, and third rotor, Figure 6. In 2005 and 2006 these were run in back to back tests without and with dimples in the linear cascade to determine the relative importance of individual stage losses

In addition, dimples have been machined on two high pressure turbine first vanes, Figure 5. Pressure transducers for the Turbine Research Facility's (TRF) rakes were upgraded for the Reynolds number range of interest. Initial tests TRF tests were run in 2004 and 2005 at nine Reynolds numbers with a rainbow array of HPT vanes. The array included 3 dimpled vanes, two rough vanes, and six clean vanes. A high Reynolds number TRF wake traverse of the rainbow array is illustrated in Figure 8.



Figure 6: Engine LPT Cascade Blades

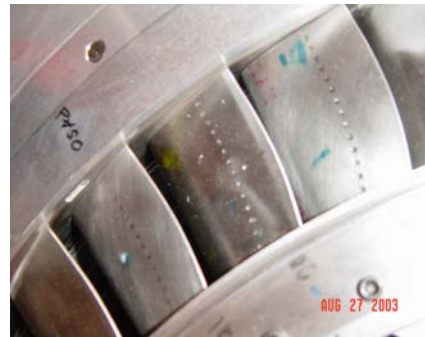


Figure 7: Dimpled HPT Vanes for TRF

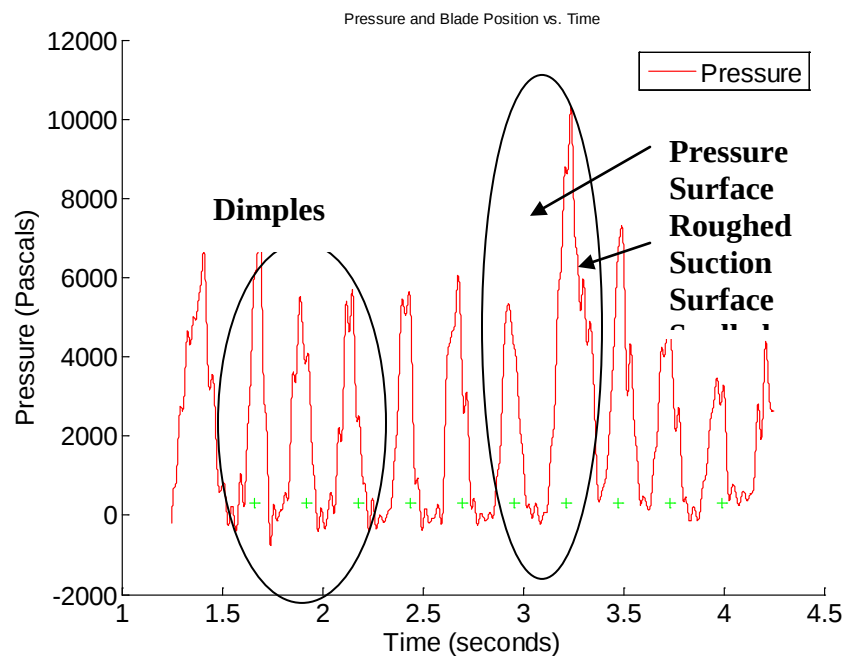


Figure 8: TRF Wake Traverse of Dimples on Roughened Vanes
 $Re = 272,500$

The TRF will be used to evaluate full scale engine LPT hardware. A non-flight worthy three stage LPT for the existing engine has been obtained and has been inspected and refurbished for a back to back test without and with Dimples. Funding for modification of TRF and the required instrumentation has been obtained and construction is continuing.

3.0 CONCLUSIONS

This project has provided a broad ranging contribution to a variety of technologies related to gas turbine engines. The results have substantially added to the understanding of high heat transfer in the presence of very high unsteadiness, as well as film cooling effectiveness in similar environments. Research performed under this project has also added to the understanding of high lift turbine aerodynamics and the mitigation and control of losses associated with both high lift and low Reynolds number turbine operations.

APPENDIX: LIST OF PUBLICATIONS

"Pulsed Film Cooling on a Turbine Blade Leading Edge," Captain James L. Rutledge, PhD Dissertation, AFIT/DS/ENY/09-S03, September 2009.

"An Experimental Investigation Studying the Influence of Dimples on a Film Cooled Turbine Blade Leading Edge," Captain Paul G. Frisinger, Master's Thesis, AFIT/GAY/ENY/09-M10 March 2009.

"Experimental Flow Visualization of Pulsed Film Cooling on a Turbine Blade Leading Edge," Rutledge, King & Rivir, AIAA-2009-5104, Proceedings of the 45th IAA/ASME/SAE/ASEE Joint Propulsion Conference & Exhibit, 2 - 5 August 2009, Denver, Colorado.

"Net Heat Flux Reduction for Pulsed Film Cooling on a Turbine Blade Leading Edge," Rutledge, King & Rivir, AIAA-2009-5103, Proceedings of the 45th AIAA/ASME/SAE/ASEE Joint Propulsion Conference & Exhibit, 2 - 5 August 2009, Denver, Colorado.

"Pulsed Film Cooling Performance on a Turbine Blade Leading Edge" Rutledge, King & Rivir, The 34th Dayton-Cincinnati AIAA Aerospace Sciences Symposium, 3 March 2009.

"Influence of Dimples on Film Cooling Performance on Turbine Blade Leading Edge", Frisinger, The 34th Dayton-Cincinnati AIAA Aerospace Sciences Symposium, 3 March 2009.

"CFD Predictions of High Frequency Pulsed Film Cooling Heat Flux on a Turbine Blade Leading Edge", Rutledge, King & Rivir, Proceedings of AIAA Aerospace sciences Meeting , Jan 5-8 2009, Orlando, Florida.

"CFD Predictions of Pulsed Film Cooling Heat Flux on a Turbine Blade Leading Edge", Rutledge, King & Rivir, ASME IMECE 2008-67276.

"Turbine Blade Surface Deterioration by Erosion," Hamed, Tabakoff, Arora, & Rivir, *ASME Journal of Turbomachinery*, Vol. 127 No 3, July 2005, pp 445-452.

"Control of Laminar and Turbulent Shear Flows Using Plasma Actuators," Jacob, Ramakumar, Anthony, and Rivir, Fourth International Symposium on Turbulence and Shear Flow Phenomena, Williamsburg, Virginia, June 27, 2005.

"Innovative Technique to Obtain Heat Transfer Coefficient and Film Effectiveness," Ou, Rivir, and Brown, *Air Force Research Laboratory Technology Horizons*, Vol. 8, No. 2, April 2005.

"Boundary Layer Control Using Plasma Induced Velocity," 2nd Lt Brian E. Balcer, AFIT Thesis, AFIT/GAE/ENY/05-M03, March 2005.

“Effects of Strong Irregular Roughness on the Turbulent Boundary Layer to Flow,” Subramanian, King, Reeder, Ou and Rivir, *Flow, Turbulence and Combustion Journal*, Vol. 72: 2004, pp 349-368.

“The Effect of Jet Pulsation and Duty Cycle on Film Cooling from a Single Jet on a Leading Edge Model,” Ekkad, Ou and Rivir, IMECE2004 -60466, International Mechanical Engineering Congress & Exposition 2004, Anaheim CA, Nov 2004, also recommended for Journal.

“Time Resolved PIV Measurements of a Plasma Actuator Discharge in Boundary Layer Flow Control,” Jacob and Rivir, 57th Annual Fluid Dynamics Meeting of the American Physical Society, Seattle, Washington, November 2004.

LIST OF ACRONYMS

<u>Acronym</u>	<u>Description</u>
IHPTET	Improved High Performance Turbine Engine Technology
TRF	Turbine Research Facility
VAATE	Versatile Affordable Adaptive Turbine Engines
VGJ	Vortex Generator Jet