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14. ABSTRACT We proposed an approach to construct spatially varying and switchable metamaterials that are based on colloidal dispersions of metal nano-rods (NRs) in dielectric fluids, in which dielectrophoretic forces, originating in the electric field gradients, create spatially varying configurations of aligned NRs. The electric field controls orientation and concentration of NRs and thus modulates the optical properties of the medium. Using gold (Au) NRs dispersed in toluene, we demonstrated electrically induced change in refractive index on the order of 0.1. By exploring local light absorption and birefringence, and by developing a model of light propagation in a medium with spatially varying composition, we determined the concentration of NRs and field-induced changes in the refractive indices as the function of spatial coordinates in a nonuniform electric field. We demonstrated that the electric-field induced condensation and alignment of gold NRs near the central region of a cylindrical shell causes bending of light rays around the region enclosed by the shell and to the mitigation of the shadow of the central electrode (nonideal cloaking effect). We also describe liquid crystal metamaterials (LCMMs), representing a composite of a liquid crystal (rather than an isotropic fluid) as a dispersion medium						
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ELECTRICALLY CONTROLLED OPTICAL METAMATERIALS BASED ON DISPERSIONS OF NANO-RODS

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Abstract: In modern transformation optics, one explores metamaterials with properties that vary from point to point in space and time, suitable for application in devices such as an “optical invisibility cloak” and an “optical black hole”.

We proposed an approach to construct spatially varying and switchable metamaterials that are based on colloidal dispersions of metal nano-rods (NRs) in dielectric fluids, in which dielectrophoretic forces, originating in the electric field gradients, create spatially varying configurations of aligned NRs. The electric field controls orientation and concentration of NRs and thus modulates the optical properties of the medium. Using gold (Au) NRs dispersed in toluene, we demonstrated electrically induced change in refractive index on the order of 0.1. By exploring local light absorption and birefringence, and by developing a model of light propagation in a medium with spatially varying composition, we determined the concentration of NRs and field-induced changes in the refractive indices as the function of spatial coordinates in a nonuniform electric field. We demonstrated that the electric-field induced condensation and alignment of gold NRs near the central region of a cylindrical shell causes bending of light rays around the region enclosed by the shell and to the mitigation of the shadow of the central electrode (nonideal cloaking effect). We also describe liquid crystal metamaterials (LCMMs), representing a composite of a liquid crystal (rather than an isotropic fluid) as a dispersion medium and solid (metal) NRs as a dispersed component. The purpose of the metal component is to vary the effective refractive indices and the resulting birefringence. By spatially distorting the optic axis of LCMMs and by controlling concentration of the metallic component, one can design different trajectories of light propagation through the medium as illustrated analytically and numerically for cylindrical samples of LCMMs. Depending on the refractive indices and configuration of the optic axis in LCMM, the light beam can be concentrated thus offering an approach for the solar energy storage, or bent around the obstacle.

1. Introduction

Optical metamaterials represent artificial composites with building blocks of a metal and dielectric nature, intertwined at a sub-wavelength scale. When properly arranged, these building units lead to fascinating optical effects, such as negative refraction and sub-wavelength imaging. Optical metamaterials in which the electric permittivity and magnetic permeability vary in space, and can be switchable, are of special interest. The reason is simple: by controlling the spatial variation of permittivity and permeability, one controls the local refractive index and thus the pathway of light in the medium. According to the Fermat's principle of least time, a light ray propagating from a point A to a point B follows a path that minimizes the travel time. For a small path element, the quantity to minimize is simply a product of the geometrical path length and the refractive index. Thus the spatially varying refractive index can make the light rays follow curved trajectories. If these trajectories are designed to avoid a certain region of the medium, one obtains an invisibility cloak, as any object placed within this region would not interact with light [1,2]. Potential applications of metamaterials with spatially varying properties are much wider than cloaking and extend from perfect magnifying lenses with sub-wavelength resolution [3] to optical "black hole" collectors [4,5], as reviewed recently by Wegener and Linden [6]. To find the pathway of light, theoretically, one uses the equivalence of coordinate transformations and renormalization of permittivity and permeability; this is why the field of study is called the "transformation optics" [1,2,7-9].

The fact that light rays follow curved trajectories in a medium with a varying refractive index has been known for a very long time in the physics of liquid crystals. In the simplest liquid crystal, the so-called uniaxial nematic, rod-like molecules align parallel to each other, along the common "director" $\hat{n}$. The director is a unit vector with a property $\hat{n} = -\hat{n}$ (the medium is non-polar); it is also a local optic axis. The associated birefringence $\Delta n = n_e - n_o$ of a typical nematic formed by low-molecular-weight organic molecules is significant: the ordinary refractive index n_o is often about 1.5, while the extraordinary index n_e is about 1.7. In liquid crystals, the local orientation of molecules and thus the local optic axis can be made varying in space and time, for example, by setting proper surface alignment at the boundaries and applying an electric field to realign $\hat{n}$ (a phenomenon at the heart of modern liquid crystal displays). The early liquid crystalline example for transformation optics has been presented by Grandjean in 1919 [10]. Grandjean considered a cylindrical nematic sample in which the director was arranged radially. When such a structure is illuminated with light polarized normally to the axis of cylinder, the rays are bent away from the central axis and leave a segment of an opening angle $2\pi(1 - n_o/n_e)$ un-illuminated [10]. This particular example represents, loosely speaking, half a cloak, as the trajectories are diverging. The limitation of a regular liquid crystal is that although the ellipsoid of refractive indices is changing its orientation in space, it cannot be shrunk or expanded at will [10,11].

In a metamaterial, the refractive index (or indices) can be made to change from point to point. An excellent example is the optical cloak proposed by the Shalaev's group [12]. A cylindrical shell of a (rigid) dielectric is penetrated with radial metal nano-wires. The metal filling factor increases as one moves from the outer to the inner surface of shell. The optic axis configuration is identical to the Grandjean's model, but in the metamaterial, n_e changes with the radial coordinate, down to zero at the

inner surface, while in the Grandjean's liquid crystal, $n_e = \text{const}$. The light trajectories in the cloaking shell first diverge and then converge, to restore a flat front as they pass around the shell [12]. By properly adjusting the radial variation of the refractive index, one can greatly reduce the visibility of an object enclosed by the shell [12]. Such a proper adjustment requires one to distribute small (sub-wavelength) elements in an essentially gradient manner, which represents a major technological difficulty [13-21]. Nowadays, metamaterials are fabricated by electron beam lithography, focused ion-beam milling [13], deposition of alternating metal and dielectric layers [16], or by growing metallic wires from

within a dielectric medium [17]. These metamaterial structures should be more properly called "metasurfaces" or "metafilms" as their functionality is determined by only one or a few layers normal to the direction of propagating light [6]. For complex architectures, involving property variations along the three spatial dimensions and switching, new approaches are needed. Among the potential candidates are bottom-up self-assembly [18], alignment of NRs by a uniform electric field [19] or assembly through a non-uniform electric field [20].

Recently, we proposed that the next wave of metamaterials with spatially varying and even switchable optical properties can be based on dispersions of small (sub-wavelength) metal nanorods (NRs) in a dielectric fluid, controlled by a nonuniform ac electric field [22]. The gradients of the electric field pull the highly polarizable NRs towards the strongest field and also align them along the field lines. The reason is that the field-induced dipole polarization experiences different pulling force at the two ends of the NRs when the field is non-uniform. The effect is known as dielectrophoresis [20]. If the electric field is radial, for example, created by two concentric cylindrical electrodes, then the NRs align radially and condense near the inner electrode [22]. The structure is similar to the cylindrical cloak proposed in [12], with the difference that the location and orientation of NRs is determined by the dielectrophoretic forces and interactions between the NRs rather than by mechanical means. We used NRs that are much smaller than the wavelength of light, of a length of about 40-70 nm, to reduce light scattering. Previously, dielectrophoretic manipulation has been demonstrated for much larger supra-micron metal wires [23-29], but the viability of downscaling is not obvious as the dielectrophoretic force acting on the particle is proportional to its volume [20] and might be too small at nanoscales. Similarly small NRs were previously studied under the action of a uniform electric field that can impose an orienting torque on the NRs [19, 30-32]. Cook et al [33] used a strong gradient dc electric field to harvest ferroelectric nanoparticles; this effect of a "permanent dipole dielectrophoresis" is different from the "induced dipole dielectrophoresis" in the ac field discussed by us. We expand the scope of the original experiments [22], present new data for different dispersions of NRs and analyze the field-induced pattern analytically and numerically, in order to obtain information about the dielectrophoretic forces acting on NRs, field-induced spatial distribution of NRs, field-modified refractive indices and coefficients of absorption.

The dielectrophoretically controlled metamaterial is discussed in the first part of the report, pages 2-26; the second part, pages 26-47, describes a liquid crystal metamaterial, for which we performed numerical and analytical simulations demonstrating the ability to control light trajectories with the distorted optical axis.

2. Experimental Materials and Methods

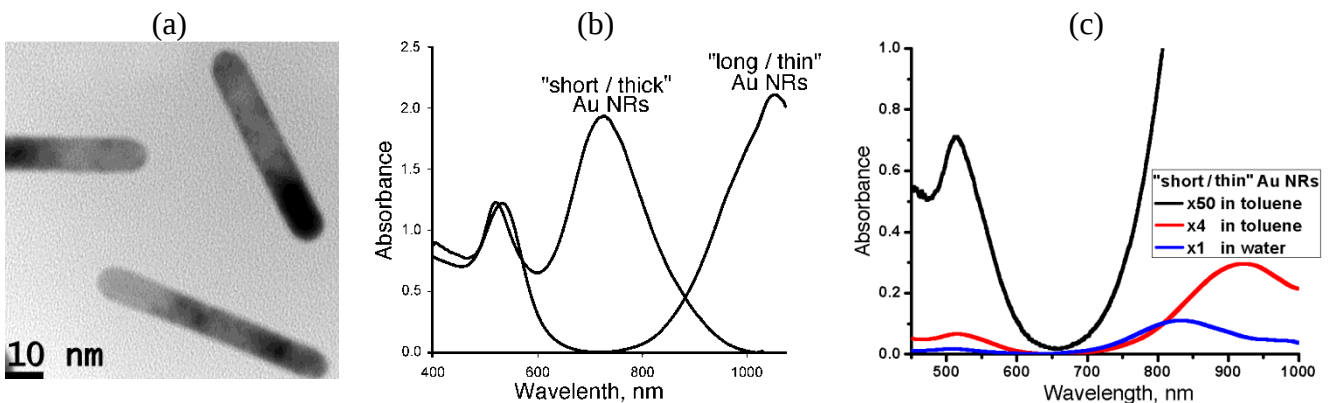
2.1. Dispersions of NRs in Toluene

We used dispersions of gold (Au) NRs in dielectric fluids, such as toluene and water. Au NRs can be grown by the so-called seed mediated process in water solutions of a cationic surfactant cetyltrimethylammonium bromide ($\text{C}_{16}\text{H}_{33}\text{N}(\text{CH}_3)_3\text{Br}$, abbreviated as CTAB). CTAB forms a charged bilayer around the NRs, preventing them from aggregation. When Au NRs reach the desirable length l_{NR} and diameter d_{NR} , the NR dispersion is centrifuged and redispersed in deionized water. We also used water dispersions of Au NRs commercially available from Nanopartz, Inc.

For optical experiments with NR dispersions in glass containers, it is convenient to match the refractive index of the dispersive medium with the refractive index of glass. We use toluene with $n_t = 1.497$ measured at $\lambda = 589.3$ nm and 293 K; n_t is close to the refractive index of borosilicate glass. To transfer Au NRs from water into toluene, we followed the approach developed by N. Kotov and P. Palfy-Muhoray groups, in which the Au NRs are functionalized with thiol terminated polystyrene [30,34]. A 2 wt% solution of thiol terminated polystyrene (molecular weight 53,000, purchased from Polymer Source, Inc) in tetrahydrofuran is added by rapid stirring to the water dispersion of CTAB-stabilized Au NRs. The mixture is incubated overnight for hydrophobization-induced precipitation of NRs. The rods are collected after supernatant removal, by re-dissolution in toluene. The volume fraction of Au NRs in toluene was increased by centrifuging to $\eta_o \approx (4 - 8) \cdot 10^{-4}$. The typical volume fraction of Au NRs in water dispersions produced by Nanopartz, Inc. was $\eta_{\text{water}} = 7.4 \cdot 10^{-6}$.

To facilitate the study of spatial structure and optical properties, we use three types of dispersions: (1) “long/thin” NRs in toluene, with an average length $l_{\text{NR}} = 70$ nm and diameter $d_{\text{NR}} = 12$ nm, showing a longitudinal plasmonic absorption peak at $\lambda \approx 1040$ nm; (2) “short/thick” NRs in toluene, with $l_{\text{NR}} = 50$ nm, $d_{\text{NR}} = 20$ nm, and the absorption maximum at 725 nm; (3) “short/thin” NRs in water and toluene with $l_{\text{NR}} = 45$ nm, $d_{\text{NR}} = 10$ nm. The spectral properties of dispersions strongly depend on the dispersive medium and NRs geometry, in particular, on the aspect ratio $l_{\text{NR}}/d_{\text{NR}}$, Figure 1(b,c).

Figure 1. Transmission electron microscope image of “long/thin” Au NRs (a), absorption spectra of toluene dispersions of “long/thin” and “short/thick” Au NRs (b), and water dispersion of “short/thin” Au NRs at volume fraction η_{water} (blue line), as well as toluene dispersions with volume fractions $4\eta_{\text{water}}$ (red line) and $50\eta_{\text{water}}$ (black line) (c).

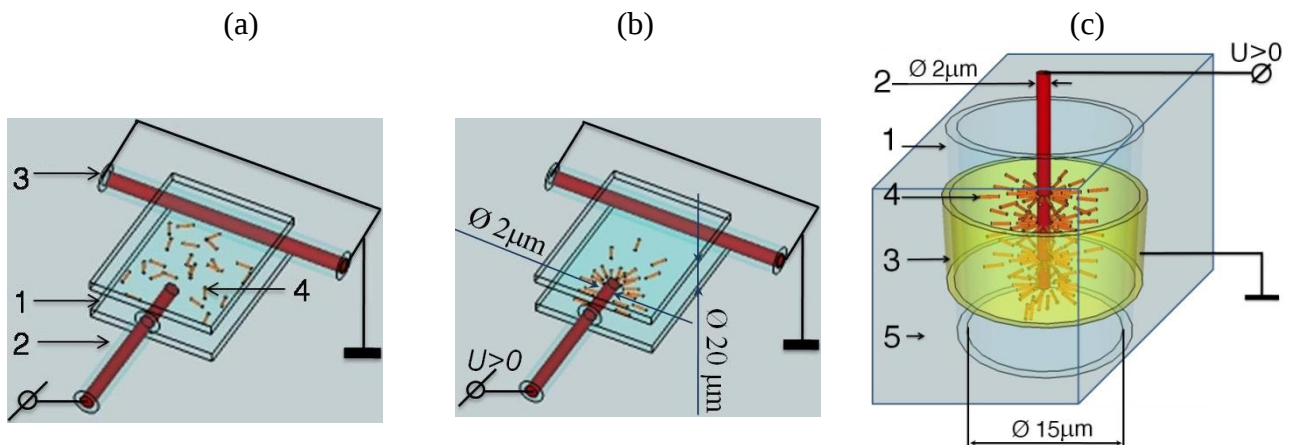


The “short/thick” NRs are suitable to explore spatial distribution and orientation of NRs by monitoring absorption near 725 nm, while the “long/thin” NRs are better suited to observe the cloaking effect. The results were similar for water and toluene dispersions. However, since the refractive index of water does not match that of glass capillaries confining the dispersions, we describe only the toluene case.

2.2. Two Types of Samples: Flat and Cylindrical Cells

We study two different geometries, flat cells and cylindrical cells. (1) The flat cells are formed between two glass plates, with two mutually perpendicular electrodes in the plane of the cell, Figure 2 (a,b). One (grounded) electrode is a copper wire, of diameter $2\ \mu\text{m}$, in a borosilicate glass shell, of diameter $20\ \mu\text{m}$, that determines the separation between the glass plates. The second electrode is a similar wire (with the glass shell stripped near the tip) connected to a waveform generator. The cell is filled with the toluene dispersion of Au NRs and sealed. The gradient electric field $\mathbf{E}_e$ in the crossed geometry of electrodes in the flat cell mimics the radial gradient in the cylindrical sample, Figure 2 (c). (2) The cylindrical sample represents a circular capillary. The electric field $\mathbf{E}_e$ is created by coaxial electrodes; one is a bare copper wire of diameter $2\ \mu\text{m}$ running along the axis and the second one is a transparent layer of indium tin oxide (ITO) deposited at the outer surface of the capillary. The space between the inner surface of glass capillary and the central electrode is filled with the dispersion of NRs that represents our electrically controlled metamaterial shell. The central electrode (2) plays a dual role, setting up the gradient electric field and also serving as the object to be “cloaked” by the shell.

Figure 2. Samples used in the experiments: The flat (a,b) sample formed between two glass plates (1) with orthogonal copper wires (2) and (3), filled with Au NRs dispersed in toluene (4) that are isotropically distributed when the electric field is off (a) and form a condensed oriented structure when the field is on (b). The cylindrical sample (c) in a glass capillary (1) with coaxial electrodes (2) and (3); the cavity is filled with Au NRs dispersed in toluene (4) and sealed by a transparent optical adhesive (5).



2.3. Dielectrophoretic Force

The size of NRs is much smaller than the characteristic scale of the electric field gradients, thus the dielectrophoretic force F_{DEP} acting on a NR can be calculated in dipole approximation [20] $F_{DEP} = -\nabla W$, where the potential W is

$$W = -\frac{1}{2} Re[\alpha^*] V E_{e,rms}^2, \quad (1)$$

V is the volume of the NR, $E_{e,rms}$ is the root-mean-square (*rms*) value of the electric field, and $Re[\alpha^*]$ is the real part of the effective complex polarizability written for an elongated particle as [20]:

$$\alpha^* = \epsilon_t \cdot \frac{\epsilon_{NR}^* - \epsilon_t^*}{\epsilon_t^* + A_d(\epsilon_{NR}^* - \epsilon_t^*)}. \quad (2)$$

Here $\epsilon^* = \epsilon - i\sigma/\omega$ is the complex permittivity of NRs and the medium (subscripts “NR” and “t”, respectively), σ is the conductivity, $\omega = 2\pi f$, A_d is the depolarization factor that depends on the orientation of the NR with respect to the electric field. With $\epsilon_t = 2.4\epsilon_0$, $\epsilon_0 = 8.854 \times 10^{-12} \text{ C/(Vm)}$, $\epsilon_{NR} = -6.9\epsilon_0$, $\sigma_{NR} = 4.5 \times 10^7 \text{ S/m}$, $\sigma_t \sim 5 \times 10^{-11} \text{ S/m}$, $f = 10^5 \text{ Hz}$, one finds $|\epsilon_{NR}^*/\epsilon_t^*| \sim 10^{13}$ so that the expression for the real part of the effective complex polarizability simplifies to

$$\alpha^* = \frac{\epsilon_t}{A_d}. \quad (3)$$

Using the typical NR volume $V = \pi d_{NR}^2 L_{NR}/4 \sim 2 \times 10^{-23} \text{ m}^3$, applied field $E_e \sim 10^7 \text{ V/m}$, and the scale of gradient $l \sim 10 \mu\text{m}$, one estimates the dielectrophoretic force acting on an isolated NR of a modest aspect ratio yielding a depolarization factor $A_d = 0.2$, as $F_{DEP} \sim 10 \text{ fN}$. The corresponding potential $W \sim F_{DEP} l \sim 10^{-19} \text{ J} \sim 10 k_B T$ (T is the room temperature) is high enough to overcome the Brownian randomization and to accumulate the NRs in the regions of maximum field. This estimate also suggests that the major axes of NRs (corresponding to the smallest depolarization factor A_d) orient along the field and that the medium becomes structurally and optically similar to a uniaxial nematic liquid crystals, with NRs being the building units.

The depolarization factor for the major axis of a NR can be calculated by using a model of prolate spheroid with axes $a_1 > a_2 = a_3$ and eccentricity $g = \sqrt{1 - a_3^2/a_1^2}$, see, e.g., [31]:

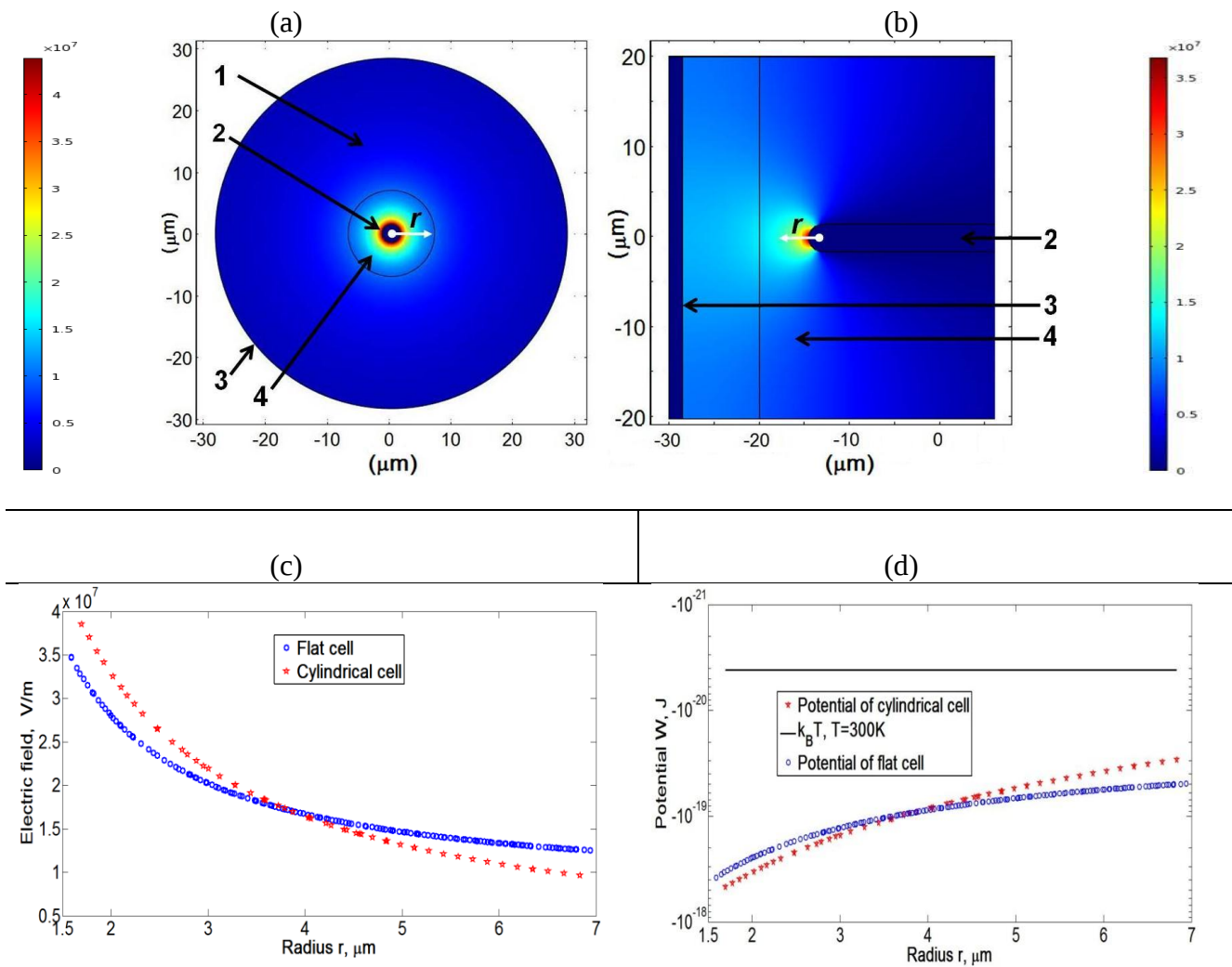
$$A_{d1} = \frac{1-g^2}{2g^3} \left(\ln \frac{1+g}{1-g} - 2g \right). \quad (4)$$

For a spheroid with the aspect ratio $a_1/a_3 = 4$, one finds $A_{d1} = 0.075$. Numerical simulations show that the difference in the depolarization factors calculated for cylinders and spheroids of the same aspect ratio is small, less than 5% [31,32].

We use a commercial Finite Element Package of COMSOL Multiphysics with AC/DC module, version 4.0a, to simulate the electric field patterns and dielectrophoretic potentials, Equations (1,3,4), in the flat and cylindrical cells, for $l_{NR}/d_{NR} = 4.5$, Figure 3. The geometry (diameter of electrodes, distance between them) and material properties chosen for simulations are close to the experimental parameters. Numerical simulations show that the dielectrophoretic potentials W in the cylindrical and flat cells are similar to each other. The flat cells thus represent a convenient experimental model of the

cylindrical cell, mimicking the cross-section of the latter which is hard to visualize in real experiments. Note, however, that for the flat cell, the simulations are 2D and do not take into account field variations along the coordinate normal to the cell, which is an oversimplification of a real experimental situation.

Figure 3. Spatial map of the electric field in the cylindrical cell filled with pure toluene, under an applied voltage 200V; 1 is the glass capillary, 2 is the central electrodes running along the axis of the cylindrical cavity, 3 is the outer electrode, and 4 is toluene, filling the gap between the central electrode and the inner surface of the glass shell (a). The same for the flat cell; 2 is the “central” electrode connected to a waveform generator, 3 is the grounded electrode perpendicular to the electrode 2, and 4 is toluene (b). The electric field (c) and the dielectrophoretic potential (d) for two cells, as the function of a radial distance r measured from the axis of the cylindrical cell in (a) and from the center of the semispherical tip of central electrode in (b).



3. Experimental Results

The model [12] considers the optical cloaking effect achieved by a metal-dielectric shell of variable composition with the outer and inner diameters $D \approx 3.2d_o$ and $d_o \approx 2 \mu m$, respectively. To yield a monotonous decrease of the effective refractive index from 1 to 0 between them, the filling factor of metal wires should gradually increase as one moves towards the inner surface. In theory [12], the feat is achieved by using a solid dielectric with metal wires piercing it along the radial directions; the filling factor increases near the inner surface and the whole structure is kept together mechanically. In our approach, the dielectric is fluid rather than solid and the filling factor is nothing else but the spatially varying volume fraction $\eta(\mathbf{E}_e(\mathbf{r}))$ of NRs. A gradient electric field $\mathbf{E}_e(\mathbf{r})$ is applied to the dispersion of metal NRs in a dielectric fluid to create a dielectrophoretic force that condenses and aligns the NRs in a radial fashion. The resulting spatially varying $\eta(\mathbf{r})$ is determined by the dielectrophoretic coupling with the applied field and also by the forces that oppose it, such as the osmotic pressure, repulsive electrostatic and steric interactions of NRs. One of the important goals of this work is to establish the dependency $\eta(\mathbf{r})$ experimentally. It is expected that the volume fraction increases towards the maximum of the field, in our particular examples, towards the central electrode.

3.1. Flat Cells

At zero field, the NRs are distributed randomly, Figure 2(a), as their volume fraction in toluene dispersion is orders of magnitude lower than the one needed to form a nematic liquid crystal of the Onsager type (caused by steric repulsions). There is no preferred alignment, and the optical appearance of the cell does not depend on light polarization. When viewed between two crossed polarizers, the cell appears dark. When the AC field $\mathbf{E}_e$ (typical frequency 100 kHz) is applied, the Au NRs, being more polarizable than toluene, move into the regions of high electric field because of the dielectrophoretic effect [20], Figure 2(b). The flat cell design is convenient for the analysis of field-induced radial gradients of structural and optical properties of the dispersions.

Observations under a microscope with two parallel polarizers reveal that the field accumulates the Au NRs near the central electrode, Figure 4. We quantify the spatial distribution of NRs by measuring the intensity of light transmitted through the cell as a function of a spatial coordinate along the line OX, crossing the central electrode of the flat cell near the tip, Figure 4. The transmission is lower for light polarization parallel to OX than for light polarized perpendicular to it, Figure 4c, suggesting that the NRs are aligned perpendicularly to the central electrode's surface.

To characterize the concentration gradients of “short/thin” Au NRs, we measured the transmittance profiles of light polarized parallel to OX, as a function of the applied voltage, for the wavelength $\lambda = 460 \text{ nm}$, for which the dependence of absorption on the orientation of NRs was found to be relatively weak. Near the central electrode, light transmittance is reduced when the voltage is on, confirming accumulation of NRs, Figure 5(c). Since the absorption depends exponentially on the concentration of absorbing particles and the cell thickness, we determine the ratio $k_{NR}(x) = \eta_U(x)/\eta_O$ as the measure of how much the local field-induced filling factor $\eta_U(x)$ of Au NRs averaged along the cell thickness, is larger than the initial (field-free) filling factor η_O . We estimate $\eta_U(x)$ from the transmittance $\ln T_{\parallel}(x) \sim -\eta_U(x)d_c$, where $d_c = 20 \mu m$ is the cell thickness. This thickness is too

small to determine η_o accurately; thus we used transmittance data $A(\lambda) = -\log_{10}T$, shown in Figure 1(c) which we obtained for a thick cell $D_c = 500 \mu\text{m}$: $A(\lambda) \sim \eta_o D_c$. Figure 5(d) shows that for $\lambda = 460 \text{ nm}$, the ratio $k_{NR}(x) = -\ln T_{\parallel}(x) D_c / (A(460 \text{ nm}) \cdot d_c \cdot \ln 10)$ reaches the values of 55 and higher near the electrode (2), which corresponds to $\eta_U \sim 0.02$.

Figure 4. Voltage-condensed ($U = 200 \text{ V}_{rms}$, $f = 100 \text{ kHz}$) cloud of “short/thin” Au NRs in toluene, accumulated near the central electrode of a flat cell. The sample is viewed under a microscope between two parallel polarizers with the transmission direction $\mathbf{E}$ either perpendicular (a) or parallel (b) to the line OX crossing the central electrode, in the spectral region (550-700) nm of the CCD camera. Light transmission along the line OX for the two polarizations (c).

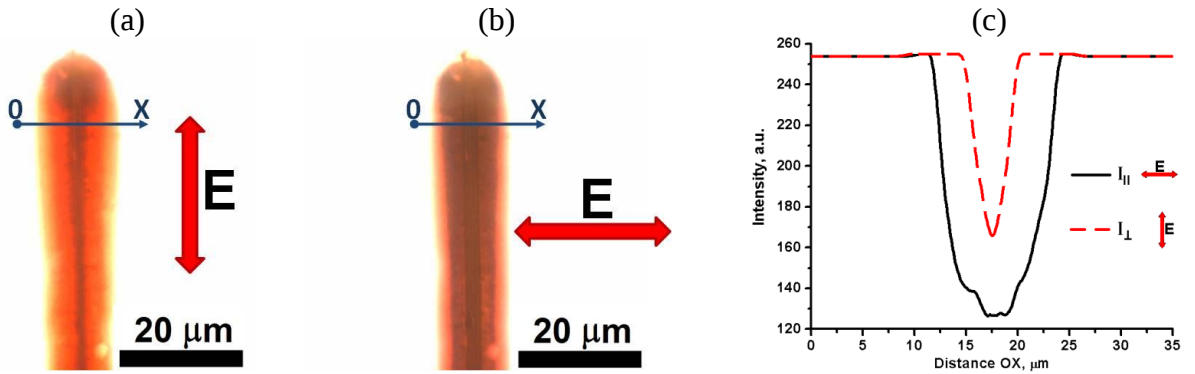
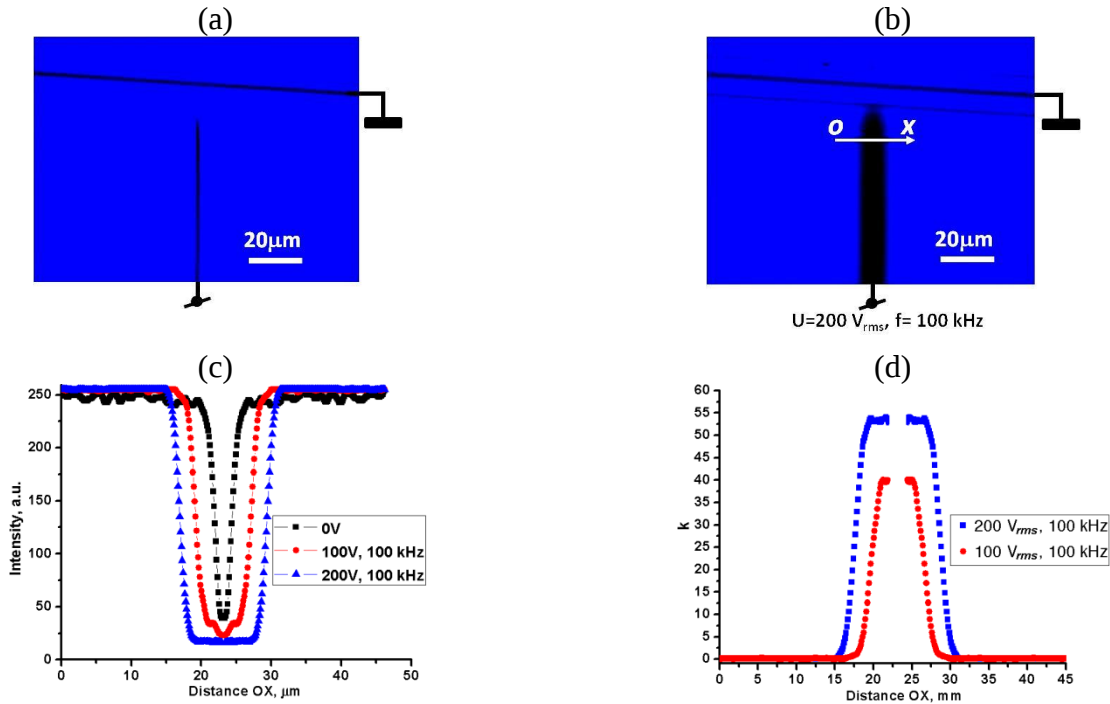


Figure 5. Optical microscope textures of the toluene dispersion of “short/ thin” Au NRs in the flat cell when the field $\mathbf{E}_e$ is off (a) and on (b); spatial profiles of transmitted light intensities (c) and local filling factors ratio $k_{NR}(x) = -\ln T_{\parallel}(x) D_c / (A(460 \text{ nm}) \cdot d_c \cdot \ln 10)$, measured in a monochromatic (460 nm) linearly polarized light (d).



3.2. Polarizing Microscopy of Toluene Dispersion of Au NRs in Flat Cells

Under the microscope with crossed polarizers, in absence of $\mathbf{E}_e$, the dispersion of NRs appears dark because it is structurally and optically isotropic. When the field is applied, the clouds of NRs assembled by the field gradients near the central electrode (2), show strong birefringence, which implies an orientational order of NRs, Figures 6,7. The sign of birefringence can be determined with the help of an optical compensator [10]. A waveplate ($\lambda = 530$ nm) inserted into the optical pathway of microscope, induces yellow (total retardation less than 530 nm) interference color in the regions where the long axes of NRs are parallel to the slow axis Z' of the waveplate, Figures 6(c,d) and 7(c,d). A blue interference color (retardation higher than 530 nm) is observed in the regions where the NRs are aligned perpendicularly to the slow axis. We conclude that the birefringence of Au NR clouds is negative, *i.e.*, the index of refraction for light polarized parallel to the long axes of Au NRs in dispersion is smaller than for the polarization perpendicular to them.

Figure 6. Polarizing microscope textures of the flat cell observed with crossed polarizers A and P. At zero electric field, the toluene dispersion of “short/thin” Au NRs is isotropic and the field of view is dark **(a)**. When the voltage is on ($U = 200$ V_{rms}, $f = 100$ kHz), a birefringent cloud of aligned Au NRs appears near the central electrode (2) **(b)**. When an optical compensator $Z'X'$, a 530 nm waveplate, is inserted between the sample and the analyzer, yellow and blue interference colors reveal that the field-induced birefringence is negative [**(c)** and **(d)**]. Note that reorientation of the sample by 90 degrees from (c) to (d) causes an interchange of the yellow and blue regions.

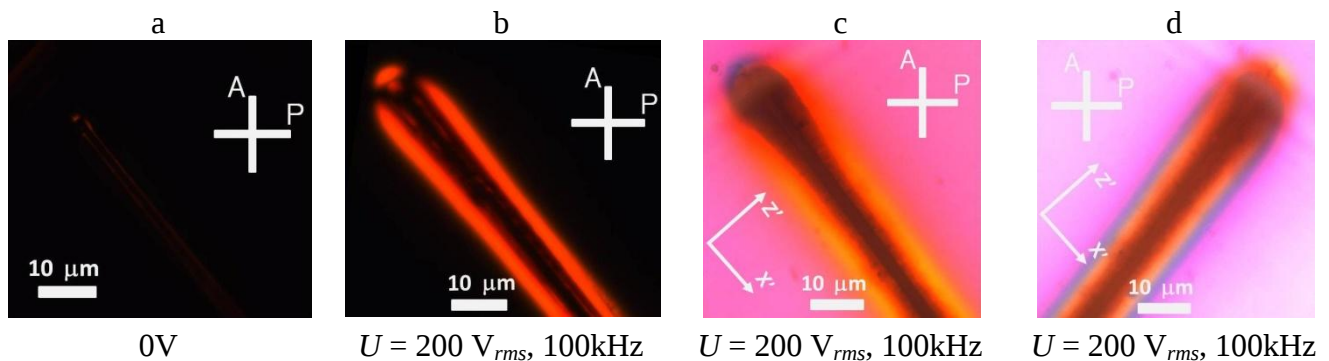


Figure 7. Polarizing microscope textures of the flat cell filled with “long/thin” Au NRs observed with crossed polarizers A and P [no field in **(a)** and with the field in **(b)**] and with an inserted waveplate [**(c)** and **(d)** with the field on, two different orientations of the sample showing the yellow and blue interference colors interchanged].

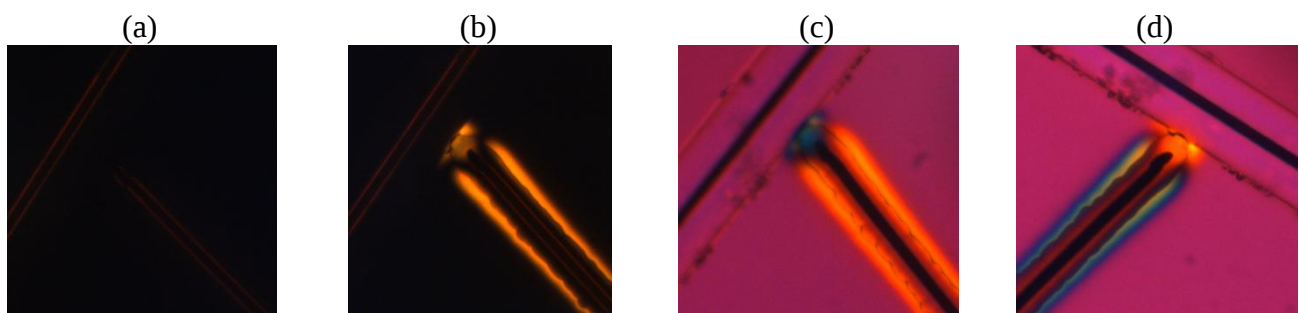


Figure 8 shows the flat cell textures for toluene dispersion of “short/thin” Au NRs viewed between *parallel* polarizers in monochromatic light ($\lambda = 656 \text{ nm}$). In zero field, the dispersion is isotropic. When the voltage is applied, the Au NRs accumulate around the central electrode (2). The texture depends on polarization $\mathbf{E}$ of the probing beam, Figure 8(b, c, d), confirming the optical anisotropy. We determined the spatial profiles of transmitted intensities $I_{\parallel}^{90}$, $I_{\parallel}^0$, and $I_{\parallel}^{45}$ along the line OX (Figure 8) that correspond to $\mathbf{E}$ making an angle 0, 45, and 90 degrees with the central electrode (2), respectively, Figure 9. In Section 4, we will use these profiles to determine the optical path difference between the ordinary and extraordinary waves and to reconstruct the spatial map of optical birefringence. For the same purpose, we determined the light transmission profile $I_{\perp}^{45}$ for crossed polarizers at the same wavelength 656 nm along the line O'X', Figure 10.

Figure 8. Polarizing microscope textures of a flat cell viewed in monochromatic light 656 nm between two *parallel* polarizers, at zero voltage **(a)**, at $U = 200 \text{ V}_{\text{rms}}$, $f = 100 \text{ kHz}$ **(b)**, **(c)**, and **(d)**. The vector $\mathbf{E}$ shows the transmission direction of polarizers.

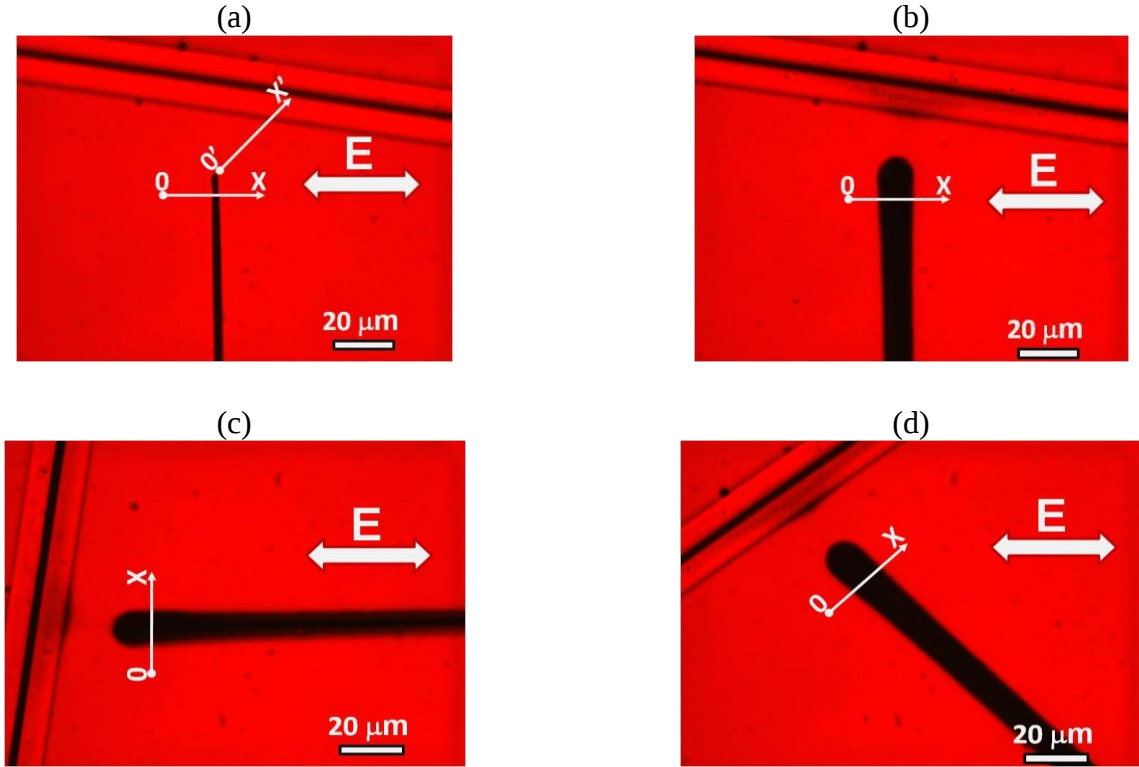


Figure 9. Profiles of intensities $I_{\parallel}^{90}$ (a), $I_{\parallel}^0$ (b), and $I_{\parallel}^{45}$ (c) vs. distance OX for the flat cell viewed in monochromatic light at 656 nm between parallel polarizers.

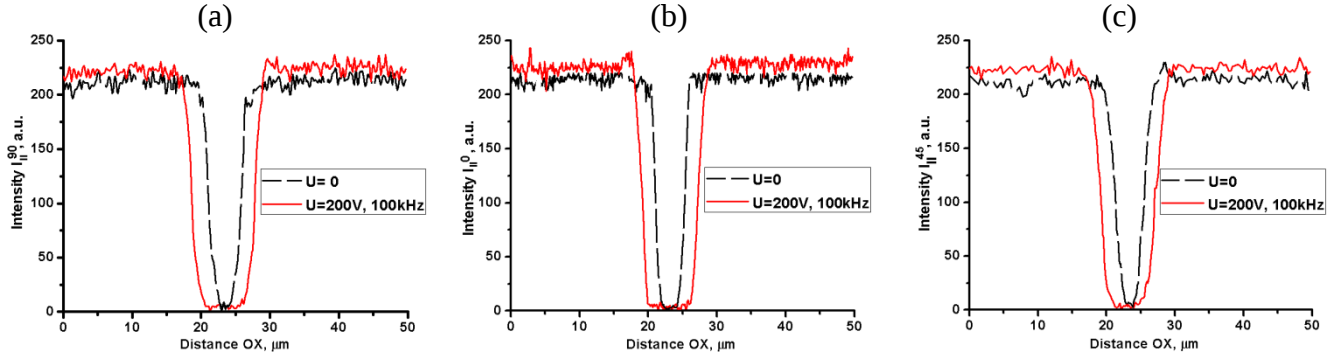
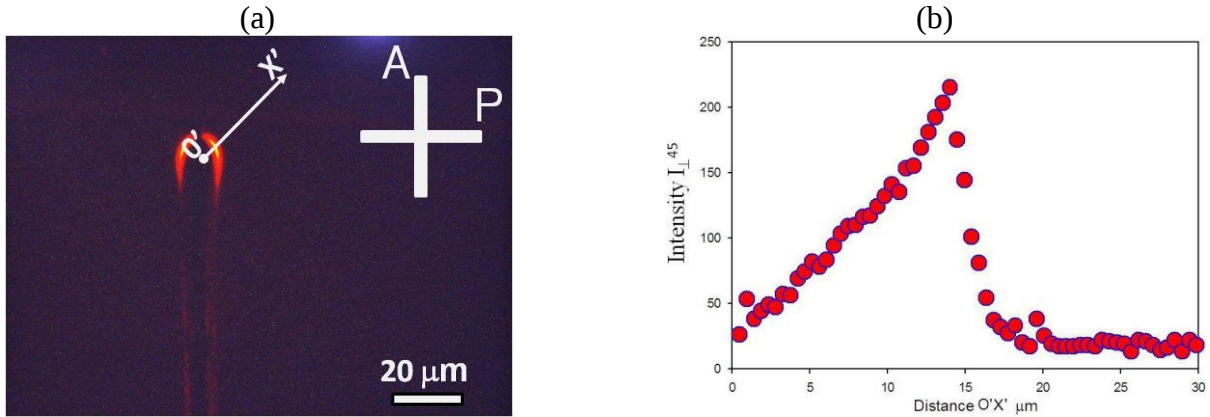


Figure 10. Texture of the flat cell with the toluene dispersion of Au NRs under an applied voltage $U = 200 \text{ V}_{rms}$, $f = 100 \text{ kHz}$, viewed in monochromatic light at 656 nm between two crossed polarizers A and P (a); transmitted light intensity $I_{\perp}^{45}$ measured along the direction O'X' (b).



3.3. Cylindrical Cell: Electrically Controlled Visibility of Central Electrode

The coaxial electrodes in the cylindrical cell create a gradient electric field $E_e \propto 1/r$ that decreases with the distance r from the central electrode, Figure 2(c). Similarly to the case of a flat cell, the AC voltage accumulates and aligns the Au NRs near the central electrode, Figures 11 and 13.

The most striking optical feature of cylindrical cells is that the applied field weakens the shadow of the central electrode, Figure 12, when the latter is observed in the orthoscopic mode under the microscope. The effect is wavelength and polarization dependent, being pronounced for light polarized perpendicularly to the capillary (and thus parallel to the Au NRs), Figure 12(a,b,c). We explored the wavelength dependence for “long/thin” NRs as for these the longitudinal peak of absorption is shifted towards the near infrared region [22]. The transmittance profiles measured for three spectral regions, “red”, “green” and “blue” (decoded from the RGB signal of CCD camera) show that the field-induced reduction of shadow is most pronounced in the “red” region with $\lambda = (550 - 700) \text{ nm}$, i.e., where the field-induced birefringence is the highest, Figure 12(a). Propagation of light with parallel polarization is hardly affected by the electric field, Figure 12(d,e,f).

Figure 11. The cylindrical cell formed by a glass capillary (1), a copper wire electrode along the capillary axis (2), and a transparent electrode at the outer surface (3). The cavity is filled with “long/thin” NRs in toluene (4) and sealed by polymerized optical adhesive (5). Microscope textures (parallel polarizers) of the capillary when the field $\mathbf{E}_e$ is off (a) and on, $U = 170 V_{rms}$, $f = 100$ kHz (b).

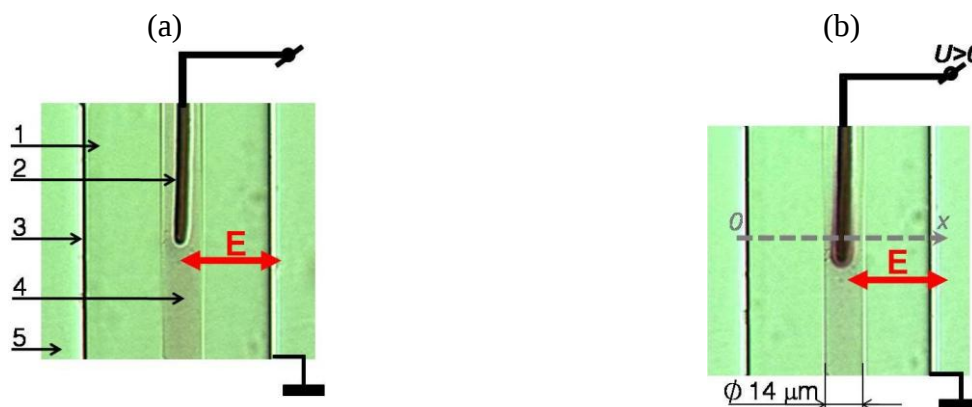


Figure 12. Electric field-induced redistribution of “long/thin” Au NRs changes the profiles of light transmission through the capillary for the light polarization perpendicular to the capillary (a), (b), (c), but not for $\mathbf{E}$ parallel to the capillary (d), (e), (f). Black traces: the field $\mathbf{E}_e$ is off, red traces: field on.

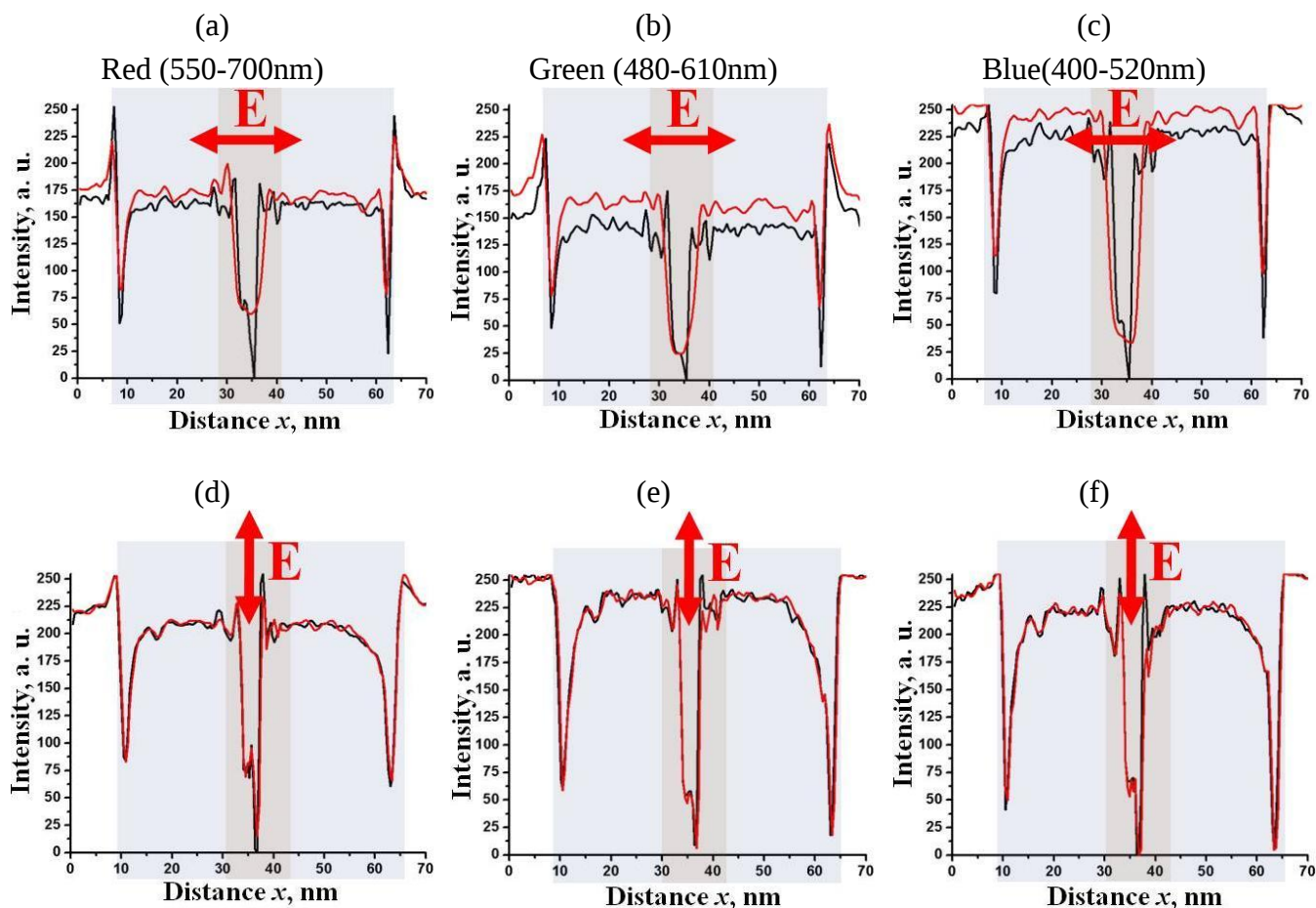
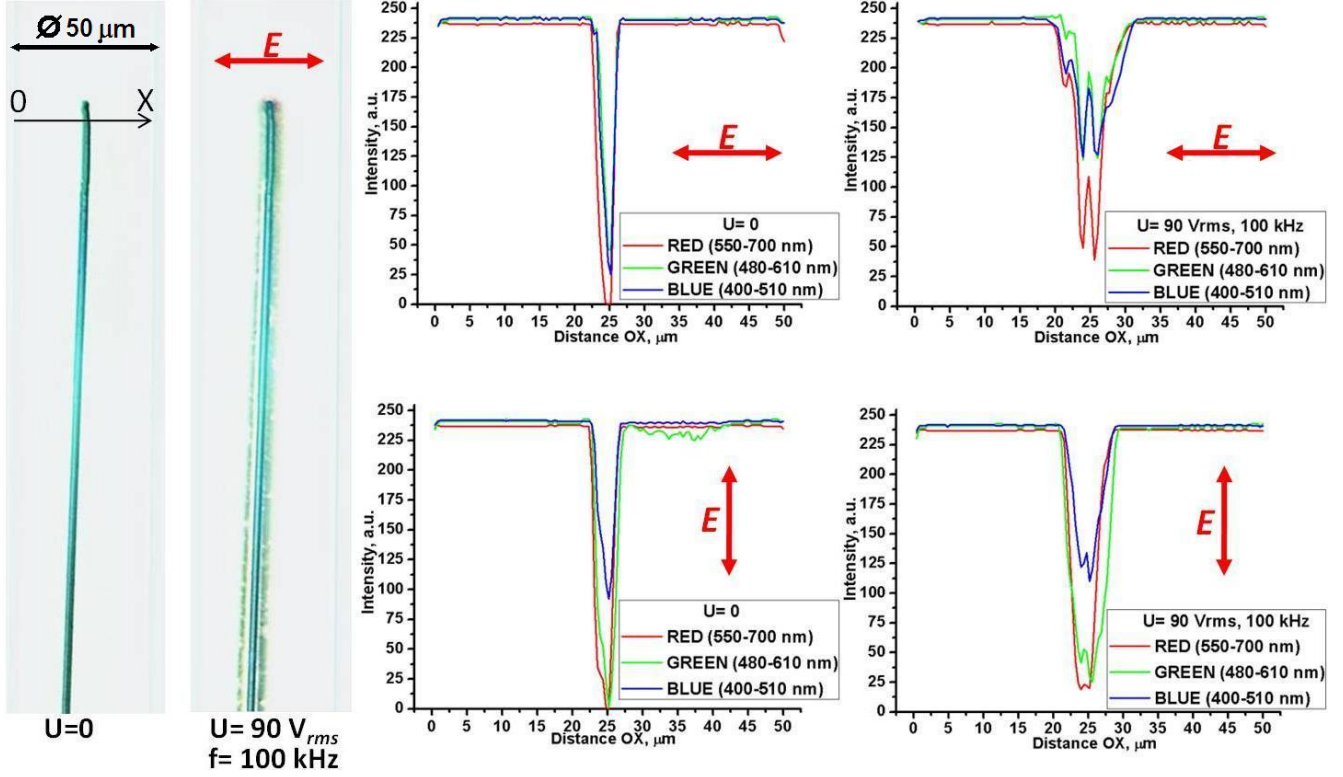


Figure 13. Variable visibility of the central electrode (2) in a cylindrical capillary (1) filled with toluene dispersion of “short/thin” Au NRs, shown by the textures at zero voltage (left texture) and at the voltage $90V_{rms}$, 100 kHz (right texture). Observation under the microscope with light polarized normally to the capillary axis. The right part of the figure illustrates how the light transmission changes along the direction OX for light polarized normally to the capillary (top row) and parallel to it (bottom row).



To obtain a better insight into the electric field-induced optical effects, below we analyze the textures theoretically.

4. Field Induced Optical Retardation in the Structure of Oriented and Concentrated Au NRs

4.1. Light Transmission Through an Absorbing Birefringent Medium

Consider propagation of a linearly polarized monochromatic wave that is normally incident on a slab with unidirectionally aligned NRs. The optic axis is tilted with respect to the slab's normal by an angle θ . The wave splits into the ordinary and extraordinary waves with different indices of refraction n_o and n_{eff} , and indices of absorption κ_o and κ_{eff} , respectively. For the ordinary wave, the refractive and absorption indices do not depend on the orientation of the optic axis, *i.e.*, $n_o = n_{\perp}$ and $\kappa_o = \kappa_{\perp}$, where the subscript $\perp$ means that the quantity was measured with the light polarized normally to the optic axis. For the extraordinary wave, n_{eff} and κ_{eff} depend on θ [35,36]:

$$n_{eff} = \frac{n_{\parallel} n_{\perp}}{\sqrt{n_{\parallel}^2 \cos^2 \theta + n_{\perp}^2 \sin^2 \theta}}, \quad (5)$$

$$\kappa_{eff} = \frac{n_{eff}^2}{n_{\perp}^2} \kappa_{\perp} \cos^2 \theta + \frac{n_{eff}^2}{n_{\parallel}^2} \kappa_{\parallel} \sin^2 \theta, \quad (6)$$

where $n_{\parallel}$ and $\kappa_{\parallel}$ correspond to the case when light propagates perpendicularly to the optic axis ($\theta = \pi/2$) with polarization $\mathbf{E}$ parallel to the optic axis.

To derive an expression for light transmittance through the slab of thickness d , viewed between two arbitrary oriented polarizers, we employ the formalism of Jones matrices. Let us choose a Cartesian coordinate system with the Z-axis directed along the wave vector of light. The polarizer P, slab and analyzer A, are perpendicular to the Z-direction. The X-axis is chosen to be along the projection of the optic axis (specified by the long axes of Au NRs) onto the plane normal to Z. The transmission direction of the linear polarizer P is oriented at an angle α with respect to X, while the analyzer's direction A makes an angle β with X. The electric field $\mathbf{E}^{ex}$ of the wave exiting the analyzer is related to the incoming electric field $\mathbf{E}$ through the product of Jones matrices:

$$\mathbf{E}^{ex} = ASPE, \quad (7)$$

where $A = \begin{pmatrix} \cos^2 \beta & \sin \beta \cos \beta \\ \sin \beta \cos \beta & \sin^2 \beta \end{pmatrix}$ is the Jones matrix of the analyzer, $S = e^{-\frac{2\pi}{\lambda}(in+\kappa)d} \begin{pmatrix} e^{-\frac{iR+D}{2}} & 0 \\ 0 & e^{\frac{iR+D}{2}} \end{pmatrix}$ is the Jones matrix for the slab with the average refractive index $n = \frac{n_{eff} + n_{\perp}}{2}$ and absorption coefficient $\kappa = \frac{\kappa_{eff} + \kappa_{\perp}}{2}$; $\mathbf{E}^{ex} = \begin{pmatrix} E_x^{ex} \\ E_y^{ex} \end{pmatrix}$ stands for the light wave exiting the analyzer, and $P\mathbf{E} = \begin{pmatrix} \cos \alpha \\ \sin \alpha \end{pmatrix}$ stands for the light wave passed through the polarizer. Note that by the last definition for $P\mathbf{E}$ we effectively normalized the amplitude of the electric field exiting the polarizer by the amplitude E of the incoming electric field. In the definition of S , we introduce two new notations: the linear birefringence R and the linear dichroism D . For a uniformly aligned slab, $R = \frac{2\pi}{\lambda}(n_{eff} - n_{\perp})$ and $D = \frac{2\pi}{\lambda}(\kappa_{eff} - \kappa_{\perp})$. For a general case, when the orientation of NRs changes with the coordinate z normal to the slab (and the director experiences splay and bend deformations but not the twist deformations), these quantities are represented by integrals:

$$R = \frac{2\pi}{\lambda} \int_0^d [n_{eff}(\theta(z)) - n_{\perp}] dz, \quad D = \frac{2\pi}{\lambda} \int_0^d [\kappa_{eff}(\theta(z)) - \kappa_{\perp}] dz. \quad (8)$$

The light transmittance through the system is $T = \mathbf{E}^{ex} \mathbf{E}^{ex*}$, where the *-symbol denotes a complex conjugate. Using Equation (7) for arbitrary α and β , we find:

$$T = e^{-\frac{4\pi}{\lambda}kd} \left\{ e^{-D} \cos^2 \alpha \cos^2 \beta + \frac{1}{2} \sin 2\alpha \sin 2\beta \cos R + e^D \sin^2 \alpha \sin^2 \beta \right\}. \quad (9)$$

For parallel polarizers ($\beta = \alpha$) the transmission reads

$$T = e^{-\frac{4\pi}{\lambda}kd} \left\{ e^{-D} \cos^4 \alpha + \frac{1}{2} \cos R \sin^2 2\alpha + e^D \sin^4 \alpha \right\}. \quad (10)$$

The expression for $T_{\parallel}$ can be rewritten in terms of the transmittances $T_{\parallel}^0$, $T_{\parallel}^{45}$, and $T_{\parallel}^{90}$ between parallel polarizers, corresponding to three different azimuthal orientations of the director, $\alpha = 0$, $\alpha = 45^\circ$, and $\alpha = 90^\circ$, respectively:

$$T_{\parallel} = T_{\parallel}^0 \cos^4 \alpha + \frac{\sqrt{T_{\parallel}^0 T_{\parallel}^{90}}}{2} \cos R \sin^2 2\alpha + T_{\parallel}^{90} \sin^4 \alpha. \quad (11)$$

Measuring $T_{\parallel}^0$, $T_{\parallel}^{45}$, and $T_{\parallel}^{90}$, one deduces the absorption indices κ_{eff} and $\kappa_{\perp}$, dichroism $\kappa_{eff} - \kappa_{\perp}$, and birefringence $\Delta n_{eff} = n_{eff} - n_{\perp}$, using the following relationships:

$$T_{\parallel}^0 = e^{-\frac{4\pi}{\lambda} \kappa_{eff} d}, T_{\parallel}^{90} = e^{-\frac{4\pi}{\lambda} \kappa_{\perp} d}, \quad (12)$$

$$\cos \frac{2\pi d \Delta n_{eff}}{\lambda} = \frac{4T_{\parallel}^{45} - (T_{\parallel}^0 + T_{\parallel}^{90})}{2\sqrt{T_{\parallel}^0 T_{\parallel}^{90}}}. \quad (13)$$

There is an alternative possibility to measure the phase retardation, by placing the sample between two crossed polarizers, in which case $\alpha = \frac{\pi}{2}$, and the transmission reads

$$T_{\perp} = \frac{1}{2} e^{-\frac{4\pi}{\lambda} \kappa d} \{\cosh D - \cos R\} \sin^2 2\alpha. \quad (14)$$

Note that Equation (14) contains three unknown parameters: κ , D and R . Since we are mostly interested in determination of R which is a measure of the field-induced birefringence in the dispersion of NRs, we need to exclude κ and D from the consideration. This can be achieved, for example, by measuring three quantities, namely, transmittance $T_{\perp}^{45}$ between crossed polarizers, for $\alpha = 45^\circ$; $T_{\parallel}^0$ determined with a pair of parallel polarizers, $\beta = \alpha = 0$ and $T_{\parallel}^{90}$ for $\beta = \alpha = \frac{\pi}{2}$. This is precisely the set of parameters that was measured in the experiments illustrated in Figure 9 and 10. Equation (14) can be rewritten as

$$T_{\perp} = \frac{1}{4} \left\{ T_{\parallel}^0 + T_{\parallel}^{90} - 2\sqrt{T_{\parallel}^0 T_{\parallel}^{90}} \cos R \right\} \sin^2 2\alpha \quad (15)$$

which leads to a straightforward expression to determine the field-induced birefringence $\Delta n_{eff} = n_{eff} - n_{\perp}$ associated with the effective extraordinary index of refraction n_{eff} :

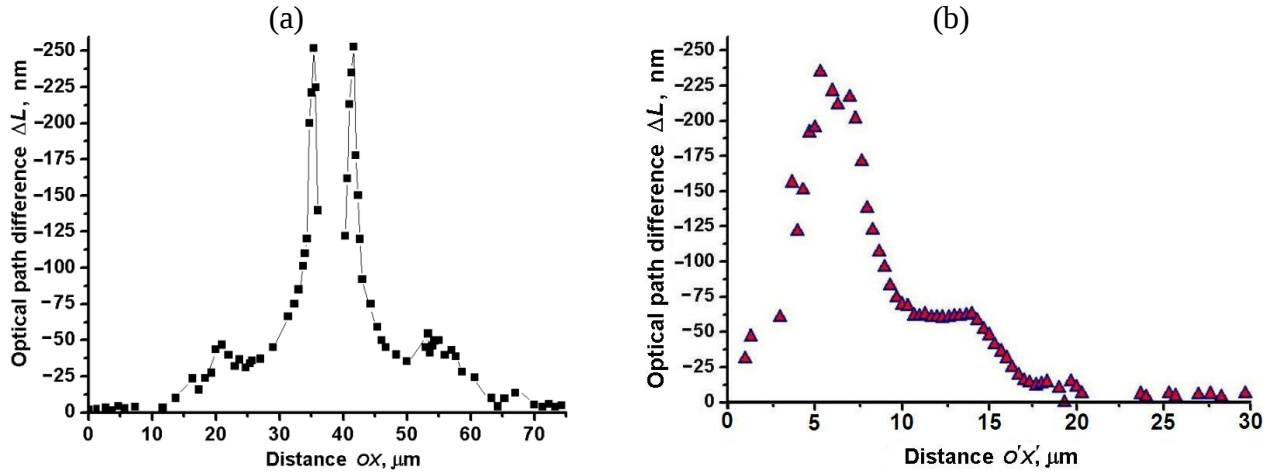
$$\cos \frac{2\pi d \Delta n_{eff}}{\lambda} = \frac{(T_{\parallel}^0 + T_{\parallel}^{90}) - 4T_{\perp}^{45}}{2\sqrt{T_{\parallel}^0 T_{\parallel}^{90}}}. \quad (16)$$

Equation (16) is similar to Equation (13), as in both cases, the ratio $(T_{\parallel}^0 + T_{\parallel}^{90}) / \left(2\sqrt{T_{\parallel}^0 T_{\parallel}^{90}} \right)$ is nothing else but the ratio of the arithmetic $\bar{T} = (T_{\parallel}^0 + T_{\parallel}^{90})/2$ and geometric mean $\hat{T} = \sqrt{T_{\parallel}^0 T_{\parallel}^{90}}$ for $T_{\parallel}^0$ and $T_{\parallel}^{90}$. The only difference is that Equation (13) uses the quantity $T_{\parallel}^{45}$, while Equation (16) deals with the quantity $T_{\perp}^{45}$; the latter might be more convenient to use as it can be measured more accurately, especially in weakly birefringent cases. We used both approaches to derive the map of spatial profile of the field-induced path difference $\Delta L = \Delta n_{eff} d$ in the flat cells. Figure 14(a) shows the profile of $\Delta L = \Delta n_{eff} d$ along the direction OX in Figure 8(b,c,d) across the central electrode, calculated using Equation (13). Figure 14(b) shows variation of ΔL along the different direction O'X' defined in Figure 10(a); in mapping ΔL , we used Equation (16) and the data shown in Figure 10(b). Both approaches produce similar maps, demonstrating that the maximum field-induced optical path difference is about (-250) nm. The approach based on Equation (16) produces somewhat smoother

features in the region of small path difference, apparently because of the higher accuracy in measuring $T_{\perp}^{45}$ as compared to $T_{\parallel}^{45}$.

Within the Au NRs cloud, concentration and orientation of the NRs vary along the Z direction. The local optical quantities such as $n_{\parallel}(r)$ and $n_{\perp}(r)$ depend on these two and also on the degree of orientational order of NRs and thus also vary with Z. The simple relationship $\Delta L = \Delta n_{eff} d$ thus produces only a rough estimate of the field-induced birefringence $\Delta n(r) = n_{\parallel}(r) - n_{\perp}(r)$. We can neglect the spatial variation of $n_{\perp}$, as light with polarization perpendicular to the optic axis “sees” only the circular cross-sections of NRs that occupy a relatively small fraction of space [12]. Assuming for a moment that the thickness of a highly concentrated part of the Au NRs cloud is approximately equal to the diameter of electrode $d_e \approx 2 \mu m$, one can roughly estimate the maximum magnitude of field-induced birefringence in Figure 14(a,b) as $\Delta n_{656nm} = \frac{\Delta L}{d_e} = -250nm/2 \mu m \approx -0.1$. As we shall see in Section 4.2 below, a more refined approach with numerical simulations of light transmittance through the flat cell produces a similar result.

Figure 14. Optical path difference $\Delta L = \Delta n_{eff} d$ vs. distance OX calculated using Equation (13) (a) and Equation (16) (b). All data correspond to the toluene dispersion of “short/thin” Au NRs, $\lambda = 656nm$, applied voltage $U = 200 V_{rms}$, $f = 100$ kHz.



4.2. Light transmission through flat samples with NR dispersions

To get a better insight into the magnitude and spatial distribution of the field-induced optical properties of the switchable metamaterial, we need to consider the radial configuration of the optic axis and account for the fact that the system is spatially limited. We calculate light transmission through the sample of thickness d , placed between two crossed polarizers. We choose the Cartesian coordinate system $\{x, y, z\}$ with the origin at the wire axis, direct the z -axis normal to the substrates, and the y -axis along the wire. We assume that the dielectric tensor at optical frequencies is uniaxial with radial ($r = \sqrt{x^2 + z^2}$) dependence of the ordinary $n_{\perp}(r)$ and extraordinary $n_{\parallel}(r)$ refractive indices and that the optic axis $\hat{n}$ is normal to the wire, $\hat{n} = \{\sin \theta, 0, \cos \theta\}$, where $\tan \theta = x/z$, Figure 15. In such a

medium, light propagates along the z -axis as an ordinary wave with the refractive index $n_{\perp}(r)$ and an extraordinary wave with the effective refractive index

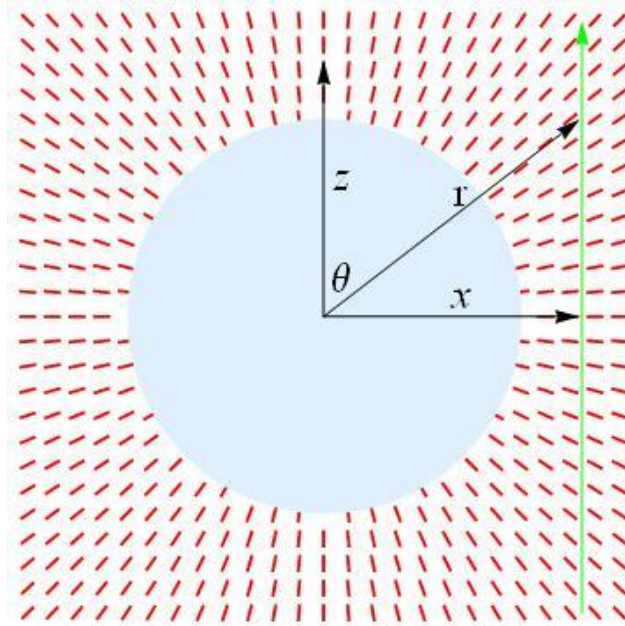
$$n_{\text{eff}}(r) = \frac{n_{\parallel}(r)n_{\perp}(r)}{\sqrt{n_{\parallel}^2(r)\cos^2\theta + n_{\perp}^2(r)\sin^2\theta}} \approx n_{\perp}(r) + \delta(r)\sin^2\theta + \tilde{\delta}(r)\sin^4\theta \quad (17)$$

where

$$\delta(r) = n_{\perp}(r) \left[n_{\parallel}^2(r) - n_{\perp}^2(r) \right] / 2n_{\parallel}^2(r), \quad \tilde{\delta}(r) = 3n_{\perp}(r) \left[n_{\parallel}^2(r) - n_{\perp}^2(r) \right]^2 / 8n_{\parallel}^4(r). \quad (18)$$

Here the expansion parameter is $\Delta n(r) = n_{\parallel}(r) - n_{\perp}(r)$, because $\delta(r) \approx \Delta n(r)$, and $\tilde{\delta}(r) \approx 3\Delta n^2(r)/4$.

Figure 15. Light propagation (vertical green arrow on the right hand side) in a medium with radial configuration of the optic axis (red bars) around the wire (grey circle).



Our goal is to recover $n_{\parallel}(r)$ from the experimentally measured optical path difference $\Delta L(x)$ shown in Figure 14(a) (the data in Figure 14(b) produce similar results). Considering $\Delta n(r) = n_{\parallel}(r) - n_{\perp}(r)$ small, we calculate

$$\Delta L(x) = \int_{-d/2}^{d/2} (n_{\parallel}(r) - n_{\perp}(r)) dz \approx \int_{-d/2}^{d/2} \delta(r) \sin^2\theta dz \quad (19)$$

We represent $\delta(r)$ as an inverse power series $\delta(r) = \sum_m \delta_m r^{-m}$. Then,

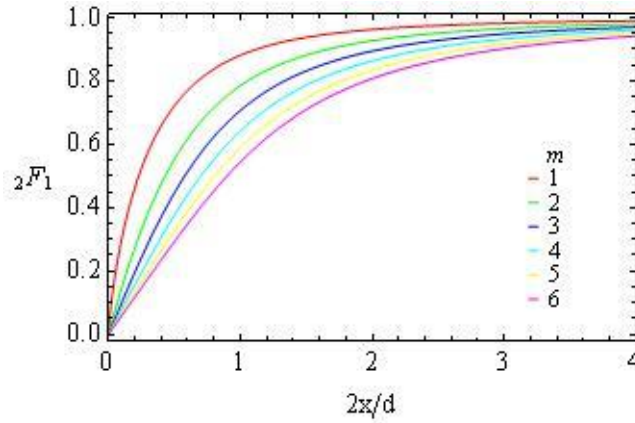
$$\begin{aligned} \Delta L(x) &= x^2 \sum_m \delta_m \int_{-d/2}^{d/2} (x^2 + z^2)^{(m+2)/2} dz = \\ &= d \sum_m \delta_m x^{-m} {}_2F_1\left(1/2, (m+2)/2, 3/2, -(2x/d)^{-2}\right). \end{aligned} \quad (20)$$

Here ${}_2F_1\left(1/2, (m+2)/2, 3/2, -(2x/d)^{-2}\right)$ are the Gauss hypergeometric functions, Figure 16, that are linear for small x and saturate to 1 for large x ,

$${}_2F_1\left(1/2, (m+2)/2, 3/2, -(2x/d)^{-2}\right) = \begin{cases} 1, & x \gg d/2 \\ \sqrt{\pi} \Gamma((m+1)/2) (2x/d) / 2 \Gamma((m+2)/2), & x \ll d/2, \end{cases} \quad (21)$$

where $\Gamma((m+1)/2)$ is the gamma function.

Figure 16. The Gauss hypergeometric functions ${}_2F_1\left(1/2, (m+2)/2, 3/2, -(2x/d)^{-2}\right)$ vs. $2x/d$ for different m .



We start the analysis of experimental data with the determination of the center of wire $x_c = 38.29 \pm 0.02 \mu\text{m}$ by fitting the left wing of the experimental plot in Figure 14(a) with an interpolation from the right wing and *vice versa*, Figure 17. Then we combine both wings in Figure 14(a) using x_c as an origin, Figure 18 and 19, and fit the optical phase retardation profile using different sets of terms in Equation (20). Figure 18 demonstrates that fitting the left wing (red), right wing (green) and all experimental data (blue) with $m = 3$ and $m = 5$ from Equation (20) results in almost the same interpolation curves.

Figure 17. Fitting the left wing (red) of Figure 14 (a) with interpolation from the right wing (green) and *vice versa* allows us to determine the center of wire $x_c = 38.29 \pm 0.02 \mu\text{m}$.

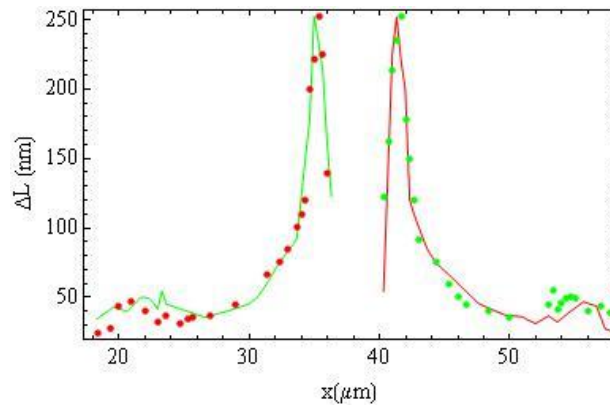


Figure 18. Fitting the left part (red), right part (green) and all experimental data (blue) with Equation (20) with $m = 3$ and $m = 5$ results in almost the same interpolation curves.

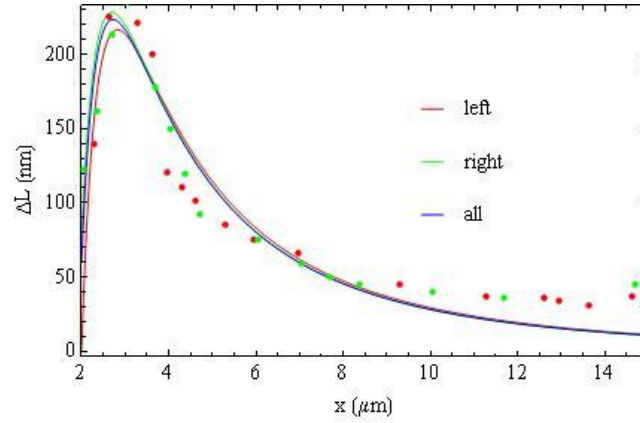


Figure 19. Fitting (all) experimental data with Equation (20) with different sets of m , shown in the legend.

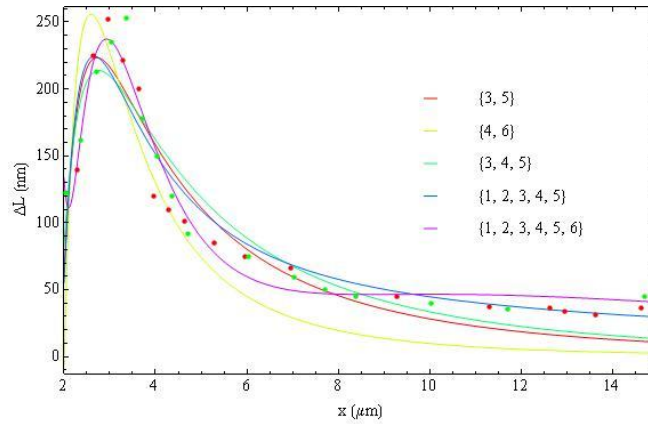
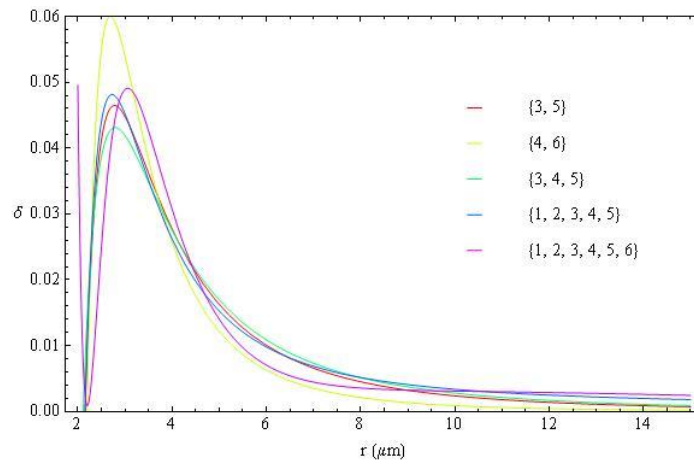
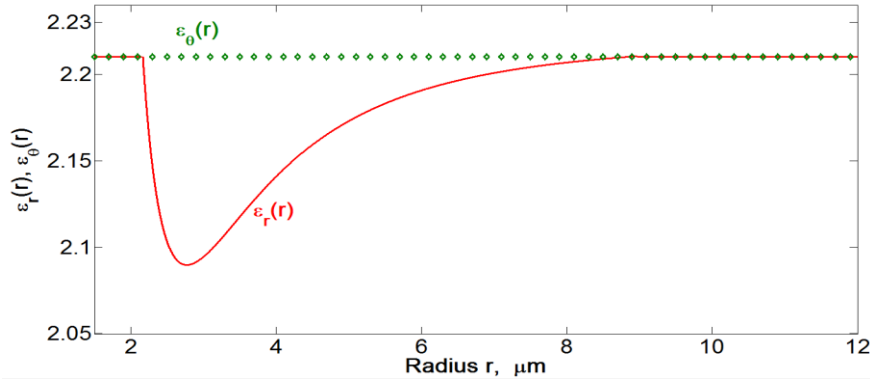


Figure 20. Radial dependence of the birefringence parameter $\delta(r)$, Equation (18), obtained from the fittings shown in Figure 19.



With Figure 19, we produce the fitting of the birefringence parameter $\delta(r)$, Equation (18), using different sets of m , Figure 20. The fitting curves for different approaches are very close to each other, signaling that the data on $\delta(r)$ are robust. Apparently, the set $m = \{3,5\}$ provides the most reliable fitting because further expansion of the basis of fitting functions does not improve the result substantially. Thus for this set we calculate the radial dependence of permittivity $\varepsilon_r(r) = n_{\parallel}^2(r) = n_{\perp}^3(r)/[n_{\perp}(r) - 2\delta(r)]$, Figure 21, assuming that the ordinary refractive index $n_{\perp}(r)$ is constant across the capillary and equal to the refractive index of toluene $n_t = 1.49$, so that $\varepsilon_{\theta}(r) = n_{\perp}^2(r) = 2.21$. The spatial distribution of the radial and azimuthal components of dielectric permittivity (refractive indices) induced by the gradient electric field ($U = 200 \text{ V}_{rms}$, $f = 100 \text{ kHz}$) in a flat cell shown in Figure 21 is one of the major results of this work. These dependences will be used in the numerical simulations of light propagation through the Au NRs dispersion in cylindrical cells, Section 4.3.

Figure 21. Radial dependence of $\varepsilon_r(r) = n_{\parallel}^2(r)$, obtained from Equation (18) and $\delta(r)$ for $m = \{3,5\}$ shown in Figure 20, with $\varepsilon_{\theta}(r) = n_{\perp}^2(r) = 2.21$. The data correspond to the toluene dispersion of “short/thin” Au NRs in the flat cell, $\lambda = 656 \text{ nm}$, $U = 200 \text{ V}_{rms}$, $f = 100 \text{ kHz}$, see Figure 14(a).



The field-dependent $n_{\parallel}$ can be estimated independently by considering the dispersion as a dielectric of permittivity ε_t pierced with parallel NRs of permittivity ε_{NR} with the field-dependent volume fraction η_U :

$$n_{\parallel} = \sqrt{(1 - \eta_U) \varepsilon_t + \eta_U \varepsilon_{NR}}. \quad (22)$$

For the experimentally determined (from light absorption data in Section 3.1) $\eta_0 = 0.02$, and for $\varepsilon_{NR} = -12.5\varepsilon_0$ at 656 nm [34], one finds $n_{\parallel} \approx 1.4$ and thus $\Delta n \approx -0.1$, the same order of magnitude as other estimates above.

Birefringence of the NRs cloud reflects the cumulative effect of the Au NRs and their polystyrene (PS) coatings. The contribution of PS to the refractive index depends on the configuration of polymer chains covalently grafted to the Au NRs. Birefringence of stretched polystyrene is negative with the refractive index along the PS chain being smaller than the refractive index perpendicular to the chain [37]. Therefore, if the PS chains are directed normally to the NR surface, they will diminish the

birefringence effect introduced by alignment of Au NRs; parallel arrangement would enhance the effect of NRs. The experimentally measured birefringence of mechanically stretched PS is $|\Delta n_{PS}| = 0.0006$ at 700 nm [37]. Therefore, if we assume that in flat cells the entire gap $d \approx 20 \mu\text{m}$ is filled with such a birefringent PS, the total optical path difference between the extraordinary and ordinary waves ΔL would be about 12 nm only, *i.e.*, an order of magnitude smaller than the experimental value of $|\Delta L| = 250\text{nm}$. The estimate suggests that the main contribution in the field-induced modification of the optical properties of the metamaterial in question is produced by the Au NRs themselves.

4.3. Simulations of optical effects caused by NR redistribution in cylindrical samples

We use a commercial Finite Element Package of COMSOL Multiphysics with Radio Frequency module version 4.0a to simulate the electromagnetic wave propagation in the cylindrical cell filled with toluene dispersion of “short/thin” Au NRs. In simulations of the “cloak on” regime, Figure 22(a), we used the dielectric permittivity profile shown in Figure 21, around the central copper electrode of the diameter $2 \mu\text{m}$. Note that the permittivity profile in Figure 22 was obtained for the flat cell but in Figure 22(a) it is used to simulate the optical performance of the cylindrical cell. This approximation is justified by the fact that the geometries of gradient electric fields and the dielectrophoretic potentials in flat and cylindrical cells are similar, Figure 3. Both parts of Figure 22 show the simulated magnetic-field component of the wave propagating throughout the cylindrical shell; the black trajectories show the power flow.

Figure 22 illustrates that when the electric field creates a cloud of Au NRs around the central electrode, Figure 22(a), the shadow of this electrode is mitigated as compared to the case when the electric field is off and the Au NRs are distributed randomly in the cylindrical cavity, Figure 22(b). The power flow near the electrode is bent towards the middle plane of the figure. The effect is the result of the reduced refractive index $n_{\parallel}$ near the central electrode. Of course, the decrease in $n_{\parallel}$ is modest, about 5% of what is used in the theoretical cloak [12], so that the cloaking effect is far from being perfect. However, the very fact that the electric field gradients are capable of aligning and condensing Au NRs to the extent that the system acquires easily detectable optical anisotropy and variation of the refractive index is very encouraging for future developments of reconfigurable and switchable optical metamaterials based on dielectrophoretic effects in dispersions of NRs.

Figure 23 demonstrates a similar comparison of the “cloak on” and “cloak off” regimes when the light intensity is measured at some distance from the electrode, after the wave travelled to the right, about $19 \mu\text{m}$ from the electrode. The system parameters are the same as in Figure 22. The plots show transmitted light intensity as a function of the vertical coordinate OY. All plots are normalized by the intensity of the incident TM plane wave. Note that light intensity in the centre of the expected shadow is much higher when the field is on as compared to the case when the field is off, reflecting the bending effect of the Au NRs clouds near the central electrode on the light trajectories. These simulated intensities are similar to the intensity profiles of the red component of RGB signal measured in the experiments with Au NRs, Figure 13.

Figure 22. Simulated light propagation in a cylindrical cell with TM illumination at $\lambda = 656 \text{ nm}$. The applied voltage 200 V_{rms} induces the radial profile of the extraordinary refractive index around central electrode and bends the trajectories of power flow around the electrode, mitigating its shadow **(a)**. At zero voltage, the cell has a spatially uniform refractive index (of toluene) and the electrode shadow is well pronounced **(b)**. The color represents the amplitude of magnetic field; see the scale on the right hand side.

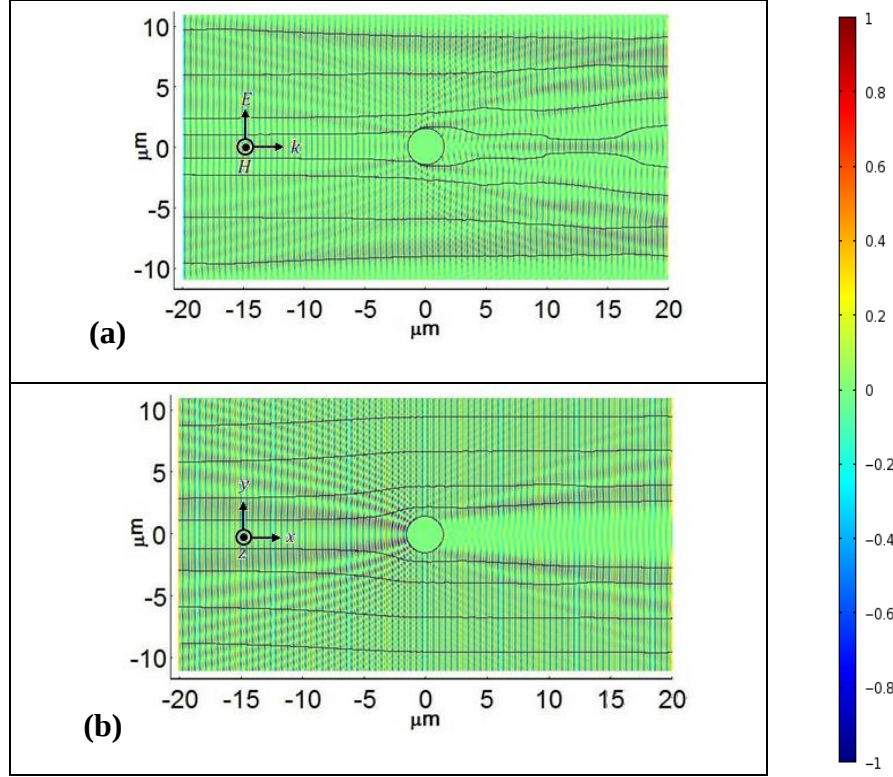
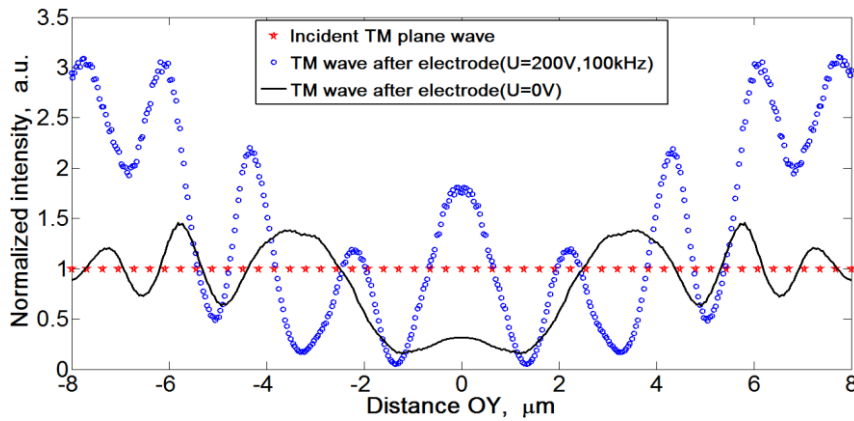


Figure 23. Normalized intensities of incident TM plane wave before the central electrode (red stars), TM wave behind the central electrode with the electric field-induced variation of the extraordinary refractive index (empty blue dots), and TM wave behind the central electrode when the electric field is switched off (solid black line). In the center of shadow, near $OY = 0$, the light intensity in the “field on” case is higher than in the “field off” case.



5. Liquid crystal metamaterials

5.1. Light propagation in liquid crystals with director distortions

The concepts of transformation optics, as was already discussed, are not entirely new to the science of LCs. In 1919, Grandjean considered a cylindrical nematic sample in which the director $\hat{n}$ was arranged radially. When such a structure is illuminated with light polarized normally to the cylinder, the rays are bent away from the central axis and leave a segment of an opening angle $2\pi(1-n_o/n_e)$ unilluminated (for a modern reproduction of the result, see the textbook[10]). This particular example represents a beam divider, as the trajectories are splitting into different pathways. This pioneering work of Grandjean has recently been substantially expanded by Sátiro and Moraes[43,44] who considered other types of director configurations, such as disclinations of strength “1/2” and “-1/2”. Light propagation was analyzed as a function of temperature- and wavelength-dependent refractive indices n_e and n_o [44].

In this work, we extend the consideration of curved light trajectories from a standard LC to a “LC metamaterial”, or LCMM, i.e. a material representing a dispersion of a solid (metallic) component such as Au NRs in a LC as a dispersion matrix. The LC matrix aligns the NRs along $\hat{n}$. The NR are much smaller than λ so that the composite is optically homogeneous. Recent experiments with NRs assembled into orientationally ordered substructures, see, for example, ref[45] and the works mentioned above, suggest that a construction of LCMMs is feasible. The optical properties of LCMM can be potentially controlled at three different levels. At the first level, by controlling the shape and concentration of solid inclusions, one can control the refractive indices. Typically, the metallic component decreases the effective refractive index (and increase light absorption). At the second level, with a given composition and concentration of the components, one can reconfigure and switch the optic axis. Finally, at the third level, the gradients of the optics axis can be supplemented by gradients of the composition. For example, as shown by Golovin et al. [22,46] for isotropic dispersion of Au NRs, application of the gradient electric field results in the condensation of Au NRs into orientationally ordered structures with spatially-varying concentration, birefringence and optical axis.

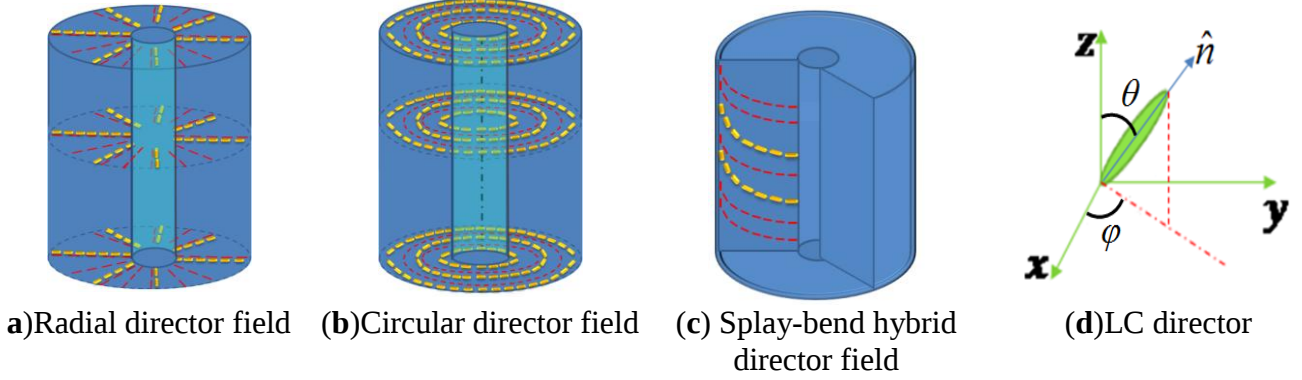
In this work, we consider LCMM properties controlled at the level 1 and 2, i.e., with birefringence set up by the concentration of metal NRs dispersed in a thermotropic LC with the distorted optical axis controlled by the boundary conditions in a sample shaped as a cylindrical shell. We first describe analytically light refraction at the isotropic-LC medium interface and light propagation for the case when the director and the wave-vector of light are confined to the same (x, y) plane. This consideration is followed by a more complex geometry, in which all three components of the director $\hat{n}$ are nonzero. The latter case is treated through numerical simulations, using COMSOL Multiphysics finite element-based electromagnetic solver.

5.2. Homogenization of LCMM anisotropic composite

The LCMMs in this work represents a dispersion of rod-like metallic particles, say, Au NRs, in a uniaxial nematic LC medium. Concentration of the metallic part controls the dielectric properties of the material and is assumed to be independent of the spatial coordinates. We consider three director

configurations of LCMM in a cylindrical shell that are stabilized by the surface anchoring at the bounding walls, Fig.24(a,b,c).

Figure 24. Director configurations for LCMM in a cylindrical shell, $R_{in} \leq r \leq R_{out}$, with the optic axis represented in the cylindrical coordinates (r, φ, z) as (a) $\hat{n} = (1, 0, 0)$; (b) $\hat{n} = (0, 1, 0)$; (c) $\hat{n} = (\sin \theta, 0, \cos \theta)$ where the polar angle θ changes from 0 at the inner boundary of the cylindrical shell to $\pi/2$ at the outer boundary; (d) director orientation in the Cartesian coordinates.



For a composite medium with two anisotropic uniaxial components, namely, the metal NRs and LC, with the same director, the effective optical properties can be described by the model of Sihvola[47]. Suppose that each NR is a spheroid with semi-axes a_x, a_y and a_z ($a_x > a_y = a_z$) and (isotropic) dielectric permittivity ε_m . The NRs are embedded into the LC characterized by a permittivity tensor $\bar{\bar{\varepsilon}}_{LC}$. We neglect the optical properties of the thin functionalizing layers at the surface of NRs that prevent aggregation of the NRs. Then the effective permittivity tensor of the LCMM is

$$\bar{\bar{\varepsilon}}_{eff} = \bar{\bar{\varepsilon}}_{LC} + \frac{f \left(\varepsilon_m \cdot \bar{\bar{I}} - \bar{\bar{\varepsilon}}_{LC} \right) \cdot \bar{\bar{\varepsilon}}_{LC}}{\bar{\bar{\varepsilon}}_{LC} + (1-f) \cdot \bar{\bar{L}} \cdot \left(\varepsilon_m \cdot \bar{\bar{I}} - \bar{\bar{\varepsilon}}_{LC} \right)}, \quad (23)$$

where $\bar{\bar{I}}$ is the identity matrix, f and $1-f$ are the volume fractions of the NRs and LC, respectively, and $\bar{\bar{L}}$ is the transformed depolarization dyadic,

$$\bar{\bar{L}} = \frac{\det \bar{\bar{A}}}{2} \int_0^\infty \frac{\bar{\bar{\varepsilon}}_{LC} \cdot ds}{\left(\bar{\bar{A}}^2 + \bar{\bar{\varepsilon}}_{LC} \cdot s \right) \sqrt{\det \left(\bar{\bar{A}}^2 + \bar{\bar{\varepsilon}}_{LC} \cdot s \right)}}; \quad (24)$$

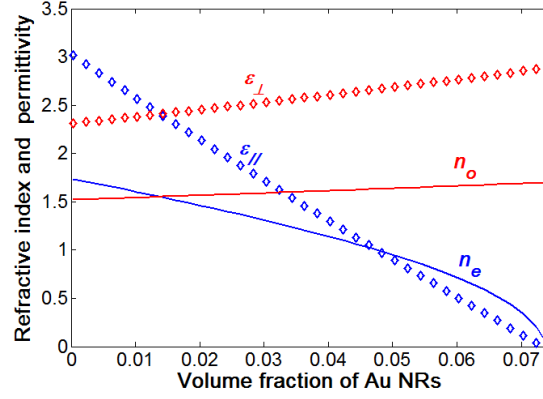
Furthermore, $\bar{\bar{A}} = \begin{bmatrix} a_x & 0 & 0 \\ 0 & a_y & 0 \\ 0 & 0 & a_z \end{bmatrix}$ and $\det \bar{\bar{A}} = a_x a_y a_z$. With the given ε_m , $\bar{\bar{\varepsilon}}_{LC}$, a_x and a_y , $\bar{\bar{\varepsilon}}_{eff}$ can be

controlled by changing the volume fraction of NRs. To describe the effective refractive indices of the LCMM we use the same notations n_e and n_o as in the case of the regular LCs; the presence of NRs in LC changes only the values of the refractive indices but does not change the general uniaxial non-polar symmetry of the medium.

Consider, for example, an LCMM composed of a LC E7 with $n_o = 1.52$ and $n_e = 1.74$, doped with Au NRs of $a_x = 60 \text{ nm}$ and $a_y = a_z = 15 \text{ nm}$. For Au, $\varepsilon_m = -16.7$ at for Au at 700nm[48]. The effective

extraordinary refractive index n_e of LCMM calculated according to equation (1), decreases sharply as a function of f , first becoming equal to n_o at $f=0.013$, and then turning zero at a relatively modest f just above 0.07, Fig.25.

Figure 25, Effective permittivity ($\epsilon_{\parallel}$, $\epsilon_{\perp}$) and effective refractive indices (n_e , n_o) of LCMM, which is composed of a LC matrix E7 with $n_o=1.52$ and $n_e=1.74$ doped with Au NRs of $a_x=60nm$ and $a_y=a_z=15nm$.



The LCMM is an anisotropic material with a non-magnetic response; its components of effective permittivity tensor write in Cartesian coordinates as

$$\begin{aligned} \epsilon_{xx} &= n_o^2 + (n_e^2 - n_o^2) \sin^2 \theta \cos^2 \varphi; & \epsilon_{xy} &= \epsilon_{yx} = (n_e^2 - n_o^2) \sin^2 \theta \cos \varphi \sin \varphi; \\ \epsilon_{yy} &= n_o^2 + (n_e^2 - n_o^2) \sin^2 \theta \sin^2 \varphi; & \epsilon_{xz} &= \epsilon_{zx} = (n_e^2 - n_o^2) \sin \theta \cos \theta \cos \varphi; \\ \epsilon_{zz} &= n_o^2 + (n_e^2 - n_o^2) \cos^2 \theta; & \epsilon_{yz} &= \epsilon_{zy} = (n_e^2 - n_o^2) \sin \theta \cos \theta \sin \varphi. \end{aligned} \quad (25)$$

where θ is polar angle of the director and φ is the azimuthal angle with respect to the x-axis, Fig.24(d).

Using equation (25), the dielectric tensor components for different director configurations in Fig.24 are calculated in cylindrical coordinates, Table1 (permeability $\bar{\mu}=1$).

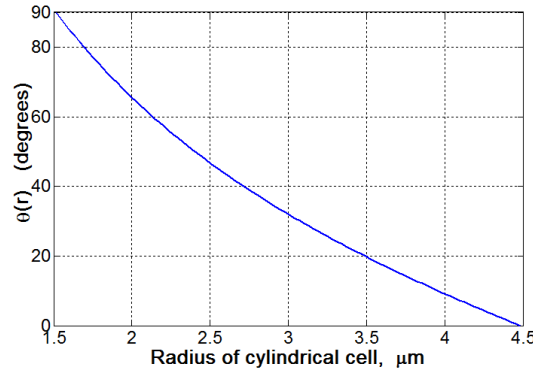
Table1: dielectric permittivity tensor for three director configurations considered in this work

Director configuration in cylindrical coordinates (r, φ, z)	Dielectric tensor in cylindrical coordinate	
$\hat{n}=(1,0,0)$	$\epsilon = \begin{bmatrix} \epsilon_{rr} & 0 & 0 \\ 0 & \epsilon_{\varphi\varphi} & 0 \\ 0 & 0 & \epsilon_{zz} \end{bmatrix}$	$\begin{aligned} \epsilon_{rr} &= n_e^2 \\ \epsilon_{\varphi\varphi} &= n_o^2 \\ \epsilon_{zz} &= n_o^2 \end{aligned}$
$\hat{n}=(0,1,0)$	$\epsilon = \begin{bmatrix} \epsilon_{rr} & 0 & 0 \\ 0 & \epsilon_{\varphi\varphi} & 0 \\ 0 & 0 & \epsilon_{zz} \end{bmatrix}$	$\begin{aligned} \epsilon_{rr} &= n_o^2 \\ \epsilon_{\varphi\varphi} &= n_e^2 \\ \epsilon_{zz} &= n_o^2 \end{aligned}$
$\hat{n}=[\sin \theta(r), 0, \cos \theta(r)]$	$\epsilon = \begin{bmatrix} \epsilon_{rr} & 0 & \epsilon_{rz} \\ 0 & \epsilon_{\varphi\varphi} & 0 \\ \epsilon_{zr} & 0 & \epsilon_{zz} \end{bmatrix}$	$\begin{aligned} \epsilon_{rr} &= n_o^2 + (n_e^2 - n_o^2) \sin^2 \theta(r) \\ \epsilon_{rz} &= \epsilon_{zr} = (n_e^2 - n_o^2) \sin \theta(r) \cos \theta(r) \\ \epsilon_{\varphi\varphi} &= n_o^2 \\ \epsilon_{zz} &= n_o^2 + (n_e^2 - n_o^2) \cos^2 \theta(r) \end{aligned}$

Fig.24 (a) shows a pure splay of $\hat{n}$, Fig.24 (b) describes a pure bend and Fig.24(c) shows a mixed splay-bend deformation. In the latter case, the director configuration depends on the ratio of the bend

K_{33} to the splay K_{11} elastic constants. It can be numerically calculated by minimizing the elastic energy of the LCMM with the fixed boundary conditions at the cylindrical boundaries of the shell, $\theta(r=R_{in})=0$; $\theta(r=R_{out})=\pi/2$. We use the values $K_{11}=12\times 10^{-12} N$, $K_{33}=19.5\times 10^{-12} N$ typical for E7 [49] to plot the director profile in the splay-bend case of Fig.24(c), see Fig.26, although one should be aware that the presence of NRs might modify the elastic properties of the LCMM.

Figure 26. The equilibrium director distribution for E7 confined in coaxial cylindrical structure, shown as the dependence of the polar angle θ on the radial coordinate within the cylindrical shell.



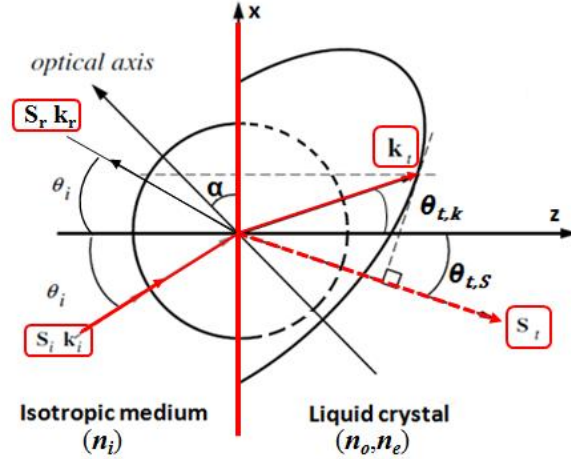
5.3 Light trajectories for planar director field

In this subsection, we consider planar director field $\hat{n}=(n_x, n_y, 0)$; the wave-vector and polarization of light are also confined to the same (x, y) plane. We first discuss light refraction at the cylindrical interfaces with (isotropic) medium adjacent to the LCMM shell.

(5.3.1.) Refraction at the interface between isotropic and anisotropic medium

Refraction at an interface of two different isotropic media is described by the Snell's law, that is based on the condition that the tangential components of wavevectors on the two sides of the interface are equal to each other [50]. The time averaged Poynting vector for the transmitted light, which defines the actual direction of the energy flow of the light, has the same direction as the transmitted wavevector. When light with an angle of incidence θ_i experiences refraction at the interface between an isotropic and an anisotropic medium, the directions of wave vector k_t and Poynting vector S_t for the transmitted light would be generally different, $\theta_{t,k} \neq \theta_{t,S}$, Fig.27.

Figure 27. Refraction at the isotropic-anisotropic media interface. The incident beam is polarized in the plane of the figure. The wave vector surfaces are shown as a solid circle for isotropic medium, as a solid ellipse for the extraordinary wave, and as a dashed circle for the ordinary wave in the anisotropic medium.



As shown in refs. [51,52] if the uniaxial medium has the optic axis tilted by an angle α with respect to the interface, and a plane incident wave is linearly polarized in the xz plane, these two angles, measured with respect to the z-axis (normal to the interface) in Fig.27, write

$$\theta_{t,k} = \tan^{-1} \left(\frac{2bn_i \sin \theta_i}{\sqrt{(c^2 - 4ab)n_i^2 \sin^2 \theta_i + 4b} - cn_i \sin \theta_i} \right); \quad (26)$$

$$\theta_{t,s} = \tan^{-1} \left(\frac{(4ab - c^2)n_i \sin \theta_i}{2b\sqrt{(c^2 - 4ab)n_i^2 \sin^2 \theta_i + 4b}} + \frac{c}{2b} \right);$$

where $a = \frac{1}{n_e^2 n_o^2} (n_o^2 \sin^2 \alpha + n_e^2 \cos^2 \alpha)$, $b = \frac{1}{n_e^2 n_o^2} (n_o^2 \cos^2 \alpha + n_e^2 \sin^2 \alpha)$, $c = \frac{1}{n_e^2 n_o^2} (n_o - n_e) \sin(2\alpha)$.

The reflection coefficient in this case can be written in the form[53]

$$r = \frac{n_i \sqrt{n_r^2 - n_i^2 \sin^2 \theta_i} - n_e n_o \cos \theta_i}{n_i \sqrt{n_r^2 - n_i^2 \sin^2 \theta_i} + n_e n_o \cos \theta_i} \quad (27)$$

where $n_r = \sqrt{n_o^2 + (n_e^2 - n_o^2) \sin^2 \alpha}$. Total reflection happens at the interface when the absolute value of r equals 1. In what follows, we use equation (26) to describe light propagation through the LCMM cylindrical shell. In some cases, such as a planar director field within the shell, the trajectories can be found analytically; this case is treated below.

(5.3.2) Light propagation through the LCMM bulk with planar director.

Propagation of light in an isotropic medium is described by Fermat's principle, stating that the trajectory of light between two points A and B corresponds to a minimum of time spent to travel, which is the product of the physical length and the refractive index, $\int_A^B N_r ds \rightarrow \min$ [36], where the refractive index N_r might vary in space. To describe an anisotropic medium, we follow Joets and

Ribotta [54] and Satiro and Moraes[42,43], who interpreted the Fermat's principle through geodesics in Finsler geometry. The Finsler geometry considers a line element of the trajectory as being dependent not only on the location but also on the orientation,

$$ds = F(x, \dot{x})dt, \quad (28)$$

where $F(x, \dot{x})$ is the Finslerian function, x and $\dot{x} = dx/dt$ are the space coordinates and its derivative with respect to the line element parameter t , respectively. In geometric optics for anisotropic medium, Finslerian function reads

$$F(x, \dot{x}) = N_r \cdot \|\dot{x}\| \quad (29)$$

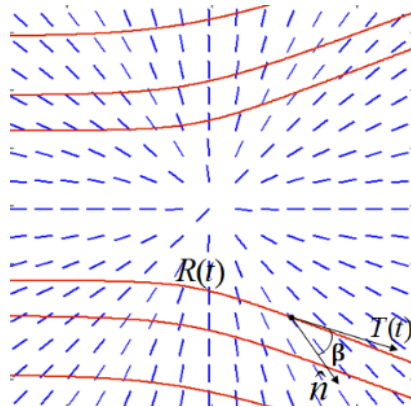
where $\|\dot{x}\| = \sqrt{\dot{x}^T \cdot \dot{x}}$ is the ordinary distance from the origin to the point $\dot{x}$ and $\dot{x}^T$ is the transpose of vector $\dot{x}$. $N_r = \sqrt{n_o^2 \cos^2 \beta + n_e^2 \sin^2 \beta}$ is the refractive index for the extraordinary ray, associated with the energy velocity, and β is the local angle made by wave vector and Poynting vector.

We study the extraordinary light propagation in LCMM with a planar director field. The wavevector and polarization of the propagating light are confined to the same plane. The director configuration is given by $\hat{n} = (\cos \phi, \sin \phi, 0)$ in Cartesian coordinates, Fig28. The light trajectory is $\mathbf{R}(t) = r \cos \phi \hat{x} + r \sin \phi \hat{y}$, combining the cylindrical coordinates r and ϕ with the Cartesian basis $\{\hat{x}, \hat{y}\}$. Then $\mathbf{T}(t) = d\mathbf{R}/dt$ is the tangential vector to the light path at each position parameterized by t ; the angle β is calculated from the formula $\cos \beta = \mathbf{T} \cdot \hat{n} / \|\mathbf{T}\|$. The path of light ray minimizes the “distance” $\int ds$, which leads to an interpretation of the light paths as a geodesic in the Finsler space[42,43,54,55],

$$\frac{d^2 x^i}{dt^2} + \sum_{j,k} \Gamma_{jk}^i \frac{dx^j}{dt} \frac{dx^k}{dt} = 0 \quad (30)$$

where t is the ray parameter along the geodesic and Γ_{jk}^i are Christoffel symbols; i, j and k are the indices representing different components of the spatial coordinates x .

Figure 28. Illustration of the light path $\mathbf{R}(t)$ in 2D liquid crystal director field, its tangential vector $\mathbf{T}(t)$ and the director $\hat{n}$ of liquid crystal.



In the cases of interest in this work, the geodesic equations (30) transform into the coupled ordinary differential equations in the cylindrical coordinates[43]

$$\begin{aligned}\frac{d^2 r}{dt^2} - \gamma^2 r \left(\frac{d\phi}{dt} \right)^2 &= 0 \\ \frac{d^2 \phi}{dt^2} - \frac{2}{r} \frac{dr}{dt} \frac{d\phi}{dt} &= 0\end{aligned}\tag{31}$$

with the solutions

$$\begin{aligned}r(t) &= \sqrt{\frac{C^2}{2E\gamma^2} + 2E(t+D)^2} \\ \phi(t) &= \frac{1}{\gamma} \arctan\left(\frac{2E\gamma(t+D)}{C}\right) + F\end{aligned}\tag{32}$$

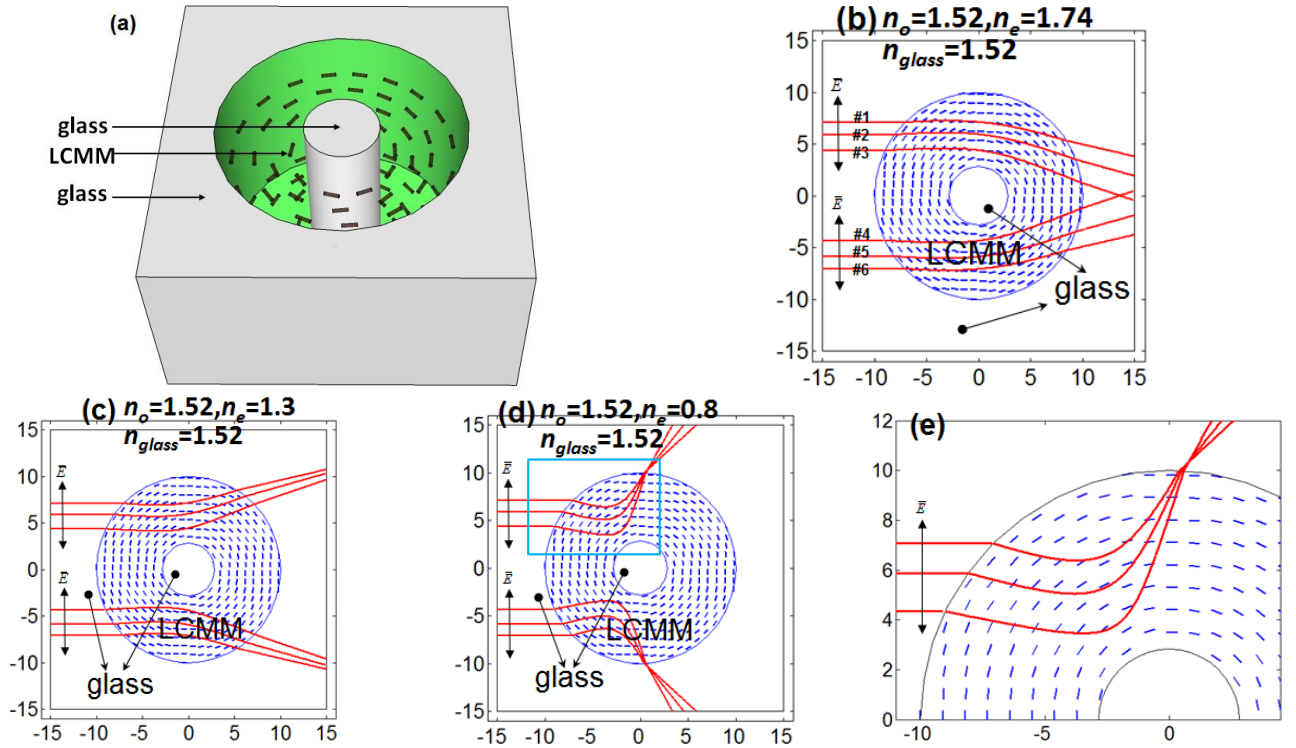
where C, D, E and F are integration constants, which can be obtained by the boundary condition, such as the position and direction of the incident light ray, and $\gamma = n_e/n_o$. The expressions are the same as those derived by Satiro and Moraes[43] with the difference that the first term in the expression for $\rho(t)$ is written as $C^2/E\gamma^2$ in ref [43] and our calculations show this term as $C^2/2E\gamma^2$.

(5.3.3) Light trajectory through a cylindrical shell with planar director

Using the rules of light refraction at the interface of isotropic-anisotropic media and light propagation in anisotropic medium as discussed above, using equations (26) and (32) we can find analytically the light trajectories for the structure shown in Fig.29(a), a cylindrical shell filled with a LCMM that has a circular director configuration, stabilized by the so-called in-plane planar surface anchoring at the two bounding cylindrical surfaces. The two adjacent media are both isotropic of the same refractive index 1.52 (glass). The values of the refractive indices are controlled by the composition of the LCMM. The wavevector of the propagating light is confined to the plane determined by the director. The polarization state of the incident light is also in the plane of the director field, Fig.29 (b-e). For the pure LC (no added NRs), the refractive indices are 1.74 and 1.52 for the extraordinary and ordinary waves, respectively. In this case, the incident parallel light beams bend towards the center, Fig.29 (b). For example, for beam No.1 in Fig.29 (a), the incident angle θ_i is 0.785; the refraction angle is $\theta_{t,s} = 0.853$ as follows from equation (26); the integration constants (C, D, E, F) in equation (32) are calculated as (-5.852 -7.551 0.439 1.297). The beam propagates through the LCMM-glass interface following equation (32) and exits from the LCMM at the point (8.371 5.470) under the angle (-0.785).

By adding NRs to the mixture, one effectively decreases n_e , but n_o changes little because the response of the NR to the electric field oriented normal to the NR is small, and at low volume fraction of Au NRs it can be neglected. For example, $n_e = 1.3$ if the LC is doped with the Au NRs (diameter 15nm, length 60nm) of volume fraction 0.041. In this case, birefringence is negative and the incident light beams bend away from the center, Fig.29 (c). Two external focusing points are obtained when the volume fraction of the Au NRs is 0.057 and $n_e = 0.8$. The incident parallel light beams bend away from the center and form two focusing spot outside the LCMM cylinder, which can be used in light concentrator for solar application.

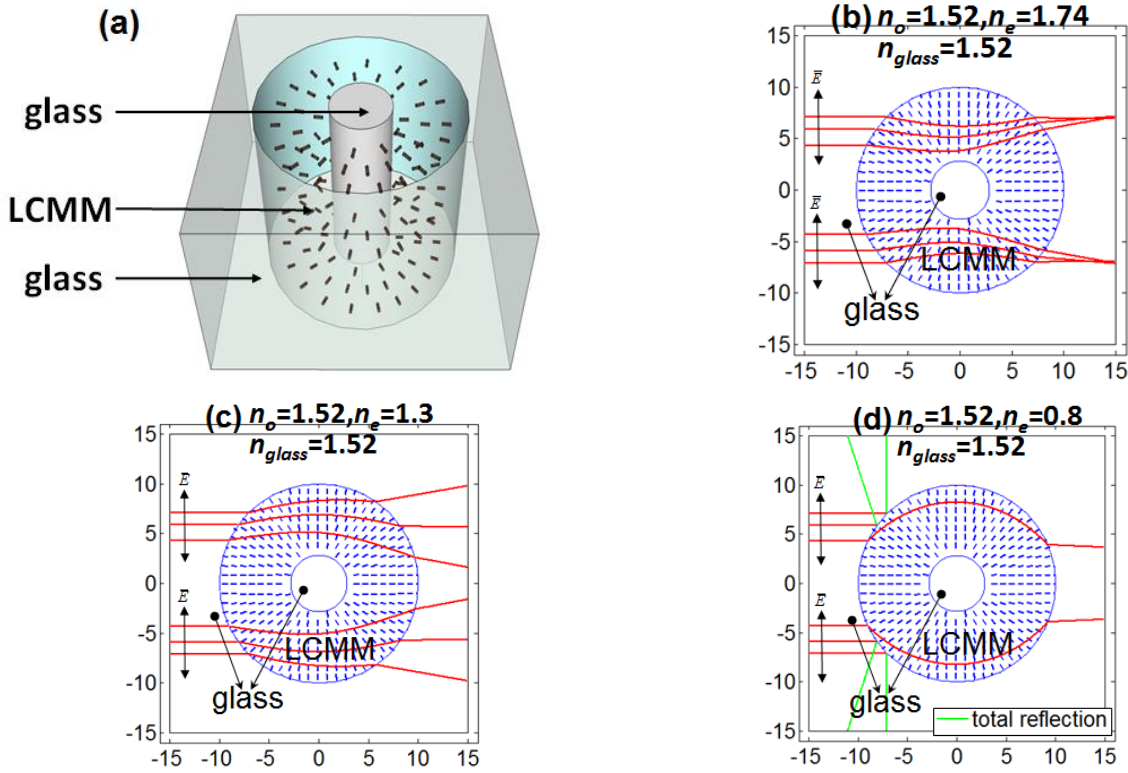
Figure 29. Light trajectory simulation of LCMM cylindrical shell sample in circular director field with different refractive indices (b) $n_o=1.52$, $n_e=1.74$; (c) $n_o=1.52$, $n_e=1.3$; (d) $n_o=1.52$, $n_e=0.8$. (e) Magnified image of rectangular area in (d). (a) illustrates the 3D structure of LCMM cylindrical shell sample. Here, we neglect the partial reflection at the glass-LCMM interface. Six parallel light rays are incident on the cylindrical shell sample from the left. Light refraction at the glass-LCMM interface and light propagation in LCMM can be calculated using equation (26) and equation (32), respectively. For example, four parallel beams(#1, #2, #3, #4, #5, #6) incident on glass-LCMM interface in Fig28 (a) at the positions $(-7.071 \ 7.071)$, $(-8.090 \ 5.878)$, $(-9.010 \ 4.339)$, $(-9.010 \ -4.339)$, $(-8.090 \ -5.878)$, $(-7.071 \ -7.071)$ and with a refractive angle $\theta_{i,s}$ 0.847, 0.688, 0.499, -0.499, -0.688, -0.847, respectively. The integration constants (C, D, E, F) in equation (31) for light rays propagation in LCMM medium are calculated as $(-5.852 \ -7.551 \ 0.439 \ 1.297)$, $(-4.960 \ -8.4730 \ 0.456 \ 1.276)$, $(-3.737 \ -9.244 \ 0.475 \ 1.258)$, $(3.737 \ -9.244 \ 0.475 \ 4.295)$, $(4.960 \ -8.473 \ 0.456 \ 4.274)$, $(5.852 \ -7.551 \ 0.439 \ 4.256)$, respectively. Finally, light beams propagate through the LCMM-glass interface at the position $(8.371 \ 5.470)$, $(9.286 \ 3.710)$, $(9.883 \ 1.524)$, $(9.883 \ -1.524)$, $(9.286 \ -3.710)$, $(8.371 \ -5.470)$, and with a refractive angle 0.785, 0.628, 0.448, -0.448, -0.628, -0.785, respectively.



The director of LCMM can be reconfigured from a circular configuration to a radial and visa versa, say, by changing the surface anchoring direction. Figure 30 shows in-plane polarized light beams propagating in this LCMM shell structure with radial director field. The refractive indices are controlled by the composition of the LCMM. As compared to the circular director field in Fig.29, the simulated results are completely different. For the pure LC with $n_e=1.74$ and $n_o=1.52$, the incident

parallel light beams focus at two spots, Fig.30 (b). When n_e is reduced to 1.3 while n_o remains the same, the parallel light beams are diverged by the LCMM shell, Fig.30 (c). When $n_e=0.8$, some of the incident beams (those that are further away from the center) are totally reflected at the glass-LCMM interface, Fig.30 (d).

Figure 30. Light trajectory simulation of LCMM cylindrical shell sample in radial director field with different refractive indices (b) $n_o=1.52$, $n_e=1.74$; (c) $n_o=1.52$, $n_e=1.3$; (d) $n_o=1.52$, $n_e=0.8$. Here, we neglect the partial reflection at the glass-LCMM interface. We only take into account the total reflection and refraction at the interface. (a) illustrates the 3D structure of LCMM cylindrical shell sample.



6. Conclusions

The experiments above demonstrate that a non-uniform electric field applied to a colloidal dispersion of submicron Au NRs is capable of concentrating the particles in the region of maximum field and also of aligning them parallel to the field lines. This field-induced “liquid crystalline metamaterial” is characterized by a gradient refractive index for polarized light and nonuniform configuration of the optic axis. We thus demonstrate that the approach based on dielectrically controlled dispersions of metal nanorods in dielectric fluids can serve as a broad platform for the development of future complex metamaterial architectures with unique features of electric switching and reconfigurability. In the cylindrical sample, the experiment reproduces the conceptual geometry of the theoretical cloak [12], as the optical axis is directed along the radial directions and the refractive

index increases as one moves from the centre of the cylinder to the periphery. The difference is that the experimentally achieved modulation of the refractive index is modest, about 0.05-0.1. Ideally, an efficient metamaterial would have a modulation in the refractive index that is about one order of magnitude higher than the level demonstrated in this work. There are a few different ways to enhance the performance. The first factor to improve is the volume fraction η_U of the NRs condensed by the gradient electric field. Our experiments reached $\eta_U = 0.02$. To obtain $n_{\parallel} = 0$, according to Equation (22), one needs to increase η_U by one order of magnitude. This appears to be achievable, if one considers the close packing of NRs with not very thick (a few nanometers) aggregation-preventing coatings. Furthermore, the efficiency can be increased by replacing Au with other materials, such as silver (Ag). As shown in reference [12], for Ag NRs, the filling factor producing a zero refractive index is only 0.125, which is within the reach of the proposed dielectrophoretic approach. Depending on the wavelength of the intended application, other materials might be more efficient, as discussed by Boltasseva and Atwater [38]. The shape of NRs can also be modified to maximize the modulation of the optical properties. For example, as shown by Park *et al.* [39], the metallic NRs dispersed in dielectric fluids (water) can be reversibly assembled either side-to-side or head-to-head, which would control the position of the plasmonic resonances and increase η_U . Using a liquid crystal (thermotropic or lyotropic) instead of the isotropic fluid as a dispersive medium can also help in optimizing the proposed reconfigurable metamaterial and enrich the means of structural control.

One of the problems in the development of metamaterials is substantial losses due to absorption. The problem can be addressed by adding gain materials such as fluorescent dyes [40,41]. This approach should be fully compatible with the proposed metamaterial, as the fluorescent dyes are solvable in dielectric fluids, either water-like, or oil-like.

The main attractive feature of the proposed approach to use metal nanoparticles in dielectric fluids subject to the gradient electric field is in the opportunity to control the optical properties from point to point in space and time. We considered only a radial configuration of the AC electric field. A dielectrophoretic force can also be created in other electrode geometries [27] and by variations in the field phase [20]. It would be of interest to supplement the dielectrophoretic mechanism with effects such as electrophoresis [20]. The electrophoretic force depends on the electric charge on the nanoparticle and is typically linear in the magnitude of the field [20]. A specific case of the electrophoretic effect, called an “induced charge electrophoresis” [42], is also known for non-symmetric particles. All these mechanisms should add new dimensions to the proposed reconfigurable metamaterials, as they would allow one a better control of nanoparticles. Note that the radial pattern of NRs described in this work is not the only one of interest. For example, simply reversing the concentration gradient of NRs in radial geometry would allow one to switch the metamaterial from the “cloaking” regime to “optical black hole” collector of light [4]. To conclude, two light wave-manipulation devices were proposed with LCMM--light beam bends and cloak invisibility, which demonstrated that LCMM offers a way to control light. It was explained how a reasonable design of beam bends can be realized with LCMM by using light trajectory simulation method. Moreover, an optical cloaking device based on LCMM with spatially distorted optic axis was presented. The simulation results showed effective invisibility of the central metal electrode.

The main attractive feature of the proposed LCMM is that the liquid crystal can align the metallic NRs in the confined geometry. By changing the surface anchoring direction or applying an electric field, LC together with NRs can be realigned, which enriches the reconfigurable states of the LCMM in the confined geometry. We considered only zero-pretilt surface anchoring condition in the cylindrical capillary structure. Different director configurations of LCMM in other confined structure can also be created with pretilt anchoring condition[56], and by variations of electric field[57]. These studies are currently in progress.

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