

SOLID STATE LI-ION BATTERIES

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1 SUMMARY

Over the last one year, we have worked on an all-solid-state Li-ion battery and demonstrated a specific energy of 225 mWh g^{-1} based upon the combined mass of both the composite anode and cathode. To realize this full cell, we pair an iron sulfide and sulfur composite cathode with a Si-based anode. The anode active material is a Si-Ti-Ni alloy with good ionic and electronic conductivity that attains a stable specific capacity of 400 mAh g^{-1} based upon the total mass of the composite anode. To our knowledge, this is the highest stable Si-based all-solid-state anode specific capacity reported to date. To utilize both a lithium free anode and cathode, we adopt a pre-lithiation technique involving stabilized lithium metal powder. This is the first time that this technique has been demonstrated in an all-solid-state battery.

2 INTRODUCTION

Bulk all-solid-state batteries made with mechanochemically prepared $\text{Li}_2\text{S-P}_2\text{S}_5$ glass-ceramic electrolytes (1-3) are a safe alternative to conventional Li-ion batteries because sulfide based glass-ceramic electrolytes are pure ionic conductors, non-volatile, non-flammable, and stable versus lithium metal. However, the use of lithium metal anodes in all-solid-state batteries (ASSBs) is not straightforward because dendritic lithium can penetrate porous cold-compacted glass-ceramic electrolyte separators. To demonstrate this point, an interfacial instability that was observed by a previous study may be better characterized as an internal short (4). To improve cell cycleability and survivability a recent study has demonstrated that the vapor deposition of thin lithium films onto $\text{Li}_2\text{S-P}_2\text{S}_5$ glass-ceramic solid-state electrolyte (SSE) pellets can improve electrolyte-lithium electrode interfacial contact (5). However, the conservative cycling parameters used in this study preclude making a conclusion on the viability of all-solid-state lithium metal anodes.

To sidestep the difficulties associated with lithium metal anodes, many ASSB studies utilize an InLi alloy (6, 7). Unfortunately, indium is not a practical anode option because of its high cost. Other ASSB studies utilize a variety of anodes like FeS_2 (8, 9), FeS (10), nano-Si (11-13), $\text{Li}_4\text{Ti}_5\text{O}_{12}$ (14-17), graphite (18, 19), $\text{Li}_{4.4}\text{Ge}_x\text{Si}_{1-x}$ (20), $\alpha\text{-Fe}_2\text{O}_3$ (21) and Sn-based glasses like $\text{SnO-Br}_2\text{O}_3$ (22) or $\text{SnS-P}_2\text{S}_5$ (23). FeS_2 , FeS , $\text{Li}_4\text{Ti}_5\text{O}_{12}$, $\alpha\text{-Fe}_2\text{O}_3$, and Sn-based glasses all have average operating voltages that are too high to make them useful as anodes while Ge is too expensive to make $\text{Li}_{4.4}\text{Ge}_x\text{Si}_{1-x}$ alloys practical. FeS_2 has such a high potential that it is better suited as a cathode. Our previous work has shown that FeS_2 's full potential will only be realized if it is used as a cathode (24). In that work, a FeS_2 cathode was paired with a lithium metal anode, however, the survivability of the test cells was diminished by the occasional internal short.

Except for the fact that they are lithium free, graphite and Si are ideal anode candidates to be paired with FeS_2 because they have low operating potentials (< 0.5 V vs. Li^+/Li). Unfortunately, the specific capacities of graphite or Si all-solid-state anodes have not achieved acceptably high values. For effective comparison, specific capacities in this paper are often presented with respect to the total composite electrode mass rather than with respect to only active material mass. For clarity, specific capacities based on active material mass are denoted by (active), while specific capacities based on total electrode mass are denoted by (cathode), (anode), or (electrode). Specific capacity or specific energy is denoted by (cathode + anode) when both electrodes of a full cell are considered. Solid-state graphite anodes have been reported with specific capacities of about 200 mAh g^{-1} (electrode) (18), but further improvement is limited by graphite's relatively low theoretical capacity of 372 mAh g^{-1} (active). At room temperature Si has a specific capacity that is an order of magnitude larger than that of graphite's, but Si's insulating nature limits its mass loading in an all-solid-state electrode. The poor solid-solid interfacial contact between SSE particles and active material particles severely hinders ionic transport to Si. For good reversibility and a high degree of Si utilization, all-solid-state Si-based anodes must be composed predominately of electronically conducting diluent and SSE. In our previous studies with Si-based all-solid-state anodes, we studied electrodes with a 1:5:1 weight ratio of Si, SSE, and conducting additive, respectively (11-13). Due to the poor mass loading of Si, these Si-based all-solid-state anodes could only achieve a stable specific capacity not much greater than 200 mAh g^{-1} (electrode).

To increase the active material mass loading of Si-based all-solid-state anodes, it is best to improve the ionic and electronic conductivity of the active material. Our recent development and characterization of a Si-Ti-Ni (STN) ternary alloy for commercial Li-ion cells suggest that this material would be ideally suited as an active material for Si-based all-solid-state anodes (25). The STN alloy has a microstructure of nano-Si particle domains embedded in an electrochemically active $\text{Ti}_4\text{Ni}_4\text{Si}_7$ matrix. During the initial lithiation of the STN alloy, the matrix irreversibly takes up some Li^+ to become a mixed conductor with a composition of approximately $\text{Li}_{3.2}\text{Ti}_4\text{Ni}_4\text{Si}_7$ and an ionic conductivity of $2.0 \times 10^{-5} \text{ S cm}^{-1}$. We apply the STN alloy to an all-solid-state battery because the $\text{Li}_x\text{Ti}_4\text{Ni}_4\text{Si}_7$ matrix provides fast ionic conduction to the embedded nano-Si particles. We report that an all-solid-state STN anode achieves a stable specific capacity of 405 mAh g^{-1} (electrode) which is over double the baseline of 200 mAh g^{-1} (electrode) set by the previously mentioned graphite and Si-based solid-state anodes.

To realize a full cell, we pair our STN composite anode with our previously described iron sulfide and sulfur ($\text{FeS} + \text{S}$) cathode (26). The pairing of a lithium free $\text{FeS} + \text{S}$ cathode and a lithium free STN anode presents an easily overcome obstacle. Our Li_3N decomposition pre-lithiation technique is not appropriate for conversion materials or for anodes with operating voltages less than $0.44 \text{ V vs. Li}^+/\text{Li}$ (27) so we adopt a lithiation technique utilizing stabilized lithium metal powder (SLMP). Previously, this method had only been demonstrated in conventional liquid cells (28, 29).

3 METHODS, ASSUMPTIONS, AND PROCEDURES

All cell fabrication and testing for this study was carried out under an inert Argon gas environment. The glass electrolyte used in this study is the previously described $77.5\text{Li}_2\text{S}:22.5\text{P}_2\text{S}_5$ glass SSE (12). The FeS + S cathode was prepared by mechanochemically combining FeS and S precursors with the glass SSE (26). The pre-lithiated Si-Ti-Ni (STN) alloy anode was fabricated in a two- step process. First, STN powder (MK electron, 66 at. % Si, air jet milled) (25), SSE, and carbon black (TimCal, C65) were mixed with an agate mortar and pestle in a ratio of either 7:3:0 or 7:3:2, respectively. Stabilized lithium metal powder (SLMP, FMC Lithium Corp., LECTRO MAX powder 100) was then combined with the 7:3:2 composition STN anode powder via vortex mixing (Vortex Genie 2) in a weight ratio of 1 to 5.21, respectively.

To measure the electronic conductivity of the STN matrix, $\text{Ti}_4\text{Ni}_4\text{Si}_7$ and $\text{Li}_{3.2}\text{Ti}_4\text{Ni}_4\text{Si}_7$ were prepared as described elsewhere (25). A potential sweep was then applied to cold-compacted pellets of $\text{Ti}_4\text{Ni}_4\text{Si}_7$ and $\text{Li}_{3.2}\text{Ti}_4\text{Ni}_4\text{Si}_7$ with Ti current collectors. The shell of our all-solid-state batteries is a titanium-polyaryletheretherketone (PEEK) test cell die (Figure 1). To fabricate each cell, the glass SSE powder was compressed to 1 metric ton inside the Ti-PEEK die to form the separator pellet. 5 mg of the FeS + S cathode powder and 8.36 mg of the pre-lithiated STN anode powder were then cold-pressed to opposite sides of the glass electrolyte pellet with 5 metric tons force. All cells were cycled under constant current constant voltage (CCCV) conditions using an Arbin BT2000 battery tester at 60°C . In this report, charge and discharge refer to the lithiation and delithiation of the STN alloy, respectively. Materials were characterized by field emission scanning electron microscopy (FESEM, JEOL JSM-7401F), energy dispersive spectroscopy (EDS) and Cu-K α X-ray (XRD) measurement.

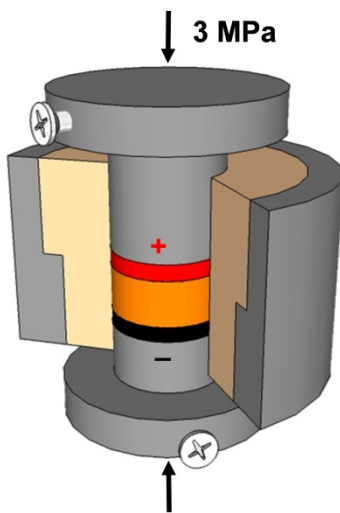


Figure 1. Schematic for our all-solid-state Li-ion battery test dies. The glass electrolyte separator pellet and composite electrodes are cold-pressed sequentially between two Ti plunger-shaped current collectors inside a PEEK-lined Ti die. Cells are cycled under an applied pressure of 3 MPa

4 RESULTS AND DISCUSSION

STN composite electrodes with and without carbon black were electrochemically characterized vs. a lithium counter electrode. Figure 2 presents the cycling data for the 7:3 and 7:3:2 weight ratio composite electrode compositions of STN:SSE and STN:SSE:carbon black, respectively. It was found that the addition of carbon black dramatically improves cell reversibility. The STN electrode with carbon black achieves a 1st cycle discharge (delithiation)

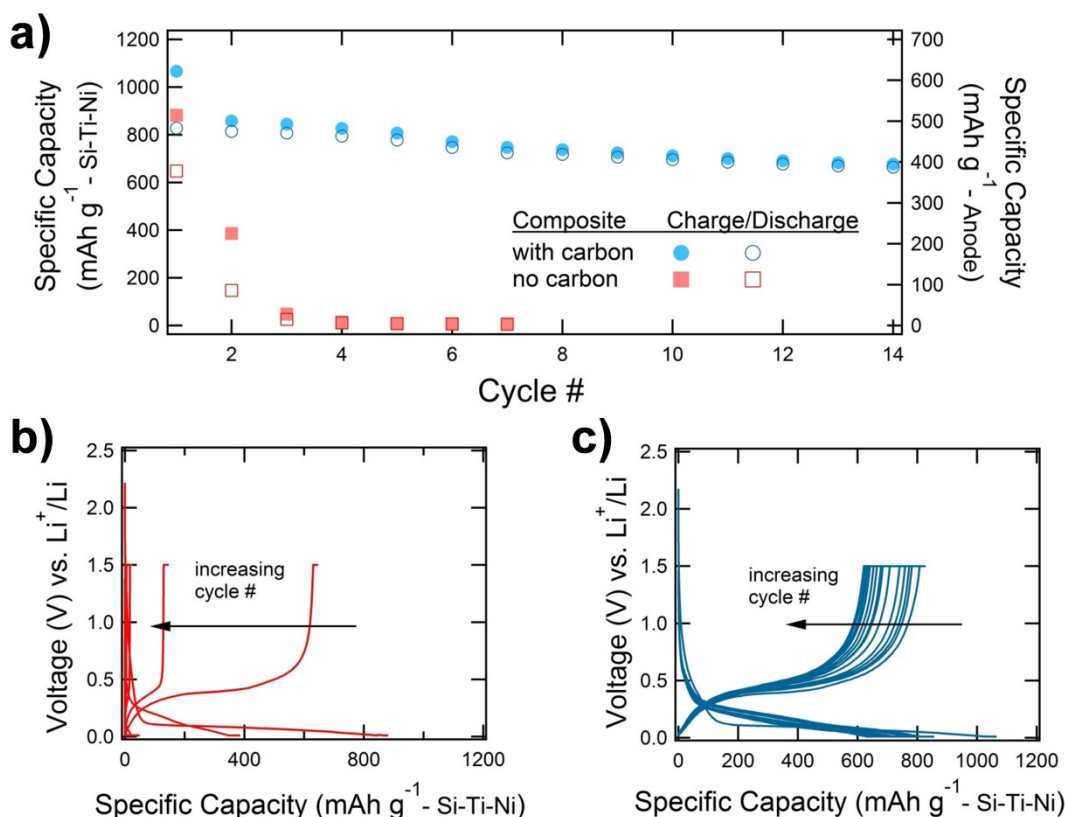


Figure 2. (a) Cyclic stability of STN electrodes without carbon black (red square) and 16.7 weight % carbon black (blue circle). Charge refers to the lithiation of the STN alloy while discharge refers to the delithiation of the STN alloy. (b) Voltage profiles for the STN electrode without carbon black. (c) Voltage profiles for the STN electrode with 16.7 weight % carbon black

specific capacity of 483 mAh g⁻¹ (electrode) and a 10th cycle discharge (delithiation) specific capacity of 405 mAh g⁻¹ (electrode). These numbers correspond to an active material specific capacity of 828 and 695 mAh g⁻¹ (active) for the 1st and 10th cycles, respectively. This same electrode also has a Coulombic efficiency that improves rapidly from 77.7% on the first cycle to 98.2% by the 10th cycle. The cell then failed with an internal short on the 15th cycle and no further data was recorded. Our previous liquid STN half cell exhibited a first cycle Coulombic efficiency of 87.7% (25). The all-solid-state half cell has a lower Coulombic efficiency because

the all-solid-state cell's comparatively larger amount of carbon black may have induced more side reactions during the initial charge cycle.

To explain why the addition of carbon black improves STN's cycleability, the electronic conductivity of the STN matrix was tested before and after lithiation. Ionic conductivities of the STN matrix were previously measured (25). The $\text{Ti}_4\text{Ni}_4\text{Si}_7$ matrix has a negligible ionic conductivity and an electronic conductivity of 10 S cm^{-1} . After electrochemical activation, the $\text{Li}_{3.2}\text{Ti}_4\text{Ni}_4\text{Si}_7$ matrix's ionic conductivity increases to $2.0 \times 10^{-5} \text{ S cm}^{-1}$ but its electronic conductivity decreases two orders of magnitude to 0.24 S cm^{-1} . The decrease in the matrix's electronic conductivity explains why the STN composite electrode without carbon black could achieve a high initial capacity, but suffered from rapid capacity fade in subsequent cycles. Our previous studies with nano-Si required a nano-Si:SSE:conducting additive ratio of 1:5:1 (11, 12). Because the $\text{Li}_x\text{Ti}_4\text{Ni}_4\text{Si}_7$ matrix is a mixed conductor, the active material to carbon black mass ratio is increased from 1 to 3.5 and the active material to SSE mass ratio is increased from 0.2 to 2.33 over those previous studies.

Figure 3a presents the FESEM characterization of the uncompressed 7:3:2 weight ratio composite electrode powder. From this micrograph, it is evident that the composite electrode is comprised primarily of particles ranging from 1 to 6 microns in diameter. Figure 3b presents the elemental mappings for Si (red) and S (blue) overlaid on the accompanying FESEM micrograph. As expected, elemental mappings of Si and S are largely segregated to separate particles. Si rich particles are identified as STN particles, while S rich particles are identified as SSE particles. It is evident that the size of the STN particles is well matched to that of the sulfide glass SSE particles. Figure 3c presents the elemental mapping of C (green) overlaid on the same FESEM micrograph. We find that the carbon black particles are well dispersed throughout the composite electrode powder for good electronic transport to accommodate the decrease in the STN's electronic conductivity after the first cycle.

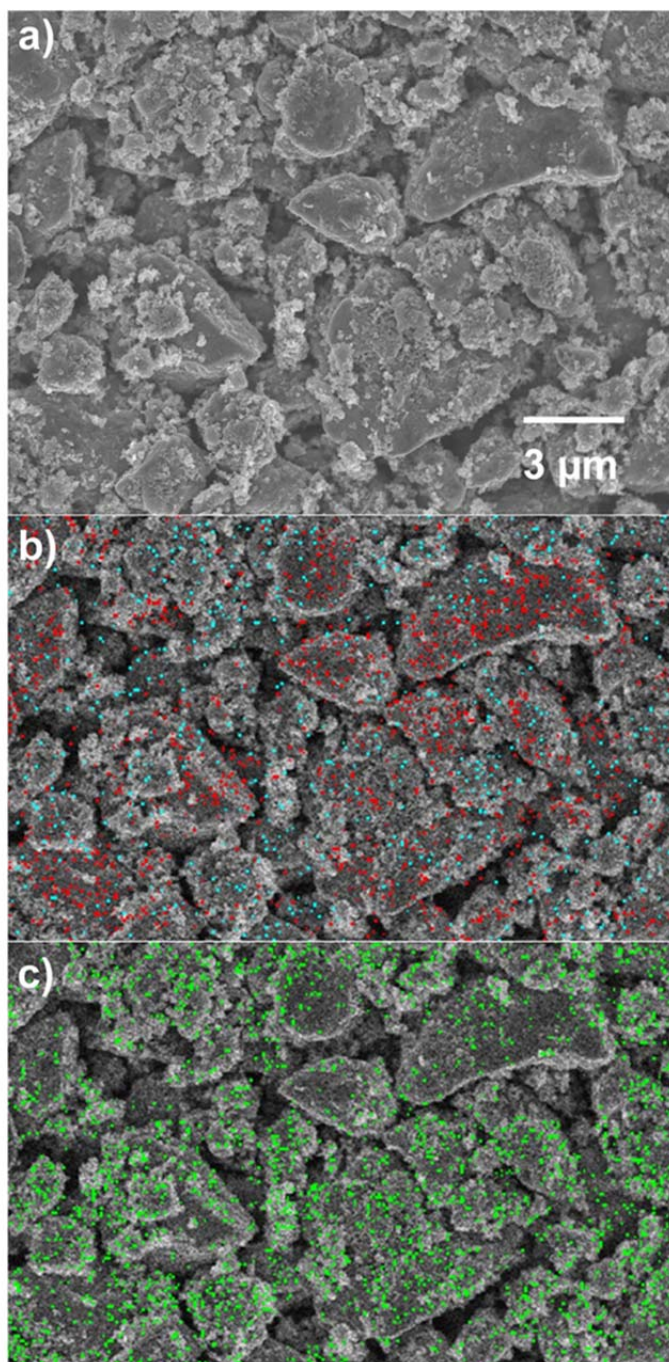


Figure 3. (a) FESEM micrograph of an uncompressed STN electrode. (b) Elemental mappings of Si (red) and S (blue) which demonstrate size compatibility of glass SSE and STN particles. (c) Elemental mapping of C (green) demonstrating good dispersion of carbon black

The next step of this study was to pair the optimized solid-state STN anode with a FeS_2 cathode. As a substitute for FeS_2 , we instead utilize a recently developed mechanochemically prepared $\text{FeS} + \text{S}$ composite active material (26) because all-solid-state electrodes made with this material can achieve higher overall specific capacities. The electrochemical characterization of a all-solid-state $\text{FeS} + \text{S}/\text{Li}$ half cell cycled at 60°C is provided in Figure 4 as a reference to the reader. The $\text{FeS} + \text{S}$ composite active material has the same theoretical capacity as FeS_2 but can be synthesized much more readily from inexpensive precursors. From Figure 4 it is observed that the capacity of a $\text{FeS} + \text{S}$ composite electrode quickly exceeds its theoretical value of 900 mAh g^{-1} (active) or 281 mAh g^{-1} (electrode). Excess capacity is provided by the electrochemical activation of inert Li_2S in the $77.5\text{Li}_2\text{S}:22.5\text{P}_2\text{S}_5$ glass electrolyte component of the composite electrode. The reversible electrochemical utilization of Li_2S in the SSE is facilitated by the good electronic conductivity of FeS as well as by the nano-size of $\text{FeS} + \text{S}$ particles. The rise, fall, and stabilization of the electrode's capacity is associated with a complex electrochemistry where the reduction of FeS , S , and electrochemically precipitated FeS_2 phases all occur concurrently. After 60 cycles, the $\text{FeS} + \text{S}$ composite electrode evolves a redox chemistry that is dominated by sulfur.

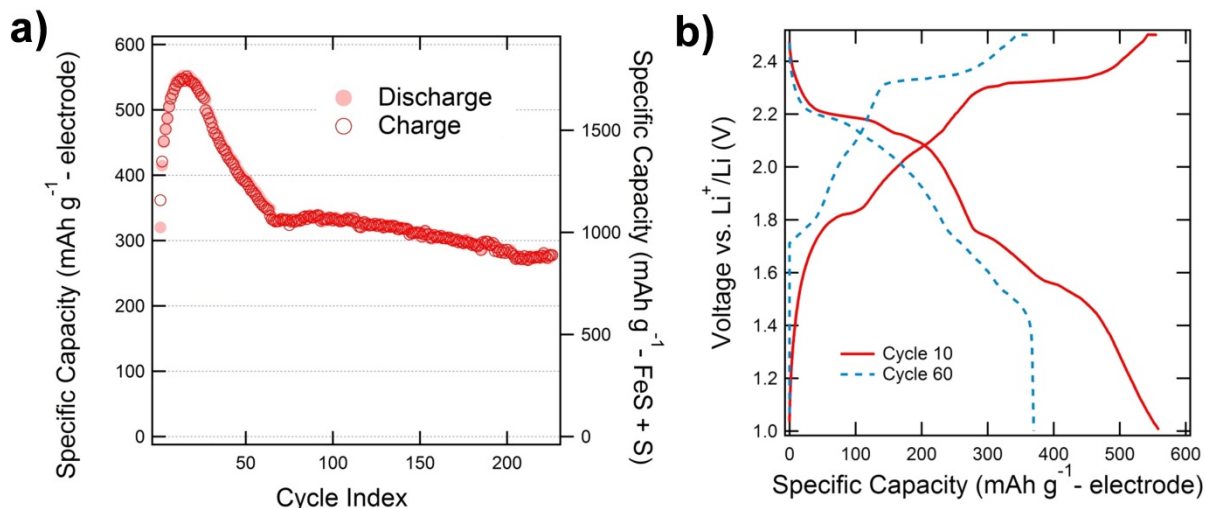


Figure 4. This figure presents the electrochemical characterization of the previously described $\text{FeS} + \text{S}$ composite electrode (26) which is used as the cathode in this study's full cell demonstration. (a) The cyclic stability of a $\text{FeS} + \text{S}/\text{Li}$ half cell. (b) The 10th and 60th voltage profiles of a $\text{FeS} + \text{S}/\text{Li}$ half cell

We adopted Jarvis et al.'s anode pre-lithiation technique (29) by incorporating SLMP into the uncompressed STN electrode powder (Figure 5a). During the cell's initial discharge the cathode is either lithiated by the direct oxidation of unreacted lithium metal or by the de-alloying of the pre-lithiated STN alloy. During subsequent cycles the cell behaves as a Li-ion battery. The cyclic stability of the $\text{FeS} + \text{S}/\text{STN}$ full cell is given in Figure 5b. The cell achieves a 1st cycle specific discharge of 295 mAh g^{-1} (cathode) which corresponds to a $\text{FeS} + \text{S}$ specific capacity of 944 mAh g^{-1} (active). This initial discharge capacity is close to the theoretical specific capacity of the $\text{FeS} + \text{S}$ active material and it is consistent with previous results presented in Figure 4 (26). As expected, the initial specific charge capacity rises dramatically to 383 mAh g^{-1} (cathode)

and the discharge voltage plateaus centered at 1.6V fade with extended cycling. Both of these results are also consistent with prior results. The increase in capacity is attributed to the electrochemical activation of excess Li_2S in the SSE component of the cathode (26, 30) and the fade of the lower voltage plateaus indicates that the sulfur redox chemistry comes to dominate the electrochemistry of the $\text{FeS} + \text{S}$ cathode. The activation of excess Li_2S also explains why the full cell's initial discharge profile is different from that of subsequent discharge profiles.

From the voltage profiles of this cell (Figure 5c), it is confirmed that the full cell functions as a Li-ion cell and not as a lithium metal cell because the average discharge potential of the full cell is depressed compared to that of a $\text{FeS} + \text{S}$ half cell (26). The full cell also has a much more stable capacity compared to that of either the individual STN half cell (Figure 2c) or the $\text{FeS} + \text{S}$ half cell (Figure 4). By the 100th cycle, the full cell maintains a specific discharge capacity of 355 mAh g^{-1} (cathode). When the mass of both composite electrodes are taken into account, the full cell delivers 225 mWh g^{-1} (anode + cathode) upon its 100th discharge.

The $\text{FeS} + \text{S}/\text{Li}$ and STN/Li half cells both behave much differently than the full cell. As discussed, the $\text{FeS} + \text{S}/\text{Li}$ half cell's capacity dramatically rises, falls, and stabilizes, while the 7:3:2 composition STN/Li half cell loses 34% of its capacity between its 1st and 10th charge (lithiation) cycles. The stability of the full cell can be explained by considering three points. First, an excess of SLMP is added to the STN composite anode powder to offset inefficiencies and improve cyclic stability (28). Second, the $\text{FeS} + \text{S}$ cathode's complex electrochemistry is uniquely capable of offsetting the initial Coulombic inefficiency and fade of Si-based anodes. The characteristic rapid rise of the $\text{FeS} + \text{S}$ cathode's capacity due to Li_2S activation in the SSE may help to offset losses from the STN anode. The result is a full cell with a stable capacity that does not rapidly rise like the $\text{FeS} + \text{S}/\text{Li}$ half cell or initially fade like the STN/Li half cell. And third, the STN anode in the full cell was not fully utilized. From Figure 5b and c it is evident that the STN anode in the full cell never achieves a specific capacity in excess of 240 mAh g^{-1} (anode). This specific capacity should be revised because the mass of the anode in the full cell now considers the 1.35 mg of SLMP added to pre-lithiate the cell. For this reason, the specific capacity is revised to 286 mAh g^{-1} (anode) for accurate comparison with the 405 mAh g^{-1} (anode) achieved by the 7:3:2 STN/Li half cell during its 10th charge (lithiation). Limiting the depth of Si lithiation has been shown to improve the cyclic stability of other Si-based anodes (31). By not fully utilizing the STN anode the same stabilization of capacity may be observed here as well. Incomplete utilization of the STN anode also suggests that further optimization of the full cell configuration may yield higher overall cell energy densities.

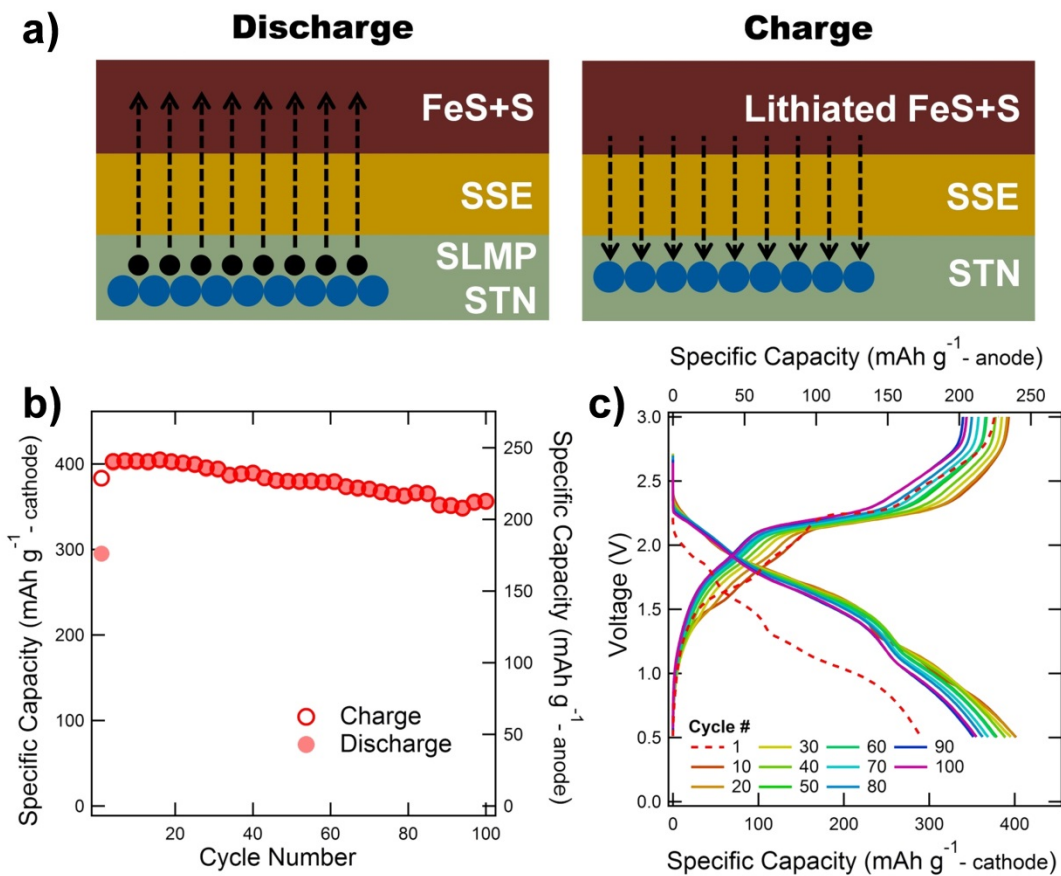


Figure 5. (a) Schematic of the lithiation mechanism. Prior to cell fabrication SLMP is combined with the STN composite anode powder via vortex mixing. (b) Cyclic stability of a full cell with a FeS + S cathode and a pre-lithiated STN anode. (c) Voltage profiles of the same full cell with respect to the mass of the cathode or anode

5 CONCLUSIONS

The Si-Ti-Ni (STN) alloy and Stabilized Lithium Metal Powder (SLMP) pre-lithiation technique were developed with conventional liquid Li-ion batteries in mind, but we find that both are also applicable to all-solid-state Li-ion batteries. STN is well suited as an all-solid-state anode active material because the $\text{Li}_x\text{Ti}_4\text{Ni}_4\text{Si}_7$ matrix of the STN alloy is a mixed conductor. All-solid-state STN composite anodes provide a stable specific capacity of 400 mAh g^{-1} (anode). For clarity, specific capacities based on active material mass are denoted by (active), while specific capacities based on total electrode mass are denoted by (cathode), (anode), or (electrode). To our knowledge, this is the highest stable Si-based all-solid-state anode specific capacity reported to date. To pre-lithiate an all-solid-state Li-ion battery we incorporated SLMP into the STN composite anode powder prior to cell fabrication. This is the first time that the SLMP pre-lithiation technique has been demonstrated in an all-solid-state battery. By pairing the pre-lithiated STN composite anode with a high capacity FeS + S cathode, an all-solid-state Li-ion battery with a specific energy of 225 mWh g^{-1} (cathode + anode) was demonstrated. The results of this study suggest that all-solid-state batteries can achieve acceptable energy densities without the need for a lithium metal anode. By avoiding the use of lithium metal anodes, the engineering challenges associated with the dendritic penetration of cold-compacted glass solid-state electrolyte (SSE) separators can be circumvented.

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LIST OF SYMBOLS, ABBREVIATIONS, AND ACRONYMS

ASSB	all-solid-state battery
CCCV	constant current constant voltage
EDS	energy dispersive spectroscopy
FESEM	field emission scanning electron microscopy
PEEK	Polyaryletheretherketone
SLMP	stabilized lithium metal powder
SSE	solid-state electrolytes
STN	Si-Ti-Ni
XRD	X-ray diffraction

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