

# Swash Zone Dynamics: Modeling and Data Analysis

Donald N. Slinn  
Department of Civil and Coastal Engineering  
University of Florida  
Gainesville, FL 32611-6590  
Phone: (352) 392-1436 x 1431 Fax: (352) 392-3466 E-mail: [slinn@coastal.ufl.edu](mailto:slinn@coastal.ufl.edu)

Award #: N00014-01-1-0152  
<http://www.ce.ufl.edu/people/faculty/alpha/slinn.htm>

## LONG-TERM GOALS

The goals of the work are to develop improved predictive capability for non-linear time-dependent dynamics in the swash zone. The work involves numerical computations, comparison with field and laboratory results, and theoretical analysis. The focus of the project is to quantify net onshore-offshore swash zone properties from Computational Fluid Dynamics (CFD) experiments and to compare model predictions with field and laboratory data to evaluate theoretical models of swash dynamics

## OBJECTIVES

1. Demonstrate capabilities of modeling non-linear interactions between incident and reflected waves on beaches using a Navier-Stokes model using the Volume of Fluid (VOF) method.
2. Conduct parameter studies, examining swash response (*e.g.*, bed shear stress, mean flow circulation, bore properties, run-up excursion length, *etc.*) to key physical parameters including beach foreshore slope, incident wave height, and wave frequency.
3. Develop a coupled fluid-sediment model to approximate sediment suspension and deposition and transport during swash events.
4. Interpret field data using insight gained from simulations with the VOF model.
5. Make a best attempt at simulating realistic swash zone events utilizing forcing conditions from observed time series of incident waves.
6. Examine model capabilities to test properties and predictions of simplified swash zone theoretical models.

## APPROACH

The work involves theoretical development, numerical computations, and comparison with field and laboratory results. Scientific understanding of swash zone dynamics has advanced primarily by careful field measurement of wave and beach interactions. We have introduced additional complexity to mathematical modeling of the swash zone by solving the time-dependent equations representing conservation of mass and momentum for the physical situation of water waves shoaling on a sloping beach. To this end we have adapted a two-dimensional Navier-Stokes solver for free-surface air-water

# Report Documentation Page

*Form Approved  
OMB No. 0704-0188*

Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.

1. REPORT DATE <b>30 SEP 2002</b>	2. REPORT TYPE	3. DATES COVERED <b>00-00-2002 to 00-00-2002</b>			
4. TITLE AND SUBTITLE <b>Swash Zone Dynamics: Modeling and Data Analysis</b>		5a. CONTRACT NUMBER			
		5b. GRANT NUMBER			
		5c. PROGRAM ELEMENT NUMBER			
6. AUTHOR(S)		5d. PROJECT NUMBER			
		5e. TASK NUMBER			
		5f. WORK UNIT NUMBER			
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) <b>Department of Civil and Coastal Engineering,,University of Florida,,Gainesville,,FL, 32611</b>		8. PERFORMING ORGANIZATION REPORT NUMBER			
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)		10. SPONSOR/MONITOR'S ACRONYM(S)			
		11. SPONSOR/MONITOR'S REPORT NUMBER(S)			
12. DISTRIBUTION/AVAILABILITY STATEMENT <b>Approved for public release; distribution unlimited</b>					
13. SUPPLEMENTARY NOTES					
14. ABSTRACT <b>The goals of the work are to develop improved predictive capability for non-linear time-dependent dynamics in the swash zone. The work involves numerical computations, comparison with field and laboratory results, and theoretical analysis. The focus of the project is to quantify net onshore-offshore swash zone properties from Computational Fluid Dynamics (CFD) experiments and to compare model predictions with field and laboratory data to evaluate theoretical models of swash dynamics</b>					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT <b>Same as Report (SAR)</b>	18. NUMBER OF PAGES <b>7</b>	19a. NAME OF RESPONSIBLE PERSON
a. REPORT <b>unclassified</b>	b. ABSTRACT <b>unclassified</b>	c. THIS PAGE <b>unclassified</b>			

flows based on the Volume of Fluid (VOF) methodology (Hirt and Nichols, 1981) appropriate for simulations of the swash zone. This model has several advantages compared to current state-of-the-art swash zone models such as Rbreak (*e.g.*, Raubenheimer *et al.*, 1995). Chief among these is the ability to represent non-linear breaking waves, depth dependency, and the ability to resolve the viscous bottom boundary layer, allowing estimates of the bed shear stress to be made. The model uses a control volume approach. The ability to handle a free surface is derived from allowing the control volumes to be full of water, empty (*i.e.*, air), or partially filled. Fluxes of water are calculated at each control surface interface. If the volume of fluid (VOF) is full, and its neighboring control volumes are also full, then the standard continuum approximation (the Navier-Stokes equations) are solved in fairly standard discretized form, *e.g.*,

$$\nabla \cdot \vec{V} = 0,$$

and

$$\frac{\partial \vec{V}}{\partial t} + \nabla \cdot (\vec{V}\vec{V}) = \frac{-1}{\rho} \nabla \cdot p + \frac{1}{\rho} \nabla \cdot \tau + \vec{g} + \frac{1}{\rho} \vec{F}_b$$

where,  $\rho$  is the fluid density,  $p$  is pressure,  $\tau$  is the viscous stress tensor,  $\vec{F}_b$  is a body force (*e.g.*, designed to force oncoming waves), and  $\vec{g}$  is the acceleration due to gravity. When a control volume is empty of fluid, then, of course, constant (atmospheric) pressure is assumed. When a control volume is partially full, or when its neighbors are partially full, the methodology becomes more complex and force balances including surface stresses and inertial forces are approximated (sometimes involving projectile motion).

## WORK COMPLETED

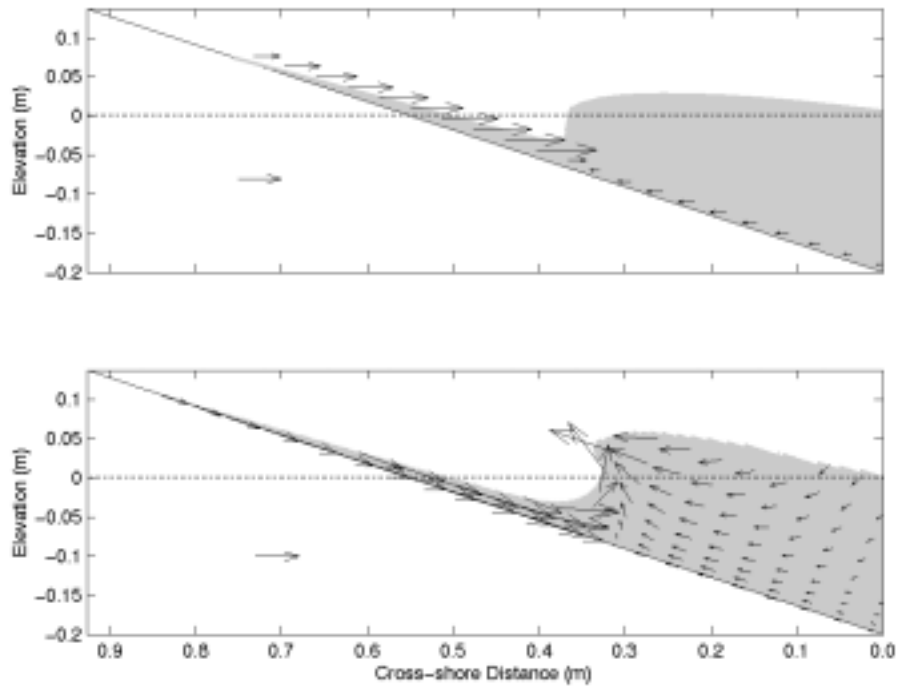
We have developed the VOF model and tested it in a series of idealized numerical experiments and against laboratory experiments we conducted at the Longshore Sediment Transport Facility (LSTF) (Figure 1.) at the Waterways Experiment Station, Army Corps of Engineers Laboratory in Vicksburg Mississippi.



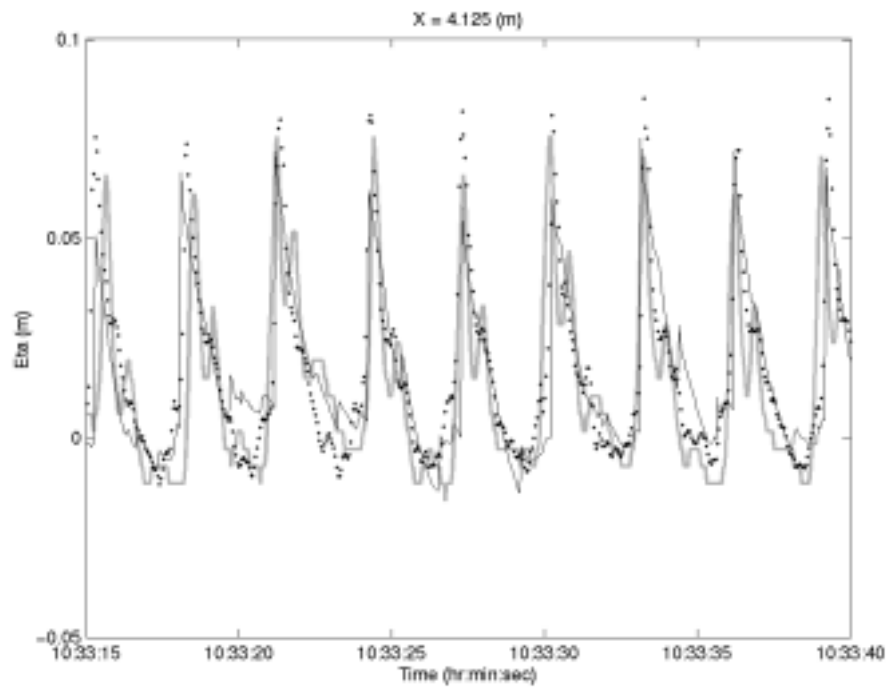
*Figure 1. LSTF showing waves, the instrumentation bridge, wave gages and ADV's.*

## **RESULTS**

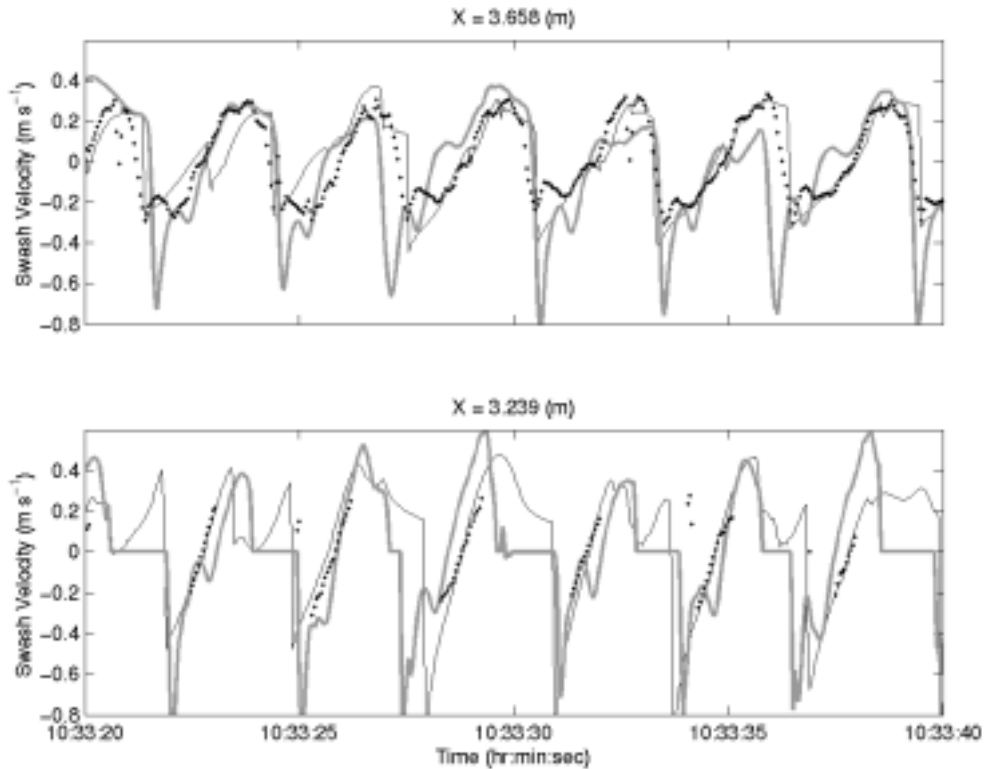
Numerical simulations of inner surf and swash zone motions were carried out using both 1D (RBREAK2) and 2D (VOF) models (Figures 2-4). We find that the 2D model more accurately displays wave breaking and yields information regarding depth dependent fluid velocities in both the cross-shore and vertical direction. Comparisons with measurements showed that both models predicted the free surface elevation well (Figure 3), however more discrepancy was observed for swash velocities. The depth averaged velocity from the 1D model in the outer swash zone had the same magnitude as the measured near bed data, but did not closely match the measured velocity time series. The magnitude comparison yielded more evidence that the flow in the swash zone is depth uniform for most of the duration of the swash cycle except in a thin boundary layer. The velocities from the VOF model had the same magnitude as those from the measured velocity data during backwash, but had a large spike below the shoreward propagating bore that exceeded the measured data (Figure 4). Furthermore, the VOF velocity estimates show smaller lag/lead relationships compared to the measured data.



**Figure 2: Flat beach ( $20^\circ$ ) simulations for RBREAK2 (upper) and VOF (lower). Vectors are depth-averaged (upper) and depth dependent (lower) fluid velocities. A  $50 \text{ cm s}^{-1}$  scale vector is shown in the lower left. Gray shading represents fluid in the model domain.**



**Figure 3: Sea surface comparison between ADV data (dots), VOF (gray), and RBREAK2 (black) in the inner surf zone.**



**Figure 4. Velocity comparison for ADV (dotted), RBREAK2 (depth averaged; black) and VOF (gray). Upper panel is for outer swash zone and lower panel for middle swash zone. Negative velocities are onshore, positive velocities offshore.**

Since the output from the 2 models was similar, one may ask, “What is the benefit to using a higher dimension model with increasing complexity especially when there is about a 70 fold increase in the required computation time?” Obviously it is a cost/benefit problem, but the 2D model is not restricted to shallow water environments and yields information as to the flow structure within the water column as opposed to being depth-averaged. Because of this information, one can now look into boundary layer structure, the time dependent nature of boundary layer formation over variable bathymetry and within the swash zone and ultimately begin to simulate time dependent bed shear stress (obtained from velocity profiles near the bed) across the nearshore profile. These processes *cannot* be extracted from a 1D model. These processes will in turn help to steer our knowledge of the important processes like wave breaking and propagation and potentially lead us to better methods for predicting sediment transport in the nearshore (where modeling capabilities severely lag those of nearshore hydrodynamics). Hence, we feel the benefit to using a model like VOF outweighs the cost.

The simulations performed here did not utilize the VOF model in its “out of the box” form and considerable work went into making the model appropriate for the surf and swash zones. However, more work needs to be done to tailor the model for nearshore hydrodynamics. Our future efforts will focus on incorporating a 2-equation turbulence closure scheme. The present model utilizes a constant eddy viscosity approach at present and we feel a 2 equation scheme such as the often used k- $\epsilon$  scheme will more accurately model the subgrid turbulence and may help in dissipating some of the high velocity spikes that were observed under the bore in the swash zone. Furthermore, this scheme will

enable a larger model domain with larger fluid volumes to be used such that the model can be forced from deep water allowing prediction of wave breaking, propagation, reformation, swash processes and boundary layer structure all from one model. Other ongoing work involves testing of various methods for forcing the model and the inclusion of tracer particles to visualize where and how sediment is transported during the breaking process and in the turbulent swash zone bore.

## **IMPACT/APPLICATIONS**

Improved understanding of the swash zone has potential benefits for society in several areas. These include shore protection against beach erosion, understanding the behavior of shoaling waves and rip currents, mitigating problems associated with sediment transport, such as keeping waterways open for shipping in harbors, ports and inlets.

## **TRANSITIONS**

The project began this year and we are testing and validating our model capabilities. The project has been joined by Jack Puleo, for his PhD dissertation, as part of the collaboration with NRL-SSC, who is adding the  $k-\epsilon$  turbulence submodel and testing the model turbulent flow conditions.

## **RELATED PROJECTS**

1. Dr. K. Todd Holland at the Naval Research Laboratory, Stennis Space Center, is leading the work on the laboratory and field experiments.
2. Dr. Britt Raubenheimer is working on swash zone measurements and theory under the ONR-YIP program.

## **REFERENCES**

Raubenheimer, B., R. T. Guza, S. Elgar, and N. Kobayashi, 1995, Swash on a gently sloping beach, *Journal of Geophysical Research*, 100, 8751-8760.

Hirt, C. W., and B. D. Nichols, 1981, *Journal of Computational Physics*, 39, 201.

Holland, K.T., Puleo, J.A. and Kooney, T., 2001, Quantification of swash flows using video-based particle image velocimetry, submitted to *Coastal Engineering*.

## **PUBLICATIONS**

J.A. Puleo, T. Holland, D. N. Slinn, E. Smith, B. Webb, 2002, Numerical Modeling of Swash Zone Hydrodynamics, International Conference on Coastal Engineering, Cardiff, Wales.