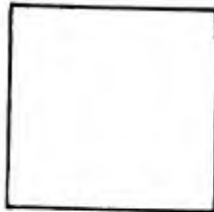


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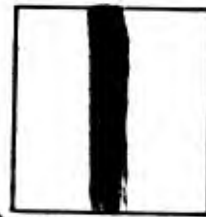
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WATERTOWN ARSENAL LABORATORY

MEMORANDUM REPORT

NO. WAL 154/12

THE TEMPERING OF MARTENSITE

BY

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DATE

1 November 1945

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WATERTOWN, MASS.

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Watertown Arsenal Laboratory Memorandum

Report Number 154/12

Problem Number H-6.2a

THE TEMPERING OF MARTENSITE

Object

To determine by means of x-ray diffraction technique the time-temperature relations for the initial tempering of martensite.

Abstract

The time-temperature relation for the loss of tetragonality of martensite was determined for a plain carbon steel (.95% C.). The time and temperature are related through a heat of activation relation. This heat of activation is of the order of 34,000 cal./gm. mol. These data indicate that appreciable tempering of the first formed martensite can occur with moderate cooling rates upon quenching if the M_s temperature is significantly above room temperature. Graphs are presented for estimating the amount of tempering, in the steel studied, during any tempering treatment, as well as during quenching.

Introduction

In several earlier studies of quenched steel specimens, microstructures were observed containing a constituent identified as either bainite or tempered martensite. There has been some controversy as to whether martensite can temper appreciably on cooling, during the quench, from the temperature at which it forms to room temperature. In order to determine whether appreciable tempering can take place under these conditions and so account for the observed microstructures, it was proposed to determine the effect of time and temperature upon the progress of the initial stage of tempering. This stage consists of precipitation of carbide* from the martensite, and in steels containing more than about .25%

*As has been discussed², there is still some question as to the exact form of the initial precipitate.

carbon is associated with a decrease in the tetragonality of the martensite lattice structure, as measured at room temperature^{1, 2}.

Furthermore, it was believed that the stabilizing of austenite (with respect to the martensite reaction), which occurs gradually in mixtures of austenite with martensite, might be associated with the tempering of the martensite already formed. If the relation between the time and temperature for the initial tempering should be found to be the same as for the stabilizing effect, a good possibility of a connection would be established. The time-temperature relation for the initial tempering is one of the two relations needed. The other is the time-temperature relation for the stabilizing effect; work on this is now under way.

As the initial stage of tempering is associated with little change of hardness, hardness could not well be used as a criterion of the degree of tempering*. Since the characteristic loss of tetragonality at room temperature accompanies the initial stage, it appeared that the progress of the tempering could be followed by x-ray diffraction measurements of the tetragonality.

Materials and Procedure

Discs 3/16" thick were cut from a bar of a plain carbon steel containing .95% carbon and .26% manganese. The specimens were ground concave on one side in order to fit the curvature of the x-ray camera. Before heat treatment the specimens were plated with a thin layer of nickel to reduce surface decarburization during heat treatment. The specimens were austenitized for 30 minutes at 900° C. in a nitrogen atmosphere and quenched in water to room temperature. They were then ground slowly to remove the nickel layer. The specimens were etched electrolytically for 30 minutes in a dilute HCl - H₂SO₄ solution at very low current density. Extreme care was taken to prevent any heating of the specimens during the removal of the surface. The specimens were then quenched in liquid nitrogen. X-ray measurements were made on all specimens to determine the original axial ratio of the tetragonal martensite. Following this measurement all specimens were stored in dry ice until they were tempered. One specimen was used for each tempering temperature. The specimen was tempered, for one time, cooled to room temperature for x-ray measurements, and then retempered for additional times. The tempering was accomplished in liquid baths controlled to within ±2° C.

In order to find the axial ratio, it was necessary to measure the interplanar distance for the (110) and the (101) planes of martensite. A Phragmen No. 2 Camera was used with unfiltered chromium radiation to

*It is for this reason that the previous publication³ throws little light upon the initial stage.

record the diffracted beams from these planes. The effects of possible variables of experiment and measurement were minimized by superimposing a standard reference x-ray line on each film. The line used was that from the (200) plane of platinum. The platinum was dusted on the face of each specimen before exposure to the x-radiation. The distances on the film between the $K\alpha$ line diffracted from the (200) plane of platinum and the lines from both the (110) and (101) planes of the martensite were measured on a densitometer. Three measurements were made on each film of the distance between the densest portions of the lines. The measurements were averaged, and the c/a ratio calculated from the average as described in Appendix A. The measured distances and the calculated interplanar spacings and c/a ratios are given in Table I.

On some films the distance between the platinum line and the martensite (110) line could not be read satisfactorily. In these cases, the interplanar spacing, d , for the (110) planes was taken as equal to the average of the $d(110)$ for other films taken of the same specimen. This procedure is believed justified because the $d(110)$ was found to change very little as tempering proceeded (Table I). This is in accord with the published finding⁴ that the axial length a , to which $d(110)$ is proportional (Appendix C), changes very little with changes in carbon content of the martensite.

Results and Discussion

The results are given in Table I, and plotted in Figure 1. In this figure the loss of tetragonality is expressed as a percentage of the total possible decrease of the c/a ratio, from the untempered value to $c/a = 1$. (a is the length of the two equal short axes of the tetragonal unit cell, while c is length of the long axis.)

Combinations of tempering temperature and tempering time that give the same loss of tetragonality were read off the curves of Figure 1, and are plotted in Figure 2. Figure 2 indicates that the loss of tetragonality follows a heat of activation relationship, with a heat of activation of approximately 34,000 calories per gram-mol. That is,

$$\text{tetragonality} = f(N), \quad (1)$$

where the parameter

$$N = te^{-q/RT} = te^{-34,000/1.986T} = t \cdot 10^{-7340/T} \quad (2)$$

Here

- t = tempering time
- T = tempering temperature in $^{\circ}\text{K}$.
- q = heat of activation
- R = universal gas constant.

In Figure 3, the loss in tetragonality is plotted as a function of the parameter N.

The rate of tempering at room temperature is of considerable practical interest. Figure 3 indicates that at a temperature of 20° C. the tetragonality will decrease 10% in about 5 months, 20% in about 5 years, 30% in 20 years, and 50% in 100 years.

To evaluate the amount of tempering that takes place during quenching, Equation 2 is put in the integral form,

$$N = \int_0^t e^{-q/RT} dt = \int_0^t 10^{-7340/T} dt, \quad (3)$$

t being measured from the instant at which the martensite formed. It is also necessary to specify the relationship between temperature and time during the quench. A relation that is widely applicable is:

$$T = T_1 + (T_0 - T_1)e^{-ct}, \quad (4)$$

where

T_1 = temperature of the quenching medium,
 T_0 = steel temperature at $t = 0$,
 c = cooling coefficient, a constant.

This exponential relationship is approached at low temperatures in almost all cases. Using Equations 3 and 4, Figure 4 has been derived, as indicated in Appendix D, for the case of a quenching medium at room temperature (20° C.). This figure gives the tempering parameter N obtained by exponential cooling to essentially room temperature as a function of the temperature at which the martensite forms and of the cooling coefficient c. The cooling coefficient c for simple shapes is given by the following equations:

$$\begin{aligned} \text{Plates: } c &= (HD)4a/D^2 = 4aH/D, \\ \text{Cylinders: } c &= 2(HD)4a/D^2 = 8aH/D, \\ \text{Spheres: } c &= 3(HD)4a/D^2 = 12aH/D. \end{aligned} \quad (5)$$

Here

H = severity of quench,
D = diameter or thickness,
a = thermal diffusivity of the steel.

More complicated shapes may be considered as composed of several simple shapes, and the c for the combination obtained by adding the c's for the component simple shapes. Thus, a short round of diameter d and length L can be considered a combination of a cylinder of diameter d and a plate of thickness L. The value of c for the round is then:

$$c = \frac{8aH}{d} + \frac{4aH}{L}$$

Since the thermal diffusivity, a , of martensite is of the order of $.01 \text{ inch}^2/\text{second}$, Equations 5 may be roughly taken as:

$$\begin{aligned} \text{Plates: } c &= .04H/D, \\ \text{Cylinders: } c &= .08H/D, \\ \text{Spheres: } c &= .12H/D, \end{aligned} \quad (6)$$

for dimensions expressed in inches and times in seconds. The quenching severity H in the martensite temperature range may vary from the order of $.01 \text{ inch}^{-1}$ for still air to the order of 10 inch^{-1} for agitated water.

A few examples may prove useful. A steel sheet $.04 \text{ inch}$ thick quenched in violently agitated water with $H = 10 \text{ inch}^{-1}$ would have a cooling coefficient, c , according to Equation 6, of $(.04)10/(.04) = 10 \text{ seconds}^{-1}$, or a $\log c$ of 1. Martensite forming at 300° C. has, by the time it approaches room temperature, tempered to the extent that $\log c + \log N = -14$, according to Figure 4. In the case mentioned, $\log N$ would then equal -15 . Figure 3 shows that, if the sheet were made of steel that tempers, initially, as fast as the steel studied experimentally, considerably more than 50% of the tetragonality would be lost before the martensite formed at 300° C. reached approximately room temperature. Martensite formed at 200° C. has a $\log c + \log N = -16.6$. For the extremely rapid cooling mentioned, $\log N$, therefore, equals -17.6 . The martensite formed at 200° C. would lose 10-15% of its tetragonality by the time it reached room temperature.

As an example of extremely slow cooling, consider a 10 inch thick plate cooling in still air with $H = .01 \text{ inch}^{-1}$. Here $\log c = -4.4$. Martensite formed at 100° C. , where $\log c + \log N = -20.6$, would temper to $\log N = -16.2$, and so lose about 35% of its tetragonality.

Another example, the air-cooled end of a standard Jominy end-quench hardenability specimen may be considered. The cooling coefficient in the martensite range can be estimated to be of the order of $.01 \text{ second}^{-1}$, so $\log c = -2$. Martensite formed at 200° C. would temper to $\log N = -14.6$, and most, if not all, of the tetragonality would be lost.

Finally, in the experimental work described in this report, the portion of the specimen used for diffraction measurements was about $1/8 \text{ inch}$ thick when quenched. The quenching severity in the martensite range might be of the order of 4 inch^{-1} . The cooling coefficient was, therefore, about 1.3 second^{-1} and $\log c$ about 0. The M_s temperature of the steel used may be estimated as approximately 200° C. Martensite formed just below the M_s temperature would, therefore, lose about 25% of its tetragonality by the time it reached room temperature. With an M_s of 200° C. , most of the martensite would form below 150° C. This martensite would lose less than 10% of its tetragonality. Thus, while some tempering had undoubtedly occurred in the nominally untempered specimens, most of the martensite had tempered only slightly. The resulting variation

in tetragonality within the specimens accounts for at least some of the observed broadness of the diffraction lines.

The establishment of the heat of activation for the initial stage of tempering gives a little information concerning the rate of diffusion of carbon through ferrite, which has never been measured. Since the initial stage of tempering undoubtedly involves diffusion of carbon through martensite, it can readily be shown that the heat of activation for this stage of tempering must be more than the heat of activation for the diffusion. The heat of activation for the diffusion of carbon through (supersaturated) ferrite (martensite) is, therefore, less than 34,000 calories per gram-mol. This accords with the deduction, from the lattice structures of ferrite and austenite, that the heat of activation for the diffusion of carbon in ferrite must be less than the 36,000 calories per gram-mol measured for the diffusion of carbon in austenite.

The loss of tetragonality of the martensite may appear to be a somewhat arbitrary measure of tempering. However, it appears to be generally accepted that, as long as the martensite is tetragonal, the tetragonality ($\frac{C}{H} - 1$) is approximately proportional to the carbon content of the martensite.

The relation between time and temperature for the initial stage of tempering, discussed above, is based upon experimental results on only one steel, and its generality has, therefore, not been established. However, consideration of the nature of the initial stage seems to indicate that the progress of the reaction, and particularly the heat of activation, will probably not be greatly affected by changes in carbon content, and will probably be affected very little by changes in alloy content.

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MM 11/7/45

TABLE I

DATA AND RESULTS

Film No.	Tempering Time in Min.	X* in mm.	X ₁ ** in mm.	d(110)	d(101)	$\frac{c}{a}$	% Possible Decrease in $\frac{c}{a}$
<u>60° C. Tempering Temperature</u>							
T2	0	4.297	6.827	2.017	2.055	1.038	0
T2-1	1	4.118	6.577	2.015	2.051	1.037	2.63
T2-2	10	4.114	6.554	2.015	2.051	1.037	2.63
T2-3	100	4.112	6.411	2.015	2.049	1.034	10.53
T2-4	1000	4.127	6.252	2.015	2.046	1.032	15.79
T2-5	10000	---	5.826	***	2.040	1.026	31.58
<u>91° C. Tempering Temperature</u>							
T10	0	4.227	6.748	2.016	2.054	1.039	0
T10-3	2.5	---	6.353	***	2.047	1.032	17.94
T10-4	8.0	4.369	6.548	2.017	2.051	1.034	12.82
T10-5	25.0	4.291	6.404	2.017	2.049	1.032	17.94
T10-6	80.0	4.163	6.171	2.015	2.044	1.030	23.08
T10-7	250.0	---	5.962	***	2.042	1.027	30.77
T10-8	800.0	---	5.372	***	2.033	1.017	56.41
<u>109° C. Tempering Temperature</u>							
T18	0	4.224	6.629	2.016	2.052	1.037	0
T18-1	.25	4.292	6.544	2.017	2.051	1.034	8.10
T18-2	.80	4.251	6.417	2.016	2.049	1.033	10.81
T18-3	2.50	4.317	6.266	2.017	2.046	1.030	18.92
T18-4	8.0	4.680	6.380	2.022	2.048	1.026	29.73
T18-5	25.0	---	5.730	***	2.038	1.022	40.54
T18-6	80.0	---	5.483	***	2.035	1.020	45.95
T18-7	250.0	---	5.257	***	2.031	1.015	59.46
<u>139° C. Tempering Temperature</u>							
T16	0	4.143	6.696	2.015	2.053	1.040	0
T16-1	.25	---	6.282	***	2.046	1.032	20.00
T16-2	.80	---	5.916	***	2.041	1.027	32.50
T16-3	2.50	---	5.616	***	2.037	1.022	45.00
T16-4	8.00	---	5.332	***	2.033	1.019	52.50

*X = distance between Platinum line and Martensite (110) line.

**X₁ = distance between Platinum line and Martensite (101) line.

***Where Martensite (110) line was unreadable a d(110) value equal to the average obtainable value for previous readings was used in calculating the $\frac{c}{a}$ ratio.

TABLE I (CONT.)

Film No.	Tempering Time in Min.	X* in mm.	X** in mm.	d(110)	d(101)	$\frac{c}{a}$	% Possible Decrease in $\frac{c}{a}$
<u>171° C. Tempering Temperature</u>							
T14	0	4.093	6.596	2.014	2.051	1.039	0
T14-2	.8	---	5.469	***	2.034	1.020	48.72
T14-3	2.5	---	5.164	***	2.030	1.016	58.97
T14-4	8.0	---	4.494	***	2.026	1.012	69.23

*X = distance between Platinum line and Martensite (110) line.

**X₁ = distance between Platinum line and Martensite (101) line.

***Where Martensite (110) line was unreadable a d(110) value equal to the average obtainable value for previous readings was used in calculating the $\frac{c}{a}$ ratio.

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APPENDIX A

METHOD OF CALCULATION

From the measured distances on the film between the platinum (200) line and the martensite (110) and (101) lines, the diffraction angles for the martensite lines are calculated by the following equation, derived in Appendix B:

$$\theta_m = 35.717 - .28364X. \quad (A1)$$

Here

θ_m = Bragg diffraction angle, in degrees, for martensite line,
X = measured distance on film, in millimeters.

From the diffraction angles, the spacing of the martensite lattice planes, d, was computed as:

$$d = \frac{\lambda}{2 \sin \theta} \quad (A2)$$

This equation is obtained directly from Bragg's Law. The wavelength λ was taken, for chromium K α radiation, as 2285.0 Siegbahn units*.

To obtain the c/a ratio, the d values were substituted in the equation,

$$c/a = \sqrt{\frac{d_2^2}{2d_1^2 - d_2^2}}. \quad (A3)$$

This equation is derived in Appendix C. d_1 represents the spacing of the (110) plane and d_2 the spacing of the (101) plane.

*The c/a ratio could have been determined directly from the diffraction angles without calculating the lattice spacing, but it was convenient to have the spacing values.

APPENDIX B

RELATION BETWEEN FILM MEASUREMENTS AND DIFFRACTION ANGLE

Since an angle formed by a chord and a tangent of a circle is measured by half the intercepted arc, the Bragg angle of incidence (θ_1) in Figure B1 is equal to half of angle a and the Bragg angle of diffraction (θ_2) equal to half angle b.

Since the angle of incidence is equal to the angle of diffraction,

$$2\theta = \frac{1}{2} a + \frac{1}{2} b \quad (B1)$$

Since an arc is measured by the angle it subtends at the center of the circle,

$$a = \frac{180}{\pi} \frac{\widehat{AB}}{R}$$

and

$$b = \frac{180}{\pi} \frac{\widehat{BC}}{R}$$

Substituting for a and b in Equation (B1),

$$2\theta = \frac{90}{\pi} \frac{\widehat{AB}}{R} + \frac{90}{\pi} \frac{\widehat{BC}}{R}$$

or

$$\theta = \frac{45}{\pi R} (\widehat{AB} + \widehat{BC}) \quad (B2)$$

From Figure 3, $\widehat{AB} + \widehat{BC}$ is found to equal $S_0 + S_1$, therefore,

$$\theta = \frac{45}{\pi R} (S_0 + S_1) \quad (B3)$$

Using the following symbols as indicated,

- θ_p = Bragg angle of incidence for platinum
- θ_m = Bragg angle of incidence for martensite
- R = radius of camera (Figure B1)
- S_p = distance from edge of film to platinum line (200) in mm. (Figure B1)
- X = distance on film from martensite line to platinum line, in mm.,

and substituting in Equation (B3),

$$\theta_p = \frac{45}{\pi R} (S_0 + S_p) \quad (B4)$$

and

$$\theta_m = \frac{45}{\pi R} (S_0 + S_p - X) \quad (B5)$$

Subtracting Equation (B5) from (B4),

$$\theta_p - \theta_m = \frac{45 X}{\pi R} \quad (B6)$$

The radius (R) for the Phragmen No. 2 Camera is 50.5 mm. and the angle θ for the (200) plane of platinum using chromium K α radiation is 35.717°. Substituting in Equation (B6),

$$35.717 - \theta_m = \frac{45X}{158.65}$$

or

$$\theta_m = 35.717 - .28364X. \quad (B7)$$

APPENDIX C

RELATION BETWEEN TETRAGONALITY AND INTERPLANAR SPACINGS

Let

d_1 = interplanar distance for the (110)
plane of martensite,

d_2 = interplanar distance for the (101)
plane of martensite.

h, k, l = Miller Indices.

Starting with the equation for a simple tetragonal lattice,

$$\frac{1}{d^2} = \frac{h^2 + k^2}{a^2} + \frac{l^2}{c^2} \quad (C1)$$

Substituting (110) for (h, k, l) ,

$$\frac{1}{d_1^2} = \frac{2}{a^2}$$

or

$$a^2 = 2d_1^2 \quad (C2)$$

Substituting (101) for (h, k, l) ,

$$\frac{1}{d_2^2} = \frac{1}{a^2} + \frac{1}{c^2}$$

Substituting $2d_1^2$ for a^2 (Equation C2),

$$\frac{1}{d_2^2} = \frac{1}{2d_1^2} + \frac{1}{c^2}$$

$$c^2 = \frac{2d_1^2 d_2^2}{2d_1^2 - d_2^2} \quad (C3)$$

Substituting a^2 for $2d_1^2$,

$$c^2 = \frac{a^2 d_2^2}{2d_1^2 - d_2^2} \quad (C4)$$

$$\frac{c}{a} = \sqrt{\frac{d_2^2}{2d_1^2 - d_2^2}} \quad (C5)$$

APPENDIX D

EVALUATION OF TEMPERING PARAMETER N FOR EXPONENTIAL COOLING

To repeat Equations (3) and (4) of the text,

$$N = \int_0^t e^{-q/RT} dt = \int_0^t 10^{-7340/T} dt \quad (D1)$$

and

$$T = T_1 + (T_0 - T_1) e^{-ct} \quad (D2)$$

Differentiating (D2),

$$dT = -c(T_0 - T_1) e^{-ct} dt \quad (D3)$$

$$dT = -c(T - T_1) dt \quad (D4)$$

Substituting for dt in Equation (D1),

$$N = -\frac{1}{c} \int_{T_s}^{T_2} \frac{10^{-7340/T}}{T - T_1} dT, \quad (D4)$$

with the boundary condition $N = 0$ at $T = T_s$.

Then,

$$cN = \int_{T_2}^{T_s} \frac{10^{-7340/T}}{T - T_1} dT. \quad (D5)$$

Taking the temperature of the medium,

$$T_1 = 20^\circ \text{ C.} = 293^\circ \text{ K.}$$

and integrating down to,

$$T_2 = 30^\circ \text{ C.} = 303^\circ \text{ K.,}$$

$$cN = \int_{303}^{T_s} \frac{10^{-7340/T}}{T - 293} dT \quad (D6)$$

The ratio,

$$\frac{10^{-7340/T}}{T - 293}$$

was then computed for various values of T as indicated in Table DI, and plotted as a function of T . By counting boxes, the area under the curve from $30^{\circ}\text{C.} = 303^{\circ}\text{K.}$ to T_g values of 100, 150, 200, 250, and 300°C. , was determined*. This area represents cN . The results are given in Table DII and plotted in Figure 4.

*Because the magnitude of the ratio varies so greatly, a separate plot with an appropriate scale had to be used for each of the T_g values.

TABLE DI

GRAPHICAL INTEGRATION FOR PARAMETER N ON EXPONENTIAL COOLING

Temp. °C.	T °K.	7340/T	$10^{-7340/T}$	T-293	$\frac{10^{-7340/T}}{T-293}$
30	303	24.22	6.03×10^{-25}	10	6.03×10^{-26}
50	323	22.72	1.90×10^{-23}	30	6.33×10^{-25}
65	338	21.72	1.90×10^{-22}	45	4.22×10^{-24}
80	353	20.79	1.62×10^{-21}	60	2.70×10^{-23}
90	363	20.22	6.03×10^{-21}	70	8.61×10^{-23}
95	368	19.95	1.12×10^{-20}	75	1.49×10^{-22}
100	373	19.68	2.09×10^{-20}	80	2.61×10^{-22}
115	388	18.92	1.20×10^{-19}	95	1.26×10^{-21}
130	403	18.21	6.17×10^{-19}	110	5.61×10^{-21}
140	413	17.77	1.70×10^{-18}	120	1.42×10^{-20}
145	418	17.56	2.75×10^{-18}	125	2.20×10^{-20}
150	423	17.35	4.47×10^{-18}	130	3.44×10^{-20}
160	433	16.95	1.12×10^{-17}	140	8.00×10^{-20}
170	443	16.57	2.69×10^{-17}	150	1.79×10^{-19}
180	453	16.20	6.31×10^{-17}	160	4.21×10^{-19}
190	463	15.85	1.41×10^{-16}	170	8.29×10^{-19}
195	468	15.68	2.09×10^{-16}	175	1.19×10^{-18}
200	473	15.52	3.02×10^{-16}	180	1.68×10^{-18}
215	488	15.04	9.12×10^{-16}	195	4.68×10^{-18}
230	503	14.60	2.51×10^{-15}	210	1.20×10^{-17}
240	513	14.31	4.90×10^{-15}	220	2.23×10^{-17}
245	518	14.17	6.76×10^{-15}	225	3.00×10^{-17}
250	523	14.03	9.33×10^{-15}	230	4.06×10^{-17}
270	543	13.52	3.02×10^{-14}	250	1.21×10^{-16}
280	553	13.27	5.37×10^{-14}	260	2.07×10^{-16}
290	563	13.04	9.12×10^{-14}	270	3.38×10^{-16}
300	573	12.81	1.55×10^{-13}	280	5.54×10^{-16}
350	623	11.78	1.66×10^{-12}	330	5.03×10^{-15}
400	673	10.91	1.23×10^{-11}	380	3.23×10^{-14}
450	723	10.15	7.08×10^{-11}	430	1.65×10^{-13}
500	773	9.495	3.20×10^{-10}	480	6.67×10^{-13}
550	823	8.919	1.20×10^{-9}	530	2.27×10^{-12}

TABLE DII

RESULTS OF INTEGRATION

$^{\circ}\text{C.}$	cN	$\log_{10} cN$
100	2.31×10^{-21}	-20.64
150	3.75×10^{-19}	-18.43
200	2.34×10^{-17}	-16.63
250	6.48×10^{-16}	-15.19
300	1.03×10^{-14}	-13.99

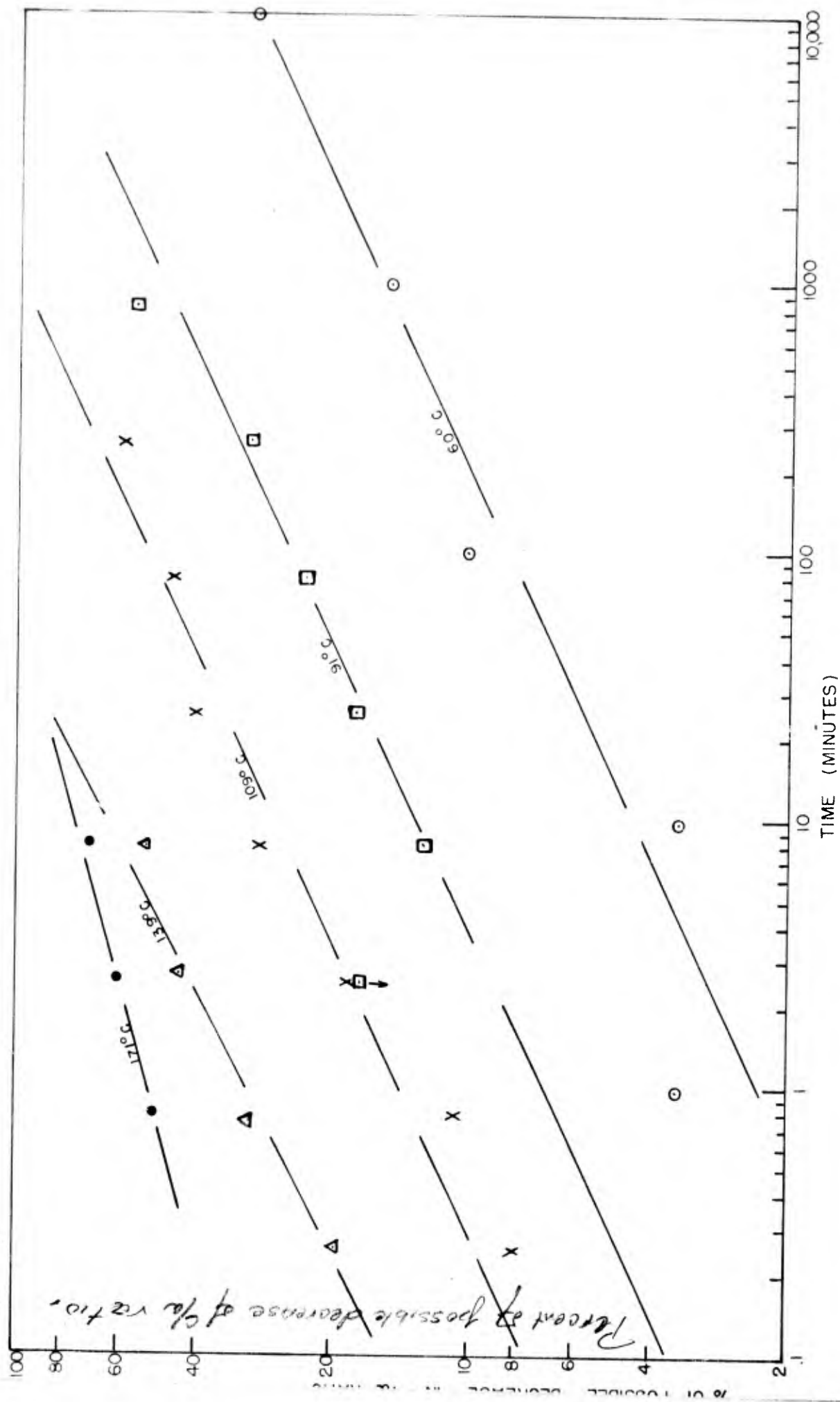


FIGURE 1

LOSS OF TETRAGONALITY AS FUNCTION OF TEMPERING TIME & TEMPERATURE

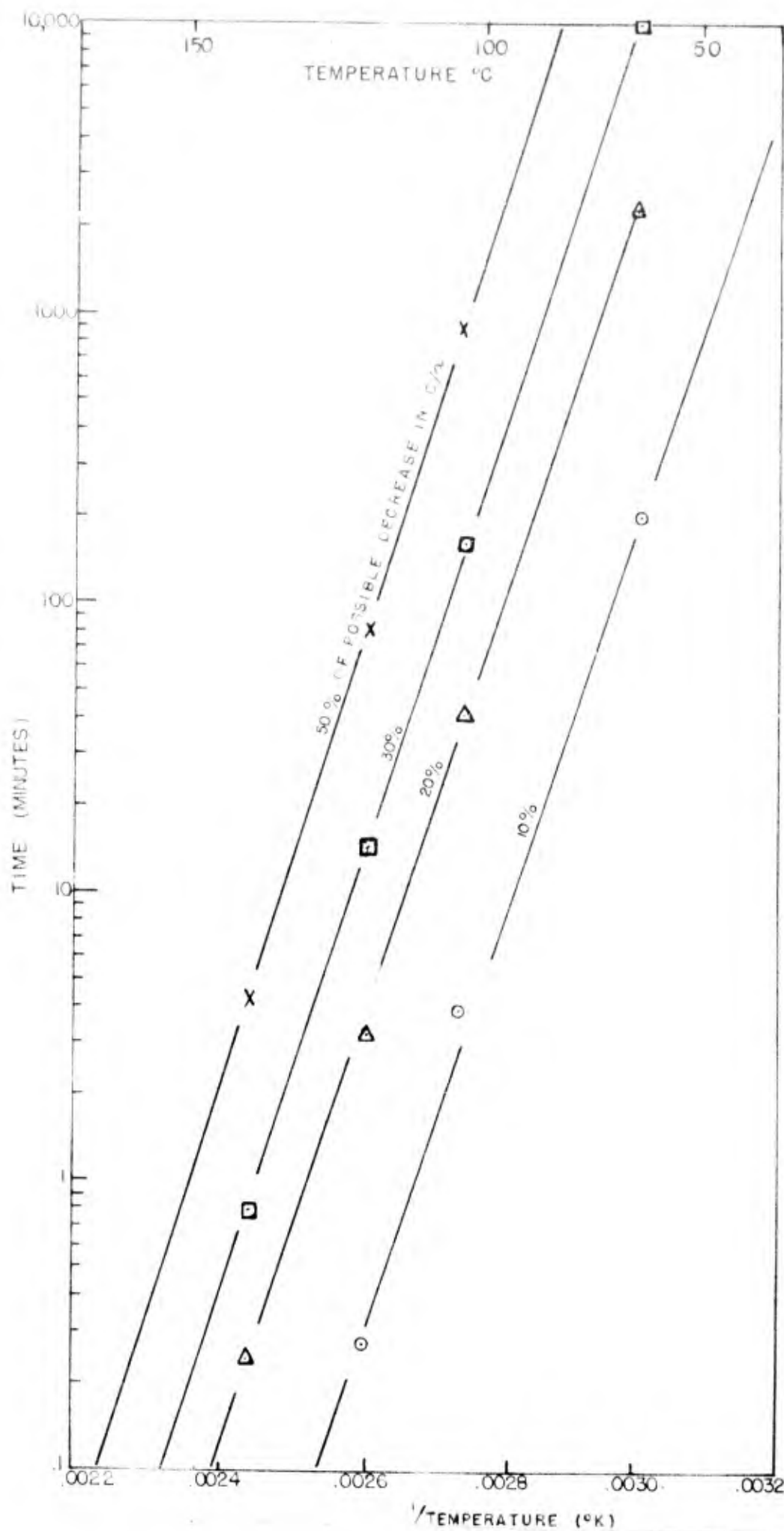


FIGURE 2

RELATION BETWEEN TIME AND TEMPERATURE FOR FIXED LOSS OF TETRAGONALITY

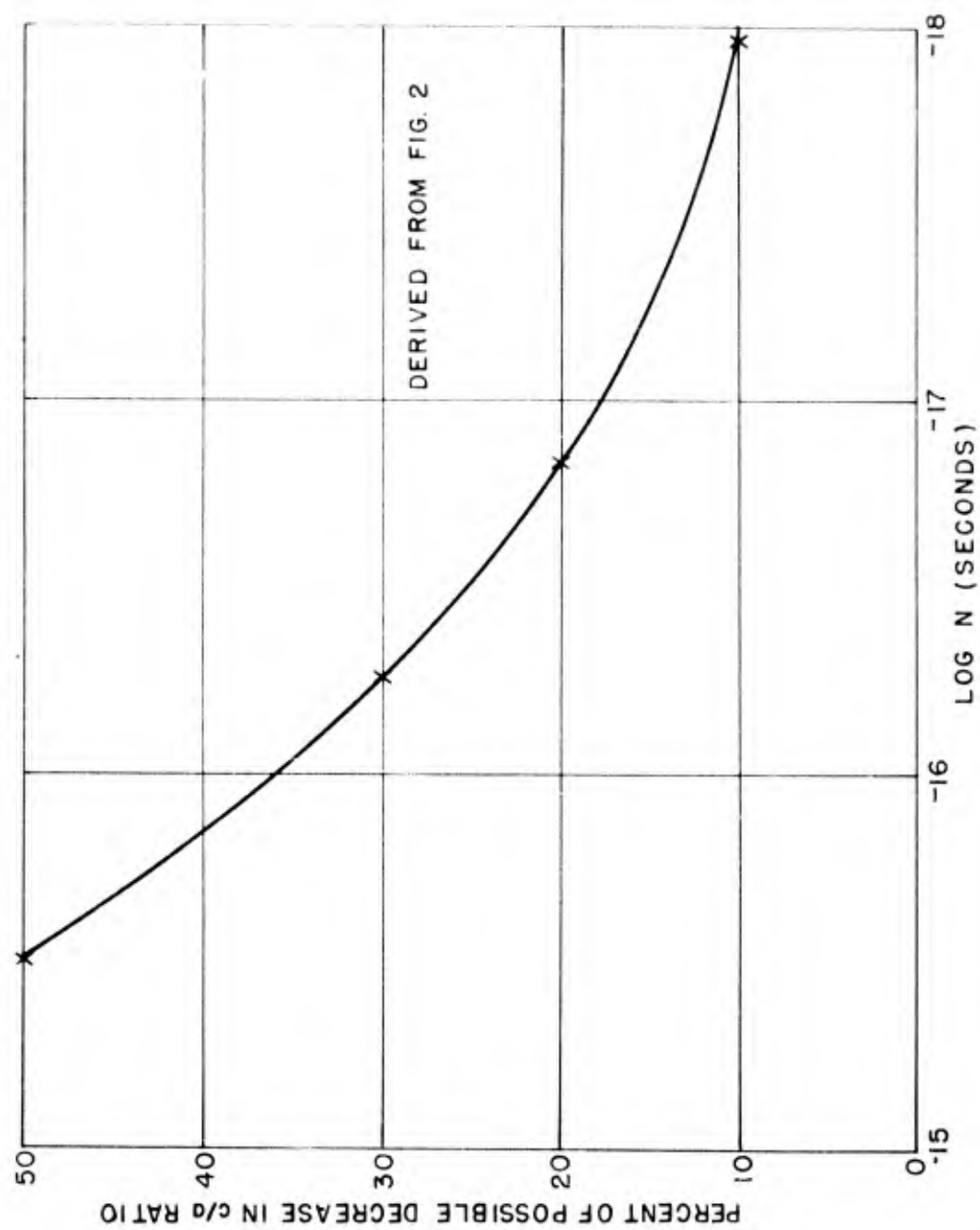


FIGURE 3
LOSS OF TETRAGONALITY AS FUNCTION OF TEMPERING
PARAMETER N .

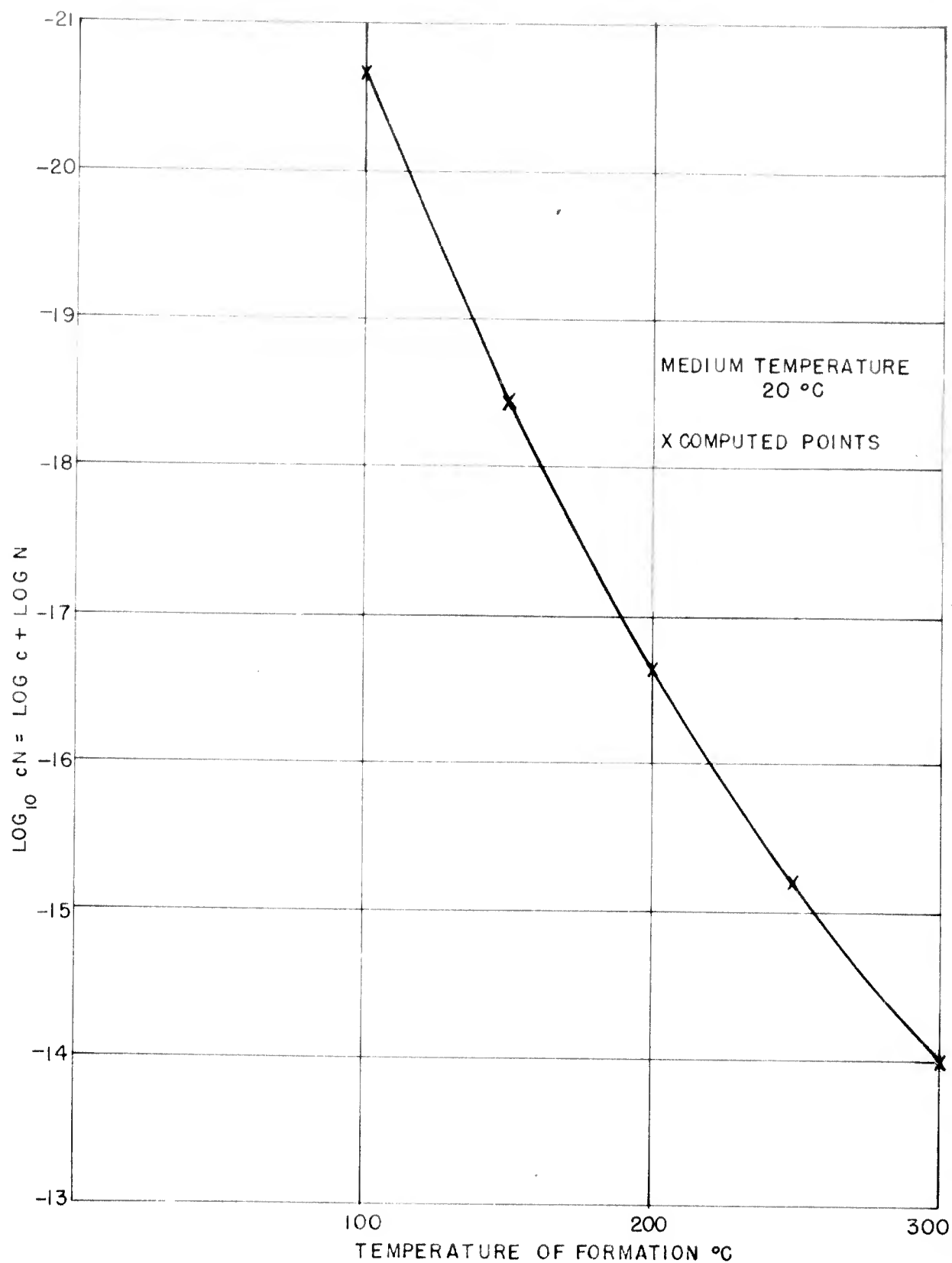


FIGURE 4

TEMPERING PARAMETER N FOR EXPONENTIAL COOLING AS
FUNCTION OF TEMPERATURE OF MARTENSITE FORMATION &
OF COOLING COEFFICIENT c.

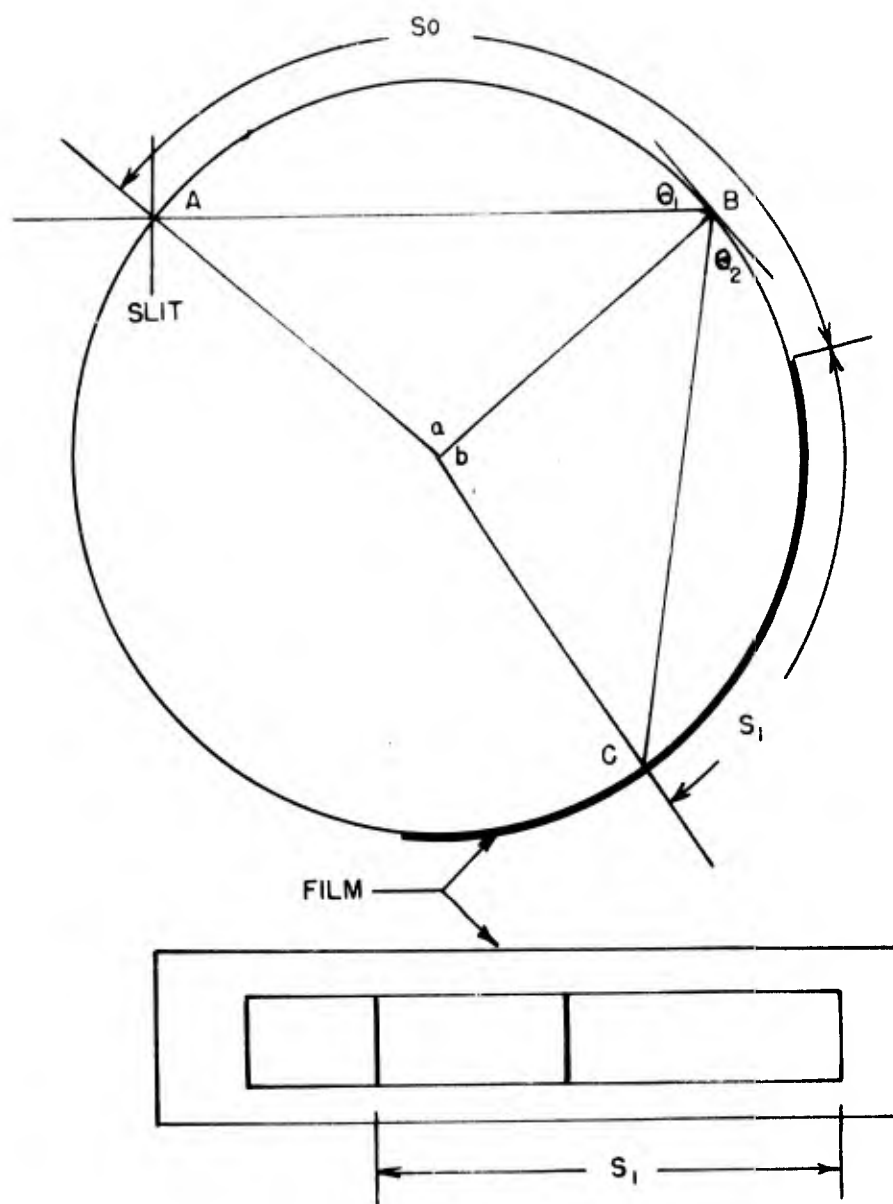


FIGURE B1
CAMERA GEOMETRY