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# WATERTOWN ARSENAL LABORATORY

## EXPERIMENTAL REPORT

NO. WAL. 640/89

### WELDING OF ARMOR

Summary of Ballistic Shock Test Results on  
1 Inch and 3/4 Inch Homogeneous Armor "H" Plates Welded with  
Austenitic Electrodes and Tested at Aberdeen Proving Ground  
during the Period from 1 October 1942 through 31 March 1943

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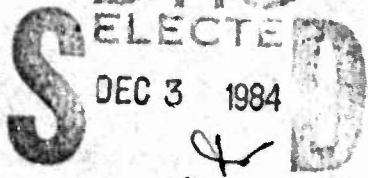
Anna M. Turkalo  
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S. A. Herres  
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Experimental Report

No. WAL. 640/89

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WELDING OF ARMOR

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1 October 1942 through 31 March 1943

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Watertown Arsenal Laboratory  
Report Number WAL 640/89  
Problem D-3.1

15 November 1943

WELDING OF ARMOR

Summary of Ballistic Shock Test Results on  
1 Inch and 3/4 Inch Homogeneous Armor "H" Plates Welded with  
Austenitic Electrodes and Tested at Aberdeen Proving Ground  
during the Period from 1 October 1942 through 31 March 1943

OBJECT

To tabulate firing record data for subject plates and to present a comparison of ballistic shock performance of plates made with various materials and welding procedures.

SUMMARY

1. Data from Aberdeen Proving Ground firing records for 156 welded armor H plates have been tabulated on accompanying charts and tables.
2. Quality of armor plate appears to be the most important variable for all hand welded plates.
  - a. Steel cleanliness and directional properties affect the amount of weld cracking during ballistic shock testing of H plates assembled from 1 inch rolled homogeneous armor.
  - b. The proportion of plate to weld cracking for H plates assembled from 1 inch cast and 3/4 inch rolled homogeneous armor is too high to allow adequate comparisons between ordinary variations in the welding procedure.

Hence, the futility of welding H plates from armor plate which has not been adequately heat treated or does not have relatively good cleanliness and soundness characteristics is quite evident.

3. There is little difference in ballistic shock test results between plates welded with the manganese and with the molybdenum modified type of austenitic electrodes. Plates welded with a narrow included angle, a small number of passes, or a straight weave technique are indicated to be slightly inferior in resistance to weld metal cracking during ballistic test.
4. Five Unionmelt plates, included in the rolled 1 inch armor group, showed shock test results slightly inferior to the average for hand welded plates.

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5. In general, failure to pass the radiographic inspection test is associated with slightly increased weld cracking during the ballistic test.

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## INTRODUCTION

On the accompanying charts (Appendix A) are tabulated data taken from firing records representing qualification and development tests of 156 H plates. The tabulation includes all firing records received by this arsenal for H plates assembled from 1 inch and 3/4 inch thick homogeneous rolled or cast armor by welding with austenitic electrodes and fired at Aberdeen Proving Ground during the period from 1 October 1942 through 31 March 1943.

The purpose of these tabulations is to make available to persons concerned with welding of armored structures information as to ballistic performance of H plates made with various materials and procedures by commercial fabricators. Previous reports (W.A. 640/73 and 640/84) have given summaries of ballistic test results for all 1 inch and 1-1/2 inch thick homogeneous armor H plates welded with ferritic electrodes and tested at Aberdeen Proving Ground through 25 February 1943, and for all 1-1/2 inch thick homogeneous armor H plates welded with austenitic electrodes and tested at Aberdeen Proving Ground during the same period as that covered by this report (1 October 1942 through 31 March 1943).

An index to fabricators, armor manufacturers, and electrode manufacturers is given in Table I. A summary of ballistic shock test specification requirements for H plates welded with austenitic electrodes and a key to the tabulation method and symbols used in this report are included in Appendix A.

## GENERAL COMMENTS

Ballistic performance of H plates is best evaluated by amount of cracking for each round, but the cracking is influenced by the variables in the ballistic test as well as those introduced by the materials and welding procedures used. It is desirable to make corrections or allowances for variations in projectile velocities and the effect of prior impacts when comparing various plates. However, tabulation of the average plate and weld cracking of the plates in this tabulation, grouped according to the severity of the ballistic test (Table II) does not provide a basis for such corrections. This is because there is an insufficient number of impacts at other than specification velocities to indicate the true effect of ballistic severity.

In the summary tables that follow, the number of rounds outside the specification limits for velocity and location will be listed and may be taken into consideration in comparing effects of armor and welding variables. Variation in thickness of the armor plate was compensated by increase in specified impact velocity of 6 f/s. for each .01 inch increase in plate thickness.

Firing record data show cracking as located in weld metal, fusion zone, heat-affected zone, or plate based only on surface appearance. Experience has shown that a crack in the vicinity of the weld may proceed

through portions of weld metal, fusion zone and heat-affected zone regardless of surface appearance. For the purpose of the tables of this report all cracking within 1/8 inch of edge of weld is included as weld cracking and the remainder as plate cracking. Inasmuch as most virgin rolled armor would not ordinarily develop cracking under the same testing conditions as those used for the welded plates and development of plate cracks materially decreases the severity of the test on the weld, it is necessary to consider plate cracking in evaluating the performance of welded H plates.

Decrease in temperature of the test plate at time of impact is known to have considerable effect in reducing the resistance to ballistic shock. Within the range of testing temperatures, 35° F. to 80° F., used for these plates it was not possible to establish the importance of this effect.

#### HAND WELDED, 1 INCH THICK ROLLED ARMOR H PLATES

Tables III through VIII show comparisons of average cracking per round for these plates in terms of welding fabricator, armor manufacturer and processing, electrode data, joint design, welding procedure, and radiographic soundness. The 57 mm. slug test is apparently less severe and not directly comparable to the 75 mm. slug test in the effect on the weld for these 1 inch rolled armor H plates.

The performance of H plates welded by any one fabricator (Table III) must be evaluated in terms of armor and electrodes as well as welding procedure and inspection control. Plates welded from Great Lakes and Youngstown armor show higher averages of both weld and plate cracking than plates welded from Jones and Laughlin armor (Table IV). Previous tabulations (WA. 640/84) have indicated that quality of steel (cleanliness and directional properties) has a greater influence upon ballistic efficiency than variations in chemical analysis or plate hardness within the ranges represented by these plates.

No correlation is shown between chemical composition of weld metal and amount of cracking. There is little difference between plates welded with Mn-Mo modified (weld analysis at least 1% Mn and 0.2% Mo) austenitic electrodes and Mn modified (weld analysis at least 1% Mn and less than 0.2% Mo) austenitic electrodes (Tables Va and Vb).

Double V joints with a 60° included angle were used on a large majority of the plates. Two plates welded with a single V, 40° included angle, and four plates welded with double V, less than 45° included angle, showed greater than average weld cracking on ballistic testing (Table VI).

Root gap varied from 1/8 to 1/2 inch, the majority of plates being welded with 3/16 inch root gap. Satisfactory plates were obtained at both extremes of root gap.

Number of passes used in completing weld varied from 4 to 45 (Table VII). The majority of plates were welded with 6 passes. There is a trend for slight improvement in ballistic performance with increase in number of passes up to 15. One plate with 4 passes was welded in vertical position and one with 45 passes in overhead position. Both failed the ballistic shock test.

A combination of beads and layers appeared more desirable than a full weave technique. A multiple bead surface layer was indicated as preferable to a single pass surface layer technique.

Two plates each were welded with mild steel backup strip and with no backup. These showed higher average weld cracking than the remaining plates welded with copper backup. The number of plates welded with preheat were insufficient to determine whether any benefit was obtained by this procedure.

In general, radiographic unsoundness is associated with increased cracking during ballistic shock test (Table VIII).

#### UNIONMELT WELDED, 1 INCH THICK ROLLED ARMOR H PLATES

Five Unionmelt plates are represented in this tabulation (Charts Nos. 44 - 46). The average weld and plate cracking were slightly higher for these plates than for either rolled or cast hand welded plates (Table IX).

Two plates were welded by Caterpillar Tractor Company, one with Great Lakes and the other with Youngstown armor plate of typical current chemical composition, with 75° included angle, single V, 3/16 inch root gap, 225° to 500° F. preheat, two passes of Unionmelt only. Both plates failed radiographic inspection due to crater cracking and there was an average of 15.6 inches of weld and 4.2 inches of plate cracking during ballistic shock test with 75 mm. test projectile.

Three plates were welded by General Motors Truck and Coach Division, all with a combination of Great Lakes and Jones and Laughlin armor plate of current chemical compositions, with 60° included angle, double V, 3/16 inch root gap, no preheat, two hand beads at root and two Unionmelt passes. These three plates passed radiographic inspection and there was an average of 6 inches of weld and 1.8 inches of plate cracking during ballistic shock test with 57 mm. test projectile.

#### HAND WELDED, 1 INCH THICK CAST ARMOR H PLATES

Ballistic performance was, in general, very poor for the cast armor H plates. In most instances, it was impossible to obtain a fair test of the weld because of excessive plate cracking. If armor plate has not been fully hardened during heat treatment, prior to welding, either

because of insufficient alloy or poor heat-treating practice, the plate metal will have very poor resistance to spreading of cracks initiated during ballistic testing of the welded H plate. Because of notches and residual stresses unavoidably introduced by welding, cracks are initiated under a ballistic shock which would not affect the virgin armor test plate. If armor is properly hardened during heat treatment and is of adequate steel quality (cleanliness and radiographic soundness), cracking during ballistic testing should be confined largely to the weld metal, fusion and heat-affected zones.

Table X shows a definite trend for improved ballistic performance in plates welded from armors known to have adequate hardenability for the given heat treatment.

Tabular comparison of welding variables does not seem justified for cast armor welded H plates so long as such a large proportion of the cracking is dependent upon the quality of the armor plate. Table XI indicates a slightly lower average weld cracking for plates which failed the radiographic inspection. Since radiographic unsoundness is usually associated with increased weld cracking, other factors seem to be of greater importance for these particular plates.

#### HAND WELDED, 3/4 INCH THICK ROLLED ARMOR H PLATES

The ballistic test for 3/4 inch plate was in the development stage during the period in which these plates were fired. The use of a 57 mm. projectile at a relatively low velocity resulted in a large number of impacts outside of the specified areas for fair testing of welds. Table XII shows a high ratio of plate to weld cracking for four of the six armor compositions involved, indicating inferior steel quality, inadequate heat treatment, or both. The one Republic plate, which did not show plate cracking during the ballistic shock test, was heat treated to a lower hardness level than the other plates and this would favor resistance to shock at the expense of resistance to ballistic penetration.

In view of the limited number of plates in this group and the large proportion of plate cracking, comparison of the electrodes or welding procedures on the basis of average cracking does not appear justified. Table XIII does, however, indicate a slightly lower average weld cracking, for plates which passed the radiographic inspection.

TABLE I  
INDEX TO PLATES

Hand Welded, 1 Inch Rolled Homogeneous "H" Plates

Chart No.	No of Plates	Fabricator	Armor Mfgr.	Electrode Mfgr.
1 - 2	6	American Car & Foundry	Jones & Laughlin	McKay Crucible Steel
3 - 13	33	Cadillac	Great Lakes Jones & Laughlin Youngstown	McKay Page Steel & Wire Lincoln Electric
14	3	Caterpillar	Youngstown Great Lakes	McKay
15	1	Firestone	Great Lakes	McKay
16 - 19	7	General Motors	Great Lakes Youngstown Jones & Laughlin	McKay Harnischfeger Lincoln Electric
20	2	Gordon Mfg.	Great Lakes Jones & Laughlin	Crucible
21 - 22	7	Heil	Jones & Laughlin Great Lakes	A. O. Smith Lincoln Electric Harnischfeger
23	1	International Harvester	Jones & Laughlin	McKay
24	1	Kay Brunner	Great Lakes	McKay
25	1	Maremont	Great Lakes	Crucible
26 - 27	5	Pullman Standard	Great Lakes	McKay Hollup
28	3	So. Calif. Div. of G.M.	Great Lakes	McKay Alloy Rcds
29 - 43	28	Ternstedt	Great Lakes Jones & Laughlin	Reid-Avery Alloy Rods Hollup McKay Crucible Allied Weldcraft

Unionmelt Welded, 1 Inch Thick Rolled Homogeneous "H" Plates

44	2	Caterpillar	Great Lakes Youngstown	Linde Air Products
45 - 46	3	General Motors	Jones & Laughlin Great Lakes	Union Carbide

TABLE I (Cont.)

Chart No.	No. of Plates	Fabricator	Armor Mfgr.	Electrode Mfgr.
-----------	---------------	------------	-------------	-----------------

Hand Welded, 1 Inch Thick Cast Homogeneous "H" Plates

47 - 53	15	Cadillac	Utility Electric Hughes Tool American McConway & Torley	McKay Lincoln Electric
54 - 55	6	Chevrolet	Kelsey Hayes	Harnischfeger McKay Alloy Rods
56	2	Ford	Ford	Crucible
57	1	General Motors	American Sivyer	McKay
58 - 61	7	Ternstedt	Hughes Tool Wehr Steel Great Lakes Jones & Laughlin	Reid Avery Lincoln Electric Hollup Alloy Rods McKay

Hand Welded, 3/4 Inch Thick Rolled Homogeneous "H" Plates

62	1	American Locomotive	Republic	Alloy Rods
63 - 69	16	Chevrolet	Chevrolet Forge Great Lakes E. C. Atkins	Alloy Rods McKay Harnischfeger Crucible
70	3	Ford	Ford	Crucible
71	2	Standard Rail- way Equip.	Carnegie-Illinois	Hollup

TABLE IIA

Ballistic Severity Table for Hand Welded 1 Inch Thick Rolled Homogeneous Armor "H" Plates

Vel. f/s	1st Round		2nd Round		3rd Round		4th Round	
	No. of Rds.	Av. Weld Cracking	No. of Rds.	Av. Plate Cracking	No. of Rds.	Av. Plate Cracking	No. of Rds.	Av. Plate Cracking
0 - 2" **								
801 - 850	1	0	3	0	9	0	1	0
*751 - 800	65	2.1"	29	3.64"	2	0	16.1"	1.0"
701 - 750	4	.5	3	0	2	0	20.0	
600 - 700			9	.4	2	0	8.4	
2 - 4" **								
801 - 850		1.4	9	6.4	2	0	8.8	
*751 - 800	11	5.4	2	0	1	0	0	
701 - 750	1	0	5	2.1	1	0	0	
600 - 700								
0 - 2" **								
1200 - 1300								
1150 - 1200	2	0	1	3.8	2	8.1	3.8	5.1
1100 - 1150	8	1.3	4	6.8	4	5.6	6.2	3.0
1050 - 1100								
1000 - 1050	1	0	1	6.5	1	0	0	
?								
1200 - 1300								
1150 - 1200	2		2	8.8				0
1100 - 1150	2		2	0				0

Projectile - 75 mm. T21

Projectile - 57 mm. T1

More than 4" \*\*  
1150 - 1200  
1100 - 1150

\* Specified velocity range

\*\* Distance from center of impact to center of weld

TABLE III

Ballistic Severity Table for 1.185 Inch Thick  
Rolled Homogeneous Armor "H" Plates

Vel. f/s	1st Round		2nd Round		3rd Round		4th Round	
	Nr. of Rds.	Av. Plate Cracking	Nr. of Rds.	Av. Plate Cracking	Nr. of Rds.	Av. Plate Cracking	Nr. of Rds.	Av. Plate Cracking
0 - 2" **								
912 - 961	1	0.3"	2	1"	1	0	1	1.0"
862 - 911	2	3.2	2	0	2	0	2	10.5
812 - 861								
2 - 4" **								
912 - 961	1	C					1	9.5"
862 - 911	1	C					1	0
812 - 861	1	C						36"

Projectile - 75 mm. T21

\*\* Distance from center of impact to center of weld

TABLE IIC

Ballistic Severity Table for Unionmelt Welded 1 Inch Thick Rolled Homogeneous Armor "H" Plates

Vel. f/s	1st Round		2nd Round		3rd Round		4th Round	
	No. of Rds.	Av. Weld Cracking	No. of Rds.	Av. Weld Cracking	No. of Rds.	Av. Weld Cracking	No. of Rds.	Av. Weld Cracking
0 - 2" **								
*750 - 800	2	2.3"	1	8.0"	1	15.3"		
700 - 750								
Projectile - 75 mm. T21								
Projectile - 57 mm. T1								
0 - 2" **								
1150-1200			2	0	1	4.4	13.3"	13.5"
1100-1150	1	0	1	2.5	1	12.5	0	0.3
1050-1100								
2 - 4" **								
1150-1200								
1100-1150	1	0						
1050-1100								
4+ " **								
1150-1200								
1100-1150	1	0						
1050-1100								

\* Specified velocity range

\*\* Distance from center of impact to center of weld

TABLE II

Ballistic Severity Table for Hand Welded 1 Inch Thick  
Cast Homogeneous Armor "H" Plates

Vel. f/s	1st Round		2nd Round		3rd Round		4th Round	
	No. of Rds.	Av. Weld Cracking	No. of Rds.	Av. Weld Cracking	No. of Rds.	Av. Plate Cracking	No. of Rds.	Av. Plate Cracking
Projectile - 57 mm. T1								
C - 1-3/4"***								
1100-1200	1	37.8"	1	0	2	1.5"	2	10.8"
1050-1100	1	1.3	3	5.9	2	7.5	2	0.9"
1000-1050	5	7.3	7	11.7	2	1.8	2	3.9
950-1000	18	11.9	8	12.2	3	6.0	2	5.4
800- 950					1	2.5	2	4.8
1-3/4 - 3"***								0
1050-1100			1	3.3		1.5		
1000-1050			1	10.5	2	18.1		
950-1000	5	8.5	1	.5				
3 - 6"***								
1000-1050			1	19.0		0		
950-1000			1	10.5	3	19.5	1	11.3
								1.7
								0
								1.5

Projectile - 75 mm. T21

0 - 2"\*\*\*  
850 - 900 1 4.8 36.0

\*\* Distance from center of impact to center of weld

TABLE IIe

Ballistic Severity Table for 3/4 Inch Thick  
Rolled Homogeneous Armor "H" Plates

Vel. f/s	<u>1st Round</u>		<u>2nd Round</u>		<u>3rd Round</u>	
	<u>Av. Plate</u>	<u>Av. Weld</u>	<u>Av. Plate</u>	<u>Av. Weld</u>	<u>Av. Plate</u>	<u>Av. Weld</u>
	<u>Cracking</u>	<u>Cracking</u>	<u>Cracking</u>	<u>Cracking</u>	<u>Cracking</u>	<u>Cracking</u>
C - 1-3/4"***			Projectile - 57 mm. T1			
700 - 775			2	0	0	6.5"
775 - 825	6	4.1"	5	3.0"	3	7.1
825 - 875	2	5.0	4	7.9	4	10.4
1-3/4 - 3"***						
700 - 775	2	0	4	0	2	3.5
775 - 825	8	2.0			4	5.5
825 - 875					1	3.8
over 3"***						
700 - 775	1	0	1	0	1	0
775 - 825	3	4.0	3	0	2	0
825 - 875			3	0		0
C - 1-3/4"***			<u>5th Round</u>		<u>6th Round</u>	
700 - 775	1	19.3	3	4.8	3	5.3
775 - 825	1	8.0	2	14.0		
825 - 875						
1-3/4 - 3"***						
700 - 775	3	0	1	0		
775 - 825	1	0	1	4.0		
825 - 875						
over 3"***						
700 - 775	2	4.0	1	0	1	0
775 - 825	1	0				
825 - 875						

\*\* Distance from center of impact to center of weld

TABLE III

Fabricators of Hand Welded 1 Inch Thick Rolled Homogeneous Armor "H" Plates

Armor Fabricator	Projectile	No. of Plates	No. of Rounds	Av. Weld Crkg./Rd.	Av. Plate Crkg./Rd.	Remarks
American Car & Foundry	75 mm. T21	6	8	22.7"	0.3"	1 rd. outside 2" limit
Cadillac	57 mm. T1	4	17	3.4	4.9	7 rds. outside 1-3/4" limit 2 " below specified velocity 5 " above " 1 " velocity lost
	75 mm. T21	29	58	13.7	1.1	10 rds. outside 2" limit 10 " below specified velocity 1 " above "
Caterpillar	75 mm. T21	3	6	9.0	0.9	1 rd. below specified velocity
Firestone	75 mm. T21	1	3	12.4	0.	1 rd. outside 2" limit 1 " below specified velocity
General Motors Truck	57 mm. T1	7	27	5.1	1.5	12 rds. outside 1-3/4" limit 1 " below specified velocity 9 " above "
Gordon Mfg.	75 mm. T21	2	3	18.7	0.	
Heil	75 mm. T21	7	15	10.2	0.5	1 rd. outside 2" limit 3 " above specified velocity
International Harvester	75 mm. T21	1	2	13.3	0.	1 rd. outside 2" limit
Kay Brunner	75 mm. T21	1	3	10.1	0.	1 rd. outside 2" limit 2 " below specified velocity
Maremont	75 mm. T21	1	1	18.3	6.0	

TABLE III (Cont.)

Armor Fabricator	Projectile	No. of Plates	No. of Rounds	Av. Weld Crkg./Rd.	Av. Plate Crkg./Rd.	Remarks
Pullman Standard	75 mm. T21	5	14	9.1	2.2	3 rds. outside 2" limit 4 " below specified velocity 2 " above "
So. California, Div. GMC	75 mm. T21	3	8	12.0	1.3	3 rds. outside 2" limit 3 " below specified velocity
Ternstedt	75 mm. T21	28	52	13.7	4.6	9 rds. outside 2" limit 10 " below specified velocity



TABLE IV (Cont.)

Mfr.	Armor	Type	Chemical Composition	°F	Heat Treatment Hold (Hrs.)	Quench	BHN	No. of Plates	No. of Rds.	Av. Crkg./Rd.	Weld	Flate	Remarks	
Jones & Laughlin		III	.32 - .36 C	1625-	2 -	Water	302-	2	10	2.7	0.5		5 rds. outside 1-3/4" limit	
		Mn-Mo	1.71 - 1.77 Mn	1650	3-1/2	Air	341						1 " below spec. vel.	
		Above	.18 - .29 Si	970-	2 -									4 " above "
		.30 C	.43 - .54 Mo	1060	4									1 " velocity lost
													Projectile - 57 mm. T1	
								1	2	12.6	0.		1 rd. outside 2" limit	
													Projectile - 75 mm. T21	
Below .31 C			.23 - .26 C	1600-	1/2 -	Water	315-	15	28	12.9	0.1		5 rds. outside 2" limit	
			1.16 - 1.75 Mn	1640	3-3/4	Air	341						1 " below spec. vel.	
			.19 - .24 Si	875-	1-1/2 -									
			.41 - .55 Mo	1060	3-1/2									
													Projectile - 75 mm. T21	
													AVERAGE 2 TYPES ( 75 mm. T21)	
													16	
													30	
													12.9	
													0.09	
													6 rds. outside 2" limit	
													5 " below spec. vel.	
Youngstown Sheet & Tube		III	.20 - .29 C	1600-	1 -	Water	285-	7	15	13.4	2.4		2 rds. outside 2" limit	
		Mn-Mo	1.12 - 1.55 Mn	1625	2-1/4	Air	334						4 " below spec. vel.	
			.10 - .44 Si	875-	2-1/2 -									
			.26 - .64 Mo	1060	4									
													Projectile - 75 mm. T21	

TABLE Va

Electrode Data for Hand Welded 1 Inch Thick Rolled Homogeneous Armor "H" Plates

Electrode Mfr.	Brand	Weld Metal Composition	Coating	No. of Plates	No. of Rounds	Av. Cracking/Rd. Plate	Remarks
Alloy Rods	Armcrarc Type A7	.09 C 1.64 - 1.90 Mn .25 - .50 Si 18.7 - 20.28 Cr 10.3 - 10.9 Ni 2.5 Mo	Titania	2	5	16.3"	0.0" 1 rd. outside 2" limit 1 " below spec. vel.
						Projectiles - 75 mm. T21	
	Armcrarc Type B	.03 - .13 C 3.5 - 4.5 Mn .35 - .70 Si 19.8 - 21. Cr 8.5 - 10.5 Ni	Titania	1	1	23.3	7.3
						Projectiles - 75 mm. T21	
	AVERAGE 2 BRANDS			3	6	17.5	1.3
Crucible	Armcrarc	.06 - .15 C 1.8 - 2.1 Mn .22 - .80 Si 18.2 - 20.5 Cr 8.1 - 10. Ni 1.61 - 2. Mo .2 V	Titania	3	4	18.5	1.5
						Projectiles - 75 mm. T21	
Harnischfeger	AW3	.1 C 1.5 - 1.75 Mn .45 - .58 Si 18.8 - 19.4 Cr 10.4 - 11.4 Ni 2.2 Mo	Lime	1	3	4.6	0. 1 rd. outside 1-3/4" limit
						Projectiles - 57 mm. T1	
				1	3	9.9	0.
						Projectiles - 75 mm. T21	

TABLE Va (Cont.)

Electrode Mfg.	Brand	Weld Metal Composition	Coating	No. of Plates	No. of Rounds	Av. Cracking/Rd. Weld	Plate	Remarks
Harnischfeger (Cont.)	AW3C	.11 - .12 C	Lime	1	4	1.1"	3.6"	2 rds. outside 1-3/4" limit
		.45 - .50 Mn		Projectile - 57 mm. T1				2 " above spec. vel.
		18.5 - 19. Cr		1	2	9.0	3.6	
		9.35 - 10.4 Ni		Projectile - 75 mm. T21				
		.92 - 1.1 Mo						
AVERAGE 2 BRANDS		(57 mm. T1) (75 mm. T21)		2	7	2.3	2.1	
				2	5	9.6	1.5	
Hollup	Armored	Not given		1	3	11.8	0.	1 rd. outside 2" limit
				Projectile - 75 mm. T21				1 " below spec. vel.
Lincoln	Armorweld	.08 - .10 C	Lime	3	9	7.1	6.5	1 rd. outside 1-3/4" limit
		3.5 - 4.5 Mn		Projectile - 57 mm. T1				1 " above spec. vel.
		.45 - .80 Si		3	5	17.0	0.	
		19. - 20.8 Cr		Projectile - 75 mm. T21				
		8. - 10.1 Ni						
		.06 - .1 Mo						
McKay	Armorloy A-5	.10 - .13 C	Lime	4	17	4.2	2.1	9 rds. outside 1-3/4" limit
		3.6 - 4.2 Mn		Projectile - 57 mm. T1				4 " above spec. vel.
		1.0 - 1.1 Si		4	4	34.3	0.	
		18.1 - 19.4 Cr		Projectile - 75 mm. T21				
		8.2 - 10.2 Ni						
		.47 - .56 Mo						
		.08 - .13 C		31	64	13.5	1.2	13 rds. outside 2" limit
		3.6 - 4.8 Mn						12 " below spec. vel.
		.42 - .80 Si						5 " above spec. vel.
		17.9 - 20.6 Cr						
		9.6 - 10.6 Ni						
		.06 - .18 Mo						
AVERAGE 2 BRANDS								
				Projectile - 75 mm. T21				



TABLE Va (Cont.)

Electrode Mfr.	Brand	Weld Metal Composition	Coating	No. of Plates	No. of Rounds	Average Cracking/Rd. Weld	Cracking/Rd. Plate	Remarks
A. O. Smith	SW-164	.08 C 3.5 Mn .35 Si 19. Cr 10. Ni 1. Mo	Lime	2	5	7.4"	0.	1 rd. outside 2" limit 1 " above spec. vel.
Projectile - 75 mm. T21								

TABLE Vb

Electrode Type	Weld Analysis	No. of Plates	No. of Rounds	Average Cracking/Rd. Weld	Cracking/Rd. Plate	Remarks
Mn-Mo Mod. 18/8	At least 1% Mn and .2% Mo	18	34	14.6"	1.3"	5 rds. outside 2" limit 4 " below spec. vel. 1 " above spec. vel. 12 rds. outside 1-3/4" limit 6 " above spec. vel. 1 " below spec. vel.
Mn Mod. 18/8	At least 1% Mn and less than .2% Mo	38	76	13.5	1.2	13 rds. outside 2" limit 14 " below spec. vel. 5 " above spec. vel. 3 rds. outside 1-3/4" limit 1 " below spec. vel. 3 " above spec. vel. 1 " velocity lost
Projectile - 57 mm. T1						

TABLE VI

Joint Design Data for Hand Welded 1 Inch Thick Rolled Homogeneous Armor "E" Plates

Angle of Bevel	Projectile	No. of Plates	No. of Rounds	Av. Cracking/Round Weld	Plate	Remarks
24° DV	75 mm. T21	2	2	42.0"	0."	
40° SV DV	75 mm. T21	2	3	15.5	1.8	
	75 mm. T21	2	2	26.6		
45° DV	75 mm. T21	7	15	12.0	0.8	3 rds. outside 2" limit 2 " above specified velocity
	57 mm. T1	6	23	5.3	1.8	10 rds. outside 1-3/4" limit 7 " above specified velocity 2 " below specified velocity
50° DV	75 mm. T21	1	1	18.3	6.0	
60° DV	75 mm. T21	70	142	13.0	2.4	27 rds. outside 2" limit 26 " below specified velocity 2 " above specified velocity
	57 mm. T1	5	21	3.6	3.9	7 rds. outside 1-3/4" limit 3 " above specified velocity 2 " below specified velocity
70° DV	75 mm. T21	2	5	6.1		1 rd. outside 2" limit 1 " below specified velocity

TABLE VI (Cont.)

Root Gap	Projectile	No. of Plates	No. of Boards	Av. Cracking/Round Weld Plate	Remarks	
1/8"	75 mm. T21	6	14	7.5"	5.2"	1 rd. outside 2" limit 1 " below specified velocity 2 " above specified velocity
5/32	75 mm. T21	7	15	13.2	1.0	2 rds. outside 2" limit 3 " below specified velocity
3/16	75 mm. T21	40	73	13.7	3.5	14 rds. outside 2" limit 11 " below specified velocity
	57 mm. T1	9	36	4.4	1.8	16 rds. outside 1-3/4" limit 8 " above specified velocity 3 " below specified velocity
1/4	75 mm. T21	16	32	13.9	0.9	6 rds. outside 2" limit 8 " below specified velocity
5/16	75 mm. T21	2	4	12.9	0.	1 rd. outside 2" limit 1 " above specified velocity
3/8	75 mm. T21	7	19	9.1	1.7	6 rds. outside 2" limit 2 " above specified velocity 4 " below specified velocity
7/16	75 mm. T21	1	2	9.8	0.	1 rd. outside 2" limit 1 " below specified velocity
1/2	75 mm. T21	2	4	17.8	0.	1 rd. below specified velocity

TABLE VI (Cont.)

Plate Preparation	Projectile	No. of Plates	No. of Rounds	Av. Cracking/Weld	Round Plate	Remarks
Flame cutting	57 mm. T1	7	27	5.1"	1.5"	11 rds. outside 1-3/4" limit 7 " above specified velocity 2 " below specified velocity
Flame cutting and grinding	75 mm. T21	70	135	14.0	2.3	27 rds. outside 2" limit 24 " below specified velocity 1 " above specified velocity
	57 mm. T1	4	17	3.4	4.9	7 rds. outside 1-3/4" limit 3 " above specified velocity 2 " below specified velocity
Flame cutting, grinding, and machining	75 mm. T21	4	7	8.6	3.5	2 rds. below specified velocity
Flame cutting, flame softening and planing	75 mm. T21	1	1	18.3	6.0	
Flame cutting, grinding machining and buttering	75 mm. T21	10	26	9.8	0.5	4 rds. outside 2" limit 4 " above specified velocity 3 " below specified velocity

TABLE VII

Welding Procedure for Hand Welded 1 Inch Thick Rolled Homogeneous Armor "H" Plates

No. of Passes	Projectile	No. of Plates	No. of Rounds	Av. Cracking/Weld	Round Plate	Remarks
4	75 mm. T21	3	5	18.1"	3.3"	1 rd. outside 2" limit
6	75 mm. T21	46	85	14.3	2.15	16 rds. outside 2" limit 14 " below specified velocity
7	57 mm. T1	1	2	13.6	0.6	
8	75 mm. T21	1	3	12.4	0.	1 rd. outside 2" limit
8	57 mm. T1	1	6	4.6	1.6	3 rds. outside 1-3/4" limit 1 " below specified velocity 2 " above specified velocity
10	75 mm. T21	15	30	12.6	1.4	5 rds. outside 2" limit 6 " below specified velocity 1 " above specified velocity
11	57 mm. T1	5	21	4.7	3.6	9 rds. outside 1-3/4" limit 1 " below specified velocity 6 " above specified velocity
12	57 mm. T1	1	4	1.8	5.9	2 rds. outside 1-3/4" limit 1 " above specified velocity 1 " below specified velocity
12	75 mm. T21	2	5	11.3	0.	1 rd. outside 2" limit 2 " below specified velocity
13	75 mm. T21	3	8	12.9	2.3	1 rd. outside 2" limit 2 " above specified velocity
14	75 mm. T21	5	10	8.6	3.7	1 rd. outside 2" limit 3 " below specified velocity 2 " above specified velocity
9	57 mm. T1	1	4	1.1	0.	2 rds. outside 1-3/4" limit 1 " below specified velocity 1 " above specified velocity

TABLE VII (Cont.)

No. of Passes	Projectile	No. of Plates	No. of Rounds	Av. Cracking/Weld	Round Plate	Remarks
15	75 mm. T21	3	8	10.3"	0."	3 rds. outside 2" limit 1 " below specified velocity
	57 mm. T1	1	4	4.4	0.	1 rd. outside 1-3/4" limit
16	75 mm. T21	4	11	7.5	6.2	2 rds. outside 2" limit 2 " below specified velocity
17	75 mm. T21	3	5	16.5	0.	1 rd. outside 2" limit
18	75 mm. T21	1	1	25.3	0.	
20	57 mm. T1	1	3	4.6	0.	1 rd. outside 1-3/4" limit
34	75 mm. T21	1	2	19.1	0.	1 rd. below specified velocity

Backing	Projectile	No. of Plates	No. of Rounds	Av. Cracking/Weld	Round Plate	Remarks
Copper	75 mm. T21	45	93	12.6"	3.0"	19 rds. outside 2" limit 18 " below specified velocity 3 " above specified velocity
	57 mm. T1	2	9	2.1	2.6	5 rds. outside 1-3/4" limit 1 " below specified velocity 1 " above specified velocity
Mild Steel	75 mm. T21	2	2	42.0		
None	75 mm. T21	2	3	15.5	1.8	

TABLE VII (Cont.)

Root Deposition Type	Projectile	No. of Plates	No. of Rounds	Av. Cracking/Round Plate	Weld	Remarks	
I Single bead at root	75 mm. T21	11	24	1.2"	13.4"	3 rds. outside 2" limit	
						2 "	2 " above specified velocity
						2 "	2 " below specified velocity
II Two beads at root	75 mm. T21	76	149	2.3	13.2	28 rds. outside 2" limit	
						26 "	26 " below specified velocity
						3 "	3 " above specified velocity
Body Deposition Type I Layers only	75 mm. T1	11	44	2.8	4.5	18 rds. outside 1-3/4" limit	
						10 "	10 " above specified velocity
						4 "	4 " below specified velocity
II Beads only	75 mm. T21	68	134	1.8	13.5	24 rds. outside 2" limit	
						23 "	23 " below specified velocity
						5 "	5 " above specified velocity
						16 rds.	16 rds. outside 1-3/4" limit
						10 "	10 " above specified velocity
III Layers and beads	75 mm. T1	4	7	3.4	4.5	4 "	
						4 "	4 " below specified velocity
						1 rd.	1 rd. outside 2" limit
						1 "	1 " below specified velocity
Crown Deposition Type I Single crown	75 mm. T21	1	3	9.7	4.6	1 rd. outside 1-3/4" limit	
						0	1 rd. outside 1-3/4" limit
						1.3	6 rds. outside 2" limit
						9.9	5 "
						0	1 rd. outside 1-3/4" limit
Crown Deposition Type I Single crown	75 mm. T1	1	4	2.1	4.4	18 rds. outside 2" limit	
						14.3	12 " below specified velocity
						1.4	3 rds. outside 1-3/4" limit
						6.8	1 " below specified velocity
						8	2 " above specified velocity

TABLE VII (Cont.)

Crown Deposition Type (Cont.)	Projectile	No. of Plates	No. of Rounds	Av. Cracking/ Round Weld	Plate	Remarks
II and III	75 mm. T21	37	80	11.7"	2.1"	14 rds. outside 2" limit
Multiple crown	57 mm. T1	9	36	3.9	3.1	14 " below specified velocity
						5 " above specified velocity
						15 rds. outside 1-3/4" limit
Preheat 'F	75 mm. T21	74	147	13.7	2.4	8 " above specified velocity
						3 " below specified velocity
						30 rds. outside 2" limit
70 - 100	57 mm. T1	11	44	4.5	2.8	26 " below specified velocity
115	75 mm. T21	2	4	9.9	1.8	3 " above specified velocity
						17 rds. outside 1-3/4" limit
						10 " above specified velocity
120	75 mm. T21	4	7	14.4		4 " below specified velocity
150	75 mm. T21	2	5	6.5		1 rd. above specified velocity
						1 rd. above specified velocity
100	75 mm. T21	1	1	18.5	6.0	1 rd. outside 2" limit
200 - 500	75 mm. T21	3	6	9.0	0.9	1 rd. below specified velocity

TABLE VIII

Radiographic Data for Hand Welded 1 Inch Thick Rolled Homogeneous Armor "H" Plates

Radiographic Results	Projectile	No. of Plates	No. of Rounds	Av. Cracking/Weld	Cracking/Round Plate	Remarks
Passing	75 mm. T21	63	130	11.9"	1.8"	24 rds. outside 2" limit
						20 " below specified velocity
	57 mm. T1	9	39	3.7	1.8	5 " above specified velocity
						17 rds. outside 1-3/4" limit
Failing	75 mm. T21	24	43	17.2	2.9	10 " above specified velocity
						4 " below specified velocity
	57 mm. T1	2	5	10.2	11.0	8 rds. outside 2" limit
						9 " below specified velocity

TABLE IX

Average Weld and Plate Cracking for 1 Inch "H" Plates

No. of Plates	Projectile	Av. Cracking/Weld	Round Plate	Remarks
1 Inch Hand Welded Rolled Armor	57 mm. T1	4.5"	2.8"	19 rds. outside 1-3/4" limit 3 " below specified velocity 14 " above specified velocity 1 " velocity lost
	75 mm. T21	13.2	2.1	30 rds. outside 2" limit 31 " below specified velocity 6 " above specified velocity
	57 mm. T1	6.0	1.8	4 rds. outside 1-3/4" limit 3 " above specified velocity 1 " below specified velocity
1 Inch Unionmelt Welded Rolled Armor	75 mm. T21	15.6	4.2	3 rds. above specified velocity
	57 mm. T21	3.6	10.3	19 rds. outside 1-3/4" limit 28 " above specified velocity 1 " below specified velocity
1 Inch Hand Welded Cast Armor	75 mm. T21	36.0	4.7	

TABLE X

Armor Data for Hand Welded 1 Inch Thick Cast Homogeneous Armor "H" Plates

Mfg.	Armor Type	Chemical Composition	Heat Treatment °F	Heat Hold (Hrs.)	Quench	BHN	No. of Plates	No. of Rds.	Av. Crkg./Rd.	Weld Plate	Remarks
American Steel Foundries	II	.33 C	1650	2	Air	277-	2	5	1.3"	13.2"	2 rds. above spec. vel.
	Mn-Cr	1.53 Mn	1525	.67	Water	321					4 " outside 1-3/4" limit
	Mo	.42 Si .34 Cr .07 Mo	1180	4	Water						
Ford	II	.30 C	1800	5	Air	241-	1	1	36.0	4.8	Projectile - 57 mm. T1
	Mn-Cr-Mo	1.10 - 1.20 Mn .47 - .50 Si .35 - .38 Mo	1700 1020	3 6 - 8	Water Water	302					
											Projectile - 75 mm. T21
Hughes Tool Co.	I	.25 - .31 C	1900	10	---	221-	9	28	3.4	3.4	6 rds. outside 1-3/4" limit
	Mn-Cr-Mo-Ni	.85 - 1.80 Mn .37 - .45 Si .28 - .70 Cr	1200 1650 1000	2 1 4	Air Water Air	366					15 " above spec. vel. 1 " below spec. vel.
		1.00 - 1.23 Ni .38 - .53 Mo									Projectile - 57 mm. T1
Kelsey Hayes	II	.28 - .31 C	1950	10	Air	286-	6	15	5.4	9.7	2 rds. outside 1-3/4" limit
	Mn-Cr-Mo	.90 - 1.28 Mn .37 - .47 Si .43 - .57 Cr .32 - .48 Mo	1250 1650 1150 1800 1650 1075	4 5 10 5 3 6	Air Air Water Air Water Water	340					4 " above spec. vel.
		.28 - .30 C 1.54 - 1.79 Mn .51 - .57 Si .06 - .12 Ni .50 - .67 Mo	1800 1600 1060	4 4 4	Air Water Water	286- 321					
McCormick & Torley	III	.28 - .30 C	1800	4	Air	286-	6	16	1.8	2.3	5 rds. outside 1-3/4" limit
	Mn-Mo	1.54 - 1.79 Mn .51 - .57 Si .06 - .12 Ni .50 - .67 Mo	1600 1060	4 4	Water Water	321					
											Projectile - 57 mm. T1



TABLE XI

Radiographic Data for Hand Welded 1 Inch Thick Cast Homogeneous Armor "H" Plates

<u>Radiographic Results</u>	<u>Projectile</u>	<u>No. of Plates</u>	<u>No. of Rounds</u>	<u>Av. Cracking/ Weld</u>	<u>Cracking/ Plate</u>	<u>Remarks</u>
Passing	57 mm. T1	22	53	3.9"	11.6"	12 rds. outside 1-3/4" limit 18 " above spec. vel.
	75 mm. T21	1	1	36.0	4.8	
Failing	57 mm. T1	8	25	3.0	8.9	7 rds. outside 1-3/4" limit 10 " above spec. vel. 1 " below spec. vel.

TABLE XII

Armor Data for Ford Welded 3/4 Inch Thick Rolled Homogeneous Armor "H" Plates

Mfr.	Armor Type	Chemical Composition	Heat Treatment °F Hold(Ers.)	Quench	BHN Plates	No. of Plates	No. of Rds.	Av. Crkg./Rd. Weld Plate	Remarks
E. C. Atkins	IV Mn-Cr- Mo-Si	.29 - .32 C .77 - .94 Mn .57 - .81 Si .61 - .70 Cr .20 - .22 Mo 0 - .08 Zr	1610- 1625 940- 1030	Water 70 min. to 2 hrs. Air	360- 364	5	22	4.4" 5.6"	10 rds. outside 1-3/4" limit 10 " above spec. vel. 2 " below spec. vel.
Carnegie-Illinois	I Mn-Ni- Cr-Mo	.26 C 1.06 Mn .19 Si .45 Cr .95 Ni .42 Mo	Not Given		332	2	5	7.4 3.3	1 rd. outside 1-3/4" limit 1 " above spec. vel. 2 " below spec. vel.
Chevrolet Forge	IV Mn-Cr- Mo-Si	.28 - .30 C .89 - .90 Mn .73 - .76 Si .61 - .65 Cr .19 - .23 Mo	1 1/2 - 1-2/3 hr. 6	Water Air	321- 339	4	19	2.1 0.6	15 rds. outside 1-3/4" limit 5 " above spec. vel. 2 " below spec. vel.
Ford Motor	II Mn-Cr- Mo	.27 - .29 C 1.38 - 1.49 Mn .25 - .30 Si .55 - .72 Cr .42 - .47 Mo	2 - 4 4 - 6	Platen Air	Not Given	3	9	4.1 4.0	5 rds. outside 1-3/4" limit 2 rds. above spec. vel. 2 " below spec. vel.
Great Lakes	IV Mn-Cr- Mo-Si	.32 C .90 Mn .75 Si .68 Cr .21 Mo	52 min - 1-2/3 hrs. 70 min. - 6 hrs.	Water Air	341- 363	6	25	5.2 3.9	13 rds. outside 1-3/4" limit 7 " above spec. vel.

TABLE XII (Cont.)

Mfg.	Armor Type	Chemical Composition	°F	Heat Treatment Hold(Hrs.)	Quench	BHT	No. of Plates	No. of Rds.	Av. Crkg./Rd. Weld Plate	Remarks
Republic	V High Alloy	.23 - .25 C .48 - .54 Mn .33 - .34 Si 4.99 - 5.0 Ni .35 - .36 Mo		Not Given		268- 272	1	3	8.4" 0."	1 rd. outside 1-3/4" limit 1 " above spec. vel. 1 " below spec. vel.

TABLE XIII

Radiographic Data for Hand Welded 3/4 Inch Thick Rolled Homogeneous Armcr "H" Plates

Radiographic Results	Projectile	No. of Plates	No. of Rounds	Av. Cracking/Round		Remarks	
				Weld	Plate		
Passing	57 mm. T1	15	61	4.1"	3.2"	37 rds. outside 1-3/4" limit	
						20 "	above spec. vel.
						5 "	below spec. vel.
Failing	57 mm. T1	7	22	5.2	3.8	9 rds. outside 1-3/4" limit	
						6 "	above spec. vel.
						4 "	below spec. vel.

KEY TO TABULATION METHOD AND SYMBOLS

Figure 2 is a sample tabulation of firing record data and gives a key to symbols and method of tabulation. A brief explanation of the items in the tabulation follows:

1. Identification of Test

Information in the first column identifies the test.

2. Armor Data

A. Plate Thickness

Plates in this tabulation are of 1 and 3/4 inch thick homogeneous armor.

B. Type Armor

The following types are used:

R (Rolled)

Typical Analysis

	<u>Type</u>	<u>C</u>	<u>Mn</u>	<u>Si</u>	<u>Cr</u>	<u>Mo</u>	<u>Ni</u>	<u>Zr</u>
I	Mn-Ni-Cr-Mo	.26	1.15	.20	.60	.20	1.00	B added
II	Mn-Cr-Mo	.27	1.30	.25	.55	.42		
III	Mn-Mo	.25	1.60	.22	--	.37		Grainal
IV	Mn-Cr-Mo-Si	.27	.86	.79	.62	.17		.09
V	High Alloy	(Compositions noted in tabulation)						
VI	Special	"	"	"	"	"	"	"

C (Cast)

I	Mn-Cr-Mo-Ni	.29	1.00	.35	.55	.40	1.00	
II	Mn-Cr-Mo	.28	1.55	.45	.40	.30		
III	Mn-Mo	.30	1.58	.40	--	.50		
IV	Special	(Compositions noted in tabulation)						

C. Carbon Content

Carbon content is listed whenever given.

D. Brinell Hardness Number (BHN)

Brinell hardness number on both the front and back of plates is tabulated when given.

E. Process

This refers to the melting practice and is tabulated as open hearth, electric, basic or acid.

F. Heat Treatment

The temperature, time of hold, and type of quench and draw are recorded as given.

3. Electrode Data

These data, often incomplete, are listed as given in each firing record.

A. Type

Since alloys are sometimes added in the coating, electrodes are typed according to the chemical analysis of the weld metal when given.

The electrodes are typed as follows:

(1) (Austenitic)

I Mn-Mo Modified 18/8 (Cr-Ni-Fe Alloy)

Weld Analysis - at least 1% Mn and .3% Mo

II Mn Modified 18/8 (Cr-Ni-Fe Alloy)

Weld Analysis - at least 1% Mn and less than .3% Mo

III Mo Modified 18/8 (Cr-Ni-Fe Alloy)

Weld Analysis - at least .3% Mo and less than 1% Mn

IV Special

B. and C. Trade Name and Coating

Trade names and types of coating are listed when given.

D. Current and Polarity

These data are tabulated as DC straight (str.), DC reversed (rev.), or AC.

4. Joint Design

A. Groove, etc.

This item includes the type of groove (Single V bevel or double V bevel), the included angle, and the width of the root face whenever given.

B. Root Gap

This is the distance between the plates as set up for welding.

C. Plate Preparation

This indicates whether the plate edges to be welded together were flame cut, ground, machined, buttered, etc.

5. Welding Procedure

A. Backing

Backing if used, i.e. back-up bar, chill, filler and spacer strips, is noted.

B. Deposition

Figure 3 shows how the weld deposition is broken up into the root, body, and crown types. The size electrode is noted with the number of passes, type of passes, and the current and voltage. Passes are divided into two kinds: (1) layer, if the pass bridges the gap; and (2), bead, if the pass does not bridge the gap. Seal beads, when used, are noted with size electrode, current and voltage.

C. Total Welding Time and Interpass Temperature

These are listed as given.

D. Remarks

Any comments on chipping, grinding, and other special techniques used and not noted above which affect the ballistic results are listed under "remarks."

6. Heat

Preheat and postheat are tabulated when given.

7. Ballistic Results

Unless otherwise specified, the 75 mm. Proof Projectile T21 was used in the tests tabulated. Hits, velocity and location of each, cracking and remarks on cracking are listed. The types of weld and plate cracking are as follows:

Type I Cracking in fusion or heat-affected zones on front and back of plate.

Type II Cracking in fusion or heat-affected zones on one side of plate and weld metal on the other.

Type III Cracking in weld metal on both front and back of plate.

Type IV Star plate cracking.

Type V Linear plate cracks.

The remarks on cracking and results of radiographic examination are recorded in the last column.

## SPECIFICATION REQUIREMENTS FOR "H" WELDED PLATES

The following extracts from Specification AXS-497, Rev. 3, describes the present ballistic shock test.

Paragraph F-3a. (2) "Shock Tests. The welded plate shown in Fig. 1 shall be tested as shown below. Fig. 1 shows the areas designated for shock impacts. For the purpose of description these are divided in four 'specified areas' one above and one below the crossbar on each of the two vertical leg welds. Aiming points are indicated in Fig. 1.

"If the first round falls outside of the one of the four specified areas, another round shall be fired at a second specified area. If the second impact falls outside of the specified area and no cracking occurs in the weld, another round will be fired at a third specified area. This shall be continued until an impact is obtained within one of the four specified areas, but no more than four rounds will be fired at one plate. If the plate withstands all four rounds, all of which fall outside the specified areas, and the weld is not cracked, the plate will be considered acceptable."

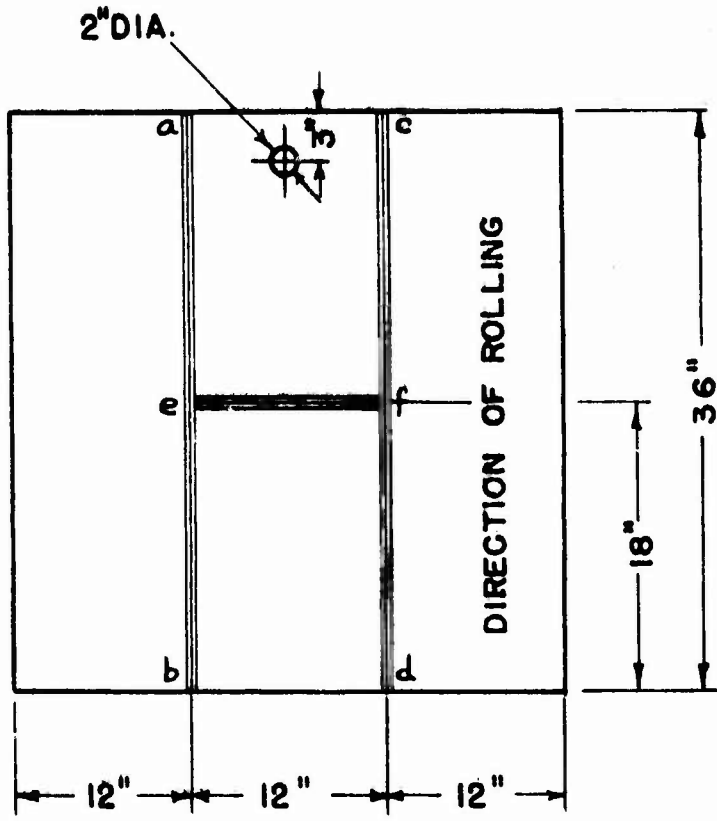
### BALLISTIC SHOCK TEST \*

Plate Thickness	Type	Projectile	Striking Velocity f/s	Allowable Distance, Center of impact to center of weld	Maximum Allowable Cracking Weld	Maximum Allowable Cracking Plate
1"	R.H.	75 mm. T21	775	2"	18"	8"
1"***	C.H.	57 mm. T1	975 ± 6 f/s per .01"	1-3/4"	8"	6"
3/4"***	R.H.	57 mm. T1	800	1-3/4"	12"	8"

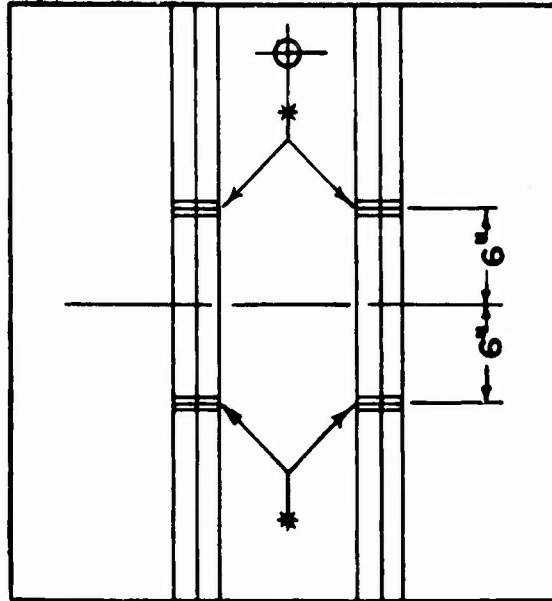
\* Effective during the period in which the plates in this tabulation were tested.

\*\*\* Specifications in a development stage.

WELD SEQUENCE:  
ab, cd, fe.



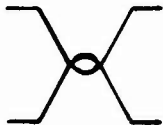
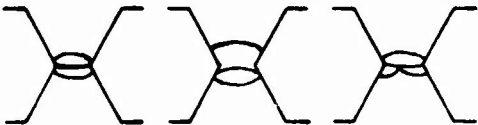
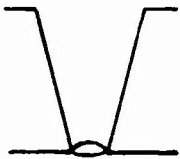
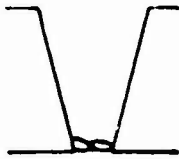
QUALIFICATION SHOCK TEST PLATE




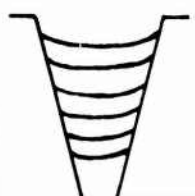




\* INTENDED AIMING POINTS

FIG. 1



ROOT TYPES	TYPE I	TYPE II
DOUBLE V BEVEL	 <p>SINGLE ROOT BEAD AT CENTER OF ROOT</p>	 <p>MORE THAN ONE BEAD AT ROOT ETC.</p>
SINGLE V BEVEL	 <p>SINGLE BEAD BRIDGING ROOT GAP</p>	 <p>MORE THAN ONE BEAD BRIDGING ROOT GAP ETC.</p>

BODY TYPES	TYPE I	TYPE II	TYPE III	TYPE IV	TYPE V
DOUBLE V BEVEL	 <p>LAYERS ONLY</p>	 <p>BEADS ONLY</p>	 <p>LAYERS &amp; BEADS</p>	UNIONMELT	SPECIAL
SINGLE V BEVEL	 <p>LAYERS ONLY</p>	 <p>BEADS ONLY</p>	 <p>LAYERS &amp; BEADS</p>	UNIONMELT	SPECIAL



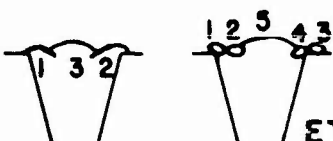
CROWN TYPES	TYPE I	TYPE II	TYPE III
DOUBLE V & SINGLE V BEVEL	 <p>SINGLE CROWN SINGLE PASS BRIDGES GAP</p>	 <p>MULTIPLE CROWN LAST BEAD TOUCHES PARENT METAL</p>	 <p>MULTIPLE CROWN LAST BEAD DOES NOT TOUCH PARENT METAL ETC.</p>

FIG. 3 WELD METAL DEPOSITION TYPES



IDENTIFICATION A. PART NUMBER B. DATE OF TEST C. P. ATE NO. D. ANNEAL MANUFACTURER E. ELECTRODE BRAND F. ANNEAL FABRICATOR	ANNEAL DATA A. PLATE THICKNESS B. PLATE GRADE C. CARBON CONTENT D. DIM E. PHASES F. HEAT TREATMENT G. TEMPER TIME	ELECTRODE DATA A. TYPE B. TRADE NAME C. COATING D. CURRENT E. POLARITY	JOINT DESIGN A. GROOVE INCLUDED B. ANGLE, ROOT FACE C. ROOT GAP D. PLATE PREPARATION	WELDING A. BACKING B. DEPOSITION C. ROOT TYPE D. ROOF TYPE E. COVER TYPE F. TOTAL WELDING TIME G. WINTER PROS H. TEMPERATURE	PROCESSES A. PASSES B. ROOF TYPE C. AMPT V D. AMPT A	HEAT A. PRE B. POST	BALLISTIC RESULTS A. LOCATION OF H B. LOC TYPE C. AMT	CRACKING A. TYPE B. AMT	REMARKS ON CRACKING A. RADIOGRAPHING RESULTS B. ETC.
A. AD-136 B. 12/15/42 C. Jones & Laughlin Steel Corp. D. McKay Company E. American Car & Foundry Co.	A. 1" R-III (1.57Mn, .23Si, .41Mo) C. .26 D. Face 323-337 E. Back 315-331 F. O.H. 1625°F. 2 hrs. 12" delay G. 975°F. 3 hrs. Air	A. A B. --- C. A-5 D. DC REV	A. 240V B. --- C. Flame Grinding Cutting	A. Mild steel B. 1. II 3/16" 1a 150 - 32 2a 185 - 32 3. I 1/4" 2a 195 - 32 1a 210 - 32 1a 300 - 32 C. S-1/2 hrs. 700 - 270°F. D.	1a 150 - 32 1a 185 - 32 2a 190 - 30 2a 200 - 30 1a 210 - 32 1a 300 - 32	A. 70°F. 1 B. None	775 1" R 9 1/2" Imp D	I 36"	Failed radiograph Incomplete fusion of 3/8" spacer strips present throughout the welds
A. AD-186 B. 1/14/43 C. Jones & Laughlin Steel Corp. D. McKay Company E. Crucible Co. F. American Car & Foundry Co.	A. 1" R-III (1.57Mn, .23Si, .41Mo) C. .26 D. Face 335-341 E. Back 335-341 F. O.H. 1625°F. 2 hrs. Full water G. 975°F. 3 hrs.	A. A B. A-5 C. DC REV	A. 600V B. 1/4" C. Flame Cutting Grinding	A. Copper B. 1. II 3/16" 1a 165 - 30 2a 190 - 30 3. I 3/16" 2a 190 - 30 1a 200 - 30 C. S-1/2 hrs. 700 - 300°F. D. Resistal was used in passes five and six. Chipping and grinding after first pass. Cracking after first pass.	1a 165 - 30 1a 190 - 30 2a 190 - 30 2a 200 - 30 1a 200 - 30	A. 70°F. 1 B. None	770 1" X 7 1/2" Imp D 3 771 3 780	I 23" III 9" V 23" III 14" III 14" I 6" II 14" III 3" 36"	Failed radiograph Excessive cracking and incomplete fusion
A. AD-188 B. 1/14/43 C. Jones & Laughlin Steel Corp. D. McKay Company E. Crucible Co. F. American Car & Foundry Co.	A. 1" R-III (1.57Mn, .23Si, .41Mo) C. .26 D. Face 337-341 E. Back 337-341 F. O.H. 1625°F. 2 hrs. Full water G. 975°F. 3 hrs.	A. A B. A-5 C. DC REV	A. 600V B. 1/4" C. Flame Cutting Grinding	A. Copper B. 1. II 3/16" 1a 165 - 30 2a 180 - 30 3. I 3/16" 2a 190 - 30 1a 200 - 30 C. S-1/2 hrs. 700 - 300°F. D. Resistal was used in passes five and six.	1a 165 - 30 1a 180 - 30 2a 190 - 30 2a 200 - 30	A. 70°F. 1 B. None	760 1" L 6 1/2" Imp D	I 8" II 11" III 20"	Passed radiograph Several small crater cracks



IDENTIFICATION	ANODIC DATA	ELECTRODE DATA	JOINT DESIGN	WELDING PROCEDURE	HEAT TREATMENT	GALLIUMS RESULTS	CRACKING	MARKS OR CRACKING
2. DATE OF TEST	2. TYPE	B. FRAME NAME	A. AMPL. ROOT FACE	B. DEPOSITION	A. POST	LOC. TYPE	MARKS OR CRACKING	MARKS OR CRACKING
3. PLATE NO.	3. CARBON CONTENT	C. COATING	B. ROOT GAP	C. DEPOSITION	B. POST	LOC. TYPE	MARKS OR CRACKING	MARKS OR CRACKING
4. ANODIC MANUFACTURER	4. SMM	C. SURF. PREP.	C. PLATE PREPARATION	D. ROOT TYPE	LOC. TYPE	MARKS OR CRACKING	MARKS OR CRACKING	MARKS OR CRACKING
5. ELECTRODE WFOF	5. PROCESS	D. POLARITY	1. ROOT TYPE	2. ROOT TYPE	LOC. TYPE	MARKS OR CRACKING	MARKS OR CRACKING	MARKS OR CRACKING
6. ANODIC FABRICATOR	6. HEAT TREATMENT	7. TEMP. TIME	2. ROOT TYPE	3. ROOT TYPE	LOC. TYPE	MARKS OR CRACKING	MARKS OR CRACKING	MARKS OR CRACKING
	7. TEMP. TIME	8. GUBSON	3. ROOT TYPE	4. ROOT TYPE	LOC. TYPE	MARKS OR CRACKING	MARKS OR CRACKING	MARKS OR CRACKING
A. AD-235	A. 1"	A. A-II	A. 60°DV	A. Not Given	A. None	4 1/2"	7"	Passed radiograph
B. 12/26/42	B. R-III	(.12-.15C, B. ---)	---	1. II 3/16"	B. None	2	3 1/2"	Large amount of incomplete fusion
C. 83	(1.77Mn, .18Si, .05Cr, .03Mn, .54Mo)	C. Flame	Cutting	2. I 1/4"		1	4 1/2"	
D. Jones & Laughlin Steel Corp.	C. 34	Grinding	Grinding	3. III 3/16"		2	5"	
E. Page Steel & Wire Company	D. Face 341			remainder not given		3	6 1/2"	
F. Cadillac Motor Car Company	O.H. 35-12.25			C. 2.26 hrs. 700 - 200°F.		3	6 1/2"	
	F. 1625°F. 2-1/4 hrs. Water 1030°F. 4 hrs. Air	D. DC REV		D. Some cracking after first pass. 10 mins. of oiling and grinding after first pass.		3	6 1/2"	
A. AD-235	A. 1"	A. A-II	A. 60°DV	A. Not Given	A. None	1 1/4"	5"	Failed radiograph
B. 2/11/43	B. R-IV	(.10C, 4.49 Mn, .52Si, .20Cr, .08Ni, .20Mo)	---	1. II 5/32"	B. None	1	5"	Failed radiograph
C. 86	(.94Mn, .86Si, .85Cr, .08Ni, .20Mo)	C. Flame	Cutting	2. I 3/16"		2	6"	Failed radiograph
D. Great Lakes Steel Corp.	C. 27	Grinding	Grinding	3. III 5/32"		3	6"	Failed radiograph
E. Lincoln Electric	D. Face 277			remainder not given		3	6"	Failed radiograph
F. Cadillac Motor Car Company	O.H. 35-12.25			C. 2.73 hrs. 700 - 1300°F.		3	6"	Failed radiograph
	F. 1625°F. 3-1/2 hrs. Water 1100°F. 4 hrs. Air	D. DC REV		D. Some cracking after first two passes.		3	6"	Failed radiograph
A. AD-161	A. 1"	A. A-II	A. 60°DV	A. Not Given	A. None	1"	4 1/2"	Failed radiograph
B. 1/1/43	B. R-V	(.09C, 4.85 Mn, .55Si, .20Mn, .11Ni, .22Mo)	---	1. II 3/16"	B. None	1	4 1/2"	Failed radiograph
C. 102	(.78Mn, .24Si, .63Cr, .11Ni, .22Mo)	C. Flame	Cutting	2. I 1/4"		2	4 1/2"	Failed radiograph
D. Great Lakes Steel Corp.	C. 28	Grinding	Grinding	3. I 5/16"		2	4 1/2"	Failed radiograph
E. McKay Company	D. Face 321			remainder not given		2	4 1/2"	Failed radiograph
F. Cadillac Motor Car Company	O.H. 35-12.25			C. 2.15 hrs. 700 - 200°F.		2	4 1/2"	Failed radiograph
	F. 1625°F. 2-1/2 hrs. Water 1030°F. 4 hrs. Draw	D. DC REV		D. Cracking after first two passes		2	4 1/2"	Failed radiograph







IDENTIFICATION A. FRAID RECORD NO. B. DATE OF TEST C. PLATE NO. D. JOINT MANUFACTURER E. ELECTRODE MPOR. F. AIRGAS FLOWMETER	ANODE METAL A. PLATE TENSILE B. GARDON CONTENT C. SIZE D. PROCESS E. HEAT TREATMENT F. TEST TIME	GALVANIC SERIES A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	JOINT PREP A. GROUND B. BEVEL C. PLATE PREPARATION	WELDING A. PROCEDURE B. WIRE C. WIRE TYPE D. WIRE SIZE E. WIRE TYPE F. WIRE SIZE G. WIRE TYPE H. WIRE SIZE I. WIRE TYPE J. WIRE SIZE	WEAR A. PACE B. POINT	BALLING RESULTS		REMARKS ON CRACKING RADIOGRAPHIC RESULTS	
						H. V/L	LOCATION OF N		
A. AD-273 B. 2/19/43 C. 123 D. Great Lakes Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-IV (.93Mn, .87Si, .63Cr, .17Mo, .07Zr) C. 27 Face 331 Back 352 E. 1650°F. 2 hrs. Water 970°F. 2 hrs. Air	A. A-II (.10C, 4.80 Mn, .6681, 17.40Cr, 9.75Ni, .08Mo) (.09C, 4.85 Mn, .5581, 10.20Ni, .15Mo) B. Armorloy C. ---- D. ----	A. 60°DV B. 5/16" C. Flame Cutting Grinding	A. Not Given B. II 3/16" 1a 160 - 25 1a 280 - 25 2. I 1/4" 1a 270 - 25 1a 240 - 25 3. III 5/32" 4b 135 - 25 remaining 3 beads not given C. 2.16 hrs. 70° - 190°F. D. Several crater cracks appeared in the first root pass.	A. None B. None	1 763	X	3 1/2" U X 5 1/2" D Imp I 23 1/2" III 1 1/2" 25"	Passed radiograph
A. AD-273 B. 2/19/43 C. 124 D. Great Lakes Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-IV (.93Mn, .87Si, .63Cr, .17Mo, .07Zr) C. 27 Face 331 Back 352 E. 1650°F. 2 hrs. Water 970°F. 2 hrs. Air	A. A-II (.10C, 4.80 Mn, .6681, 17.90Cr, 9.75Ni, .08Mo) (.09C, 4.85 Mn, .5581, 10.20Ni, .15Mo) B. Armorloy C. ---- D. ----	A. 60°DV B. 7/16" C. Flame Cutting Grinding	A. Not Given B. II 1/4" 1a 200 - 25 1a 240 - 25 2. I 1/4" 1a 260 - 25 1a 240 - 25 3. III 5/32" 2b 140 - 25 1b 280 - 25 remaining 3 beads not given C. 2.36 hrs. 70° - 305°F. D. ----	A. None B. None	1 750 2 665	1 1/2" R 2 1/2" R 1 1/2" D	Imp I 19" II 19 1/2" 19 1/2"	Passed radiograph
A. AD-309 B. 2/23/43 C. 114 D. Great Lakes Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-IV (.93Mn, .8381, .71Cr, .10Ni, .23Mo) C. 34 Face 302 Back 302 E. 1630°F. 3-1/2 hrs. Water 1020°F. 4 hrs. Air	A. A-II (.09C, 4.85 Mn, .5581, 21.00Cr, 10.20Ni, .15Mo) (.12C, 4.65 Mn, .6481, 18.00Cr, 9.62Ni, .07Mo) B. Armorloy C. ---- D. ----	A. 60°DV B. 3/16" C. Flame Cutting Grinding	A. Not Given B. II 3/16" 2a 180 - 25 2. I 3/16" 2a 180 - 25 3. I 1/4" 2a 240 - 25 C. 1.70 hrs. 70° - 160°F. D. ----	A. None B. None	1 752 2 787 3 794	1 1/2" R 4 1/2" L 2 1/2" L 4 1/2" D	Imp I 11" II 4 1/2" I 2 1/2" I 1 7/8" 3 1/2"	Passed radiograph Small crater cracks Small amount of incomplete fusion

PLATE DATA		PLATE TREATMENT		PLATE ANALYSIS		PREPARATION		EXAMINATION		QUALITY CONTROL		REMARKS	
A. PLATE NO.	B. TYPE	C. TREATMENT	D. TREATMENT	E. ANALYSIS	F. ANALYSIS	G. PREPARATION	H. EXAMINATION	I. QUALITY CONTROL	J. QUALITY CONTROL	K. REMARKS	L. QUALITY CONTROL	M. QUALITY CONTROL	N. REMARKS
1. PLATE NO.	2. TYPE	3. TREATMENT	4. TREATMENT	5. ANALYSIS	6. ANALYSIS	7. PREPARATION	8. EXAMINATION	9. QUALITY CONTROL	10. QUALITY CONTROL	11. REMARKS	12. QUALITY CONTROL	13. QUALITY CONTROL	14. REMARKS
A. AD-297 B. 3/6/43 C. 125 D. Youngstown Sheet & Tube Company E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-III (1.12Mn, .1981, .08Ni, .64Mo) C. .26 D. Face 286 Back 321 E. McKay Company F. Cadillac Motor Car Company	A. 1625°F. 1/2 hr. Water 101°F. 4 hrs. Air	A. 60°Dy B. 3/16" C. Flame Grinding	A. A-II (.10C, 4.80 Mn, .66Si, 17.90Cr, 9.75Ni, .08Mo) B. .85 C. .85 D. DC NEV	A. Not given B. II 5/32" 2a 140 - 25 1. II 3/16" 2a 180 - 25 2. I 5/32" 2b 130 - 25 3. III 1/4" 1b 240 - 25 5/32" 2b 140 - 25 C. 2.57 hrs. given 70° - 150°F.	A. None B. None	1 760 2 655	I 17" Imp L D 1" U O Imp R 1"	A. None B. None	Passed radiograph Small amount of incomplete fusion			
A. AD-297 B. 3/6/43 C. 127 D. Great Lakes Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-IV (.93Mn, .87Si, .63Cr, .17Mo, .07P) C. .27 D. Face 331 Back 353 E. 1650°F. 2 hrs. Water 970°F. 2 hrs. Air	A. 60°Dy B. --- C. Flame Grinding	A. A-II (.09C, 4.85 Mn, .66Si, 20.10Cr, 10.20Ni, .15Mo) B. .85 C. .85 D. DC NEV	A. Not given B. II 3/16" 1a 150 - 25 1. II 3/16" 1a 160 - 25 2. I 1/4" 2a 240 - 25 3. I 5/16" 2a 360 - 25 C. 1.77 hrs. given 75° - 190°F.	A. None B. None	1 775 2 760	I 16" Imp U 5" R 7" D O R 2 1/2"	A. None B. None	Passed radiograph				
A. AD-329 B. 3/15/43 C. 131 D. Youngstown Sheet & Tube Company E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-III (1.16Mn, .1891, .52Mo) C. .23 D. Face 331 Back 341 E. McKay Company F. Cadillac Motor Car Company	A. 60°Dy B. 3/16" C. Flame Grinding	A. A-II (.10C, 4.80 Mn, .66Si, 17.90Cr, 9.75Ni, .08Mo) B. .85 C. .85 D. DC NEV	A. Not given B. II 5/32" 1a 135 - 25 1. II 5/32" 7a 140 - 25 2. I 3/16" 1a 180 - 25 3. III 1/4" 1a 196 - 25 1b 240 - 25 3/32" 2b 140 - 25 C. --- D. --- given 70° - 145°F.	A. None B. None	1 779 2 767	I 14" Imp U 4" R 5" D R 17" 33"	A. None B. None	Passed radiograph Some incomplete fusion				

PLATE DATA		PLATE TREATMENT		PLATE ANALYSIS		PLATE IDENTIFICATION		PLATE HISTORY		PLATE CONDITION		PLATE LOCATION		PLATE WEIGHT		
A. YEAR	B. DATE	C. PLATE NO.	D. PLATE TYPE	E. PLATE SIZE	F. PLATE WEIGHT	G. PLATE TREATMENT	H. PLATE ANALYSIS	I. PLATE IDENTIFICATION	J. PLATE HISTORY	K. PLATE CONDITION	L. PLATE LOCATION	M. PLATE WEIGHT	N. PLATE WEIGHT	O. PLATE WEIGHT	P. PLATE WEIGHT	
A. AD-329	B. 3/15/43	C. 133	D. Great Lakes Steel Corp.	E. 10.10MI, .36Mo	F. 1650°F. 3 hrs. Water 970°F. 3 hrs. Air	G. 1. 100% Passed radiograph	H. A. I (.10C, 3.73 Mn, .36Si, 19.50Cr, 10.10MI, .36Mo) A-II (.10C, 4.80 Mn, .66Si, 17.90Cr, 9.75MI, .08Mo) B. Armorloy C. --- D. DC REV	I. 100% Passed radiograph	J. A. Not given B. 1. II 1/8" 1a 90 - 25 2a 110 - 25 3. I 5/32" 2a 110 - 25 3. I 5/32" 2a 130 - 25 C. 5.86 hrs. 70° - 105°F. D.	K. A. None B. None	L. 761	M. 8 1/2" L	N. 8 1/2" L	O. 8 1/2" L	P. 8 1/2" L	
A. AD-328	B. 3/23/43	C. 128	D. Youngstown Sheet & Tube Company	E. 10.10MI, .36Mo	F. 1650°F. 3 hrs. Water 970°F. 3 hrs. Air	G. 1. 100% Passed radiograph	H. A. I (.13C, 3.60 Mn, .48Si, 20.10Cr, 10.60MI, .11Mo) A-II (.12C, 3.45 Mn, .46Si, 19.60Cr, 10.40MI, .15Mo) B. Armorloy C. --- D. DC REV	I. 100% Passed radiograph	J. A. Not given B. 1. I 3/16" 1a 165 - 34 2. I 1/4" 1a 280 - 30 3/8" 1a 480 - 35 3/8" 1a 400 - 25 C. 92-1/2 mins. 900 - 285°F. D. Some cracking and 40 mins. of chipping and grinding after first pass.	K. A. None B. None	L. 783 2"	M. 6" U	N. 6" U	O. 6" U	P. 6" U	
A. AD-338	B. 3/23/43	C. 128	D. Great Lakes Steel Corp.	E. 10.10MI, .36Mo	F. 1650°F. 3 hrs. Water 970°F. 3 hrs. Air	G. 1. 100% Passed radiograph	H. A. I (.09C, 4.85 Mn, .55Si, 22.05Cr, 10.55MI, .10Mo) A-II (.08C, 4.50 Mn, .42Si, 20.40Cr, 10.10MI) B. Armorloy C. --- D. DC REV	I. 100% Passed radiograph	J. A. Not given B. 1. II 3/16" 1a 185 - 25 2. I 3/16" 1a 145 - 25 3. I 1/4" 2a 200 - 25 3. I 5/16" 2a 300 - 25 C. 1.68 hrs. 70° - 300°F. D.	K. A. None B. None	L. 751 1 1/2"	M. 5 1/2" D	N. 5 1/2" D	O. 5 1/2" D	P. 5 1/2" D	Q. 5 1/2" D

IDENTIFICATION	ANNEAL DATA	PLATE DATA	CHEMICAL DATA	JOINT DESIGN	WELDING PROCEDURE	WELD METAL	RADIATION RESULTS		REMARKS ON CRACKING
							WEL. TYPE	CRACKING	
A. PARTS USED IN TEST	A. PLATE THICKNESS	A. PLATE NUMBER	A. PLATE GRADE	A. JOINT DESIGN	A. WELDING PROCEDURE	A. WELD METAL	WEL. TYPE	CRACKING	REMARKS ON CRACKING
A. AD-338 B. 3/23/43 C. 139 D. Jones & Laughlin Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-III (.71Mn, .21Si, .45Mo) C. 36 D. Face 321 Back 340 E. McKay Company F. Cadillac Motor Car Company	A. 1650°F. 2 hrs. Water 970°F. 2 hrs. Air	A. A-II (.10C, 4.80 Mn, .68Si, 17.90Cr, 9.75Ni, .08Mo) B. 43Si, Mn, .45Si, 20.40Cr, 10.10Ni C. --- D. DC REV	A. 60DV B. 1/4" C. Flame Cutting Grinding	A. Not given B. II 5/32" 2a --- - 25 I 1/4" 2a --- - 25 III 5/32" 4b --- - 25 1/4" 1b --- - 25 C. 2.54 hrs. 700 - 190°F. D. Some cracking after first pass.	A. None B. None	7" U 3 1/2" R 9" D 1 1/2" 25"	I 11 1/2" II 11 1/2" I 1 1/2" II 2 1/2"	Failed radiograph Excessive incomplete fusion
A. AD-339 B. 3/23/43 C. 135 D. Youngstown Sheet & Tube Company E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-III (.14Mn, .21Si, .26Mo) C. 26 D. Face 321 Back 332 E. McKay Company F. Cadillac Motor Car Company	A. 1600°F. 1/2 hr. Water 875°F. 2-1/2 hrs. Air	A. A-II (.10C, 4.80 Mn, .68Si, 17.90Cr, 9.75Ni, .08Mo) B. 55Si, Mn, .55Si, 20.20Cr, 10.20Ni, .15Mo C. --- D. DC REV	A. 60DV B. 1/4" C. Flame Cutting Grinding	A. Not given B. II 5/32" 1a 135 - 25 I 1/4" 1a 165 - 25 III 5/32" 2a 240 - 25 1/4" 1b 240 - 25 C. 2.31 hrs. 700 - 150°F. D. ---	A. None B. None	4" L 7" U 6 1/2" D I 21" III 22"	Passed radiograph	
A. AD-339 B. 3/23/43 C. 136 D. Great Lakes Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-IV (.93Mn, .87Si, .62Cr, .17Mo) C. 27 D. Face 340 Back 302 E. --- F. 1650°F. 1-1/2 hrs. Water 970°F. 1-1/2 hrs. Air	A. 1650°F. 1-1/2 hrs. Water 970°F. 1-1/2 hrs. Air	A. A-I (.16C, 3.73 Mn, .36Si, 19.50Cr, 10.10Ni, .36Mo) B. 68Si, Mn, .68Si, 17.90Cr, 9.75Ni, .08Mo C. --- D. DC REV	A. 60DV B. 1/4" C. Flame Cutting Grinding	A. Not given B. II 1/8" 2a 90 - 25 I 5/32" 2a 115 - 25 III 5/32" 2a 115 - 25 C. 8.70 hrs. 700 - 95°F. D. ---	A. None B. None	1" L 4 1/2" D 1 1/2" X 6 1/2" R 3 692 4" 5" U 4 710 1 1/2" R 7" D 5 702 1 1/2" L 5" U 11 7" 11 1/2" 11 1/2" 11 1/2"	II 8 1/2" III 1 1/2" I 1 1/2" III 1 1/2" I 1 1/2" III 1 1/2" I 1 1/2" III 1 1/2" I 1 1/2" III 1 1/2" I 1 1/2" III 1 1/2"	Passed radiograph Small amount of slag inclusions

IDENTIFICATION	ANODE DATA	ELECTRODE DATA	WELDING PROCEDURE	HEAT TREATMENT	BALLBET RESULTS			REMARKS ON CRACKING RADIOGRAPH RESULTS, ETC.
					H V/W	LOCATION OF H	CRACKING	
A. FORD REPORT NO.	A. PLATE NUMBERING	A. TYPE	A. WELDING	A. NONE	L.L.	U.L.	LOC TYPE	AMT
B. DATE OF TEST	B. TYPE	B. TRADE NAME	B. DEPOSITION	B. NONE				
C. PLATE NO.	C. GARDON CONTENT	C. COATING	C. SIZE EL. NO. TYPE AMT					
D. MANUFACTURER	D. SIZE	D. CURRENT & POLARITY	D. ROOT TYPE					
E. ELECTRODE SPEC.	E. PROCESS	E. POLARITY	E. ROOT TYPE					
F. ANODE FABRICATOR	F. HEAT TREATMENT	F. AC REV	F. ROOT TYPE					
	F. TIME TIME CURRENT		F. TOTAL WELDING TIME & ENTER PASS TEMPERATURE					
A. AD-339 B. 3/23/43 C. 139 D. Great Lakes Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-IV C. .93Mn, .87Si, .63Cr, .17Mo D. Face 311 E. Back 302 F. 1650°F, 1-1/2 hrs. Water 970°F, 1-1/2 hrs. Air	A. A-I (.10C, 3.73 Mn, .36Si, 19.50Cr, 10.10Ni, .36Mo) B. 66Si C. 3/16" Flame D. Cutting E. Grinding	A. Not given B. II 1/8" 2a 90 - 25 C. I 5/32" 2a 115 - 25 D. 5/32" 2a 115 - 25 E. 4.29 hrs. 70° - 165°F.	A. None B. None	1/2" L	6" Imp D	I III V	2" Passed radiograph
A. AD-339 B. 3/23/43 C. 141 D. Great Lakes Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-IV C. .93Mn, .87Si, .63Cr, .17Mo D. Face 311 E. Back 302 F. 1650°F, 1-1/2 hrs. Water 970°F, 1-1/2 hrs. Air	A. A-II (.09C, 4.85 Mn, .55Si, 22.05Cr, 10.55Ni, .10Mo) B. 43Si C. 3/16" Flame D. Cutting E. Grinding	A. Not given B. II 3/16" 2a 180 - 25 C. I 1/4" 2a 260 - 25 D. 5/16" 2a 360 - 25 E. 1.97 hrs. 70° - 200°F.	A. None B. None	1/2" L	5" U 6" R 7" R U	I III II III	Passed radiograph Several inches of incomplete fusion
A. AD-339 B. 3/23/43 C. 142 D. Great Lakes Steel Corp. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. R-IV C. .93Mn, .87Si, .63Cr, .17Mo D. Face 311 E. Back 302 F. 1650°F, 3 hrs. Water 970°F, 3 hrs. Air	A. A-II (.10C, 4.80 Mn, .66Si, 17.90Cr, 9.75Ni, .08Mo) B. 53Si C. 3/16" Flame D. Cutting E. Grinding	A. Not given B. II 5/32" 1a 135 - 25 C. I 3/16" 1a 140 - 25 D. 5/32" 2a 180 - 25 E. 5/32" 4b 140 - 25 F. 1/4" 1b 240 - 25 G. remainder not given H. 2.64 hrs. 70° - 195°F. I. Some cracking after 7th and 8th passes.	A. None B. None	1/2" R	4" Imp U 9" O L D Imp	I III II III	Passed radiograph Some scattered slag inclusions



GENERAL INFORMATION	ANALYSIS DATA	WELDING DATA	WELDING PROCEDURE	WELDING MATERIAL	WELDING EQUIPMENT	WELDING POSITION	WELDING SPEED	WELDING DEFECTS	WELDING TESTS	WELDING RESULTS	REMARKS ON CHEMICAL ANALYSIS
A. AD-33 B. 10/9/43 C. H-4 D. Youngstown Sheet & Tube E. McKay Company F. Caterpillar Tractor Co.	A. 1" B. P-III (1.30Mn., .1581, .04Cr., .50Mo) C. .20 D. Face 321 E. Back 331 F. B.O.H. 16350F. 2-1/4 hrs. Water 10600F. 4 hrs.	A. A-II (.22C, 3.43 Mn., .65Si, 13.4Cr., 7.1Mn., .12Mo) B. Armorloy C. Heavy D. DC REV	A. 40°SV B. 5/32" C. Machining	A. None B. I 5/32" 1a 170 - 25 2a 175 - 26 2b 280 - 28 3a 1/4" 1a 280 - 26 2a 280 - 26 3. I 5/32" 1a 188 175 - 26 C. 3-3/4 hrs. 1600 - 500°f. D. Ground root after first pass. Time 3 hrs.	A. 2000 F. B. None	1 775 2 778	8" Imp D 2" 2 1/2" U L	II 10" V 4" II 7" III 1 1/2" V 1 1/2" II 4" III 2 1/2" 38"	Passed radiograph		
A. AD-74 B. 10/24/43 C. H-5 D. Great Lakes Steel Corp. E. McKay Company F. Caterpillar Tractor Co.	A. 1" B. R-IV (.94Mn., .81Si, .70Cr., .22Mo, .09Zr) C. .32 D. Face 393 E. B.O.H. 16500F. 3 hrs. Water 1200F. 4 hrs. Air 10500F. 2 hrs.	A. A-II (.22C, 3.43 Mn., .65Si, 13.4Cr., 7.1Mn., .12Mo) B. Armorloy C. Lime D. DC REV	A. 60°Py B. 1/8" C. Machining	A. Copper B. I II 5/32" 2a 160 - 24 2b 220 - 24 3a 1/4" 2a 280 - 24 C. 1.85 hrs. 1500 - 300°f. D. Root side of first pass on crossweld cracked nearly full length. Ground out and re-welded. Small amount of chipping. Time 4.50 hrs.	A. 2000 F. B. None	1 758 2 701 3 767	1" 8 1/2" R 2" 8" U 3" 2 1/2" L L	I 1" II 2 1/2" III 2 1/2" 7 1/2"	Passed radiograph Small crack in crossbar		
A. AD-33 B. 10/9/43 C. H-1 D. Great Lakes Steel Corp. E. McKay Company F. Caterpillar Tractor Co.	A. 1" B. R-IV (.94Mn., .81Si, .70Cr., .22Mo, .09Zr) C. .32 D. Face 393 E. B.O.H. 16500F. 3 hrs. Water 1200F. 4 hrs. Air 10500F. 2 hrs.	A. A-II (.22C, 3.43 Mn., .65Si, 13.4Cr., 7.1Mn., .12Mo) B. Armorloy C. Heavy D. DC REV	A. 40°SV B. 5/32" C. Machining	A. None B. I I 5/32" 1a 160 - 23 2a 170 - 25 2b 280 - 27 3a 1/4" 1a 280 - 27 3. I 5/32" 1b 170 - 25 C. 3-1/2 hrs. 1800°f. D. Small amount of chipping to remove weld spatter and slag. Time 2-1/2 hrs.	A. 2350 F. B. None	1 789	X 7 1/2" U	I 16" II 4" III 2 1/2" 2 1/2"	Passed radiograph		

Weld Metal Analysis Questionable

IDENTIFICATION	ANODE DATA	ELECTROLYTE DATA	CATHODE DESIGN	WELDING PROCEDURE	HEAT	BALLISTIC RESULTS		REMARKS ON CRACKING			
						H VEL. P/S	LOCATION OF H. CRACKING	CRACKING	RADIOGRAPHIC RESULTS		
A. PART NUMBER NO.	A. PLATE THICKNESS	A. TYPE	A. GROOVE INCLUDES	A. WELDING	A. POST	L.L.	R.L.	O.B.	LOC. TYPE	ASST	
B. DATE OF TEST	B. TYPE	B. TRADE NAME	B. ANGLE, ROOT FACE	B. DEPOSITION	B. NONE	1"	7"	Imp	II	8"	
C. PLATE NO.	C. GROSS WEIGHT	C. COATING	C. ROOT GAP	C. ROOT TYPE	B. None	L	D	D	III	SE	
D. MANUFACTURER	D. DIM	D. CORROSION POLARITY	D. PLATE PREPARATION	D. ROOT TYPE		3/16"	6 1/2"	O	III	incomplete penetration	
E. ELECTROLYTE SPEC.	E. PROCESS	E. POLARITY	E. GRINDING	E. GROWN TYPE		1/4"	U	O	III		
F. ANODE FABRICATOR	F. TREATMENT	F. POLARITY	F. GRINDING	F. TOTAL WELDING TIME @ ENTER PASS TEMPERATURE		5/16"	4 1/2"	O	II		
						X	D	Imp	I		
									II		
									20"		
									37 1/2"		
A. AD-288 B. 3/3/43 C. 31 D. Great Lakes Steel Corp. E. McKay Company F. Firestone Tl. & Rubber Co. E. Elec.	A. 1" B. R-IV (.68Mn, .74Si, .65Cr, .20Mo, .08Zr) C. .28 D. --- E. --- F. ---	A. A-II (.10C, 4.49 Mn, .65Si, 9.10Mn) B. Armorloy C. Lime D. DC REV	A. 60°BY B. 3/16" C. Flame Cutting Grinding	A. Copper B. 1. I 5/32" 1a 150 - 26 2. I 3/16" 1a 200 - 24 1/4" 3a 255 - 24 3. I 5/16" 2a 300 - 23 C. 2:31 hrs. 100°F. D. Some cracking, chipping and grinding after first pass.	A. 1000° F.	1 749	1"	7"	Imp	II	8"
						3 780	3/16"	6 1/2"	O	III	SE
						3 775	X	4 1/2"	O	II	
									Imp	I	
									II	20"	
										37 1/2"	

Weld Metal

A. PART NUMBER B. DATE OF TEST C. PLATE NO. D. MANUFACTURER E. SIZE OF PLATE F. WEIGHT OF PLATE G. TYPE OF PLATE H. TYPE OF PLATE	A. PLATE THICKNESS B. TYPE C. GARDEN CENTER D. SIZE E. PROCESS F. HEAT TREATMENT G. TEST TIME	A. TYPE B. TRADE NAME C. COATING D. CONCENTRATION E. POLARITY	A. GRAIN SIZE B. SURFACE C. PLATE PREPARATION	A. DATE B. OPERATIONS C. BODY TYPE D. GROUND TYPE E. TOTAL WELDING TIME & OTHER PEGS F. TEMPERATURE	A. NONE B. NONE	H. V/L I. R.L. II. S.E. III. TYPICAL	A. GRAINING B. TYPE C. GRAINING	A. NONE B. NONE	A. NONE B. NONE
A. AD-43 B. 10/3/42 C. 32 D. Great Lakes Steel Corp. Youngstown E. Sheet & Tube F. McKay Company G. General Motors Truck & Coach	A. 1" G L B. R-IV C. (.94Mn, .81Si, .70Cr, .22Mo, .02r) D. R-III Y E. (1.35Mn, .17Si, .50Mo) F. C-23 G. Face 321 to Back 341 H. B.O.H. Both I. 16350 G L J. 2-1/4 hrs. Water K. 10600F. Draw L. 16250F. Y M. 1/2 hr. Water N. 10000F. 4-1/2 hrs. Draw	A. A-1 B. (.10C, 3.66 Mn, 1.1381, 18.1Cr, 10.2Mn, .47Mo) C. Armorloy A-5 D. Lime E. DC REV	A. 450DY B. 3/16" C. Flame Cutting	A. Not Given B. I. II 5/32" la 95 - C. I 5/32" la 135 - D. I 1/4" 2a 225 - E. III 5/32" 4b 95 - F. III 3/16" 2b 165 - G. 10 hrs. 1500 - 2000F. H. Grinding after first pass. I. Left and lower center sections by Great Lakes, Youngstown, right and upper center sections by Youngstown. Total chipping and grinding time 3 hrs., details not given.	A. None B. None	1 1168 2 1124 3 1/2" 3 1165 9 1/2" 4 1170 4" 5 1115 4" 6 1118 2 1/2"	X 4 1/2" Imp 10" D 11 1/2" Imp 11 1/2" D 5 1/2" O 4 1/2" Imp 4 1/2" U 4 1/2" U 4 1/2" U	I 3 1/2" II 9 1/2" V 11" II 3" I 1 1/2" II 4 1/2" III 37"	Passed radiograph 2-1/2" incomplete fusion
A. AD-43 B. 10/3/42 C. 35 D. Jones & Laughlin Steel Corp. Great Lakes E. Steel Corp. F. Harnischfeger G. General Motors Truck & Coach	A. 1" J&L B. R-III C. (.75Mn, .24Si, .52Mo) D. R-IV G L E. (.94Mn, .81Si, .70Cr, .22Mo, .02r) F. 16350F. J&L G. 2-1/4 hrs. Water H. 10750F. 4 hrs. Draw I. 16350F. G L J. 2-1/4 hrs. Water K. 10600F. Draw	A. A-1 B. (.10C, 1.75 Mn, .58Si, 19.38Cr, 11.40Mn, 3.2Mo) C. AW-3 D. Lime E. DC REV	A. 450DY B. 3/16" C. Flame Cutting	A. Not Given B. I. II 5/32" la 100 - C. II 5/32" la 135 - D. III 5/32" 12b 135 - E. 8 hrs. 2000F. F. Total chipping or grinding time 3 hrs., details not given	A. None B. None	1 1101 2 1135 2 1/2" 3 1140 1"	X 3 1/2" Imp 6" D 6 1/2" Imp 6 1/2" U 6 1/2" U	III 2 1/2" I 2" II 9 1/2" II 13 1/2"	Passed radiograph







PLATE INFORMATION		PLATE TREATMENT		PLATE ANALYSIS		PLATE IDENTIFICATION		PLATE CONDITION		PLATE HISTORY		PLATE TESTING		PLATE RESULTS	
A. PLATE NO.	B. DATE OF TEST	C. PLATE NO.	D. DATE OF TEST	E. PLATE NO.	F. DATE OF TEST	G. PLATE NO.	H. DATE OF TEST	I. PLATE NO.	J. DATE OF TEST	K. PLATE NO.	L. DATE OF TEST	M. PLATE NO.	N. DATE OF TEST	O. PLATE NO.	P. DATE OF TEST
AD-77	10/20/42	R-IV	10/20/42	A-I	10/20/42	A. 450V	10/20/42	A. 120C	10/20/42	10 Imp	10/20/42	10/20/42	10/20/42	10/20/42	10/20/42
H-1	12/12/42	R-III	12/12/42	A-II	12/12/42	A. 450V	12/12/42	A. 100C	12/12/42	10 Imp	12/12/42	12/12/42	12/12/42	12/12/42	12/12/42
Great Lakes Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.
Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company
Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company
Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company	Gordon Mfg. Company	Laughlin Steel Corp.	Crucible Steel Company

IDENTIFICATION	MATERIAL	ELECTRIC DATA	WELDING PROCEDURE	HEAT TREATMENT	M. VEL. F/3	BALLISTIC RESULTS	REMARKS ON CRACKING RADIOGRAPHIC RESULTS, ETC.
A. AD-39	A. 1"	A. A-I	A. 60°DV	A. Not given	1 759	1 7 1/2 Imp	II 2 1/2 Passed radiograph
B. 10/10/42	B. R-III	(.08C, 3.5 Mn., .35Si, 19.0Cr, 10.0Mn, 1.0Mo)	B. 1/8" C. Machining	1. II 5/32" 1a 125 - 25	2 791	2 5 1/2 U	II 2 1/2 Passed radiograph
C. H-12	C. .25	D. Face 321	C. Machining	2. III 3/16" 3a 195 - 30	3 781	3 2 1/2 Imp	I 2 1/2
D. Jones & Laughlin	D. Back 341	E. ---	C. Buttering	3. III 5/32" 4b 150 - 30			II 5 1/2
E. A. O. Smith Corp.	E. ---	F. ---	C. Lime	C. III 5/32" 4b 150 - 30			III 1 1/2
F. The Well Co.	F. ---	F. ---	D. DC REV	C. 16 hrs. 1200F.			III 1 1/2
A. AD-39	A. 1"	A. A-	A. 60°DV	A. Not given	1 802	1 7 Imp	II 3 1/2 Passed radiograph
B. 10/10/42	B. R-III	(.12C, 1.50 Mn., .45Si, 18.8Cr, 10.4Mn, 2.25Mo)	B. 1/8" C. Machining	1. II 5/32" 1a 130 - 30	2 790	2 5 1/2 U	III 1 1/2
C. H-13	C. .25	D. Face 321	C. Machining	2. III 5/32" 2a 150 - 30			III 1 1/2
D. Jones & Laughlin	D. Back 341	E. ---	C. Buttering	3. III 5/32" 4b 200 - 30			III 1 1/2
E. Lincoln Electric Co.	E. ---	F. ---	D. DC REV	C. 21 hrs. 1200F.			III 1 1/2
F. The Well Co.	F. ---	F. ---	D. Grinding after first five passes, ninth, 12th and 15th. Holes ground out.	D. Grinding after first pass.			III 1 1/2
A. AD-131	A. 1"	A. A-I	A. 60°DV	A. Not given	1 758	1 4 1/2 Imp	I 3 1/2 Passed radiograph
B. 12/3/42	B. R-IV	(.12C, 1.50 Mn., .45Si, 18.8Cr, 10.4Mn, 2.25Mo)	B. 5/32" C. Machining	1. I 3/16" 1a 150 - 25	2 772	2 6 U	II 1 1/2
C. H-14	C. .26	D. Face 321	C. Machining	2. III 5/32" 5a 180 - 30			II 1 1/2
D. Great Lakes Steel Corp.	D. Back 341	E. ---	C. Buttering	3. III 1/8" 4b 90 - 25			III 1 1/2
E. Harnitchefer Corp.	E. ---	F. ---	D. DC REV	C. 15 hrs. 1200F.			III 1 1/2
F. The Well Co.	F. ---	F. ---	D. Grinding after all passes. Time 3-1/2 hrs.	D. Grinding after first pass.			III 1 1/2
A. AD-131	A. 1"	A. A	A. 60°DV	A. Not given	1 756	1 7 Imp	I 2 1/2 Failed radiograph
B. 12/3/42	B. R	(.12C, 1.50 Mn., .45Si, 18.8Cr, 10.4Mn, 2.25Mo)	B. 5/32" C. Machining	1. I 5/32" 1a 145 - 25	2 772	2 6 U	II 3 1/2 crack
C. H-15	C. ---	D. Face 321	C. Machining	2. III 5/32" 1a 150 - 30			II 2 1/2
D. Great Lakes Steel Corp.	D. ---	E. ---	C. weld	3. III 5/32" 2a 180 - 30			II 2 1/2
E. Lincoln Electric Co.	E. ---	F. ---	D. DC REV	C. 16 hrs. 1200F.			II 2 1/2
F. The Well Co.	F. ---	F. ---	D. Grinding after first pass.	D. Grinding after first pass.			II 2 1/2

INSTRUCTIONS	ANNEALING DATA			MATERIALS DATA			WELDED JOINTS			WELDED PROCEDURE			HEAT TREATMENT			RADIATION RESULTS			REMARKS ON DRAWING RADIOGRAPHIC RESULTS, ETC.
	A. PLATE NUMBER	B. TYPE	C. GRADE	A. TYPE	B. GRADE	C. POLARITY	A. PROCEDURE	B. PROCEDURE	C. PROCEDURE	A. PREP	B. PREP	C. PREP	A. PREP	B. PREP	C. PREP	A. PREP	B. PREP	C. PREP	
A. AD-268 B. 2/16/43 C. H-17 D. Great Lakes Steel Corp. E. A. O. Smith Corp. F. The Heil Co.	A. 1" B. R-IV (.93Mn, .0781, .63Cr, .17Mo) C. .27 D. --- E. --- F. ---	A. A-I (.08C, 3.5 Mn, .35Si, 19.0Cr, 10.0Mn, 1.0Mo) B. SW-164 C. Lims D. DC REV	A. 600DV B. 1/8" C. Machining D. Buttering	A. Not given B. I 5/32" 1a 150 - 30 C. I 5/32" 3a 150 - 30 D. I 5/32" 4a 190 - 30 E. III 5/32" 4b 150 - 30 F. III 5/32" 4c 150 - 30 G. 19 hrs. 120°F. H. One bead buttered on tip of bevel	A. 1200° B. None	1 776 2 834	II I 14" II 14" III 9" 35"	5" D 8" U	1" R	14" 14" 9" 35"	Passed radiograph								
A. AD-268 B. 2/16/43 C. H-17 D. Great Lakes Steel Corp. E. Harnischfeger Corp. F. The Heil Co.	A. 1" B. R-IV (.93Mn, .0781, .63Cr, .17Mo) C. .27 D. --- E. --- F. ---	A. A-I (.08C, 3.5 Mn, .35Si, 19.0Cr, 10.0Mn, 1.0Mo) B. SW-164 C. Lims D. DC REV	A. 600DV B. 1/8" C. Machining D. Buttering	A. Not given B. I 5/32" 1a 145 - 30 C. I 5/32" 3a 145 - 30 D. I 5/32" 4a 195 - 30 E. III 5/32" 4b 145 - 30 F. III 5/32" 4c 230 - 30 G. 17 hrs. 115°F. H. One bead buttered on tip of bevel	A. 1150° B. None	1 756 2 849	II III 120" 21"	9" D 8" U	X	14" 120" 21"	Passed radiograph								
A. AD-268 B. 2/16/43 C. H-17 D. Great Lakes Steel Corp. E. Harnischfeger Corp. F. The Heil Co.	A. 1" B. R-IV (.93Mn, .0781, .63Cr, .17Mo) C. .27 D. --- E. --- F. ---	A. A-I (.12C, 3.65 Mn, .50Si, 19.0Cr, 9.3Mn, .92Mo) B. SW-3-C C. Lims D. DC REV	A. 600DV B. 1/8" C. ---	A. Not given B. I 5/32" 1a 140 - 30 C. I 5/32" 3a 150 - 30 D. I 5/32" 4a 190 - 30 E. III 5/32" 4b 150 - 30 F. III 5/32" 4c 240 - 30 G. 18 hrs. 115°F. H. One bead buttered on tip of bevel	A. 1150° B. None	1 757 2 781	II III 10" V 35"	5" D 9" U	L 2"	14" 10" 5" 35"	Passed radiograph Two small cracks								





<p>A. PART NUMBER OR SERIAL NO. B. DATE OF TEST C. PLATE NO. D. JAWS OR INSTRUMENTS E. SURFACE AREA F. JOINT PREPARATION</p>	<p>A. PLATE THICKNESS B. TYPE C. GRADE D. ORN E. PROCESS F. HEAT TREATMENT G. TEST TEMPERATURE</p>	<p>A. TYPE B. TRADE NAME C. GRADE D. COMPOSITION E. POLARITY</p>	<p>A. JOINT DESIGN B. JOINT TYPE C. JOINT POSITION D. PLATE PREPARATION</p>	<p>A. WELDING PROCEDURE B. DEPOSITION RATE C. WELD TYPE D. WELD TYPE E. WELD TYPE F. TOTAL WELDED TIME G. TEST TEMPERATURE</p>	<p>A. WELDING PROCEDURE B. DEPOSITION RATE C. WELD TYPE D. WELD TYPE E. WELD TYPE F. TOTAL WELDED TIME G. TEST TEMPERATURE</p>	<p>A. WELDING PROCEDURE B. DEPOSITION RATE C. WELD TYPE D. WELD TYPE E. WELD TYPE F. TOTAL WELDED TIME G. TEST TEMPERATURE</p>	<p>A. WELDING PROCEDURE B. DEPOSITION RATE C. WELD TYPE D. WELD TYPE E. WELD TYPE F. TOTAL WELDED TIME G. TEST TEMPERATURE</p>	<p>A. WELDING PROCEDURE B. DEPOSITION RATE C. WELD TYPE D. WELD TYPE E. WELD TYPE F. TOTAL WELDED TIME G. TEST TEMPERATURE</p>
<p>A. AD-109 B. 12/9/42 C. H-1000 D. Great Lakes Steel Corp. E. Crucible Steel F. Marmon Auto-motive Products, Inc.</p>	<p>A. 1/8" B. R-IV C. (.76% C, .03% Si, .59% Cr, .19% Mo, .08% P) D. 321 to 341 E. B.O.N. F. 1640°F. G. 1-1/2 hrs. Water 1020°F. H. 1-1/2 hrs.</p>	<p>A. A-1 B. (.15C, 2.0 Mn, .60Si, 18.20Cr, 8.10Ni, 1.85-2.00 Mo) C. Armoxize D. Resizal E. Titanium F. DC REV</p>	<p>A. 50DD, 1/8" RF B. 3/16" C. Flame D. Flame E. Softening F. Planing</p>	<p>A. Not given B. I. II 5/32" 2a 150 - 44 C. III 3/16" 2a 190 - 48 D. II 3/16" 5b 190 - 48 E. 7 hrs. 150° - 200°F.</p>	<p>A. 1600 B. None</p>	<p>I 12" Passed radiograph II 6" III 34"</p>	<p>I 12" Passed radiograph II 6" III 34"</p>	<p>I 12" Passed radiograph II 6" III 34"</p>

MATERIALS		ANALYSIS		TREATMENT		TESTS		RESULTS		REMARKS	
A. NAME	B. SIZE	C. TYPE	D. GRADE	E. HARDENING	F. TEMPERING	G. TENSILE	H. YIELD	I. ELONGATION	J. CHARPY	K. LOCATION OF DEFECTS	L. COMMENTS
A. AD-208 B. 1/23/43 C. WCH-51 D. Great Lakes Steel Corp. Heat treated by - Detroit Steel Products E. McKay Company F. Pullman Standard Car Mfg. Company	A. 1.185" B. R-IV (.91Mn, .75Si, .69Cr, .19Mo, .10Zr) C. .29 D. Face 335 Back 333 E. Acid-Elec. F. ---	A. A B. Armorloy C. A D. DC REV	A. 45°DV B. 3/8" C. Flame Cutting Grinding Machined Buttering	A. 750-100° F. B. None	1 881 2 884	3 1/2" 4" D 5" 3/4" R 6" U	7" D 8" 7" U 9" 4" U 10" 2"	III V II 23 III 2 V 2 II 1 III 1 I 36 V 9 54	Passed radiograph		
A. AD-208 B. 1/23/43 C. WCH-53 D. Great Lakes Steel Corp. Heat treated by - Detroit Steel Products E. McKay Company F. Pullman Standard Car Mfg. Company	A. 1.185" B. R-IV (.90Mn, .74Si, .70Cr, .22Mo, .07Zr) C. .30 D. Face 341 Back 341 E. McKay Company F. Acid-Elec.	A. A B. Armorloy C. A D. DC REV	A. 45°DV B. 3/8" C. Flame Cutting Grinding Machined Buttering	A. 750-100° F. B. None	1 874 2 882 3 919 4 1012	1" R 2" U 3" 9/16" R 4" 5/8" R 5" D 6" 9/16" U 7" 5/8" U	III V II 23 III 2 V 2 II 1 III 1 I 36 V 9 54	Passed radiograph			
A. AD-315 B. 3/12/43 C. 60 D. Great Lakes Steel Corp. Heat treated by - Detroit Steel Products E. Mollup Corp. F. Pullman Standard Car Mfg. Company	A. 1.185" B. R-IV (.91Mn, .75Si, .69Cr, .19Mo) C. .29 D. Face 335 Back 333 E. B.O.H. F. ---	A. A B. Armorloy C. A D. DC REV	A. 60°DV B. 3/8" C. Flame Cutting Grinding Machined Buttering	A. None B. None	1 849 2 857 3 868	2 1/2" L 3" L 4" L	7" D 8" 7" U 9" 4" U 10" 2"	III V II 23 III 2 V 2 II 1 III 1 I 36 V 9 54	Passed radiograph Scattered porosity and slag inclusions thru-out plate		

STRUCTURE A. PANS B. DATE OF TEST C. PLATE NO. D. MANUFACTURER E. SERVICE AREA F. ASPECT	MATERIAL A. PLATE THICKNESS B. TYPE C. GRADE D. HEAT TREATMENT E. PROCESS F. YEAR	SURFACE A. TYPE B. COATING C. CORROSION D. POLARITY	JOINT DESIGN A. GROOVE B. ROOT GAP C. PLATE PREPARATION	WELDING A. PROCEDURE B. DEPOSITION C. ROOT TYPE D. ROOT TYPE E. ROOT TYPE F. TOTAL WELDING TIME & WELDING TEMPERATURE	HEAT A. PREHEAT B. POST HEAT	BALLISTICS RESULTS		REMARKS ON CRACKING A. BALLS B. BALLS			
						H VEL. / F/S	LOCATION OF N. CRACKS				
A. AD-315 B. 3/12/43 C. MCH-61 D. Great Lakes Steel Corp. Heat treated by - Detroit Steel Products E. McKay Company F. Pullman Standard Car Mfg. Company	A. 1.185" B. A-IV (.91Mn, .75Si, .69Cr, .19Mo) C. .29 D. Face 335 Back 333 E. B.O.H. F. ---	A. A B. Armorloy C. Lime D. DC REV	A. 60°DV B. 3/8" C. Flame Grinding Machined	A. Copper B. 1. II 3/16" 1a 160 - 20 1a 170 - 23 2a 220 - 28 4b 220 - 28 C. 6 hrs. 190° - 380°F. D. Grater cracking after first pass. Chipping and grinding after first pass. Chipping after all passes.	A. None B. None	1	843	1" L	6" Imp D	I 5" II 14" V 19" 25"	Passed radiograph Scattered porosity and slag inclusions
A. AD-315 B. 3/12/43 C. MCH-62 D. Great Lakes Steel Corp. Heat treated by - Detroit Steel Products E. McKay Company F. Pullman Standard Car Mfg. Company	A. 1.185" B. A-IV (.90Mn, .74Si, .70Cr, .22Mo) C. .30 D. Face 341 Back 341 E. B.O.H. F. ---	A. A B. Armorloy C. Lime D. DC REV	A. 60°DV B. 3/8" C. Flame Grinding Machined Buttering	A. Copper B. 1. II 3/16" 1a 160 - 21 1a 170 - 20 2a 290 - 29 4b 290 - 29 C. 7-1/2 hrs. 170° - 390°F. D. Grater cracking after first and fifth passes. Grinding after first pass and chipping after a.l. passes. Three passes buttered at root in cross-bar.	A. None B. None	1 2 3 4	833 847 909 892	2" R D L L L L L	2" R D 7" Imp U 2" L U 7" D D	III 5" III 1" III 1" I 1" I 1"	Passed radiograph Scattered porosity and slag inclusions

IDENTIFICATION		ANODIZING DATA		ELECTRODE DATA		ANODE DESIGN		WELDING PROCEDURE		WEAT		M VEL.		BALLETIC DETAILS		REMARKS ON UNDERLINE	
A. PART NO.	B. DATE OF TEST	C. PLATE NO.	D. ANODE MANUFACTURER	E. ELECTRODE MPER.	F. ANODE FABRICATOR	A. PLATE THICKNESS	B. TYPE	C. ANODIZING CURRENT	D. DENS.	E. PROCESS	F. ANODE TREATMENT	G. TEST TIME	H. VEL.	I. LOCATION OF H	J. LOCATION OF H	K. LOCATION OF H	L. LOCATION OF H
A. AD-92	10/24/42		Great Lakes Steel Corp.		So. California Div.	A. 1" R-IV (.85Mn, .74Si, .08Cr, .10Mo, .32 Cr, 9-6-10, 15Mn, .98-1.00 Mo)	A. 60ODV B. 5/32" C. Flame Grinding	A. Copper	1. I 5/32" la 140 - 25 2. III 5/32" 1a 140 - 25 3. III 5/32" 4b 170 - 26 4b 140 - 25 2b 200 - 26 C. 3:30 hrs. 125° - 225°F. D. Four minutes of chipping after each pass.	A. 100° F. B. None	1 773 X 2 677 3 677	7 1/2 Imp U 3 1/2 13 1/2 L D 2" 3" L U	II III II III V O III V O III 25	4" Passed radiograph			
A. AD-177	1/7/43		Great Lakes Steel Corp.		Alloy Rods Co. Div.	A. 1" R-IV (.81Mn, .63Si, .63Cr, .21Mo, .09Zr, .28)	A. 60ODV B. 5/32" C. Flame Cutting Grinding	A. Copper	1. I 1/8" la 125 - 24 2. I 1/8" 6a 125 - 24 3. III 1/8" 6b 125 - 24 C. 4:12 hrs. 105° - 150°F. D. Eight minutes of chipping after each pass. One more pass in crossbar.	A. 100° F. B. None	1 755 2 773 3 768	2" L 5 1/2 Imp D 4 1/2 Imp L	II III II III I 34 1/2 43"	7" Passed radiograph			
A. AD-282	2/26/43		Great Lakes Steel Corp.		Alloy Rods Co. Div.	A. 1" R-IV (.88Mn, .73Si, .66Cr, .21Mo, .11Zr, .27)	A. 60ODV B. 5/32" C. Flame Cutting Grinding	A. Copper	1. II 5/32" 2b 125 - 22 2. II 1/8" 2b 110 - 22 3. II 5/32" 17b 125 - 22 3. II 5/32" 13b 125 - 22 C. 5:53 hrs. 100° - 160°F. D. Five minutes of chipping after each pass. Three more passes in left leg and eleven more passes in crossbar. Plate welded in overhead position, welder standing.	A. 100° F. B. None	1 787 2 739	1 1/2 L 3 1/2 D 1 1/2 R	I III III III III III III III III 38 1/2	16 1/2 Passed radiograph			



A. PLATE NO. B. DATE OF TEST C. TH-65 D. GREAT LAKES E. STEEL CORP. F. REID-AVERY G. COMPANY H. MFG. DIV.	A. PLATE NUMBER B. TYPE C. GASKET ORIENTY D. SIZE E. PROCESS F. HEAT TREATMENT G. YEAR TIME	A. TYPE B. TRADE NAME C. COATING D. ORIENTY E. POLARITY	A. COAT B. ANGLE C. ROOT GAP D. PLATE PREPARATION	A. WELDING B. DEPOSITION C. ROOT TYPE D. WELD TYPE E. WELD TYPE F. TOTAL WELDING TIME G. WELDER	A. NONE B. POST	A. WEL. B. P/B C. L D. E.L. E. S.B. F. LOC TYPE G. AMT	A. PASSING B. CRACKING C. RADIOGRAPHING D. NEMTS, ETC.	A. I B. II C. III D. IV E. V F. VI G. VII H. VIII I. IX J. X K. XI L. XII M. XIII N. XIV O. XV P. XVI Q. XVII R. XVIII S. XIX T. XX U. XXI V. XXII W. XXIII X. XXIV Y. XXV Z. XXVI	A. I B. II C. III D. IV E. V F. VI G. VII H. VIII I. IX J. X K. XI L. XII M. XIII N. XIV O. XV P. XVI Q. XVII R. XVIII S. XIX T. XX U. XXI V. XXII W. XXIII X. XXIV Y. XXV Z. XXVI	A. I B. II C. III D. IV E. V F. VI G. VII H. VIII I. IX J. X K. XI L. XII M. XIII N. XIV O. XV P. XVI Q. XVII R. XVIII S. XIX T. XX U. XXI V. XXII W. XXIII X. XXIV Y. XXV Z. XXVI
A. AD-130 B. 12/1/42 C. TH-63 D. Great Lakes E. Steel Corp. F. Alloy Rods Co. G. Ternstedt H. Mfg. Div.	A. I B. R-IV C. (.94Mn, .81Si, .70Cr, .22Mo, .09Zr) D. .32 E. Face 321-323-321 F. B.O.H. G. 1600°F. 1/2 hr. Water H. 900°F. 1-1/2 hrs. Air	A. A-II B. (.03-.13C, 3.5-4.5Mn, .35-.70Si, 19.8-21. Cr, 8.5-10.5Ni) C. Armox D. B	A. 60DV B. 3/16" C. Flame D. Cutting E. Grinding	A. Copper B. II 3/16" C. I 3/8" D. I 3/8" E. 200 - 25 F. 200 - 25 G. 450 - 32 H. 450 - 32 I. 70° - 270°F. J. 5 hrs.	A. None B. None	A. I B. X C. 787 D. 787 E. 787 F. 787 G. 787 H. 787 I. 787 J. 787 K. 787 L. 787 M. 787 N. 787 O. 787 P. 787 Q. 787 R. 787 S. 787 T. 787 U. 787 V. 787 W. 787 X. 787 Y. 787 Z. 787	A. I B. II C. III D. IV E. V F. VI G. VII H. VIII I. IX J. X K. XI L. XII M. XIII N. XIV O. XV P. XVI Q. XVII R. XVIII S. XIX T. XX U. XXI V. XXII W. XXIII X. XXIV Y. XXV Z. XXVI	A. I B. II C. III D. IV E. V F. VI G. VII H. VIII I. IX J. X K. XI L. XII M. XIII N. XIV O. XV P. XVI Q. XVII R. XVIII S. XIX T. XX U. XXI V. XXII W. XXIII X. XXIV Y. XXV Z. XXVI		
A. AD-130 B. 12/1/42 C. TH-65 D. Great Lakes E. Steel Corp. F. Reid-Avery G. Company H. Ternstedt I. Mfg. Div.	A. I B. R-IV C. (.90Mn, .76Si, .65Cr, .21Mo, .09Zr) D. .30 E. Face 307-311-302 F. B.O.H. G. 1600°F. 1/2 hr. Water H. 900°F. 1-1/2 hrs. Air	A. A-I B. (.076C, 1.81Mn, .46Si, 17.6Cr, 10.33Ni, 1.03Mo) C. Reid-Avery D. Armox E. T1 O2 F. AC	A. 60DV B. 3/16" C. Flame D. Cutting E. Grinding	A. Copper B. II 3/16" C. I 3/8" D. I 3/8" E. 190 - 25 F. 190 - 25 G. 400 - 30 H. 400 - 30 I. 800 - 260°F. J. 5 hrs.	A. None B. None	A. I B. L C. 779 D. 779 E. 779 F. 779 G. 779 H. 779 I. 779 J. 779 K. 779 L. 779 M. 779 N. 779 O. 779 P. 779 Q. 779 R. 779 S. 779 T. 779 U. 779 V. 779 W. 779 X. 779 Y. 779 Z. 779	A. I B. II C. III D. IV E. V F. VI G. VII H. VIII I. IX J. X K. XI L. XII M. XIII N. XIV O. XV P. XVI Q. XVII R. XVIII S. XIX T. XX U. XXI V. XXII W. XXIII X. XXIV Y. XXV Z. XXVI	A. I B. II C. III D. IV E. V F. VI G. VII H. VIII I. IX J. X K. XI L. XII M. XIII N. XIV O. XV P. XVI Q. XVII R. XVIII S. XIX T. XX U. XXI V. XXII W. XXIII X. XXIV Y. XXV Z. XXVI		

\*Weld Metal

INFORMATION	ANODE DATA	ELECTRODE DATA	JOINT DESIGN	WELD DATA	PROCEDURE	HEAT TREATMENT	RADIATION OF H. CRACKING			REMARKS ON CRACKING RADIOGRAPHIC RESULTS, ETC.	
							N	VEL. F/8	LOC. TYPE AMT.		
A. PAPER RECORD NO. B. DATE OF TEST C. PLATE NO. D. MANUFACTURER E. ELECTRODE MPAN F. ANODE FABRICATOR	A. PLATE THICKNESS B. TYPE C. GASKET CONTENT D. SIZE E. PROCESS F. HEAT TREATMENT TEMP. TIME GASKET	A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	A. GROOVE INCLUDED B. ANGLE ROOT FACE C. ROOT GAP D. PLATE PREPARATION	A. BACKING B. DEPOSITION C. ROOT TYPE D. ROOT TYPE E. GASKET TYPE F. TOTAL WELDING TIME @ SETTER PRESS TEMPERATURE	A. TO 100°F. B. None C. None	A. FAN B. POST	L.L.	L.R.	U.B.	LOC. TYPE AMT.	
A. AD-119 B. 12/12/42 C. TH-76 D. Great Lakes Steel Corp. E. McKay Company F. Ternstedt Alloy Rods Co. Mfg. Div.	A. 1" R-IV (.94Mn, .81Si, .70Cr, .22Mo, .09Zr) C. 32 D. Face 321-319 E. B.O.H. 319-319 F. 1600°F. 1/2 hr. Water 900°F. 1-1/2 hrs. Air	A. A-II (.10-.12C, 3.9-4.5Mn, 19.2-21.5C, 10.2-11.5 Ni, .80Mo) B. Armoxley A-5 C. Lime-Mn D. DC REV	A. 60DPV B. 1/4" C. Flame Cutting Grinding	A. Copper B. II 1/4" 2a 275 - 28 3. I 5/16" 2a 390 - 30 3. I 5/16" 2a 390 - 30 C. 5 hrs. 100° - 280°F.	A. To 100°F. B. None		768	2 1/2 L	5 3/4 D	1 7/8 I 0 I 7 1/2 V Imp V 18 25	Passed radiograph
A. AD-119 B. 12/12/42 C. TH-76 D. Great Lakes Steel Corp. E. McKay Company F. Ternstedt Alloy Rods Co. Mfg. Div.	A. 1" R-IV (.94Mn, .81Si, .70Cr, .22Mo, .09Zr) C. 32 D. Face 325-321-319 E. B.O.H. 321-319 F. 1600°F. 1/2 hr. Water 900°F. 1-1/2 hrs. Air	A. A-II (.10-.12C, 3.9-4.5Mn, 19.2-21.5C, 10.2-11.5 Ni, .80Mo) B. Armoxley A-5 C. Lime-Mn D. DC REV	A. 60DPV B. 1/4" C. Flame Cutting Grinding	A. Copper B. II 1/4" 2a 290 - 28 3. I 3/8" 2a 450 - 32 3. I 3/8" 2a 450 - 32 C. 4 hrs. 800 - 280°F.	A. None B. None		746		1 1/2 L 7 1/2 U	Imp V 36 3 3 41	Failed radiograph Crater cracks in both junctions in 10" fusion zone Some root pass cracks in crossbar cracks in crossbar and right leg weld
A. AD-119 B. 12/12/42 C. TH-80 D. Great Lakes Steel Corp. E. Reid-Avery Company F. Ternstedt Mfg. Div.	A. 1" R-IV (.94Mn, .81Si, .70Cr, .22Mo, .09Zr) C. 32 D. Face 331-329-321 E. B.O.H. 329-321 F. 1600°F. 1/2 hr. Water 900°F. 1-1/2 hrs. Air	A. A-I (.07-.15C, 3.50-4.50 Mn, .75Si, 18.0-20.0 Cr, B.5-10, 5Mn 1.25Mo) B. Reid-Avery C. Ti base D. DC REV	A. 60DPV B. 1/4" C. Flame Cutting Grinding	A. Copper B. II 1/4" 2a 290 - 28 3. I 5/16" 2a 390 - 30 3. I 5/16" 2a 390 - 30 C. 5 hrs. 800 - 250°F.	A. None B. None		755		2 1/2 H 5 1/2 D	15 1/2 I 11 1/2 II 13 1/2 III 30 1/2	Failed radiograph Crossbar is entirely cracked

Weld Metal

IDENTIFICATION		ANION DATA		ELECTRODE DATA		JOINT DESIGN		WELDING PROCEDURE		HEAT TREATMENT		RADIATING RESULTS		REMARKS ON CHANGES		
A. PART NUMBER OR B. DATE OF TEST	C. PLATE NO.	D. PLATE NO.	E. PLATE NO.	F. PLATE NO.	G. PLATE NO.	H. PLATE NO.	I. PLATE NO.	J. PLATE NO.	K. PLATE NO.	L. PLATE NO.	M. PLATE NO.	N. PLATE NO.	O. PLATE NO.	P. PLATE NO.	Q. PLATE NO.	
A. PLATE THICKNESS	B. TYPE	C. GARDEN CONTENT	D. SIZE	E. PROCESS	F. HEAT TREATMENT	G. TEST TIME	H. POSITION	I. DEPOSITION	J. DEPOSITION	K. DEPOSITION	L. DEPOSITION	M. DEPOSITION	N. DEPOSITION	O. DEPOSITION	P. DEPOSITION	
A. AD-144 B. 12/23/42 C. TH-82 D. Great Lakes Steel Corp. E. Alloy Rods Co., C. 32 F. Ternstedt Mfg. Div.	A. 1" B. R-IV (.94Mn, .81Si, .70Cr, .22Mo, .09Zr) C. 32 D. Face 321-McKay Company E. B.O.H. F. 1600°F. 1/2 hr. Water 800°F. 1-1/2 hrs. Air	A. A-II B (.08-.13C, 3.5-4.5Mn, .35-.70Si, 19.0-21.0Cr, 8.5-10.5Ni)* A-II A-5 (.12C, 3.5-4.5Mn, .80Si, 19.00-21.00Cr, 9.20-10.20Ni)* B. Armorarc B C. Titanium D. AC	A. 60°DV B. 1/4" C. Flame Grinding	A. Copper B. 1. II 1/4" 2a 290 - 28 2-d 3. I 7/16" 1a 550 - 34 1/2" 1a 640 - 35 80° - 340°F. C. 3 hrs. D.	A. None B. None	1 768	5" U 1 1/2" L	III 12" II 11" I 4" V 31" II 25" O 32"	Failed radiograph Scattered porosity thru-out 31" 25" incomplete fusion. Crater crack at left junction							
A. AD-172 B. 1/5/43 C. TH-86 D. Great Lakes Steel Corp. E. McKay Company F. Ternstedt Mfg. Div.	A. 1" B. R-IV (.90Mn, .75Si, .67Cr, .22Mo, .10Zr) C. 30 D. Face 352-Company E. B.O.H. F. 1600°F. 1/2 hr. Water 800°F. 1-1/2 hrs. Air	A. A-II McK. A-5 B. Titanium C. Lime-Mn D. AC	A. 60°DV B. 1/4" C. Flame Grinding	A. Copper B. 1. II 5/32" 2a 175 - 20 5/16" 2a 375 - 28 3. I 5/16" 2a 375 - 28 70° - 140°F. C. 7 hrs. D.	A. None B. None	1 768	1 1/2" R 6 1/2" D	I 14" V 8" 23"	Passed radiograph Several small crater cracks							

SPECIFICATIONS	MATERIALS	PLATE TYPE	TEST PROCEDURE	RESULTS	REMARKS ON SPECIMENS	BALLISTIC RESULTS		CRACKING	REMARKS
						NO. OF BALLS	NO. OF BALLS		
<p>A. AD-172</p> <p>B. 1/5/43</p> <p>C. TH-87</p> <p>D. Great Lakes Steel Corp.</p> <p>E. Mollup Corp.</p> <p>F. Crucible Steel Co. Face 326-Company 298-306</p> <p>G. B.O.H.</p> <p>H. 1/2 hr.</p> <p>I. 1-1/2 hrs.</p> <p>J. Air</p>	<p>A. A-I N</p> <p>B. (.08C, 3.36 B, 3/16" Mn, 18.95 Cr, 10.27 Ni, 1.03Mo, .45Si)</p> <p>C. A-I Crud</p> <p>D. (.11C, 3.58 Mn, 19.60 Cr, 9.78Ni, 1.19Mo, .34Si)</p> <p>E. Armored</p> <p>F. Armored-Resistal</p> <p>G. T1 O2</p> <p>H. DC REV</p>	<p>A. GOODY</p> <p>B. 3/16"</p> <p>C. Flame Cutting Grinding</p>	<p>A. 1"</p> <p>B. R-IV (.90Mn, .75Si, .67Cr, .22Mo, .10Zr)</p> <p>C. .30</p> <p>D. Face 339-341-345</p> <p>E. B.O.H.</p> <p>F. 1600 hr.</p> <p>G. 3-1/2 hrs.</p> <p>H. Water</p> <p>I. 910°F. 3-3/4 hrs.</p> <p>J. Air</p>	<p>A. 1"</p> <p>B. R-IV (.77Mn, .71Si, .56Cr, .20Mo, .09Zr)</p> <p>C. .27</p> <p>D. Face 339-341-345</p> <p>E. B.O.H.</p> <p>F. 1600 hr.</p> <p>G. 3-1/2 hrs.</p> <p>H. Water</p> <p>I. 910°F. 3-3/4 hrs.</p> <p>J. Air</p>	<p>A. None</p> <p>B. None</p>	<p>A. Copper</p> <p>B. II 5/32"</p> <p>C. I 5/16"</p> <p>D. I 5/16"</p> <p>E. 7 hrs.</p>	<p>A. 104 Imp</p> <p>B. D</p>	<p>A. 104 Imp</p> <p>B. D</p>	<p>A. Passed radiograph</p> <p>B. I 1"</p> <p>C. III 4"</p> <p>D. V 2"</p> <p>E. 2"</p>
<p>A. AD-217</p> <p>B. 1/26/43</p> <p>C. TH-88</p> <p>D. Great Lakes Steel Corp.</p> <p>E. Mollup Corp.</p> <p>F. Ternstedt</p> <p>G. Mfg. Div.</p>	<p>A. A-I N</p> <p>B. (.076C, 1.81B, 1/4" Mn, 48Si, C. Flame</p> <p>C. 10.33Cr, 7.61Ni, 1.03Mo)</p> <p>D. A-I N-A</p> <p>E. (.07C, 3.50-4.50Mn, 75Si, 18.0-20.0 Cr, 8.5-10.5Ni, 1.25Mo)</p> <p>F. Armored</p> <p>G. 18-B-B</p> <p>H. T1 Base</p> <p>I. DC REV</p>	<p>A. GOODY</p> <p>B. 1/4"</p> <p>C. Flame Cutting Grinding</p>	<p>A. 1"</p> <p>B. R-IV (.77Mn, .71Si, .56Cr, .20Mo, .09Zr)</p> <p>C. .27</p> <p>D. Face 339-341-345</p> <p>E. B.O.H.</p> <p>F. 1600 hr.</p> <p>G. 3-1/2 hrs.</p> <p>H. Water</p> <p>I. 910°F. 3-3/4 hrs.</p> <p>J. Air</p>	<p>A. 1"</p> <p>B. R-IV (.77Mn, .71Si, .56Cr, .20Mo, .09Zr)</p> <p>C. .27</p> <p>D. Face 339-341-345</p> <p>E. B.O.H.</p> <p>F. 1600 hr.</p> <p>G. 3-1/2 hrs.</p> <p>H. Water</p> <p>I. 910°F. 3-3/4 hrs.</p> <p>J. Air</p>	<p>A. None</p> <p>B. None</p>	<p>A. Copper</p> <p>B. II 3/16"</p> <p>C. I 1/4"</p> <p>D. I 1/4"</p> <p>E. 7-3/4 hrs.</p>	<p>A. 54 Imp</p> <p>B. U</p>	<p>A. 54 Imp</p> <p>B. U</p>	<p>A. Passed radiograph</p> <p>B. I 1"</p> <p>C. III 4"</p> <p>D. V 2"</p> <p>E. 2"</p>

IDENTIFICATION A. PART NUMBER B. DATE OF TEST C. PLATE NO. D. ANNEAL MANUFACTURER E. ELECTRODE BRAND F. ANNEAL PARAMETERS	ANNEAL DATA A. PLATE THICKNESS B. GANDED ORIENT C. DIA. D. PRESSURE E. HEAT TREATMENT F. TEST TIME	SUBSTRATE DATA A. TYPE B. TRADE NAME C. COATING D. ORIENT & POLARITY	JOINT DESIGN A. GROOVE ANALYSIS B. ROOT GAP C. PLATE PREPARATION	WELDING PROCEDURE A. WIRE B. DEPOSITION SIZE EL. NO. TYPE AIR V. C. ROOF TYPE D. SLOTTED TYPE E. COVER TYPE F. TOTAL WELDING TIME @ ENTER ROOM TEMPERATURE	WELD METAL A. None B. None	QUALITY RESULTS			REMARKS ON OPERATIONS UNDISCUSSED RESULTS, ETC.
						H	V/L	LOCATION OF CRACKS L.L. R.L. U.L. U.R.	
A. AD-217 B. 1/26/43 C. TH-89 D. Great Lakes Steel Corp. E. Hollup Corp. F. Reid-Avery Company G. Ternstedt Mfg. Div.	A. 1" Face 352-358-361 B. R-IV (.90Mn, .75Si, .07Cr, .22Mo, .10Zr) C. 30 D. Face 352-358-361 E. P.O.H. F. 1600°F. 1-1/2 hrs. Water 1018°F. 2 hrs. Air	A. A-I H. (.076C, 1.81Mn, 4.6Si, 10.23Cr, 7.61Mn, 1) B. Armored 18-B-B C. Mn+Mo D. DC REV	A. 60°DV B. 3/8" C. Flame Cutting Grinding	A. Copper B. II 3/16" 1. II 1/4" 2a 300 - 28 2a 300 - 28 3. I 1/4" 2a 300 - 28 70° - 160°F. C. 9 hrs. D.	A. None B. None	H 1 V/L 750 3" L	6" U	II 4" II 17" III 6" III 31"	Passed radiograph
A. AD-217 B. 1/26/43 C. TH-90 D. Great Lakes Steel Corp. E. Reid-Avery Company F. Ternstedt Mfg. Div.	A. 1" Face 307-307-306 B. R-IV (.77Mn, .71Si, .09Cr, .20Mo, .09Zr) C. 27 D. Face 307-307-306 E. P.O.H. F. 1600°F. 3-1/2 hrs. Water 910°F. 3-3/4 hrs. Air	A. A-I R-A (.07-.15C, 3.50-4.50 Mn, .75Si, 18.0-20.0 Cr, 8.5-10.5Mn, 1.25Mo) A-I H. (.076C, 1.81Mn, 4.6Si, 10.33Cr, 7.61Mn, 1) B. Armored 18-B-B C. Ti Base Mn+Mo D. DC REV	A. 60°DV B. 1/2" C. Flame Cutting Grinding	A. Copper B. II 3/16" 1. II 1/4" 2a 300 - 28 2a 300 - 28 3. I 1/4" 2a 300 - 28 70° - 210°F. C. 10 hrs. D.	A. None B. None	H 1 V/L 763 704 1 1/4" R	1" 5/8" L D 4 1/2" U	I 6" II 6" II 2" III 2" Imp 2" II 4" III 23"	Passed radiograph Metal deposit irregular



SPECIFICATIONS	ANNEALING	MATERIALS	WELDER	TEMPERATURE	HEAT	H	V	L	CRACKING		REMARKS ON CRACKING		
									LL	UL			
<p>A. AD-237</p> <p>B. 2/7/43</p> <p>C. TH-98</p> <p>D. Great Lakes Steel Corp.</p> <p>E. Reid-Avery Company</p> <p>F. Ternstedt Mfg. Div.</p>	<p>A. 1" R-IV</p> <p>B. (.97Mn, .87Si, .63Cr, .17Mo, .072r)</p> <p>C. 27</p> <p>D. Face 315-317-317</p> <p>E. B.O.H.</p> <p>F. 16500F. 1-1/2 hrs. Water 9700F. 1/2 hr. Air</p>	<p>A. A-I (.07-.15C, 3.50-4.50 Mn, .75Si, 18.0-20.0 Cr, 8.5-10.5Mn, 1.25Mo)</p> <p>B. 18-8-B</p> <p>C. Ti Base +Mn</p> <p>D. DC REV</p>	<p>A. 60DV</p> <p>B. 3/3"</p> <p>C. Flame Cutting Grinding</p>	<p>A. Copper</p> <p>B. 1. II 1/4"</p> <p>2. I 1/4"</p> <p>3. I 1/4"</p> <p>C. 8 hrs.</p> <p>D.</p>	<p>A. None</p> <p>B. None</p>	1	755	1 1/2"	7 1/2"	Imp D	II III III III	2" 6" 6" 18"	<p>Passed radiograph</p> <p>Crater crack in lower left leg</p>
<p>A. AD-237</p> <p>B. 2/7/43</p> <p>C. TH-99</p> <p>D. Great Lakes Steel Corp.</p> <p>E. McKay Company</p> <p>F. Reid-Avery Co. Ternstedt Mfg. Div.</p>	<p>A. 1" R-IV</p> <p>B. (.97Mn, .87Si, .63Cr, .17Mo, .072r)</p> <p>C. 27</p> <p>D. Face 306-302-306</p> <p>E. B.O.H.</p> <p>F. 16500F. 1-1/2 hrs. Water 9700F. Air</p>	<p>A. A-II McK (.12C, 3.5-4.5Mn, .80 Si, 19.0-21.0Cr, 9.2-10.2 Mn)</p> <p>A-I R-A (.07-.15C, 3.5-4.5Mn, .75Si, 18.0-20.0 Cr, 8.5-10.5Mn, 1.25Mo)</p> <p>B. Armorloy A-5</p> <p>C. Lime+Mn Ti base +Mn</p> <p>D. DC REV</p>	<p>A. 60DV</p> <p>B. 1/2"</p> <p>C. Flame Cutting Grinding</p>	<p>A. Copper</p> <p>B. 1. II 3/16"</p> <p>2. I 1/4"</p> <p>3. I 1/4"</p> <p>C. 8 hrs.</p> <p>D.</p>	<p>A. None</p> <p>B. None</p>	1	786	1 1/2"	3 1/2"	Imp L D	II III III III	10" 12" 5" 1" 48"	<p>Passed radiograph</p> <p>Crater cracks at junctions</p>

A. NAME OF PARTY	B. DATE	C. TYPE OF WORK	D. TYPE OF WORK	E. TYPE OF WORK	F. TYPE OF WORK	G. TYPE OF WORK	H. TYPE OF WORK	I. TYPE OF WORK	J. TYPE OF WORK	K. TYPE OF WORK	L. TYPE OF WORK	M. TYPE OF WORK	N. TYPE OF WORK	O. TYPE OF WORK	P. TYPE OF WORK	Q. TYPE OF WORK	R. TYPE OF WORK	S. TYPE OF WORK	T. TYPE OF WORK	U. TYPE OF WORK	V. TYPE OF WORK	W. TYPE OF WORK	X. TYPE OF WORK	Y. TYPE OF WORK	Z. TYPE OF WORK	
A. AD-237 B. 2/7/43 C. 74-100 D. Great Lakes Steel Corp. E. McKay Company F. Reid-Avery Co G. Ternstedt Mfg. Div.	A. 1" B. R-IV C. .97Mn, .87Si, .62Cr, .17Mo, .072r D. Face 319-317 E. B.O.H. F. 16500F G. 1-1/2 hrs. H. WatGF 1/2 hr. Air	A. A-I McK (.13C, 3.5-4.5Mn, .80Si, 13.0-14.0Cr, 1.0-1.2Mo) B. A-I R-A (.07-.15C, 3.5-4.5Mn, .75Si, 18.0-20.0Cr, 8.5-10.5Mn, 1.25Mo) C. Armorloy A-5 D. 18-8-B E. Lime-Mn F. Ti Base G. Mn H. DC REV	A. 60°DV B. 1/4" C. Flame D. Cutting E. Grinding	A. Copper B. 1. II 3/16" 2a 200 - 25 2. I 1/4" 2a 300 - 30 3. I 1/4" 2a 300 - 30 C. 8 hrs. D.	A. None B. None	1 766 2 733 3 719	X 64° 7° 14° 54° R D R D	II Imp III II II II III III	54° 7° 14° 38° 14° 18°	Failed radiograph 4" crack and in- termittent cracks in crossbar Small crater cracks in both leg welds																
A. AD-270 B. 2/19/43 C. 74-94 D. Great Lakes Steel Corp. E. Reid-Avery Company F. Ternstedt Mfg. Div.	A. 1" B. R-IV C. .77Mn, .71Si, .58Cr, .20Mo, .072r D. Face 292-285 E. B.O.H. F. 16000F G. 3-1/2 hrs. H. WatGF 9100F, 3-3/4 hrs. Air	A. A-I (.07-.15C, 3.5-4.5Mn, .75Si, 18.0-20.0Cr, 8.5-10.5Mn, 1.25Mo) B. 18-8-B C. Ti Base D. DC REV	A. 60°DV B. 1/4" C. Flame D. Cutting E. Grinding	A. Copper B. 1. II 3/16" 2a 180 - 25 2. II 3/16" 4b 170 - 25 3. III 3/16" 2b 300 - 30 C. 10 hrs. D.	A. None B. None	1 775 2 774	5° 14° 6° R R D	III Imp U III III III	84° 14° 3° 26°	Passed radiograph Two small crater cracks and some slag inclusions																

IDENTIFICATION A. FROM RECORD NO. B. DATE OF TEST C. PLATE NO. D. ADAMS MANUFACTURER E. ELECTRODE USED F. ADAMS FABRICATOR	ADAMS DATA A. PLATE THICKNESS B. TYPE C. GAMMA CONTENT D. SHM E. PROCESS F. HEAT TREATMENT G. TEST METHOD	ELECTRODE DATA A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	JOINT DESIGN A. GROOVE INCLUDED B. ANGLE, ROOT FACE C. ROOT GAP D. PLATE PREPARATION	WELDING PROCEDURE A. WELDING B. DEPOSITIONS C. ROOT TYPE D. ROOT TYPE E. ROOT TYPE F. ROOT TYPE G. TOTAL WELDING TIME & WETTER PASS TEMPERATURE	HEAT TREATMENT A. FROM B. POST	H. VEL. P/W	I. LOCATION OF N. L. L. N. L. G. L. L. TYPE ANY	CRACKING A. TYPE B. TYPE C. TYPE D. TYPE E. TYPE F. TYPE G. TYPE H. TYPE I. TYPE J. TYPE K. TYPE L. TYPE M. TYPE N. TYPE O. TYPE P. TYPE Q. TYPE R. TYPE S. TYPE T. TYPE U. TYPE V. TYPE W. TYPE X. TYPE Y. TYPE Z. TYPE	REMARKS OR CRACKING RADIOGRAPH RESULTS, ETC.
A. AD-274 B. 2/19/43 C. TH-96 D. Great Lakes Steel Corp. E. McKay Company F. Allied-Weldcraft, Inc. G. Ternstedt Mfg. Div.	A. 1" B. R-IV (.87Mn, 1.87S, .63Cr, 1.0Ni, 1.7Mo) C. .28 D. Face 323-317-300 E. E.O.H. 1/2 hr. Water F. 1030°F. 1 hr. Air	A. A-II Mck (.12C, 3.5-4.5Mn, .80-21.0Cr, 9.2-10.2 Ni) A-II A W (.08C, 1.8-2.1Mn, .40-51.18-O, 21.0Cr, 10.25-11.75Ni) B. Armorloy A-5 C. Limestone Carb. Ti O2 Sod. Silicate Binder D. DC REV	A. GOODY B. 3/16" C. Flame Cutting Grinding	A. Copper B. II 3/16" 1a 175 - 27 1b 200 - 37 2a 150 - 25 2b 150 - 25 3a 190 - 28 3b 190 - 28 C. 16 hrs. 70° - 150°F. D.	A. None B. None	775	1" L	II 7/8 III 8/8 VI 7/8 I 2/8 II 6/8 V 50/8 93	Failed radiograph Excessive amount of incomplete penetration
A. AD-274 B. 2/19/43 C. TH-97 D. Great Lakes Steel Corp. E. McKay Company F. Ternstedt Mfg. Div.	A. 1" B. R-IV (.87Mn, 1.87S, .63Cr, 1.0Ni, 1.7Mo) C. .28 D. Face 313-326-326 E. E.O.H. 1/2 hr. Water F. 1030°F. 1 hr. Air	A. A-I R-A (.08-15C, 3.5-4.5Mn, .75Si, 18.0-20.0 Cr, 8.5-10.5Ni, 1.25Mo) A-II Mck (.12C, 3.5-4.5Mn, .80-21.0Cr, 9.2-10.2 Ni) B. 18-8-B C. Ti Base +Mn D. DC REV	A. 60° DV B. 3/16" C. Flame Cutting Grinding	A. Copper B. II 3/16" 1a 200 - 25 1b 300 - 30 2a 385 - 30 2b 385 - 30 C. 9 hrs. 70° - 210°F. D.	A. None B. None	760 771	X 2" R	I 11/8 II 6/8 V 23/8 I 4" II 2/8 V 36/8 84/8	Passed radiograph Crater cracks at weld junctions



GENERAL INFORMATION		MATERIALS		PROCESSING		WELDING		EXAMINATION		REMARKS	
A. PART NO.	B. DATE OF TEST	C. PLATE NO.	D. ANNEALING	E. PREPARATION	F. WELDING	G. WELDING	H. WELDING	I. WELDING	J. WELDING	K. WELDING	L. WELDING
A. AD-337 B. 3/23/43 C. TH-103 D. Jones & Laughlin E. McRay Company F. Alloy Rods Co. Mfg. Div.	A. PLATE THICKNESS B. TYPE C. GRADE D. SIZE E. PROCESS F. HEAT TREATMENT G. TENSILE	A. TYPE B. GRADE C. SIZE D. WEIGHT E. POLARITY	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING
A. AD-337 B. 3/23/43 C. TH-103 D. Jones & Laughlin E. McRay Company F. Alloy Rods Co. Mfg. Div.	A. PLATE THICKNESS B. TYPE C. GRADE D. SIZE E. PROCESS F. HEAT TREATMENT G. TENSILE	A. TYPE B. GRADE C. SIZE D. WEIGHT E. POLARITY	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING	A. WELDING B. WELDING C. WELDING D. WELDING E. WELDING F. WELDING G. WELDING H. WELDING I. WELDING J. WELDING K. WELDING L. WELDING

TESTING DATA		PLATE INFORMATION		WELDING DATA		WELDING PROCEDURE		WELDING RESULTS		WELDING DEFECTS	
A. DATE OF TEST	B. PLATE NO.	C. WELDING PROCEDURE	D. WELDING POSITION	E. WELDING TIME	F. WELDING CURRENT	G. WELDING SPEED	H. WELDING POLARITY	I. WELDING DEFECTS	J. WELDING RESULTS	K. WELDING DEFECTS	L. WELDING DEFECTS
A. AD-337 B. 3/23/43 C. TH-104 D. Jones & Laughlin Steel Corp. E. McKay Company F. Reid-Avery Co. Alloy Rods Co. F. 16000F. 1/2 hr. Water Ternstedt Mfg. Co. 8750F. 1-1/2 hrs. Air	A. 1" R-III (1.48Mn, .22Si, .42Mo) C. 24 D. Face 333-323-321 B. O.H.	A. A-II Mck (.12C, 3.5-4.5Mn, .80 Si, 19.0-21.0Cr, 9.2-10.2 Ni)* A-I R-A (.07-.15C, 3.5-4.5Mn, .75Si, 18.0-20.0 Cr, 8.5-10.5Ni, 1.25Mo)* A-II A.R. (.08-.13C, 3.5-4.5Mn, .35-.70Si, 19.0-21.0 Cr, 8.5-10.5Ni)* B. Armorloy A-5 18-8-B Armorsarc B C. Lime+Mn Titanium +Mn D. DC REV	A. 700DV B. 3/16" C. Flame Cutting Grinding	A. Copper B. II 3/16" 1. II 3/16" la 190 - 25 2. I 3/16" la 200 - 25 3. I 1/4" 2a 290 - 27 5/16" 2a 400 - 30 C. 9 hrs. D.	A. None B. None	1 753 2 772 3 768	34" L 74" D 24" U 14" L 24" U	Imp II III 3 9	Passed radiograph Some incomplete penetration. Two small crater cracks		





IDENTIFICATION A. FROM RECORD NO. B. DATE OF TEST C. PLATE NO. D. MANUFACTURER E. ELECTRODE SPEC. F. ANNEAL FABRICATOR	ANION DATA A. PLATE THICKNESS B. TYPE C. CARBON CONTENT D. PHN E. PROCESS F. HEAT TREATMENT G. YIELD STRENGTH	ELECTRODE DATA A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	JOINT DESIGN A. GROOVE INCLUDED B. ROOT GAP C. PLATE PREPARATION	WELDING PROCEDURE A. BACKING B. DEPOSITION RATE C. ROOT TYPE D. ROOT TYPE E. ROOT TYPE F. TOTAL DELTA TIME & WTER COOL TEMPERATURE	WELD METAL A. ANAL. % C. B. ANAL. % S. C. ANAL. % P. D. ANAL. % Mn. E. ANAL. % Si. F. ANAL. % Ni. G. ANAL. % Mo. H. ANAL. % Cr. I. ANAL. % Cu. J. ANAL. % Nb. K. ANAL. % Ti. L. ANAL. % Al. M. ANAL. % Fe.	M. VEL. F/3	BALLISTIC RESULTS LOCATION OF N. CRACKING LOC. TYPE	REMARKS ON CRACKING RADIOGRAPHIC RESULTS, ETC.
A. AD-33 B. 10/9/42 C. H-2 D. Great Lakes Steel Corp. E. Linde Air Products Co. F. Caterpillar Tractor Co.	A. 1" B. R-IV (.84Mn, .82Si, .66Cr, .04N, .19Mo, .10Zr) C. .32 D. Face 302 Back 302 E. B.O.H. Water F. 1640°F. 1050°F.	A. A-II (.25C, 3.95 Mn, .89Si, 7.85Cr, 7.4Ni, .15Mo) B. Orweld #42 C. #80 D. AC	A. 40°SV B. 3/16" C. Machining	A. Baked Sand Core B. 1. Unionmelt 1/4" 1160 - 35 C. 1-3/4 hrs. 300° - 500° D. Hand welded in low spots on root side. The postheat used in welding this plate consisted of passing OXY-ACETYLENE flames on either side of the weld bead about 12" behind the arc. This was used on Welds 1 and 2 only. Preheat for weld 3 was 500°F. for about 4" on either side of the cross-weld and correspondingly across the side plates.	A. 2350 F. 500°F. B. None	769	R D I III V	294 31 41 36 Some incomplete fusion
A. AD-33 B. 10/9/42 C. H-3 D. Youngstown Sheet & Tube Company E. Linde Air Products Co. F. Caterpillar Tractor Co.	A. 1" B. R-III (.130Mn, .15Si, .04Cr, .50Mo) C. .20 D. Face 321 Back 331 E. B.O.H. 1625°F. 2-1/4 hrs. Water F. 1060° 4	A. A-II (.24C, 3.95 Mn, .89Si, 7.85Cr, 7.4Ni, .15Mo) B. Orweld #42 C. #80 D. AC	A. 40°SV B. 3/16" C. Machining	A. Baked Sand Core B. 1. Unionmelt 1/4" 1160 - 35 C. 1-3/4 hrs. 300°F. in this test were rolled to 1-1/8" thick, planed down to 1". Due to excessive "burning in" of the back up core the weld #2 was shallow on the face so hand welding was used to build it up flush with the plate.	A. 2000 F. 500°F. B. None 2	777 785	L U L D I V	Failed radiograph Small crater cracks in center of crossbar weld

Weld Metal Questionable

PLATE INFORMATION		PLATE TREATMENT		PLATE IDENTIFICATION		PLATE CHARACTERISTICS		WELDING PROCEDURE		WELDING RESULTS		REMARKS ON QUALITY	
A. PLATE NUMBER OR DATE OF TEST	B. PLATE NO.	C. MANUFACTURER	D. SIZE	E. PROCESS	F. HEAT TREATMENT	A. TYPE	B. GRADE	C. CHEMISTRY	D. POLARITY	A. POSITION	B. SIZE	C. NO. OF PASSES	D. WELD TYPE
PLATE INFORMATION		PLATE TREATMENT		PLATE IDENTIFICATION		PLATE CHARACTERISTICS		WELDING PROCEDURE		WELDING RESULTS		REMARKS ON QUALITY	
A. PLATE NUMBER OR DATE OF TEST	B. PLATE NO.	C. MANUFACTURER	D. SIZE	E. PROCESS	F. HEAT TREATMENT	A. TYPE	B. GRADE	C. CHEMISTRY	D. POLARITY	A. POSITION	B. SIZE	C. NO. OF PASSES	D. WELD TYPE
A. AD-43 B. 10/3/43 C. 24 D. Great Lakes Steel Corp. Jones & Laughlin Steel Corp. Great Lakes Steel Corp. E. McNay Company F. General Motors Truck & Coach	A. 1" (1.75Mn, .24Si, .55Mo) B. R-III J&L C. R-IV G L D. .94Mn, .81Si, .70Cr, .22Mo, .09Zr E. .25 F. 321 to Back 321 to Back 341 to Back 341 to	A. A- B. Armorloy A-5 Oxweld #42 C. #80 (20XD) & (8X200) D. AC DC REV	A. 60°DV B. 3/16" Cutting C. Flame	A. Not given B. None C. 8 hrs. 1500 - 200°P. and grinding after first pass. Root passes were hard welded. Right and upper center sections by Jones & Laughlin, left and lower center sections by Great Lakes. Total chipping and grinding time 4 hrs., details not given.	1 L109 2 L164	4 1/2" Imp D 8" Imp U	II III II III	2" Passed radiograph 6 1/2"					
A. AD-43 B. 10/3/43 C. 24 D. Great Lakes Steel Corp. Jones & Laughlin Steel Corp. Great Lakes Steel Corp. E. Harnischfeger F. General Motors Truck & Coach	A. 1" (.94Mn, .81Si, .70Cr, .22Mo, .09Zr) B. R-IV G L C. .94Mn, .81Si, .70Cr, .22Mo, .09Zr D. .25 E. 321 to Back 321 to Back 341 to Back 341 to F. B.O.H. Both 1625°P. J&L 2-1/4 hrs. Water 1075°F. 4 hrs. Draw 1625°P. G L 2-1/4 hrs. Water 1030°F. 4 hrs. Draw	A. A B. AW-3 Oxweld # 42 C. #80 (20XD) & (8X200) D. AC DC REV	A. 60°DV B. 3/16" Cutting C. Flame	A. Not given B. None C. 8 hrs. 1500 - 200°P. Root passes were hand welded. Right and upper center sections by Great Lakes, left and lower center sections by Jones & Laughlin. Total chipping and grinding time 3 hrs., details not given.	1 L106 2 L183 3 L177	2 1/2" L 9 1/2" L 1 1/2" Imp D	6" D 9 1/2" U 1 1/2" Imp III 1 1/2" D V	2" Passed radiograph 10 1/2" 36 1/2"					

IDENTIFICATION A. FROM RECORD NO. B. DATE OF TEST C. PLATE NO. D. ASSESS MANUFACTURER E. ELECTRODE BRAND F. AMPER FURNISHMENT	ANODE AREA A. PLATE THICKNESS B. TYPE C. GUNION CONTENT D. SIZE E. PROCESS F. HEAT TREATMENT G. TEST TIME	WELDER DATA A. TRADE NAME B. COATING C. CURRENT & POLARITY	JOINT DESIGN A. GROOVE SHAPED B. BEVEL ROOT FACE C. ROOT GAP D. PLATE PREPARATION	WELDING PROCEDURE A. SA OTHER B. DEPOSITION SIZE EL. NO. TYPE AMR V C. SLOTTED TYPE D. SLOTTED TYPE E. TOTAL WELDING TIME CENTER PASS TEMPERATURE	HEAT A. PRE B. POST	M VEL. F/W	BALLING RESULTS		REMARKS ON CRACKING RADIOGRAPHIC RESULTS, ETC.
							LOCATION OF N	CRACKING	
A. AD-43 B. 10/6/42 C. J4 D. Jones & Laughlin Steel Corp. Great Lakes Steel Corp. E. Harrischfefer C. 25 F. Linde Air Prod. General Motors Truck & Coach	A. 1" R-III J&L (1.75Mn, .24Si, .55Mo) R-IV G L (.94Mn, .81Si, .70Cr, .22Mo, .09Zr) C. 25 D. Face 321 to Back 341 E. B.O.H. Both 16250F. J&L 2-1/4 hrs. Water 10750F. 4 hrs. Draw 16250F. C L 2-1/4 hrs. Water 10300F. 4 hrs. Draw	A. A B. AV-3 Oxweld #42 C. #80 (20XD) & (8X200) D. AC DC REV	A. GOODY B. 3/16" C. Flame Cutting	A. Not given B. 1. II 5/32" Ia 100 - 135 - 2. IV 3/16" IUM 640 - 680 C. 8 hrs. 150° - 200°F. D. Root passes hand welded. Right and lower center sections by Great Lakes, left and upper center sections by Jones & Laughlin. Total chipping and grinding time 3 hrs., details not given.	A. None B. None	1 1102 2 1147 3 1097 4 1083 5 1144	57" U 81" L 1" D 11" U 1" imp U 57MM Tl projectile	II 5" III 7" V 2" III I 3" II 8" III 5" V 2" 34"	Passed radiograph

IDENTIFICATION	ANVIL AREA	ELECTRODE AREA	WELDING PROCEDURE	WELT	BALLISTIC RESULTS		REMARKS ON CRACKING
					WELT	LOCATION OF H	
A. PART NUMBER OR DATE OF TEST	A. PLATE THICKNESS	A. TYPE	A. ELECTRODE	A. WELDING	A. WELT	A. BALLISTIC	A. REMARKS
B. PLATE NO.	B. TYPE	B. TRADE NAME	B. ANGLE, INCL. OR	B. DEPOSITION	B. WELT	B. BALLISTIC	B. REMARKS
C. ANNEALING	C. COATING	C. GRINDING	C. FLAME	C. SIZE EL.	C. WELT	C. BALLISTIC	C. REMARKS
D. MANUFACTURER	D. ORIENT	D. POLARITY	D. CUTTING	D. TYPE	D. WELT	D. BALLISTIC	D. REMARKS
E. ELECTRODE SPAC.	E. HEAT TREATMENT	E. DC REV	E. GRINDING	E. TEMPERATURE	E. WELT	E. BALLISTIC	E. REMARKS
F. ANNEALING	F. TEMPERATURE	F. DC REV	F. GRINDING	F. TEMPERATURE	F. WELT	F. BALLISTIC	F. REMARKS
A. AD-111 B. 10/26/42 C. 75 D. Utility Electric Co. E. McKay Company F. Cadillac Motor Car Company	A. 1" B. C-II (1.61Mn, .0251 .15Cr, .18Ni, .45Mo) C. .36 D. Face 269-277 E. Acid-Elec. F. Questionable	A. A B. Armorloy C. Gray Flux D. DC REV	A. 60°DV B. 3/16" C. Flame Cutting Grinding	A. None B. None C. 2-1/2 hrs. 75° - 180° D. One more pass in crossbar. Little cracking, chipping and grinding after first pass. Time 10 mins.	1 1133	2" L 5 1/2" D Imp III V 3 3/4" 3 3/4" 3 3/4"	Passed radiograph Small amount of piping in cast plate Two small crater cracks
A. AD-111 B. 10/26/42 C. 77 D. Hayes Tool Company E. McKay Company F. Cadillac Motor Car Company	A. 1" B. C-I (1.10Mn, .42Si, .38Cr, .10Ni, .38Mo) C. .15 D. Face 269 E. Acid-Elec. F. 1900° F. 10 hrs. F.C. to 1650° F. A.C. 1200° F. 2 hrs. 1650° F. 1 hr. Water. 1000° F. 4 hrs. Air	A. A B. Armorloy C. --- D. DC REV	A. 60°DV B. 3/16" C. Flame Cutting Grinding	A. None B. None C. 2.49 hrs. 80° - 150° D. Little cracking, chipping and grinding after first pass. Time 1.31 hrs.	1 1004 2 1020	1 1/4" L 5 1/2" U Imp III V 6 1/2" D II 1 1/2" III 2 1/2" III 1 1/2" IV 4 1/2" V 1 1/2" VI 2 1/2"	Passed radiograph
A. AD-112 B. 10/26/42 C. 78 D. American Steel Foundries E. McKay Company F. Cadillac Motor Car Company	A. 1" B. C-II (1.53Mn, .42Si, .34Cr, .10Ni, .07Mo) C. .33 D. Face 277 E. Back 311 F. 1650° F. 2 hrs. Air G. 1535° F. .67 hrs. Water H. 850° F. 4 hrs. Water	A. A-II (.18C, .475 Mn, .70Si, 20.45Cr, 8.60Ni, .22Al) B. .50Cr, Mn, .53Si, 20.90Cr, 9.80Ni) C. Armorloy D. DC REV	A. 60°DV B. 3/16" C. Flame Cutting Grinding	A. Not given B. 1. II 5/32" 1a 120 - 35 5/32" 1a 180 - 30 2. I 3/16" 2a 180 - 30 3. III 5/32" 2b 120 - 25 1/4" 1b 200 - 25 C. 3.04 hrs. 80° - 140° D. Some cracking after first grinding after first and second passes. Little chipping and grinding time 3 hrs., details not given.	1 1017 2 1014	5 1/2" L 6 1/2" R 5 1/2" U Imp II V V 19" 28" 28"	Passed radiograph Some incomplete fusion and penetration in legs Small cracks in crossbar

IDENTIFICATION	ANOD. DATA	BASE METAL	JOINT DESIGN	WELDING	PROCESSING	HEAT	BALLISTIC RESULTS		CRACKING	COMMENTS ON CRACKING RADIOGRAPHIC RESULTS, ETC.
							VEL. FT/S	LOCATION OF N		
A. PART NUMBER	A. PLATE THICKNESS	A. TYPE	A. GROOVE INCLUDES	A. WELDING	A. PROCEDURE	A. PART	LI	EL	LOG TYPE	AMT
B. DATE OF TEST	B. TYPE	B. GRADE	B. ANGLE, BEVEL FACE	B. DEPOSITION	B. SIZE EL. NO. TYPE AMT V.	B. POST				
C. PLATE NO.	C. SANDWICH ORIENT	C. COATING	C. PLATE PREPARATION	C. 1.0007 TYPE	C. 2.0007 TYPE					
D. SURFACE MANUFACTURER	D. DIM	D. CORR.	D. CORR.	D. 3.0007 TYPE	D. 4.0007 TYPE					
E. SURFACE FINISH	E. PROCESS	E. CORR.	E. CORR.	E. 5.0007 TYPE	E. 6.0007 TYPE					
F. SURFACE TREATMENT	F. RELY TREATMENT	F. CORR.	F. CORR.	F. 7.0007 TYPE	F. 8.0007 TYPE					
G. SURFACE PREPARATION	G. TEST TIME	G. CORR.	G. CORR.	G. 9.0007 TYPE	G. 10.0007 TYPE					
A. A1-235 B. 2/7/43 C. #4 D. H. J. Corp. E. McKay Company F. Calline Motor G. Call Division	A. .39" B. C-11 (1.60Mn, .37Si, .41Cr, .12Ni, .53Mo) C. .21 D. Face 341 E. Back 331 F. 1900F, 10 hrs. G. 1000F, 10 hrs. H. 1200F, 2 hrs. I. 1650F, 1 hr. J. Water K. 1000F, 4 hrs. L. Air	A. A-11 (.10C, .45 Mn, .54Si, 19.40Cr, 10.15Ni, .08Mo) (.09C, .480 Mn, .65Si, 20.70Cr, 10.00Ni, .08Mo) E. Armorloy F. C. --- G. DC REV	A. 60°DV B. --- C. Flame Cutting Grinding	A. Not given B. 1. II 5/32" 1a 140 - 25 3/16" 1a 200 - 25 1/4" 2a 850 - 25 2. I 1/4" 2a 850 - 25 3. III 5/32" 4b 120 - 25 remaining two beads not given C. 2.29 hrs. 70° - 1900F. D.	A. None B. None	A. None B. None	6 1/2" D 2" L	Imp V 5"	"Failed radiograph incomplete fusion present along lower left leg. Some scattered slag inclusions	
A. A1-234 B. 2/4/43 C. 106 D. McCannay & Wiley E. McKay Company F. Calline Motor G. Call Division	A. .39" B. C-11 (1.72Mn, .57Si, .41Ni, .67Mo) C. .25 D. Face 302 E. Back 302 F. 1600F, .4 hrs. Air 1600F, .4 hrs. Water 1050F, .4 hrs. Water	A. A-11 (.09C, .495 Mn, .55Si, 21.00Cr, 10.20Ni, .15Mo) (.12C, .4.65 Mn, .65Si, 18.00Cr, 9.62Ni, .07Mo) B. Armorloy C. --- D. ---	A. 60°DV B. 3/16"	A. Not given B. 1. II 3/16" 1a 185 - 25 3/16" 1a 210 - 25 2. I 1/4" 2a 280 - 25 3. I 5/16" 2a 360 - 25 C. 2.01 hrs. 70° - 1900F. D.	A. None B. None	A. None B. None	1 1/2" L 1 1/2" R 3 1/2" D 5 1/2" D 57mm. Tl projectile	Imp V 5" 3 1/2" Imp V 5" 5 1/2" Imp V 3 1/2" 20"	Passed radiograph Several small cracks throughout 1" thr welds	

INVESTIGATION A. SYMBOL NO. B. DATE OF TEST C. PLATE NO. D. MANUFACTURER E. ELCTRODE MARK F. AMPER FABRICATOR	WELDING DATA A. TYPE B. CLASSIFICATION C. SIZE D. PROCESS E. HEAT TREATMENT F. WELDING TIME	ELECTRODE DATA A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	WELDING DEFECTS A. CRACKS B. ROOT GAP C. PLATE PREPARATION	WELDING PROCEDURE A. BACKING B. DEPOSITION SIZE C. ROOT TYPE D. WELD TYPE E. WELD TYPE F. TOTAL WELDING TIME & ENTER PASSES G. REMARKS	HEAT A. PAZ B. POST	BALL BEING REPAIRED		REMARKS ON CRACKING RADIOGRAPHIC RESULTS ETC.	
						M	VEL. 1/8"		
A. AD-234 B. 2/4/43 C. 109 D. McCorway & Torley E. McKay Company F. Cadillac Motor Car Division	A. 1.13" B. C-III (1.65Mn, .56Si, .18Al, .60Mn) C. 1/8" D. Face 321 E. Back 302 F. 1600OF. 4 hrs. Air 1600OF. 4 hrs. Water 1060OF. 4 hrs.	A. A-II (.10C, 4.80 Mn, .66Si, 17.90Cr, 9.75Ni, .08Co) B. Mn, .55Si, 20.10Cr, 10.20Ni, .15Mo) C. --- D. --- E. --- F. --- G. --- H. --- I. --- J. --- K. --- L. --- M. --- N. --- O. --- P. --- Q. --- R. --- S. --- T. --- U. --- V. --- W. --- X. --- Y. --- Z. ---	A. 60 <sup>0</sup> VD B. --- C. Flame D. Grinding	A. Not Given B. 1. II 5/32" 1a 130 - 25 2. I 3/16" 2a 200 - 25 3. III 5/32" 4b 140 - 25 C. 2.70 hrs. 700 - 1950F. D. Some cracking after first and second passes.	A. None B. None	1	376	2 1/2" R 18" charred small piece off U top of plate 2 1/2" R 9 1/2" Imp V 14" Falled radiograph Several cracks present in cross bar 3 1/2" R 3 1/2" Imp V 11 1/2" Large amount of incomplete fusion scattered through out the welds 4 1/2" R 3 1/2" Imp III 12" V 12" Several inches of linear slag present 5 1002 2 1/2" R 9 1/2" Imp III 2 1/2" V 4 1/2" sent	
A. AD-241 B. 2/9/43 C. 86 D. Utility Electric Co. E. McKay Company F. Cadillac Motor Car Division	A. 1.13" B. C-III (1.65Mn, .12Si, .30Cr, .21Ni, .46Co) C. Face 341 D. Back 262 E. 1950OF. 10 hrs. Air 1350OF. 5 hrs. Air 1650OF. 6 hrs. Water	A. A-II (.09C, 4.85 Mn, .55Si, 20.10Cr, 10.20Ni, .15Mo) B. Mn, .65Si, 18.00Cr, 9.62Ni, .07Mo) C. --- D. --- E. --- F. --- G. --- H. --- I. --- J. --- K. --- L. --- M. --- N. --- O. --- P. --- Q. --- R. --- S. --- T. --- U. --- V. --- W. --- X. --- Y. --- Z. ---	A. 60 <sup>0</sup> VD B. --- C. Flams D. Grinding	A. Not Given B. 1. II 3/16" 1a 120 - 25 2. I 1/4" 1a 200 - 25 3. III 5/32" 4b 120 - 25 C. 2.03 hrs. 800 - 2050F. D. Some cracking after first and second passes.	A. None	1	1111	3 1/2" Imp III 3 1/2" Failed radiograph Small crater cracks in cross-section 1" 8 1/2" Imp V 4 1/2" bar end at left junction 7 1/2" Some slag inclusions	

GENERAL INFORMATION		ANALYSIS DATA		ELEMENTARY ANAL.		WELDING PROCEDURE		HEAT TREATMENT		BALLING ORNAMENT		X-RAY	
A. PART NO.	B. DATE OF TEST	C. PLATE NO.	D. PLATE MANUFACTURER	E. PLATE THICKNESS	F. PLATE TYPE	G. TRADE NAME	H. COATING	I. ORNAMENT	J. POLARITY	K. TYPE OF WELD	L. LOCATION OF BALLING	M. BALLING ORNAMENT	N. X-RAY
AD-240	2/11/43	85	American Steel Foundries	1.78In. .56S1, .23Cr, .18Ni, .09Mo	C-II B-55	A-II McVA 60DV	Mn.19.47 Cr.10.15 Ni.54S1, .06Mo	1. II 3/16" 2a 190 - 25 2. I 3/16" 2a 190 - 25 3. III 5/32" 4b 130 - 25	A. None B. None	3" L	4" Imp D	V	7" Passed radiograph Some incomplete fusion and slag inclusions
Lincoln Electric Co.			McKay Company	(1.40Mn, .43S1, .20Cr, .30Ni, .07Mo)	C-II B-55	Mn.19.47 Cr.10.15 Ni.54S1, .06Mo	Cutting Grinding			3 1/2" L	5 1/2" Imp U	V	
Cadillac Motor Car Company				(1.35Mn, .48S1, .21Cr, .06Ni, .09Mo)	A-II Lin.					3 1/2" R	7" Imp D	I II V	
				.58 B-57 .30 B-55 .28 B-55						57MM Tl projectile			
				Face 293 Back 321									
				1650°F. B-67 2 hrs. Air 1525°F. 40 mins. Water 1160°F. 4 hrs. Water 1650°F. 1575 C. --- weld 2 hrs. Air 1525°F. 40 mins. Water 900°F. 4 hrs. Water 1650°F. B-55 2 hrs. Air 1525°F. 40 mins. Water 1180°F. 4 hrs. Water									



A. PLATE NUMBER AND DATE OF TEST B. PLATE NO. C. JAMES MANUFACTURER D. SELECTING SPEC. E. JAMES FABRICATOR	A. PLATE THICKNESS B. TYPE C. GARDNER CERTIFY D. DIM. E. PROCESS F. HEAT TREATMENT TEMP. TIME ORDER	A. TYPE B. TENSILE MARK C. COATING D. CORROSION E. POLARITY	A. COATING B. SURFACE C. PLATE PREPARATION	WELDS A. SA BEING B. REPRESENTATION C. EL. SA TYPE D. JOINT TYPE E. GROOVE TYPE F. TOTAL WELDED TIME & INTER PASS TEMPERATURE G. REMARKS	HEAT A. P.M. B. POST	H	V/L 7/8	BALLISTIC RESULTS			REMARKS ON CRACKING RADIOGRAPHING RESULTS, ETC.	
								LI	EL	UL		CRACKING LOAD TYPE IMP
A. AD-309 B. 2/23/43 C. 115 D. McConway & Torley E. McKay Company F. Cadillac Motor Car Division	A. 1.02" B. C-III (1.61Mn, .51Si, .03Cr, .08Ni, .06Mo) C. 28 D. Face 286 E. Back 321 F. 1800°F. 4 hrs. Air 1600°F. 4 hrs. Water 1060°F. 4 hrs. Water	A. A-II (.10C, 4.80 Mn, .66Si, 17.90Cr, 9.75Ni, .09Mo) B. .55Si, .09C, 4.85 Mn, .55Si, 20.10Cr, 10.20Ni, .15Mo) C. Armorloy D. --- E. ---	A. 60°DV B. 3/16" C. Flame Cutting	A. Not Given B. 1. II 5/32" 2a 140 - 25 2. I 3/16" 1a 180 - 25 5/32" 1a 140 - 25 3. III 1/4" 2b 240 - 25 5/32" 1b 140 - 25 remaining three beads not given C. 2.77 hrs. 70° - 190°F. D. Some cracking after first pass.	A. None B. None	1	997	1 1/4" L	10 3/8" Imp D	I 1 1/2" II 1 1/2" V 4 1/4"	Passed radiograph	
A. AD-295 B. 2/5/43 C. 116 D. McConway & Torley E. McKay Company F. Cadillac Motor Car Division	A. 1.25" B. C-III (1.54Mn, .56Si, .08Ni, .50Mo) C. 28 D. Face 302 E. Back 321 F. 1800°F. 4 hrs. Air 1600°F. 4 hrs. Water 1060°F. 4 hrs. Water	A. A-II (.09C, 4.85 Mn, .55Si, 20.10Cr, .15Mo) B. .42Si, .08C, 4.50 Mn, .42Si, 20.40Cr, 10.10Ni) C. Armorloy D. DC REV	A. 60°DV B. --- C. Flame Grinding	A. Not Given B. 1. II 3/16" 2a 180 - 25 2. I 1/4" 2a 240 - 25 3. I 5/16" 2a 360 - 25 C. 2.40 hrs. 70° - 190°F. D.	A. None B. None	1	1137	2 1/2" R	4 1/2" Imp D	II 1 1/2" III 1 1/2" V 2 1/2"	Passed radiograph Some incomplete fusion Several small crater cracks in crossbar	
						2	1133	1 1/2" L	7" Imp U	I 1 1/2" II 4 1/4" V 5 1/4" 3 1/4"		
								57mm. Tl projectile				



INDICATIONS A. FRAM NUMBER AND DATE OF TEST B. PLATE NO. C. MANUFACTURER D. ELECTRODE MPAN E. PROCESS F. ANODE FLUX	ANODE DATA A. PLATE THICKNESS B. TYPE C. GANION CONTENT D. SIZING E. PROCESS F. HEAT TREATMENT G. TEST TIME	ELECTRODE DATA A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	JOINT DESIGN A. GROOVE INCLUDED B. HOLE, NOT PADE C. NOT SLD D. PLATE PREPARATION	WELDER A. BAORING B. DESCRIPTION C. ROOT TYPE D. GROOVER TYPE E. TOTAL WELDING TIME & INTER PASS TEMPERATURE	WELT A. NONE B. POINT	RADIOGRAPH RESULTS		REMARKS ON RADIOGRAPH RADIOGRAPHIC RESULTS, ETC.
						H. VEL. 7/8	I. LOCATION OF H. L.L. L.L. G.S. LOCAL TYPE ANY	
A. AD-106 B. 11/19/42 C. KW-163-F D. Kelsey Hayes Wheel Corp. E. Harnischfeger Corp. F. Chevrolet Motor Co.	A. 1" (.90Mn., .3781) B. C-11 (.43Cr., .32Mo) C. .30 D. Face 293-340 E. B. Elec. 1950°F. 10 hrs. Air F. 1250°F. 4 hrs. Air G. 1650°F. 5 hrs. Water H. 1150°F. 10 hrs. Air	A. A-1 (.15C, 4.47 Mn., .65Si, 9.5Ni, 1.07Mo)* (.14C, 3.89 Mn., .61Si, 19.7Cr, 10.1Ni, .97Mo)* B. AW-3-C C. Lime D. DC REV	A. 49°DV, 3/32" RF B. 3/16" RF C. Machining	A. Not given B. 1. I 5/32" 1a 110-140 - 24-25 2. I 3/16" 2a 140-175 - 25-26 5/32" 1a 110-140 - 24-25 3. II 3/16" 2b 140-175 - one side 25-26 III 5/32" 2b 110-140 - other side 24-25 3/16" 1b 140-175 - 25-26 C. 12 hrs. 800 - 1800°F. D.	A. None B. None	2" R 6" Imp D 6 1/2" Imp L U 3 1/2" Imp R D 57MM Tl projectile	I 5" Passed radiograph II 1" Large amount of porosity present III 1 1/2" in cast plate V 8" Two small cracks near right weld VI 7" junction V 22 1/2" 53	
A. AD-106 B. 11/19/42 C. KW-164-F D. Kelsey Hayes Wheel Corp. E. McKay Company F. Chevrolet Motor Co.	A. 1" (.90Mn., .3781) B. C-11 (.43Cr., .32Mo) C. .30 D. Face 293-340 E. B. Elec. 1950°F. 10 hrs. Air F. 1250°F. 4 hrs. Air G. 1650°F. 5 hrs. Water H. 1150°F. 10 hrs. Air	A. A-1 (.12C, 4.26 Mn., .52Si, 19.1Cr, 9.4Ni)* (.07C, 4.20 Mn., .63Si, 19.5Cr, 9.3Ni)* B. Armorloy AC-5 C. Lime D. DC REV	A. 60°DV, 3/32" RF B. 3/16" RF C. Machining	A. Not given B. 1. I 5/32" 1a 110-140 - 24-25 2. I 3/16" 3a 140-175 - 25-26 3. II 3/16" 2b 140-175 - one side 25-26 III 5/32" 2b 110-140 - other side 24-25 3/16" 1b 140-175 - 25-26 C. 15 hrs. 800 - 1450°F. D.	A. None B. None	2" R 10" Imp D 2" Imp L D 57MM Tl projectile	II 2 1/2" Felled radiograph V 18 1/2" General condition of incomplete fusion along left 3 1/2" leg, some in right leg VI 16 1/2" 46 1/2"	
A. AD-106 B. 11/19/42 C. KW-165-F D. Kelsey Hayes Wheel Corp. E. Alloy Rods Co. F. Chevrolet Motor Co.	A. 1 1/2" (.90Mn., .3781) B. C-11 (.43Cr., .32Mo) C. .30 D. Face 293-340 E. Acid-O.M. 1950°F. 10 hrs. Air F. 1250°F. 4 hrs. Air G. 1650°F. 5 hrs. Water H. 1150°F. 10 hrs. Air	A. A-1 (.10C, 1.25 Mn., .36Si, 17.6Cr, 8.9Ni, 2.43Mo)* A-11 (.12C, 3.58 Mn., .36Si, 18.6Cr, 8.8Ni)* B. Armorloy B C. Ti O2 D. DC REV	A. 60°DV, 3/32" RF B. 3/16" RF C. Machining	A. Not given B. 1. I 5/32" 1a 110-140 - 24-25 2. I 1/4" 2a 200-250 - 27-28 5/32" 1a 110-140 - 24-25 3. II 1/4" 2b 200-250 - one side 27-28 III 5/32" 2b 110-140 - other side 24-25 1/4" 1b 200-250 - 27-28 C. 10 hrs. 800 - 1900°F. D.	A. None B. None	4" R 12" Imp D 2 1/2" Imp L D 1" Imp R D 3 1/2" Imp O D 57MM Tl projectile	III 6 1/2" Passed radiograph V 24" two small cracks in crossbar VI 1" Scattered slag inclusions VII 8" 27 1/2" VIII 5" IX 2 1/2" X 10 1/2" XI 6 1/2" 65 1/2"	54

eWeld Metal



IDENTIFICATION	MATERIALS	WELDING PROCEDURE	WELDING POSITION	WELDING PARAMETERS	WELDING RESULTS	REMARKS ON GRINDING RADIOGRAPHIC RESULTS, ETC.
<p>A. AD-228</p> <p>B. 11/16/42</p> <p>C. W-37</p> <p>D. Ford Motor Co.</p> <p>E. Crucible Steel Corp.</p> <p>F. Ford Motor Co.</p>	<p>A. 1-3/16"</p> <p>B. C-II</p> <p>(1.10Mn, .50Si, .50Cr, .38Mo)</p> <p>C. .30</p> <p>D. Face 241 Back 302</p> <p>E. Elec.</p> <p>F. 1800°F. 5 hrs. Air 1700°F. 3 hrs. Water 1020°F. 6 hrs. Water</p>	<p>A. 450DV</p> <p>B. 3/16"</p> <p>C. Flame Cutting Grinding</p>	<p>A. A-I (.07C, 1.40 Mn, .27Si, 18.00Cr, 10.2Mn, 2.0Mo)</p> <p>B. Armorize reziatal</p> <p>C. TITANIA</p> <p>D. DC REV</p>	<p>A. II 5/32" la 130 - 30</p> <p>5/32" la 125 - 20</p> <p>3/16" 3a 180 - 22</p> <p>3/16" 1a 190 - 22</p> <p>1/4" 1a 215 - 22</p> <p>3/16" 1a 175 - 22</p> <p>1/4" 2a 215 - 22</p> <p>980 - 1550°F.</p> <p>D. Cracking and grinding after first pass. Cross-weld was not welded last. Each pass was completely welded throughout the entire H before the subsequent pass was made.</p>	<p>A. None</p> <p>B. None</p>	<p>7" R</p> <p>Imp</p> <p>I 36"</p> <p>V 42"</p> <p>40"</p> <p>Passed radiograph</p>
<p>A. AD-166</p> <p>B. 11/25/42</p> <p>C. W-76</p> <p>D. Ford Motor Co.</p> <p>E. Crucible Steel Corp.</p> <p>F. Ford Motor Co.</p>	<p>A. 1"</p> <p>B. C-II</p> <p>(1.20Mn, .47Si, .61Cr, .35Mo)</p> <p>C. .30</p> <p>D. ---</p> <p>E. B. Elec.</p> <p>F. 1800°F. 5 hrs. Air 1700°F. 3 hrs. Water 1040°F. 8 hrs. Air</p>	<p>A. 450DV</p> <p>B. 1/4"</p> <p>C. Flame Cutting</p>	<p>A. A-I (.07C, 1.82 Mn, 30.09 Cr, 9.97E 2.00Mo)</p> <p>B. Armorize reziatal</p> <p>C. TITANIA</p> <p>D. DC REV</p>	<p>A. II 5/32" 2a 135 - 22</p> <p>3/16" 2a 175 - 22</p> <p>1/4" 1a 218 - 22</p> <p>1/4" 1a 240 - 22</p> <p>C. 2-3/4 hrs. 1380 - 2350°F.</p> <p>D. Cracking and grinding after first pass. Bottom of root pass ground out.</p>	<p>A. None</p> <p>B. None</p>	<p>6 1/2" D</p> <p>Imp</p> <p>I 1"</p> <p>II 2 1/2"</p> <p>III 1 1/2"</p> <p>V 11"</p> <p>8" L</p> <p>1 1/2" Imp</p> <p>III 1"</p> <p>III 2 1/2"</p> <p>V 17 1/2"</p> <p>1" L</p> <p>998</p> <p>2</p> <p>3</p> <p>988</p> <p>4</p> <p>988</p> <p>57MM T1 projectile</p> <p>Passed radiograph</p>

IDENTIFICATION A. FORM NUMBER B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. ELEMENTS WELD F. WELDER	ANNEAL DATA A. PLATE THICKNESS B. TYPE C. GROUND SURFACE D. SURFACE E. PROCESS F. HEAT TREATMENT TEMP. TIME	WELDING DATA A. WELD TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	JOINT DESIGN A. GROOVE OR UNDRILLED B. BUTT GAP C. PLATE PREPARATION	WELDING PROCEDURE A. BACKING B. DEPOSITION SIZE EL. NO. TYPE AMP. V. C. ROOT TYPE D. GROUNDED TYPE E. TOTAL WELDING TIME & INTER PASS TEMPERATURE	HEAT TREATMENT A. PRE B. POST	N VEL. F/S	BALLISTIC RESULTS		REMARKS OR CRACKING RADIOGRAPHIC RESULTS, ETC.
							LOCATION OF N. L.L. N.L. S.B.	CRACKING EXP. TYPE AMT	
A. AD-223 B. 11/4/43 C. 41 D. American Steel Foundries E. Siver Steel Coating F. McKay Company G. General Motors Truck & Coach Division	A. 1" B. C-II Am. (1.52Mn, .45Si, .32Cr, .06Mo) C. I. Siv. (.87Mn, .36Si, .45Cr, .49Ni, .41Mo) D. 32 E. 23 F. Face 331-352 Back 341-363 E. B.C.H. F. 16500 Am. 2 hrs. Air 15250F. 6 hrs. Water 930F. 4 hrs. Water 1900F. Siv. 4 hrs. Air 1600F. 4 hrs. Water 10500F. 6 hrs. Water	A. A-I (.10C, 3.66 Mn, 1.13Si, 18.10Cr, 10.20Ni, .47Mo) B. Armorloy A-5 C. Lime D. DC REV	A. 45°DV B. 3/16" C. Flame Cutting	A. Not given B. I. II 5/32" 1a 90 - 3/16" 1a 125 - 3/16" 3a 175 - 3/16" 4b 175 - C. 6-1/2 hrs. Under 200° & 300°F. D. Little grinding after each pass. Left and upper center sections by Siv. Steel and the right and lower center sections by American Steel.	A. None B. None	1 1050 2 1054	1/2" L 1/2" R	1 1/2" Imp D 7" 0 V U Imp I. 28 V. 15 57 1/2	5" Passed radiograph
									57MM TI projectile
									Weld Metal

A. PART NUMBER OR IDENTIFICATION OF PART	B. PLATE NO.	C. MANUFACTURER	D. PART NAME	E. MATERIAL	F. FINISH	G. HARDNESS	H. TENSILE STRENGTH	I. ELONGATION	J. IMPACT	K. TYPING	L. WEIGHT	M. COMMENTS	N. ANALYSIS	
													O. C	P. S
A. AD-158 B. 10/23/42 C. Hughes Tool Company D. Relia-Avery E. Relia-Avery F. Ternstedt Mfg. Div.			A. I B. C-I (.85Mn., .39Si, .43Cr, 1.23Ni, .45Mo) C. .25 D. Face 359-361-363 E. Acid-Elec. F. 1900°F. 1C hrs. in furnace to 1650°F. Water 1200°F. 2 hrs. Air 1650°F. 1 hr. Water 1000°F. 4 hrs. Air	A. A-I (.07-15C 3.50-4.50 Mn., .75Si, 18.00, 20.00Cr, 8.50-10.5 Ni, 1.25 Mo) B. 18-8-B C. --- D. AC	A. 60°DV B. 3/16" C. Flame Cutting Grinding	A. Copper B. 1. II 3/16" 1a 200 - 27 5/16" 1a 400 - 30 2. I 3/8" 1a 450 - 30 5/16" 1a 400 - 30 C. 5-1/2 hrs. 70° - 180°F. D.		1 1074 2 1096 3 1130	X X X	5" Imp U 7" Imp X 4 3/8" O III 0 Imp III 5 1/2" V 10 1/2"	4 1/2" Passed radiograph 1 1/2" Slag in upper left leg 2 1/2" Incomplete fusion in crossbar			
A. AD-158 B. 11/4/42 C. Hughes Tool Company D. Lincoln Electric Co. E. Ternstedt Mfg. Div.			A. I B. C-I (.85Mn., .39Si, .43Cr, 1.23Ni, .45Mo) C. .25 D. Face 341-350-345 E. Acid-Elec. F. 1900°F. 10 hrs. in furnace to 1650°F. Water 1200°F. 2 hrs. Air 1650°F. 1 hr. Water 1000°F. 4 hrs. Air	A. A-II (.08-10C 3.50-4.25 Mn., .45-.80 Si, 19.00-20.50Cr, 8.5-10.0 Ni) B. Armorweld C. Lime D. DC REV	A. 60°DV B. 1/4" C. Flame Cutting Grinding	A. Copper B. 1. II 1/4" 2a 300 - 25 5/16" 2a 390 - 30 3. I 5/16" 2a 390 - 30 C. 3 hrs. D.		1 1037 2 1110 3 1037 4 1066	X X X X	4 1/2" Imp U 1 1/2" Imp D 11" Imp III 2 1/2" Imp D 0 Imp III 1 1/2" 18 1/2"	6" Passed radiograph			

A. PART NUMBER B. DATE OF TEST C. PLATE OR D. MANUFACTURER E. SURFACE OPER. F. SURFACE FINISH	A. TYPE B. TENSILE STRENGTH C. YIELD STRENGTH D. ELONGATION E. REDUCTION OF AREA F. TENSILE REDUCTION	A. TYPE B. TENSILE STRENGTH C. YIELD STRENGTH D. ELONGATION E. REDUCTION OF AREA F. TENSILE REDUCTION	A. TYPE B. TENSILE STRENGTH C. YIELD STRENGTH D. ELONGATION E. REDUCTION OF AREA F. TENSILE REDUCTION	A. TYPE B. TENSILE STRENGTH C. YIELD STRENGTH D. ELONGATION E. REDUCTION OF AREA F. TENSILE REDUCTION	A. TYPE B. TENSILE STRENGTH C. YIELD STRENGTH D. ELONGATION E. REDUCTION OF AREA F. TENSILE REDUCTION	A. TYPE B. TENSILE STRENGTH C. YIELD STRENGTH D. ELONGATION E. REDUCTION OF AREA F. TENSILE REDUCTION	A. TYPE B. TENSILE STRENGTH C. YIELD STRENGTH D. ELONGATION E. REDUCTION OF AREA F. TENSILE REDUCTION	A. TYPE B. TENSILE STRENGTH C. YIELD STRENGTH D. ELONGATION E. REDUCTION OF AREA F. TENSILE REDUCTION
A. AD-255 B. 2/3/43 C. TH-64 D. Hughes Tool Company E. Alloy Metals Co. F. Ternstedt Mfg. Div.	A. 1.015" B. C-I (.85Mn, .3981, .45Cr, 1.23Mn, .45Mo) C. .25 D. Face 347-348-345 E. Acid-Elec. F. 1900°F. 10 hrs. in furnace to 1650°F. 1 hr. Water G. 1200°F. 2 hrs. Air H. 1650°F. 1 hr. Water I. 1000°F. 4 hrs. Water	A. A-I Hollis (.08C, .336 Mn, .45Si, 18.95Cr, 10.27Mn, 1.03Mo) B. A-II All. (.08-.13C, 3.5-4.5Mn, .35-.70Si, 19.21Cr, 8.5-10.5 Ni) C. Armored Armoraro D. Ti O2 E. Titanium F. AC	A. 60°D B. 3/16" Cutting C. Flame Grinding	A. Copper B. None C. None	A. II 3/16" 1a 190 - 25 B. I 3/8" 2a 200 - 25 C. I 3/8" 2a 400 - 30 D. 80° - 180° E. 5 hrs.	1 1002 X	1 <sup>st</sup> Imp D 2 <sup>nd</sup> R U 3 <sup>rd</sup> R U 4 <sup>th</sup> Imp V 5 <sup>th</sup> V 6 <sup>th</sup> V 7 <sup>th</sup> V 8 <sup>th</sup> V 9 <sup>th</sup> V 10 <sup>th</sup> V 11 <sup>th</sup> V 12 <sup>th</sup> V 13 <sup>th</sup> V 14 <sup>th</sup> V 15 <sup>th</sup> V 16 <sup>th</sup> V 17 <sup>th</sup> V 18 <sup>th</sup> V 19 <sup>th</sup> V 20 <sup>th</sup> V 21 <sup>st</sup> V 22 <sup>nd</sup> V 23 <sup>rd</sup> V 24 <sup>th</sup> V 25 <sup>th</sup> V 26 <sup>th</sup> V 27 <sup>th</sup> V 28 <sup>th</sup> V 29 <sup>th</sup> V 30 <sup>th</sup> V 31 <sup>st</sup> V 32 <sup>nd</sup> V 33 <sup>rd</sup> V 34 <sup>th</sup> V 35 <sup>th</sup> V 36 <sup>th</sup> V 37 <sup>th</sup> V 38 <sup>th</sup> V 39 <sup>th</sup> V 40 <sup>th</sup> V 41 <sup>st</sup> V 42 <sup>nd</sup> V 43 <sup>rd</sup> V 44 <sup>th</sup> V 45 <sup>th</sup> V 46 <sup>th</sup> V 47 <sup>th</sup> V 48 <sup>th</sup> V 49 <sup>th</sup> V 50 <sup>th</sup> V 51 <sup>st</sup> V 52 <sup>nd</sup> V 53 <sup>rd</sup> V 54 <sup>th</sup> V 55 <sup>th</sup> V 56 <sup>th</sup> V 57 <sup>th</sup> V 58 <sup>th</sup> V 59 <sup>th</sup> V 60 <sup>th</sup> V 61 <sup>st</sup> V 62 <sup>nd</sup> V 63 <sup>rd</sup> V 64 <sup>th</sup> V 65 <sup>th</sup> V 66 <sup>th</sup> V 67 <sup>th</sup> V 68 <sup>th</sup> V 69 <sup>th</sup> V 70 <sup>th</sup> V 71 <sup>st</sup> V 72 <sup>nd</sup> V 73 <sup>rd</sup> V 74 <sup>th</sup> V 75 <sup>th</sup> V 76 <sup>th</sup> V 77 <sup>th</sup> V 78 <sup>th</sup> V 79 <sup>th</sup> V 80 <sup>th</sup> V 81 <sup>st</sup> V 82 <sup>nd</sup> V 83 <sup>rd</sup> V 84 <sup>th</sup> V 85 <sup>th</sup> V 86 <sup>th</sup> V 87 <sup>th</sup> V 88 <sup>th</sup> V 89 <sup>th</sup> V 90 <sup>th</sup> V 91 <sup>st</sup> V 92 <sup>nd</sup> V 93 <sup>rd</sup> V 94 <sup>th</sup> V 95 <sup>th</sup> V 96 <sup>th</sup> V 97 <sup>th</sup> V 98 <sup>th</sup> V 99 <sup>th</sup> V 100 <sup>th</sup> V	72 <sup>nd</sup> Failed radiograph 1 <sup>st</sup> Crack in left leg 1 <sup>st</sup> in crossbar
A. AD-255 B. 2/3/43 C. TH-75 D. Hughes Tool Company E. Lincoln Electric Co. F. Ternstedt Mfg. Div.	A. 1.015" B. C-I (.85Mn, .3981, .45Cr, 1.23Mn, .45Mo) C. .25 D. Face 363-363 E. Acid-Elec. F. 1900°F. 10 hrs. in furnace to 1650°F. 1 hr. Water G. 1200°F. 2 hrs. Air H. 1650°F. 1 hr. Water I. 1000°F. 4 hrs. Air	A. A-II L.E.A. (.08-.10C, 3.5-4.25 Mn, .45-.80 Si, 19.20-20 Ni) B. A-I R-A (.07-.15C, 3.5-4.5Mn, .75Si) C. Armored D. AC	A. 60°D B. 1/4" Cutting C. Flame Grinding D. Machining	A. Copper B. None C. None	A. II 1/4" 2a 275 - 28 B. I 5/16" 2a 390 - 30 C. I 5/16" 2a 390 - 30 D. 90° - 260° E. 5 hrs.	1 1000	2 <sup>nd</sup> L 3 <sup>rd</sup> L 4 <sup>th</sup> L 5 <sup>th</sup> L 6 <sup>th</sup> L 7 <sup>th</sup> L 8 <sup>th</sup> L 9 <sup>th</sup> L 10 <sup>th</sup> L 11 <sup>th</sup> L 12 <sup>th</sup> L 13 <sup>th</sup> L 14 <sup>th</sup> L 15 <sup>th</sup> L 16 <sup>th</sup> L 17 <sup>th</sup> L 18 <sup>th</sup> L 19 <sup>th</sup> L 20 <sup>th</sup> L 21 <sup>st</sup> L 22 <sup>nd</sup> L 23 <sup>rd</sup> L 24 <sup>th</sup> L 25 <sup>th</sup> L 26 <sup>th</sup> L 27 <sup>th</sup> L 28 <sup>th</sup> L 29 <sup>th</sup> L 30 <sup>th</sup> L 31 <sup>st</sup> L 32 <sup>nd</sup> L 33 <sup>rd</sup> L 34 <sup>th</sup> L 35 <sup>th</sup> L 36 <sup>th</sup> L 37 <sup>th</sup> L 38 <sup>th</sup> L 39 <sup>th</sup> L 40 <sup>th</sup> L 41 <sup>st</sup> L 42 <sup>nd</sup> L 43 <sup>rd</sup> L 44 <sup>th</sup> L 45 <sup>th</sup> L 46 <sup>th</sup> L 47 <sup>th</sup> L 48 <sup>th</sup> L 49 <sup>th</sup> L 50 <sup>th</sup> L 51 <sup>st</sup> L 52 <sup>nd</sup> L 53 <sup>rd</sup> L 54 <sup>th</sup> L 55 <sup>th</sup> L 56 <sup>th</sup> L 57 <sup>th</sup> L 58 <sup>th</sup> L 59 <sup>th</sup> L 60 <sup>th</sup> L 61 <sup>st</sup> L 62 <sup>nd</sup> L 63 <sup>rd</sup> L 64 <sup>th</sup> L 65 <sup>th</sup> L 66 <sup>th</sup> L 67 <sup>th</sup> L 68 <sup>th</sup> L 69 <sup>th</sup> L 70 <sup>th</sup> L 71 <sup>st</sup> L 72 <sup>nd</sup> L 73 <sup>rd</sup> L 74 <sup>th</sup> L 75 <sup>th</sup> L 76 <sup>th</sup> L 77 <sup>th</sup> L 78 <sup>th</sup> L 79 <sup>th</sup> L 80 <sup>th</sup> L 81 <sup>st</sup> L 82 <sup>nd</sup> L 83 <sup>rd</sup> L 84 <sup>th</sup> L 85 <sup>th</sup> L 86 <sup>th</sup> L 87 <sup>th</sup> L 88 <sup>th</sup> L 89 <sup>th</sup> L 90 <sup>th</sup> L 91 <sup>st</sup> L 92 <sup>nd</sup> L 93 <sup>rd</sup> L 94 <sup>th</sup> L 95 <sup>th</sup> L 96 <sup>th</sup> L 97 <sup>th</sup> L 98 <sup>th</sup> L 99 <sup>th</sup> L 100 <sup>th</sup> L	Passed radiograph Crater crack at left junction
A. AD-255 B. 2/3/43 C. TH-75 D. Hughes Tool Company E. Lincoln Electric Co. F. Ternstedt Mfg. Div.	A. 1.015" B. C-I (.85Mn, .3981, .45Cr, 1.23Mn, .45Mo) C. .25 D. Face 363-363 E. Acid-Elec. F. 1900°F. 10 hrs. in furnace to 1650°F. 1 hr. Water G. 1200°F. 2 hrs. Air H. 1650°F. 1 hr. Water I. 1000°F. 4 hrs. Air	A. A-II L.E.A. (.08-.10C, 3.5-4.25 Mn, .45-.80 Si, 19.20-20 Ni) B. A-I R-A (.07-.15C, 3.5-4.5Mn, .75Si) C. Armored D. AC	A. 60°D B. 1/4" Cutting C. Flame Grinding D. Machining	A. Copper B. None C. None	A. II 1/4" 2a 275 - 28 B. I 5/16" 2a 390 - 30 C. I 5/16" 2a 390 - 30 D. 90° - 260° E. 5 hrs.	1 1000	2 <sup>nd</sup> L 3 <sup>rd</sup> L 4 <sup>th</sup> L 5 <sup>th</sup> L 6 <sup>th</sup> L 7 <sup>th</sup> L 8 <sup>th</sup> L 9 <sup>th</sup> L 10 <sup>th</sup> L 11 <sup>th</sup> L 12 <sup>th</sup> L 13 <sup>th</sup> L 14 <sup>th</sup> L 15 <sup>th</sup> L 16 <sup>th</sup> L 17 <sup>th</sup> L 18 <sup>th</sup> L 19 <sup>th</sup> L 20 <sup>th</sup> L 21 <sup>st</sup> L 22 <sup>nd</sup> L 23 <sup>rd</sup> L 24 <sup>th</sup> L 25 <sup>th</sup> L 26 <sup>th</sup> L 27 <sup>th</sup> L 28 <sup>th</sup> L 29 <sup>th</sup> L 30 <sup>th</sup> L 31 <sup>st</sup> L 32 <sup>nd</sup> L 33 <sup>rd</sup> L 34 <sup>th</sup> L 35 <sup>th</sup> L 36 <sup>th</sup> L 37 <sup>th</sup> L 38 <sup>th</sup> L 39 <sup>th</sup> L 40 <sup>th</sup> L 41 <sup>st</sup> L 42 <sup>nd</sup> L 43 <sup>rd</sup> L 44 <sup>th</sup> L 45 <sup>th</sup> L 46 <sup>th</sup> L 47 <sup>th</sup> L 48 <sup>th</sup> L 49 <sup>th</sup> L 50 <sup>th</sup> L 51 <sup>st</sup> L 52 <sup>nd</sup> L 53 <sup>rd</sup> L 54 <sup>th</sup> L 55 <sup>th</sup> L 56 <sup>th</sup> L 57 <sup>th</sup> L 58 <sup>th</sup> L 59 <sup>th</sup> L 60 <sup>th</sup> L 61 <sup>st</sup> L 62 <sup>nd</sup> L 63 <sup>rd</sup> L 64 <sup>th</sup> L 65 <sup>th</sup> L 66 <sup>th</sup> L 67 <sup>th</sup> L 68 <sup>th</sup> L 69 <sup>th</sup> L 70 <sup>th</sup> L 71 <sup>st</sup> L 72 <sup>nd</sup> L 73 <sup>rd</sup> L 74 <sup>th</sup> L 75 <sup>th</sup> L 76 <sup>th</sup> L 77 <sup>th</sup> L 78 <sup>th</sup> L 79 <sup>th</sup> L 80 <sup>th</sup> L 81 <sup>st</sup> L 82 <sup>nd</sup> L 83 <sup>rd</sup> L 84 <sup>th</sup> L 85 <sup>th</sup> L 86 <sup>th</sup> L 87 <sup>th</sup> L 88 <sup>th</sup> L 89 <sup>th</sup> L 90 <sup>th</sup> L 91 <sup>st</sup> L 92 <sup>nd</sup> L 93 <sup>rd</sup> L 94 <sup>th</sup> L 95 <sup>th</sup> L 96 <sup>th</sup> L 97 <sup>th</sup> L 98 <sup>th</sup> L 99 <sup>th</sup> L 100 <sup>th</sup> L	Passed radiograph Crater crack at left junction
A. AD-255 B. 2/3/43 C. TH-75 D. Hughes Tool Company E. Lincoln Electric Co. F. Ternstedt Mfg. Div.	A. 1.015" B. C-I (.85Mn, .3981, .45Cr, 1.23Mn, .45Mo) C. .25 D. Face 363-363 E. Acid-Elec. F. 1900°F. 10 hrs. in furnace to 1650°F. 1 hr. Water G. 1200°F. 2 hrs. Air H. 1650°F. 1 hr. Water I. 1000°F. 4 hrs. Air	A. A-II L.E.A. (.08-.10C, 3.5-4.25 Mn, .45-.80 Si, 19.20-20 Ni) B. A-I R-A (.07-.15C, 3.5-4.5Mn, .75Si) C. Armored D. AC	A. 60°D B. 1/4" Cutting C. Flame Grinding D. Machining	A. Copper B. None C. None	A. II 1/4" 2a 275 - 28 B. I 5/16" 2a 390 - 30 C. I 5/16" 2a 390 - 30 D. 90° - 260° E. 5 hrs.	1 1000	2 <sup>nd</sup> L 3 <sup>rd</sup> L 4 <sup>th</sup> L 5 <sup>th</sup> L 6 <sup>th</sup> L 7 <sup>th</sup> L 8 <sup>th</sup> L 9 <sup>th</sup> L 10 <sup>th</sup> L 11 <sup>th</sup> L 12 <sup>th</sup> L 13 <sup>th</sup> L 14 <sup>th</sup> L 15 <sup>th</sup> L 16 <sup>th</sup> L 17 <sup>th</sup> L 18 <sup>th</sup> L 19 <sup>th</sup> L 20 <sup>th</sup> L 21 <sup>st</sup> L 22 <sup>nd</sup> L 23 <sup>rd</sup> L 24 <sup>th</sup> L 25 <sup>th</sup> L 26 <sup>th</sup> L 27 <sup>th</sup> L 28 <sup>th</sup> L 29 <sup>th</sup> L 30 <sup>th</sup> L 31 <sup>st</sup> L 32 <sup>nd</sup> L 33 <sup>rd</sup> L 34 <sup>th</sup> L 35 <sup>th</sup> L 36 <sup>th</sup> L 37 <sup>th</sup> L 38 <sup>th</sup> L 39 <sup>th</sup> L 40 <sup>th</sup> L 41 <sup>st</sup> L 42 <sup>nd</sup> L 43 <sup>rd</sup> L 44 <sup>th</sup> L 45 <sup>th</sup> L 46 <sup>th</sup> L 47 <sup>th</sup> L 48 <sup>th</sup> L 49 <sup>th</sup> L 50 <sup>th</sup> L 51 <sup>st</sup> L 52 <sup>nd</sup> L 53 <sup>rd</sup> L 54 <sup>th</sup> L 55 <sup>th</sup> L 56 <sup>th</sup> L 57 <sup>th</sup> L 58 <sup>th</sup> L 59 <sup>th</sup> L 60 <sup>th</sup> L 61 <sup>st</sup> L 62 <sup>nd</sup> L 63 <sup>rd</sup> L 64 <sup>th</sup> L 65 <sup>th</sup> L 66 <sup>th</sup> L 67 <sup>th</sup> L 68 <sup>th</sup> L 69 <sup>th</sup> L 70 <sup>th</sup> L 71 <sup>st</sup> L 72 <sup>nd</sup> L 73 <sup>rd</sup> L 74 <sup>th</sup> L 75 <sup>th</sup> L 76 <sup>th</sup> L 77 <sup>th</sup> L 78 <sup>th</sup> L 79 <sup>th</sup> L 80 <sup>th</sup> L 81 <sup>st</sup> L 82 <sup>nd</sup> L 83 <sup>rd</sup> L 84 <sup>th</sup> L 85 <sup>th</sup> L 86 <sup>th</sup> L 87 <sup>th</sup> L 88 <sup>th</sup> L 89 <sup>th</sup> L 90 <sup>th</sup> L 91 <sup>st</sup> L 92 <sup>nd</sup> L 93 <sup>rd</sup> L 94 <sup>th</sup> L 95 <sup>th</sup> L 96 <sup>th</sup> L 97 <sup>th</sup> L 98 <sup>th</sup> L 99 <sup>th</sup> L 100 <sup>th</sup> L	Passed radiograph Crater crack at left junction
A. AD-255 B. 2/3/43 C. TH-75 D. Hughes Tool Company E. Lincoln Electric Co. F. Ternstedt Mfg. Div.	A. 1.015" B. C-I (.85Mn, .3981, .45Cr, 1.23Mn, .45Mo) C. .25 D. Face 363-363 E. Acid-Elec. F. 1900°F. 10 hrs. in furnace to 1650°F. 1 hr. Water G. 1200°F. 2 hrs. Air H. 1650°F. 1 hr. Water I. 1000°F. 4 hrs. Air	A. A-II L.E.A. (.08-.10C, 3.5-4.25 Mn, .45-.80 Si, 19.20-20 Ni) B. A-I R-A (.07-.15C, 3.5-4.5Mn, .75Si) C. Armored D. AC	A. 60°D B. 1/4" Cutting C. Flame Grinding D. Machining	A. Copper B. None C. None	A. II 1/4" 2a 275 - 28 B. I 5/16" 2a 390 - 30 C. I 5/16" 2a 390 - 30 D. 90° - 260° E. 5 hrs.	1 1000	2 <sup>nd</sup> L 3 <sup>rd</sup> L 4 <sup>th</sup> L 5 <sup>th</sup> L 6 <sup>th</sup> L 7 <sup>th</sup> L 8 <sup>th</sup> L 9 <sup>th</sup> L 10 <sup>th</sup> L 11 <sup>th</sup> L 12 <sup>th</sup> L 13 <sup>th</sup> L 14 <sup>th</sup> L 15 <sup>th</sup> L 16 <sup>th</sup> L 17 <sup>th</sup> L 18 <sup>th</sup> L 19 <sup>th</sup> L 20 <sup>th</sup> L 21 <sup>st</sup> L 22 <sup>nd</sup> L 23 <sup>rd</sup> L 24 <sup>th</sup> L 25 <sup>th</sup> L 26 <sup>th</sup> L 27 <sup>th</sup> L 28 <sup>th</sup> L 29 <sup>th</sup> L 30 <sup>th</sup> L 31 <sup>st</sup> L 32 <sup>nd</sup> L 33 <sup>rd</sup> L 34 <sup>th</sup> L 35 <sup>th</sup> L 36 <sup>th</sup> L 37 <sup>th</sup> L 38 <sup>th</sup> L 39 <sup>th</sup> L 40 <sup>th</sup> L 41 <sup>st</sup> L 42 <sup>nd</sup> L 43 <sup>rd</sup> L 44 <sup>th</sup> L 45 <sup>th</sup> L 46 <sup>th</sup> L 47 <sup>th</sup> L 48 <sup>th</sup> L 49 <sup>th</sup> L 50 <sup>th</sup> L 51 <sup>st</sup> L 52 <sup>nd</sup> L 53 <sup>rd</sup> L 54 <sup>th</sup> L 55 <sup>th</sup> L 56 <sup>th</sup> L 57 <sup>th</sup> L 58 <sup>th</sup> L 59 <sup>th</sup> L 60 <sup>th</sup> L 61 <sup>st</sup> L 62 <sup>nd</sup> L 63 <sup>rd</sup> L 64 <sup>th</sup> L 65 <sup>th</sup> L 66 <sup>th</sup> L 67 <sup>th</sup> L 68 <sup>th</sup> L 69 <sup>th</sup> L 70 <sup>th</sup> L 71 <sup>st</sup> L 72 <sup>nd</sup> L 73 <sup>rd</sup> L 74 <sup>th</sup> L 75 <sup>th</sup> L 76 <sup>th</sup> L 77 <sup>th</sup> L 78 <sup>th</sup> L 79 <sup>th</sup> L 80 <sup>th</sup> L 81 <sup>st</sup> L 82 <sup>nd</sup> L 83 <sup>rd</sup> L 84 <sup>th</sup> L 85 <sup>th</sup> L 86 <sup>th</sup> L 87 <sup>th</sup> L 88 <sup>th</sup> L 89 <sup>th</sup> L 90 <sup>th</sup> L 91 <sup>st</sup> L 92 <sup>nd</sup> L 93 <sup>rd</sup> L 94 <sup>th</sup> L 95 <sup>th</sup> L 96 <sup>th</sup> L 97 <sup>th</sup> L 98 <sup>th</sup> L 99 <sup>th</sup> L 100 <sup>th</sup> L	Passed radiograph Crater crack at left junction





GENERAL INFORMATION	ANODE METAL	CATHODE METAL	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	
A. DATE OF TEST	B. TYPE OF TEST	C. DATE OF TEST	D. DATE OF TEST	E. DATE OF TEST	F. DATE OF TEST	G. DATE OF TEST	H. DATE OF TEST	I. DATE OF TEST	J. DATE OF TEST	K. DATE OF TEST	L. DATE OF TEST	M. DATE OF TEST	N. DATE OF TEST	O. DATE OF TEST	P. DATE OF TEST	Q. DATE OF TEST	R. DATE OF TEST	S. DATE OF TEST	T. DATE OF TEST	U. DATE OF TEST	
A. AD-103 B. 10/23/42 C. 246 D. Republic Steel Heat treated by - American Car & Foundry Co. E. Alloy Rods Co. F. American Loco-Fotive Co.	A. 3/4" B. R-V (.48-.54Mn, .17S, .33-.34Cr, 4.99-5.0Mn, .35-.36Mo, .23-.25C) C. .35-.36Mo D. Face 268 E. Back 272 F. ---	A. A-III (.10C, .50Mn, 5081, 20,00Cr, 9.5Mn, 2.50Mo) A-II (.10C, 4.0Mn, 5081, 20,00Cr, 9.5Mn) B. Armox C. Titanium D. DC REV	A. DV B. 3/16" C. Flame Cutting Grinding Buttering	A. Not given B. I C. I D. I E. I F. I G. I H. I I. I J. I K. I L. I M. I N. I O. I P. I Q. I R. I S. I T. I U. I	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None	A. None B. None

weld Metal







A. FIRM B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. ORDER DATE F. ORDER QUANTITY	A. PLATE THICKNESS B. TYPE C. GRADE D. SIZE E. PROCESS F. HEAT TREATMENT	A. TYPE B. TRADE NAME C. CHEMISTRY D. COMPOSITION E. POLARITY	A. COATING B. ANGLE C. PLATE PREPARATION	A. MOTION B. SPEED C. PRESSURE D. TEMPERATURE	A. MOUNTING B. POSITION	H. VOL. / P.P.	C. CRACKING			D. DEFECTS		
							L. L. L. L. L. L.	M. M. M. M. M. M.	N. N. N. N. N. N.			
A. AD-227 B. 11/19/42 C. XV-151-F D. E.C. Atkins Co E. Alloy Rods Co F. Chevrolet Motor Co.	A. 3/4" B. R-IV C. .94Mn, .61Si, .70Cr, .22Mo, .09Zr D. Face 360 E. Back 360 F. B.O.H. G. 1610°F. 1 hr. Water H. 1030°F. 2 hrs. Air	A. A-I (.10C, 1.25 Mn, .36Si, 17.6Cr, 8.9Mn, 2.43) A-II (.12C, 3.58 Mn, .26Si, 18.6Cr, 9.8Mn) B. Armorarc C. T102 D. DC REV	A. 60°DV B. 3/16" C. Grinding	A. Not given B. 1. I 5/32" 1a 140 - 25 2. 1/4" 5/32" 1a 140 - 25 3. Three layers 5/32" 1a 140 - 25 C. 6 hrs. Peening - first and third passes.	A. None B. None	1 779 2 741 3 835	L L L	1 1/2" 1 1/2" 1 1/2"	4 1/2" D 1 1/2" D 4 1/2" U	II III 10"	II III 10"	Failed radiograph Several weld cracks along crossbar
A. AD-227 B. 11/19/42 C. XV-152-F D. E.C. Atkins Co E. Alloy Rods Co F. Chevrolet Motor Co.	A. 3/4" B. R-IV C. .77Mn, .57Si, .61Cr, .20Mo, .08Zr D. Face 364 E. Back 364 F. B.O.H. G. 1625°F. 1 hr. Water H. 940°F. 70 mins. Air	A. A-I (.10C, 1.25 Mn, .36Si, 17.6Cr, 8.9Mn, 2.43Mo) A-II (.12C, 3.58 Mn, .26Si, 18.6Cr, 9.8Mn) B. Armorarc C. T102 D. DC REV	A. 60°DV B. 3/16" C. Grinding	A. Not given B. 1. I 5/32" 1a 140 - 25 2. 1/4" 5/32" 1a 140 - 25 3. Three layers 5/32" 1a 140 - 25 C. 10 hrs. Peening - first and third passes.	A. None B. None	1 836 2 802 3 832	R L L	5 1/2" 5 1/2" 5 1/2"	1 1/2" D 1 1/2" U 1 1/2" R U	II III V	II III V	Failed radiograph General condition of incomplete weld fusion, also some scattered slag in- clusions

Weld Metal



IDENTIFICATION	ANNEAL MEDIA	MATERIALS DATA	HEAT TREATMENT	CHEMICAL ANALYSIS	MACHINING	WELDING	PROCESSING	HEAT TREATMENT	WELT	M	VEL. F/S	BALLISTIC RESULTS		REMARKS ON DRAWING
												LOCATION OF H	CRACKING	
A. PART NUMBER	A. PLATE THICKNESS	A. TYPE	A. TYPE	A. GROOVE, INCLUDING ANGLE, ROOT FACE	A. BACKING	A. BACKING	A. DEPOSITION	A. NONE	A. NONE	1		L	L	REMARKS ON DRAWING
B. SIZE OF TEST	B. TENSILE STRENGTH	B. TENSILE STRENGTH	B. TENSILE STRENGTH	B. ROOT GAP	B. 3/16"	B. 3/16"	B. DEPOSITION	B. NONE	B. NONE	2		L	L	REMARKS ON DRAWING
C. PLATE PA.	C. GROSS WEIGHT	C. COATING	C. COATING	C. PLATE PREPARATION	C. Machining	C. Machining	C. III	C. NONE	C. NONE	3		L	L	REMARKS ON DRAWING
D. ALUMINUM	D. SIZE	D. SIZE	D. SIZE	D. SIZE	D. Machining	D. Machining	D. III	D. NONE	D. NONE	4		L	L	REMARKS ON DRAWING
E. SURFACE	E. SURFACE	E. SURFACE	E. SURFACE	E. SURFACE	E. Machining	E. Machining	E. III	E. NONE	E. NONE	5		L	L	REMARKS ON DRAWING
F. SURFACE	F. SURFACE	F. SURFACE	F. SURFACE	F. SURFACE	F. Machining	F. Machining	F. III	F. NONE	F. NONE	6		L	L	REMARKS ON DRAWING
A. AD-46 B. 10/1/42 C. XW-120-F D. Chevrolet E. Crucible Steel F. Chevrolet Motor Co.	A. 3/4" B. R-IV (.90Mn, .75Si, .51Cr, .19Mo) C. 30 D. Face 331 Back 321 E. B.O.H. F. 1600F. 1-2/3 hrs. Water 930F. 6 hrs. Air	A. A-I (.14C, 3.58 Mn, .31Si, 19.7Cr, 10.4Ni, 1.17Mo) (.10C, 3.56 Mn, .33Si, 20.2Cr, 10.4Ni, 1.10Mo) B. Armoxize "A" C. T102 D. DC REV	A. 480DV B. 3/32" RF C. Machining	A. Not given B. I 5/32" 1a 140 - 25 2. I 3/16" 2a 175 - 26 3. III 3/16" 3b 175 - 26 5/32" 2b 140 - 25 C. 11 hrs. 80° - 180°F. D. Peening - first, second and fifth passes.	3" 1/2" U 6" 5/8" D 13" D 2 1/2" U 7 1/2" U	3" 1/2" U 6" 5/8" D 13" D 2 1/2" U 7 1/2" U	Passed radiograph Some scattered areas of incomplete fusion							
A. AD-132 B. 12/2/42 C. XW-165-F D. Great Lakes E. Harnischfeger F. Chevrolet Motor Co.	A. 3/4" B. R-IV (.90Mn, .75Si, .68Cr, .21Mo) C. 32 D. Face 341 Back 341 E. B.O.H. F. 1600F. 52 mins. Water 1000F. 4 hrs. Air	A. A-I (.15C, 4.47 Mn, .65Si, 19.52Cr, 9.5Ni, 1.07Mo) A-II (.13C, 4.20 Mn, .47Si, 19.0Cr, 10.7Ni) B. AW-3-C C. Lime D. DC REV	A. 600DV B. 3/32" RF C. Grinding	A. Not given B. I 5/32" 1a 140 - 25 2.4 Three layers 1/4" 2a 250 - 28 5/32" 1a 140 - 25 C. 9 hrs. 90° - 120°F. D. Peening - first and third passes.	2 1/2" 6" 7" L 6 1/2" L 3" R 6 1/2" L 8 1/2" L 1 1/2" L 1 1/2" L	2 1/2" 6" 7" L 6 1/2" L 3" R 6 1/2" L 8 1/2" L 1 1/2" L 1 1/2" L	Passed radiograph							



IDENTIFICATION		ANNEALING DATA		PLATE DATA		TREATMENT DATA		WELDER DATA		PRESSURE		WELD		WELDING		REMARKS ON CRACKS	
A. PART NUMBER OR DATE OF TEST	B. PLATE NO.	C. ANNEALING DATA	D. ANNEALING DATA	E. CRACKING DATA	F. CRACKING DATA	G. CRACKING DATA	H. CRACKING DATA	I. CRACKING DATA	J. CRACKING DATA	K. CRACKING DATA	L. CRACKING DATA	M. CRACKING DATA	N. CRACKING DATA	O. CRACKING DATA	P. CRACKING DATA	Q. CRACKING DATA	R. CRACKING DATA
A. AD-228 B. 11/11/42 C. W-32 D. Ford Motor Co. E. Crucible Steel Corp. F. Ford Motor Co.	A. 3/4" B. R-II C. 1.38Mn, .25Si, .55Cr, .47Mo D. --- E. B.O.H. F. 1650°F. 4 hrs. Platen 1000°F. 6 hrs. Air	A. A-I (.07C, 1.40 Mn, .27Si, 18.00Cr, 10.2Mn, 2.0Mo) B. Armorize C. Titanium D. DC REV	A. 45°SV B. 1/8" C. Flame Cutting Grinding	A. Copper B. I 1/8" C. I 5/32" D. I 3/16" E. I 1/4" F. I 3/16" G. 6 hrs. Grinding of oraters after first pass.	la 95 - 22 la 130 - 22 la 175 - 22 la 180 - 24 la 210 - 26 la 210 - 26 la 188 180 - 22 1000° - 1700°	1 826 A. None B. None	1 826 I Imp II D III V IV V	7" 5" 2 1/2" 7" 9"	Passed radiograph Sector displaced								
A. AD-166 B. 11/25/42 C. W-72 D. Ford Motor Co. E. Crucible Steel Corp. F. Ford Motor Co.	A. 3/4" B. R-II C. 1.43Mn, .29Si, .56Cr, .10Ni, .44V D. --- E. B.O.H. F. 1650°F. 2 hrs. Platen 1000°F. 4 hrs. Air	A. A-I (.07C, 1.82 Mn, .30Si, 2.00Mo) B. Armorize C. Titanium D. DC REV	A. 45°SV B. 3/16" C. Grinding	A. Copper B. I 5/32" C. III 3/16" D. I 1/4" E. I 1/4" F. 3/16" G. 5-3/4 hrs. Grinding of oraters after first pass.	la 145 - 22 la 190 - 22 2b 155 - 22 la 250 - 22 la 250 - 22 188 200 - 22 142° - 253°	1 779 A. None B. None	1 779 I D II D III Imp IV U V U VI U VII U VIII U IX U X U XI U XII U XIII U XIV U XV U XVI U XVII U XVIII U XIX U XX U XXI U XXII U XXIII U XXIV U XXV U XXVI U XXVII U XXVIII U XXIX U XXX U	7" 5" 2 1/2" 7" 9"	Passed radiograph								
A. AD-264 B. 2/17/43 C. W-3 D. Ford Motor Co. E. Crucible Steel Corp. F. Ford Motor Co.	A. 3/4" B. R-II C. 1.49Mn, .30Si, .72Cr, .07Ni, .42Mo D. --- E. Back 331 F. 1650°F. 3-1/2 hrs. Spray 1030°F. 4-1/2 hrs. Air	A. A --- B. Armorize C. --- D. DC REV	A. 45°SV B. 1/4" C. Flame Cutting Grinding	A. Copper B. I 3/16" C. II 1/4" D. 3/16" E. 5 hrs. F. Two more passes in cross-bar.	la 205 - 24 3a 320 - 25 2b 220 - 24 188 220 - 24 70° - 240°	1 805 A. None B. None	1 805 I D II D III U IV U V U VI U VII U VIII U IX U X U XI U XII U XIII U XIV U XV U XVI U XVII U XVIII U XIX U XX U XXI U XXII U XXIII U XXIV U XXV U XXVI U XXVII U XXVIII U XXIX U XXX U	5" 4 1/2" 2 1/2" 3 1/2" 3 1/2"	Passed radiograph Small crack in crossbar								

AS SHOWN ON DRAWING OR PHOTOGRAPH	A. NAME OF MANUFACTURER	B. SIZE	C. QUANTITY	D. DATE	E. GRADE	F. WEIGHT	G. PART NUMBER	H. PART NUMBER	I. PART NUMBER	J. PART NUMBER	K. ANALYSIS		L. COMMENTS	M. REMARKS	
											1. PERCENT	2. PERCENT			
A. AD-204 B. 1/20/43 C. 1 D. Carnegie Illinois Steel Corp. E. HOLLUP CORP. F. Standard Rollway Equip. Mfg. Co.	A. 3/4" B. R-1 (1.06Mn., 1.95Si, .42Cr, .95Mn, .42Mo) C. Face 332 Back 332 E. Acid-Elec. F. ---	A. A-1 (.079C, 3.41B, 5/32 Mn., .33Si, 17.7Cr, 12.6Ni, 1.64Mo) B. Airarod C. Mineral D. DC MEV	A. 45097 B. 5/32" C. Flame Cutting Grinding	A. Not Given B. II 5/32" 2a 150 - 26 2. I 5/32" 2a 150 - 26 3. I 5/32" 2a 150 - 26 C. 8 hrs. --- D. One more pass in right leg and crossbar. Grinding after first and third passes.	A. 7097 B. None	2 802	2 802	2 802	2 802	2 802	2 802	2 802	2 802	2 802	2 802
A. AD-206 B. 3/5/43 C. 2 D. Carnegie Illinois Steel Corp. E. HOLLUP CORP. F. Standard Rollway Equip. Mfg. Co.	A. 3/4" B. R-1 (1.06Mn., 1.95Si, .42Cr, .95Mn, .42Mo) C. Face 332 Back 332 E. Acid-Elec. F. ---	A. A-1 (.079C, 3.41B, 5/32 Mn., .33Si, 17.7Cr, 12.6Ni, 1.64Mo) B. Airarod C. Mineral D. DC MEV	A. 60797 B. 3/16" C. Flame Cutting Grinding	A. Not Given B. II 5/32" 2a 150 - 23 2. I 5/32" 2a 150 - 23 3. II 5/32" 4B 150 - 23 C. 10 hrs. --- D. Grinding after first pass.	A. 7097 B. None	2 713	2 713	2 713	2 713	2 713	2 713	2 713	2 713	2 713	2 713

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ATI- 38765

TITLE: Welding of Armor

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## ABSTRACT:

Tests were conducted to obtain firing record data for subject plates and to present a comparison of ballistic shock performance of plates made with various materials and welding procedures. After a series of tests and investigations the following data were derived: steel cleanliness and directional properties affect the amount of weld cracking during ballistic shock testing of H plates assembled from one-inch rolled homogeneous armor. There is little difference in ballistic shock test results of plates welded with the manganese and with the molybdenum modified type of austenitic electrodes. Plates welded with a narrow included angle, a small number of passes, or straight weave technique are indicated to be slightly inferior in resistance to weld metal cracking during ballistic test. Five Unionmelt plates, included in the rolled 1-inch armor group, showed shock test results slightly inferior to the average for hand-welded plates.

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