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DATA PROCESSING SHEET

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## REPORT DOC

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| 4. TITLE (and Subtitle)<br>Compendium of Shock Wave Data. Section C. Organic Compounds Excluding Hydrocarbons. Section D. Mixtures. Section E. Mixtures and Solutions Without Chemical Characterization. Compendium Index.                                                                                                                                                                          |  | 5. TYPE OF REPORT & PERIOD COVERED                          |                               |
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| 7. AUTHOR(s)<br>M. van Thiel<br>J. Shaner<br>E. Salinas (editors)                                                                                                                                                                                                                                                                                                                                   |  | 8. CONTRACT OR GRANT NUMBER(s)<br>W-7405-ENG-48             |                               |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS<br>Lawrence Livermore Laboratory<br>P.O. Box 808<br>Livermore, CA 94550                                                                                                                                                                                                                                                                                 |  | 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS |                               |
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| 16. DISTRIBUTION STATEMENT (of this Report)<br>Distribution limited to U. S. Government Agencies only. All other requests, both foreign and domestic, must be referred to [REDACTED] Lawrence Livermore Laboratory, P.O. Box 808, Livermore, CA 94550. <b>THE 22 OCT 1979</b>                                                                                                                       |  |                                                             |                               |
| 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)                                                                                                                                                                                                                                                                                                          |  |                                                             |                               |
| 18. SUPPLEMENTARY NOTES                                                                                                                                                                                                                                                                                                                                                                             |  |                                                             |                               |
| 19. KEY WORDS (Continue on reverse side if necessary and identify by block number)<br>shock waves                      organic compounds<br>handbook                        thermodynamic properties<br>alloys                            very high pressures<br>equations of state            mixtures                                                                                             |  |                                                             |                               |
| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)<br>This volume consists of 4 parts including the index for the three volume compendium. Section C lists shock wave data for organic compounds. Section D contains shock wave data for mixtures of organic and inorganic data. Section E lists data for incompletely defined engineering and geological materials. |  |                                                             |                               |



**LAWRENCE LIVERMORE LABORATORY**

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UCLR-50108 Vol. 3

## **COMPENDIUM OF SHOCK WAVE DATA**

Section C - Organic Compounds  
Excluding Hydrocarbons  
Section D - Mixtures  
Section E - Mixtures and Solutions  
Without Chemical  
Characterization  
Compendium Index

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MS. date: June 1977

79 10 19 094



# COMPENDIUM OF SHOCK WAVE DATA

SECTIONS C-E

M. van Thiel

June 1977

## Notice

The completeness of this compilation depends upon its users. To assure its continued usefulness, users are urged to send any missing or new shock wave data and corrections to the Editor, M. van Thiel, Lawrence Livermore Laboratory, P.O. Box 808, Livermore, California, U.S.A., 94550.

New and revised pages will be distributed as necessary.



SECTION C  
-----

ORGANIC COMPOUNDS EXCLUDING HYDROCARBONS

23-2-1(1-4-1)---1  
METHANOL

$\text{H}_3\text{-C-O-H} = \text{C-H}_4\text{-O}$

$T_0 = 15\text{-}24$  DEG. CENTIGRADE  
 $V_0 = 1.255\text{-}1.271$  CC/G.

$C_0 = 1.125$  KM/SEC.  
AT 20 DEG CENTIGRADE

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| $T_0$ | $\rho_{H_2O}$ | $U_S$ | $U_P$ | $P$   | $V/V_0$ |
|-------|---------------|-------|-------|-------|---------|
| 24    | 0.7868        | 5.51  | 2.525 | 109.5 | 0.542   |
| 15    | 0.7968        | 3.95  | 1.483 | 46.6  | 0.625   |

$U_S = 1.73 + 1.50 \cdot U_P$  KM/SEC

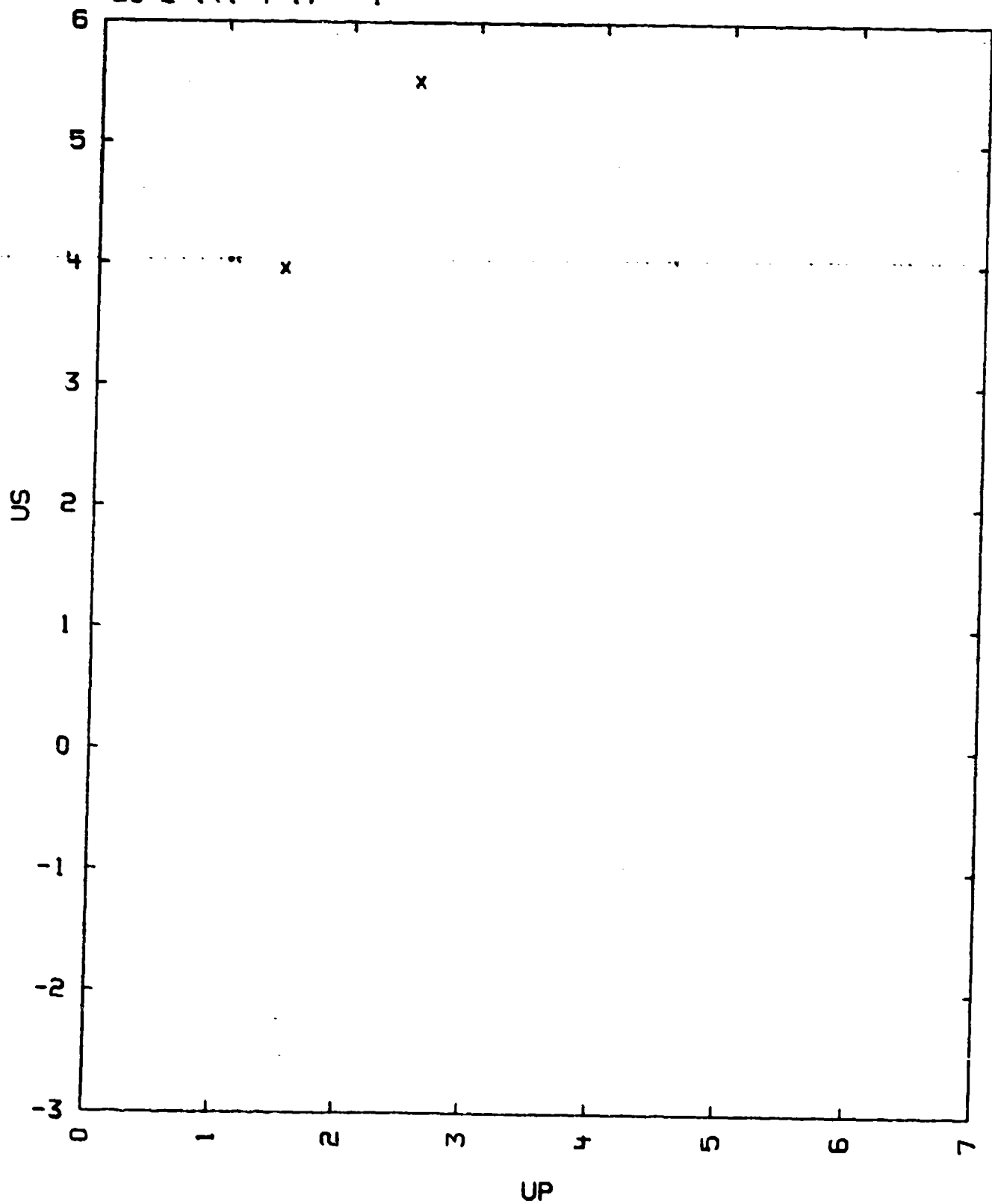
## COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 24ST ALUMINUM
- 3)  $C_0$  WAS OBTAINED FROM: BERGMANN, DER ULTRASCHALL (S. HIRZEL VERLAG  
STUTTGART, GERMANY, 1954).
- 4) ALSO FROM BERGMANN THE TEMPERATURE DERIVATIVE  $DC/DT = 0.0033$  KM/SEC  
( $DC/DT$ ) =  $-0.0033$  KM/(SEC\*DEG)

TABLE 1

METHANOL

23-2-1(1-4-1)---1



23-2-1(2-8-1)---1

ETHYL ALCOHOL

 $\text{H}_3\text{-C-C(H}_2\text{)-O-H} = \text{C}_2\text{-H}_5\text{-O}$ 

T0 = 21-26 DEG. CENTIGRADE

V0 = 1.267-1.275 CC/G

C0 = 1.141-1.162 KM/SEC.

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| T0 | RH00   | US   | UP    | P     | V/V0  |
|----|--------|------|-------|-------|-------|
| 26 | 0.7843 | 5.63 | 2.500 | 110.4 | 0.556 |
| 21 | 0.7893 | 4.03 | 1.487 | 47.3  | 0.631 |

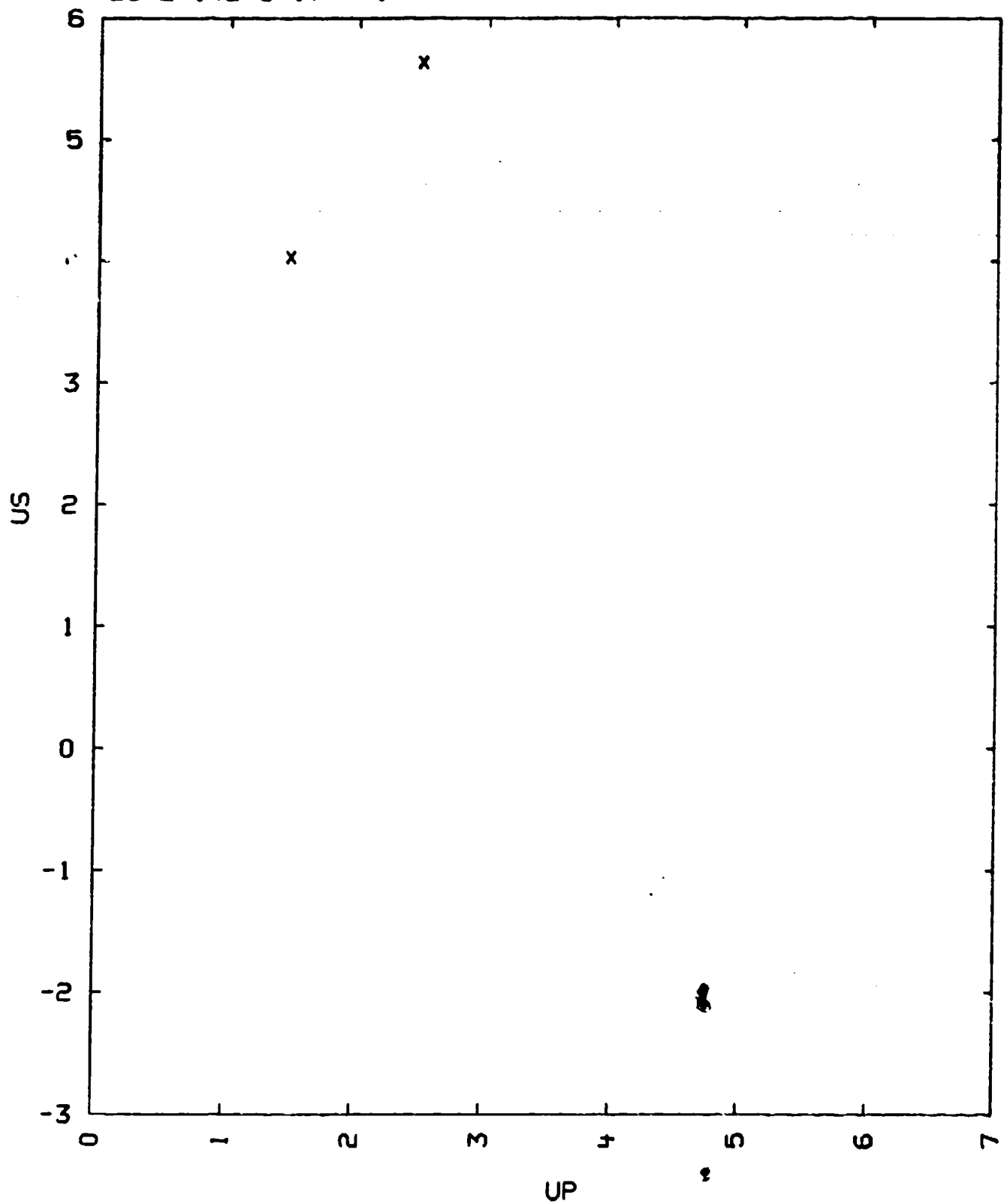
US = 1.68 + 1.58\*UP KM/SEC

## COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE VALUES FOR C0 WERE DETERMINED BY INTERPOLATING THE DATA POINTS OBTAINED FROM THE AMERICAN INSTITUTE OF PHYSICS HANDBOOK, (MCGRAW-HILL BOOK CO., N. Y. 1963) 2ND ED.

TABLE 1

ETHYL ALCOHOL  
23-2-1(2-6-1)---1





23-2-112-6-1)---2  
ETHANOL

C(H3)-C(H2)-O-H

T0 =25-30  
V01=1.2738-1.2808 G/CC

CO(T=20 DEG.C.)=1.162 KM/SEC

THE TABLE LISTS T IN DEG. C., RH00 IN G/CC, VELOCITIES IN KM/SEC AND  
PRESSURE IN KBAR. RI IS REFRACTIVE INDEX. AL IS 2024 AL, BR: 346 BRASS

TABLE

| - - - - - SAMPLE - - - - - |        |      |       |       |        |       | -DRIVER- |     |
|----------------------------|--------|------|-------|-------|--------|-------|----------|-----|
| T0                         | RH00   | US   | UP    | P     | V/V0   | RI    | UFS      | MAT |
| 30.                        | 0.7807 | 3.74 | 1.32  | 35.8  | 0.6471 | 1.564 | 1.55     | AL  |
| 28.                        | 0.7825 | 4.13 | 1.485 | 48.0  | 0.6404 | 1.562 | 1.77     | AL  |
| 25.                        | 0.7851 | 6.04 | 2.84  | 134.7 | 0.5298 | 1.688 | 3.23     | BR  |
| 20.                        | 0.7894 |      |       | 0.0   | 1.00   | 1.362 |          |     |

US =

COMMENTS:

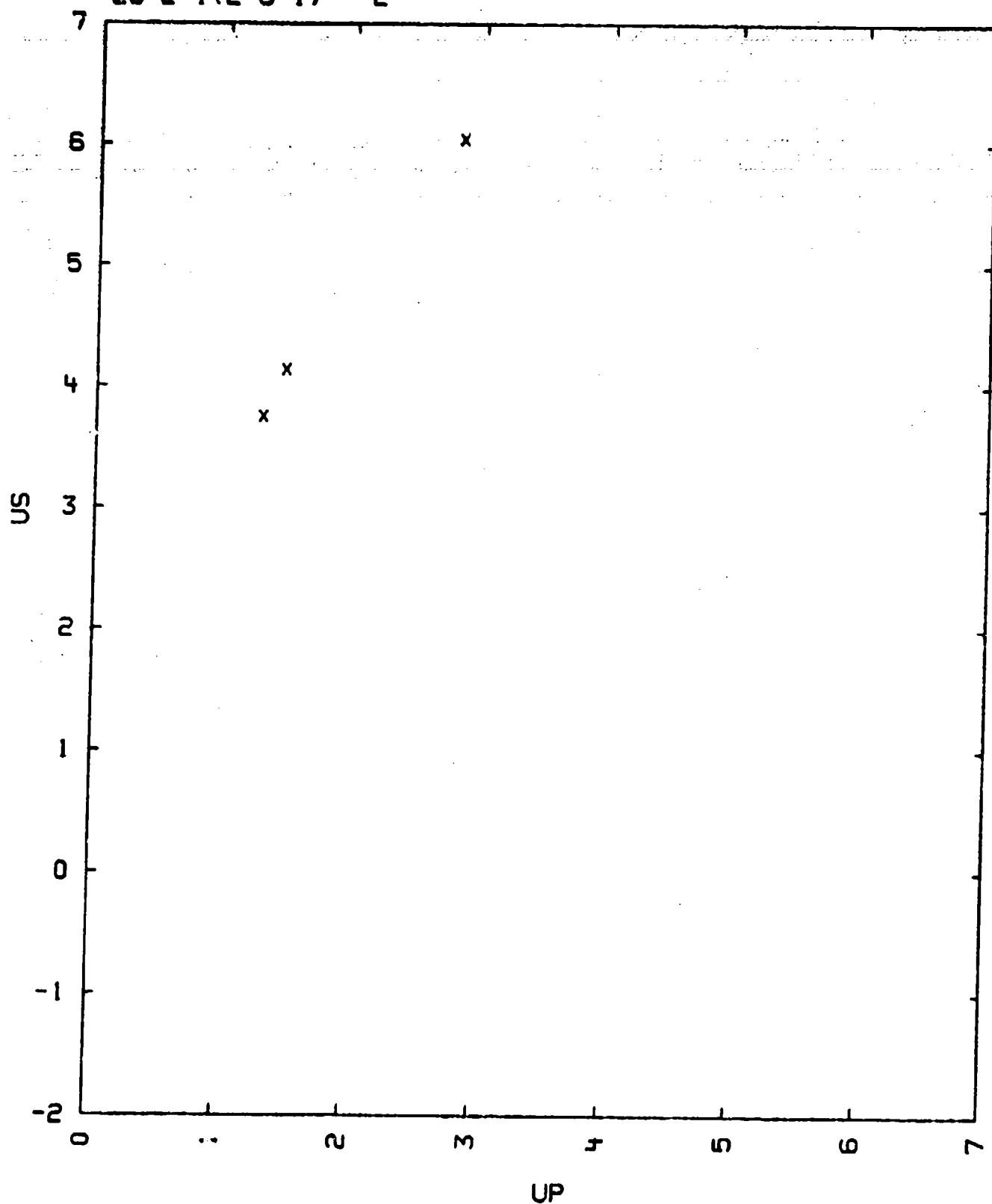
- 1) SOURCE: AHRENS T.J. AND RUDERMAN M.H.  
J. APPL. PHYS. V.40, P.3044 (1969)
- 2) EXPERIMENTAL TECHNIQUE: D AN C1  
DATA REDUCTION METHOD : B
- 3) V01 AND RH00 WERE CALCULATED FROM:  

$$RH00 = 0.78506 - 8.591E-4(T-25) - 5.6E-7(T-25)^2 - 5.E-9(T-25)^3$$
 AMERICAN INST. OF PHYS. HANDBOOK, D.E. GRAY EDITOR (MCGRAW HILL BOOK CO 1972) 3RD.ED.
- 4) UNCERTAINTIES: US =1-1.5 PERCENT  
 UP =2.5 - MAXIMUM  
 RI =1.3 -
- 5) CO SAME SOURCE AS V01

TABLE 1

ETHANOL

23-2-1(2-6-1)---2



23-2-1(2-8-2)---3

ETHANOL

 $C(H_3)-C(H_2)-O-H$ 

T0 = 20-38 DEG.C.

V01 = 1.2889-1.2923 CC/G

THE TABLE LISTS T0 IN DEG.C., RH00 IN G/CC., VELOCITIES IN KM/SEC. AND P IN KBAR. RI IS REFRACTIVE INDEX

TABLE

| T0  | RH00   | US   | UP   | P    | V/V0   | RI    |
|-----|--------|------|------|------|--------|-------|
| 20. | 0.7894 | 7.18 | 3.62 | 205. | 0.4958 | 1.739 |
| 36. | 0.7755 | 7.06 | 3.63 | 199. | 0.4858 | 1.73  |
| 32. | 0.7790 | 7.98 | 4.14 | 257. | 0.4812 | 1.741 |
| 38. | 0.7738 | 7.21 | 3.70 | 206. | 0.4868 | 1.757 |

US =

## COMMENTS:

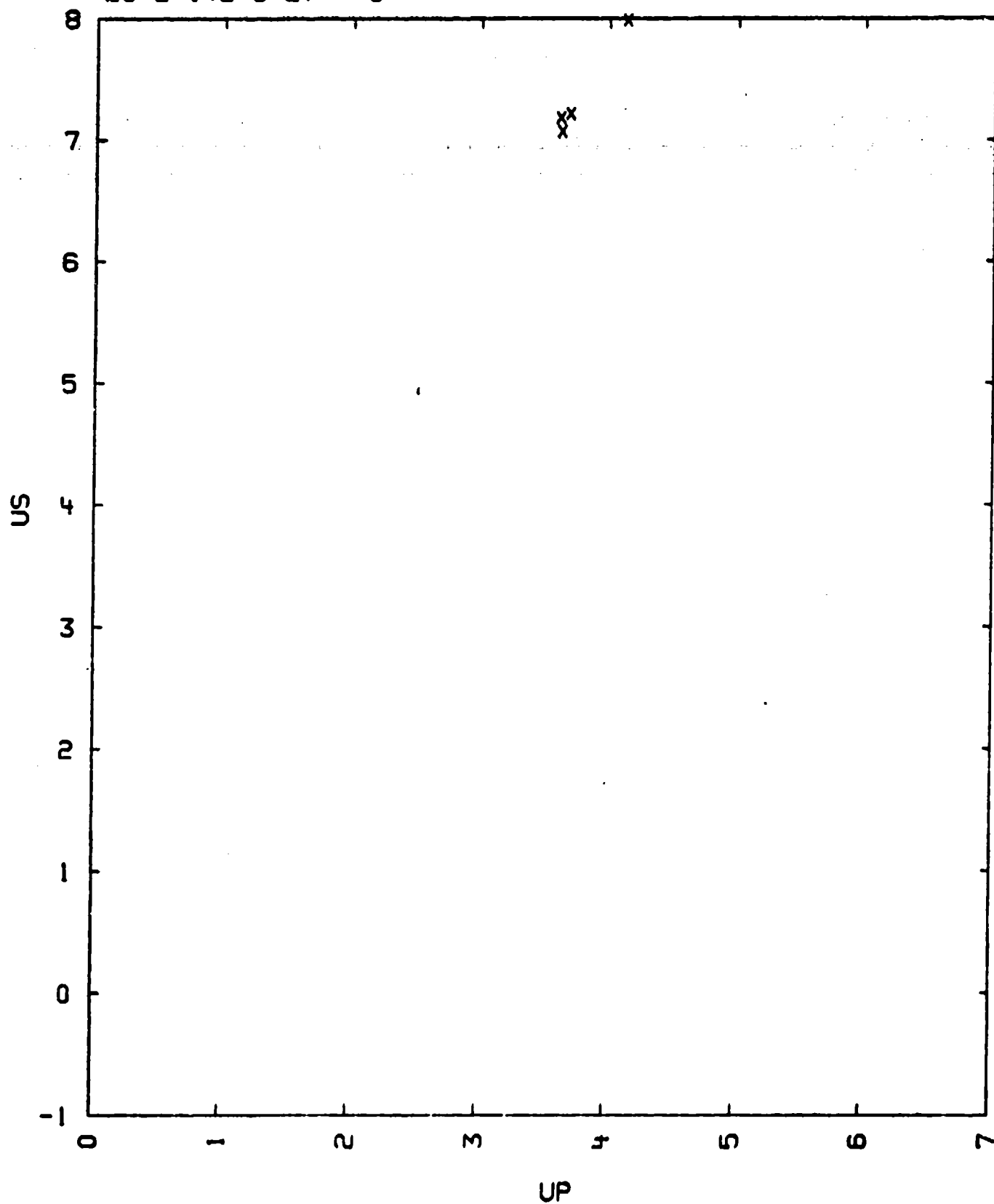
- 1) SOURCE: PETERSEN C.F. AND ROSENBERG J.T.  
J. APPL. PHYS. V.40, P.3044 (1969)
- 2) EXPERIMENTAL TECHNIQUE: D AND C1  
DATA REDUCTION METHOD : B
- 3) V01 AND RH00 WERE CALCULATED FROM  

$$RH00 = 0.78506 - 8.5E-4(T-25) - 5.6E-7(T-25)^2 - 5.0E-9(T-25)^3 \text{ G/CC}$$
 AMERICAN INST. OF PHYS. HANDBOOK, D.E. GRAY, EDITOR (MCGRAW HILL BOOK CO. 1972) 3RD. ED.

TABLE 1

ETHANOL

23-2-1(2-6-2)---3



23-2-113-8-1)---1  
ACETONE

H3-C-C(10)-C-H3 = C3-H8-O

T0 = 26-30 DEG. CENTIGRADE

V0 = 1.274 - 1.279 CC/G

C0 = 1.18 - 1.18 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| T0 | RH00   | US   | UP    | P     | V/V0  |
|----|--------|------|-------|-------|-------|
| 26 | 0.7849 | 5.37 | 2.510 | 105.8 | 0.533 |
| 30 | 0.7819 | 3.97 | 1.495 | 48.4  | 0.623 |

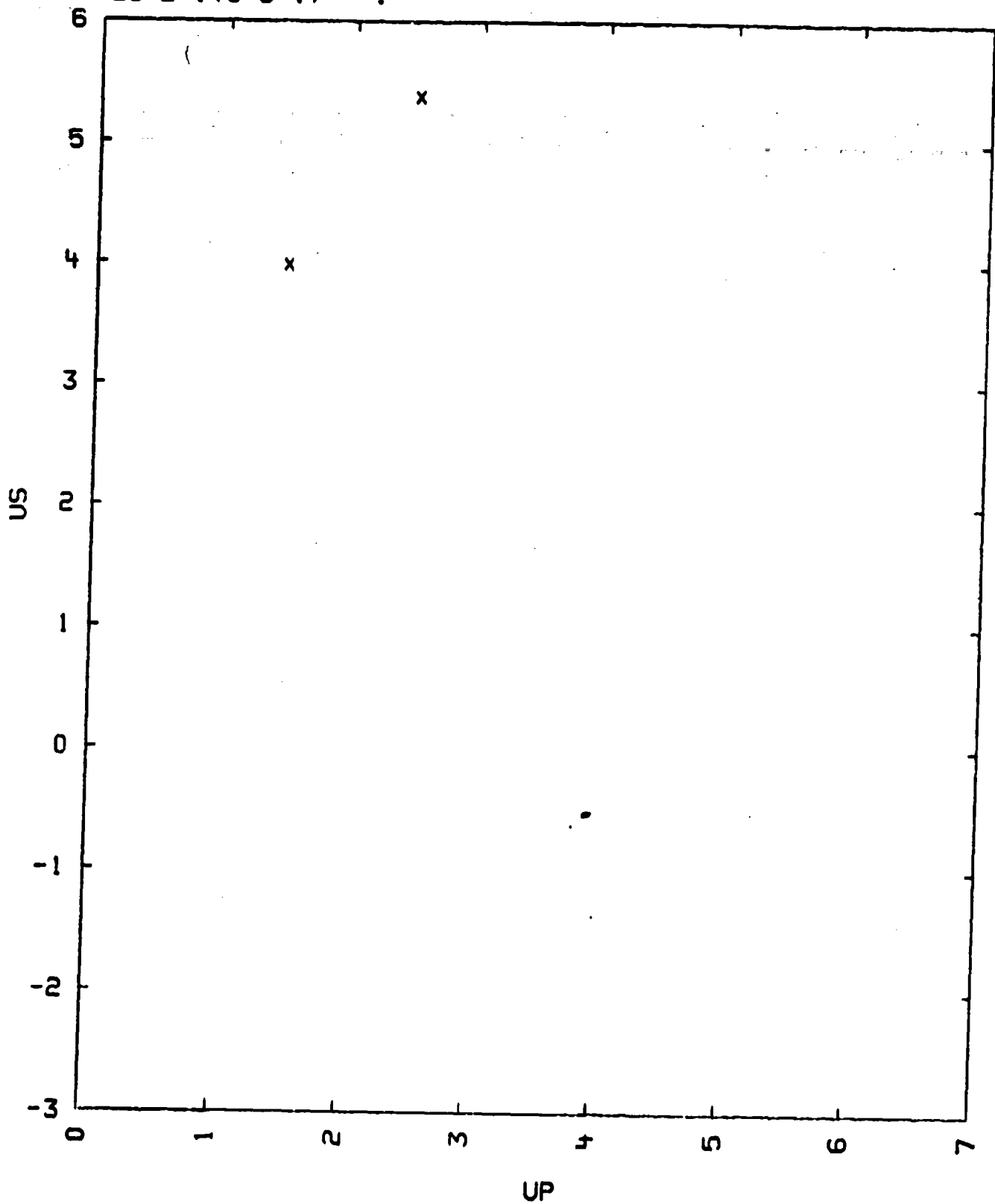
US = 1.91 + 1.38\*UP KM/SEC

COMMENTS:

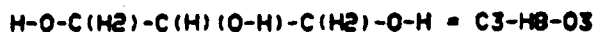
- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 245T ALUMINUM
- 3) THE VALUES FOR C0 WERE OBTAINED FROM THE AMERICAN INSTITUTE OF PHYSICS HANDBOOK, (MCGRAW-HILL BOOK CO., N. Y. 1963) 2ND ED.

TABLE 1

ACETONE  
23-2-1(3-6-1)---1



23-2-1(3-8-3)---1  
GLYCERINE



$T_0 = 18\text{-}30$  DEG. CENTIGRADE  
 $V_0 = 0.794\text{-}0.798$  CC/G.

$C_0 = 1.923$  KM/SEC  
AT  $T = 20$  DEG CENTIGRADE

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC AND TEMPERATURE IN DEG. CENTIGRADE

TABLE

| $T_0$ | $\text{RH}_00$ | $U_S$ | $U_P$ | $P$   | $V/V_0$ |
|-------|----------------|-------|-------|-------|---------|
| 30    | 1.253          | 6.07  | 2.240 | 170.3 | 0.631   |
| 18    | 1.259          | 4.58  | 1.328 | 76.6  | 0.710   |

$$U_S = 3.07 + 1.34 \cdot U_P \text{ KM/SEC}$$

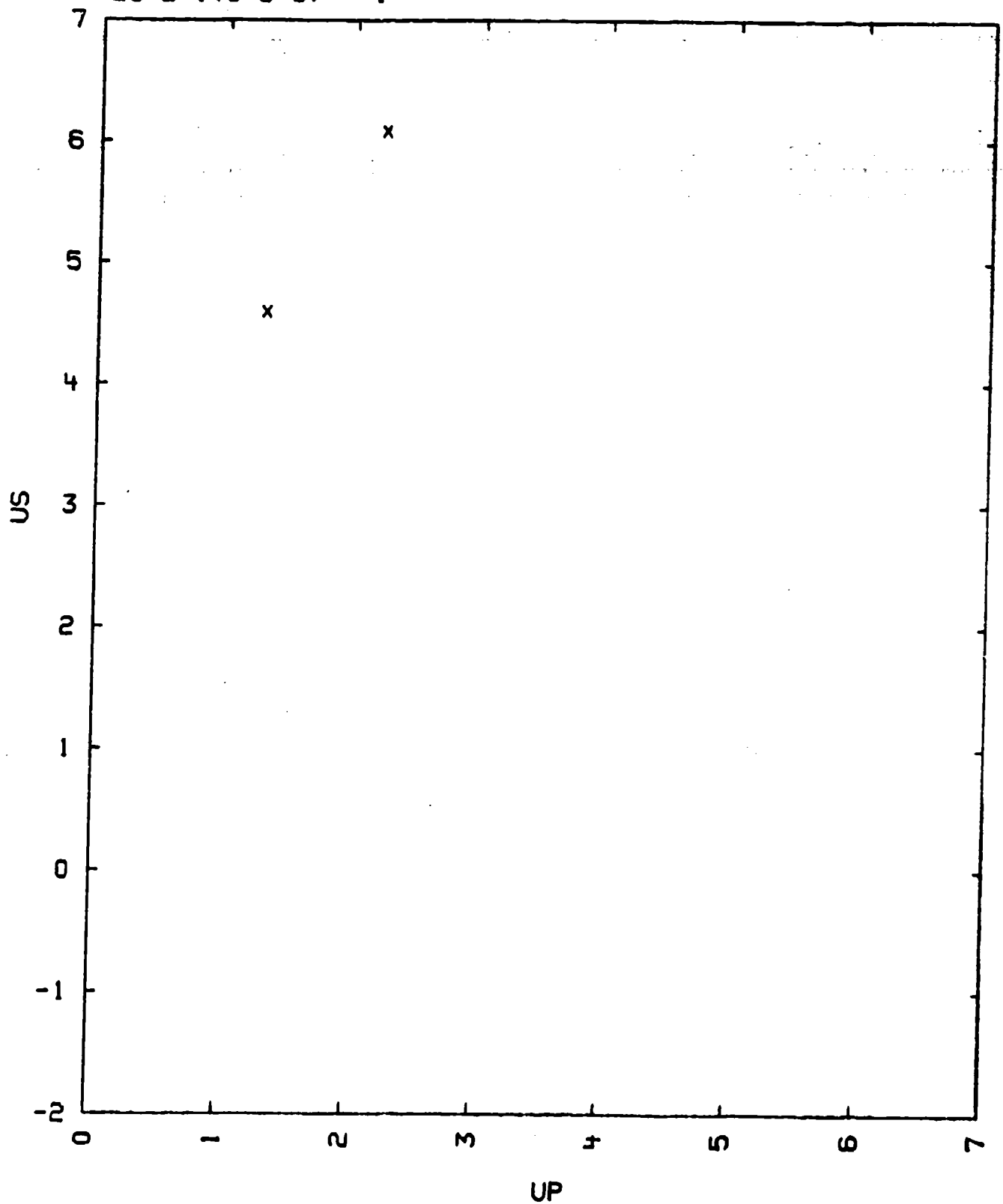
## COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS. VOL. 26. P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE VALUE OF  $C_0$  AND THE DERIVATIVE  $(dC_0/dT) = -0.0018$  KM/(SEC.DEG)  
FROM: BERGMANN, DER ULTRASCHALL, S. (S. HIRZEL VERLAG, STUTTGART 1954)
- 4) ONE DATA POINT WAS OBTAINED BY:  
J. B. RAMSAY PRIVATE COMMUNICATION (1968)  
LOS ALAMOS SCIENTIFIC LAB., LOS ALAMOS, NEW MEXICO.

| $T_0$ | $\text{RH}_00$ | $U_S$ | $U_P$ | $P$  | $V/V_0$ |
|-------|----------------|-------|-------|------|---------|
| 20    | 1.261          | 5.770 | 2.02  | 146. | 0.650   |

TABLE I

GLYCERINE  
23-2-1(3-8-3)---1





23-2-1(3-8-3)---2  
GLYCERIN (GLYCEROL)

H-O-C(H<sub>2</sub>)-C(H)(O-H)-C(H<sub>2</sub>)-O-H = C3-H8-O3      REMAINDER  
H<sub>2</sub>-O      SEE COMMENT 6

T0 = 25-28 DEG.C.  
V0 = 0.8010-0.8022  
V01 = 0.7956-0.7968

THE TABLE LISTS T IN DEGREES C, RH0 IN G/CC., VELOCITIES IN KM/SEC AND  
P IN KBARS. RI IS REFRACTIVE INDEX. AL IS 2024 ALUMINUM. BR 346 BRASS

TABLE

| - - - - - SAMPLE - - - - - |       |      |      |      |       |       |      | -DRIVER- |  |
|----------------------------|-------|------|------|------|-------|-------|------|----------|--|
| T0                         | RH00  | US   | UP   | P    | V/V0  | RI    | UFS  | MAT      |  |
| 28.                        | 1.246 | 4.28 | 1.10 | 58.7 | 0.743 | 1.610 | 1.46 | AL       |  |
| 25.                        | 1.248 | 4.54 | 1.32 | 74.8 | 0.709 | 1.667 | 1.77 | AL       |  |
| 25.                        | 1.248 | 4.59 | 1.32 | 75.6 | 0.712 | 1.656 | 1.77 | AL       |  |
| 25.                        | 1.248 | 6.67 | 2.64 | 220. | 0.604 | 1.755 | 3.23 | BR       |  |
| 24.                        | 1.249 | 1.92 | 0.0  | 0.0  | 1.000 | 1.468 | 0.0  |          |  |

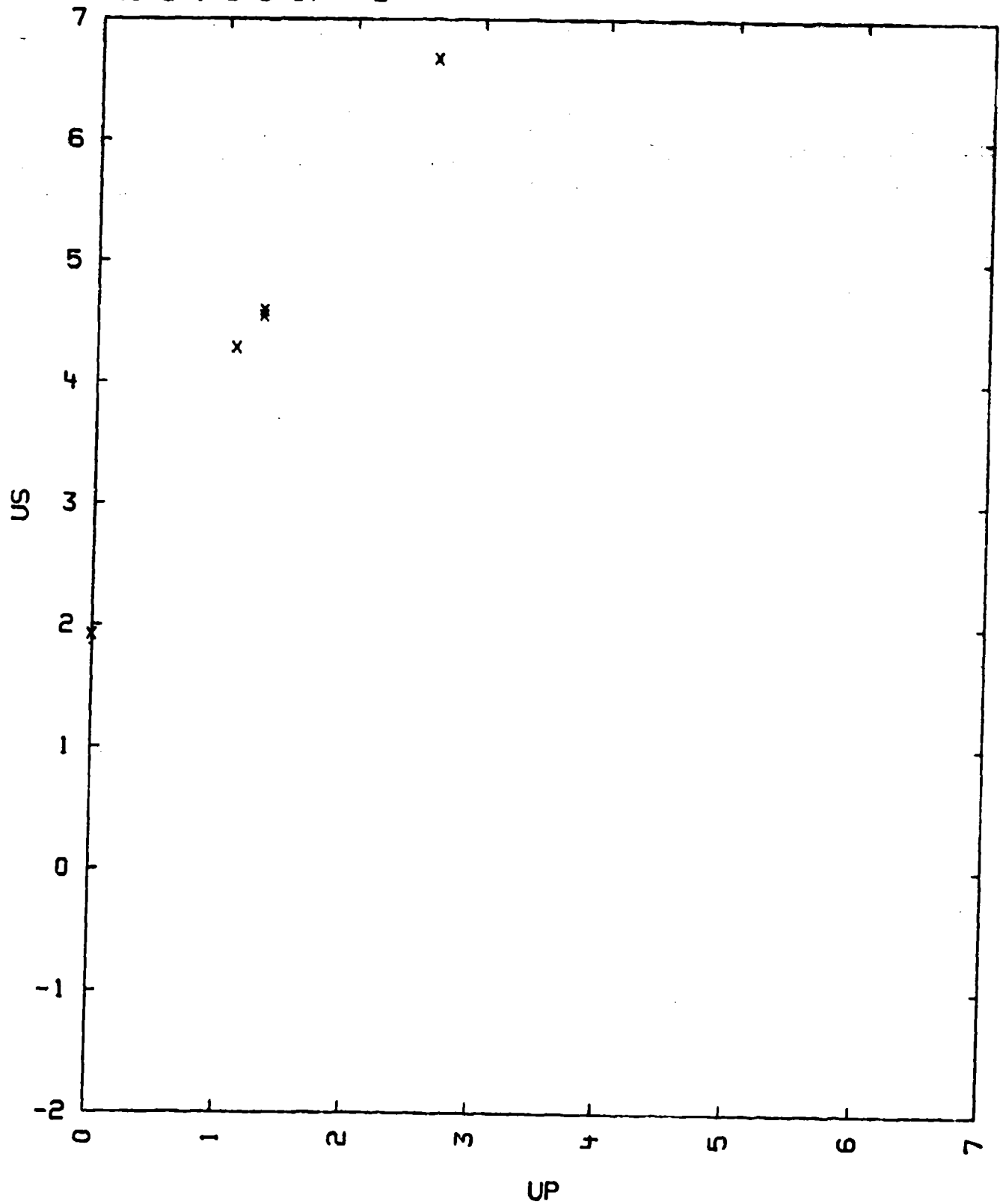
US =

## COMMENTS:

- 1) SOURCE: AHRENS T.J. AND RUDERMAN M.H.  
J. APPL. PHYS. V.37 P.4758 (1966)
- 2) EXPERIMENTAL TECHNIQUE: D AND C1  
DATA REDUCTION METHOD : B
- 3) V01 IS CALCULATED FROM  $V = (0.505(T-20) + 1)V_{20} = (1 + .4853T + .4895 \cdot T^2)V_0$   
WHERE T IS IN DEG. C. AND V IN CC/G. V0 IS THE VALUE AT T=0.0 DEG. C.  
AMERICAN INST. OF PHYS. HANDBOOK, D.E.GRAY EDITOR (MCGRAW-HILL BOOK  
CO. 1972) 3RD ED.
- 4) V WAS CALCULATED FROM A DENSITY MEASUREMENT AT 23.8 DEG.C. = 1.2492 +  
OR- 0.0005 G/CC.; SIMILARLY RH00.
- 5) UNCERTAINTIES US=1-1.5 PERCENT  
UP=2.5  
RI=1.3
- 6) ALL RI VALUES ARE NORMALIZED TO THE VALUE AT P=0 OBTAINED FROM  
 $0.965 \cdot RI(\text{GLYC.}) + 0.035 \cdot RI(\text{WATER}) = 1.468$

TABLE I

GLYCERIN (GLYCEROL)  
23-2-1(3-8-3)---2



23-2-113-8-3)---3  
GLYCERIN (GLYCEROL)

H-O-C(H2)-C(H)(O-H)-C(H2)-O-H = C3-H8-O3 99.4 PERCENT OR GREATER

T0 = 20-38 DEG.C.  
VOI = 0.7935-0.8009 CC/G

CO(T=20 DEG.C.) = 1.923 KM/SEC.

THE TABLE LISTS T0 IN DEG.C., VELOCITIES IN KM/SEC. RH00 IN G/CC AND P IN KBARS. RI IS REFRACTIVE INDEX

TABLE

| T0  | RH00  | US   | UP   | P    | V/VO  | RI    |
|-----|-------|------|------|------|-------|-------|
| 20. | 1.260 | 7.76 | 3.17 | 310. | 0.591 | 1.714 |
| 36. | 1.250 | 7.74 | 3.17 | 307. | 0.590 | 1.732 |
| 32. | 1.252 | 8.52 | 3.83 | 408. | 0.550 | 1.813 |
| 38. | 1.249 | 7.88 | 3.42 | 337. | 0.566 | 1.802 |

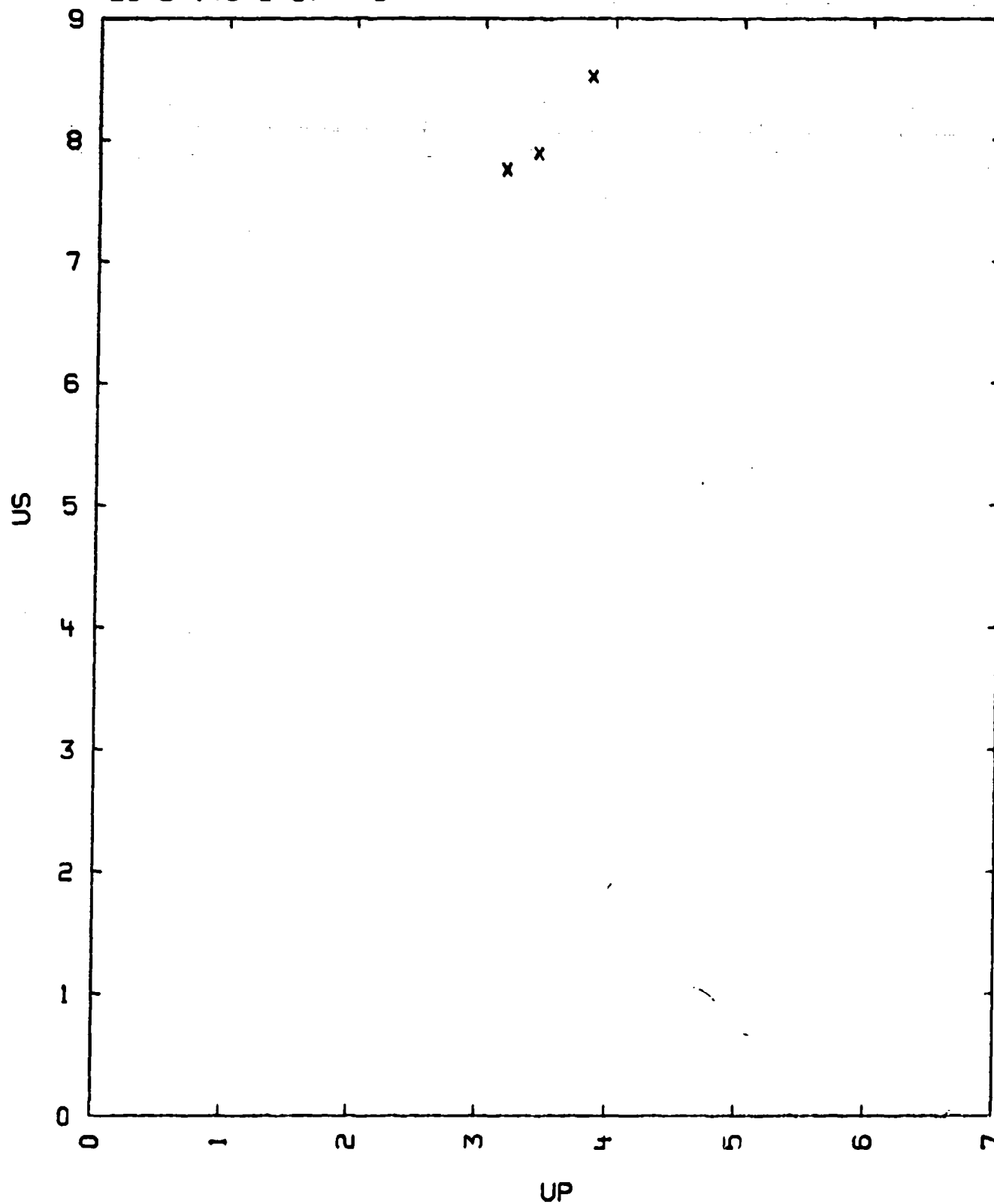
US =

COMMENTS:

- 1) SOURCE: PETERSEN C.F. AND ROSENBERG J.T.  
J. APPL. PHYS. V.40 P.3044 (1969)
- 2) EXPERIMENTAL TECHNIQUE: D AND C1  
DATA REDUCTION METHOD : B
- 3) VOI AND RH00 FROM  $V = (1 + .4853E-3 \cdot T + .4895E-6 \cdot T^2) V_0$ . HERE V0 IS THE VOLUME AT T=0 DEG. C. AMERICAN INST. OF PHYS. HANDBOOK. D.E. GRAY, EDITOR (MCGRAW HILL BOOK CO. 1972) 3RD. ED.
- 4) CO FROM L. BERGMAN, DER ULTRASCHALL. (S. HIRZEL VERLAG, STUTTGART 1954)

TABLE 1

GLYCERIN (GLYCEROL)  
23-2-1(3-8-3)---3



23-2-114-10-1)---1  
ETHYL ETHER (ETHER)

C2(H5)-O-C2(H5) = C4-H10-O

V0 = 1.41 CC/G  
V01 = 1.4015 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICRO-  
SEC, AND PRESSURE IN KILOBARS.

TABLE

| RHO0 | US    | UP   | P   | V/V0 |
|------|-------|------|-----|------|
| 0.71 | 6.71  | 3.50 | 170 | .478 |
| -    | 6.86  | 3.55 | 175 | .487 |
| -    | 7.11  | 3.59 | 180 | .496 |
| -    | 8.12  | 4.58 | 260 | .434 |
| -    | 7.92  | 4.72 | 261 | .387 |
| -    | 8.36  | 4.67 | 275 | .455 |
| -    | 8.15  | 4.74 | 278 | .415 |
| -    | 13.46 | 8.47 | 810 | .371 |
| -    | 14.21 | 8.52 | 860 | .400 |

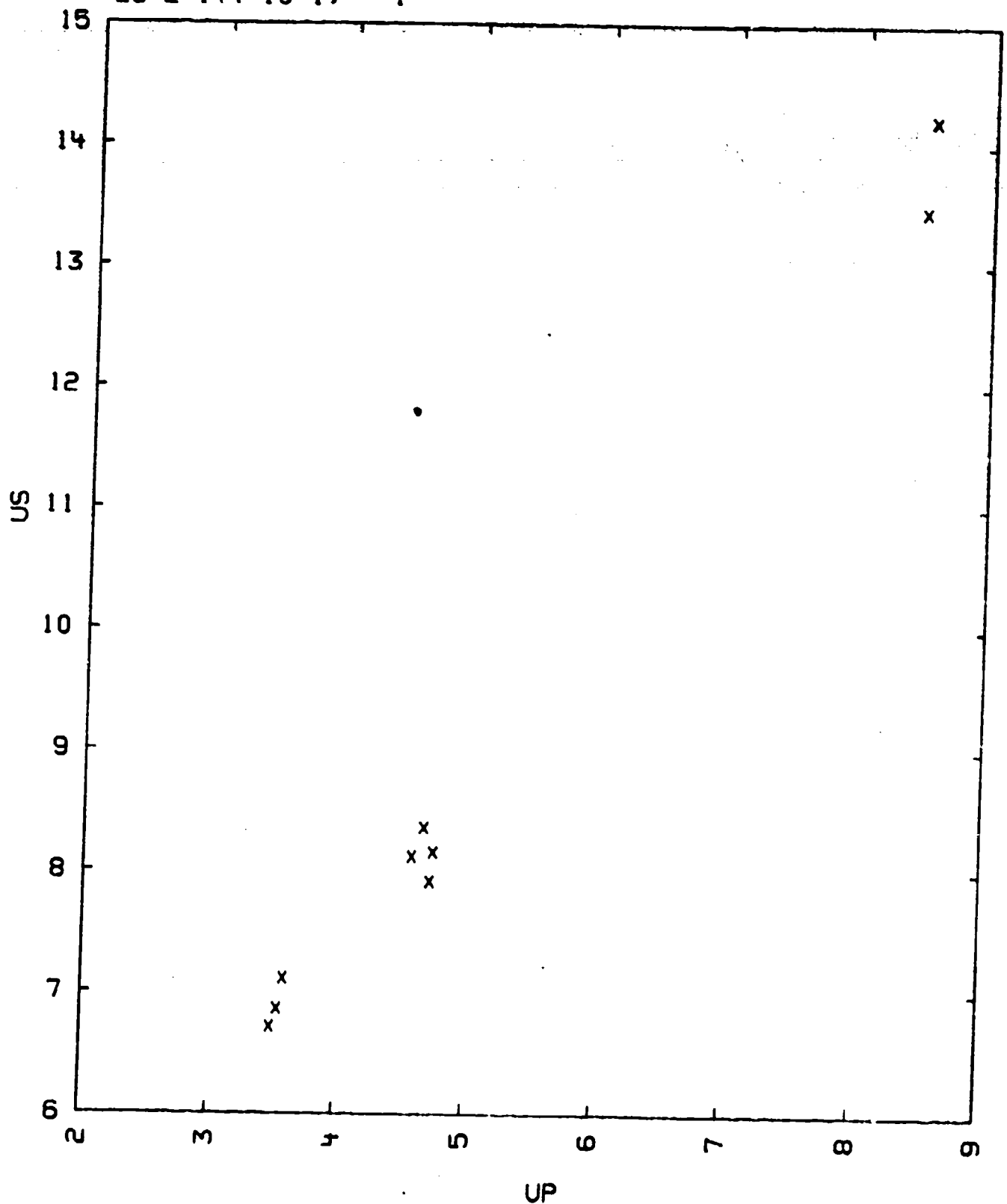
$$US = 1.69 + (1.42)UP \text{ MM/MICROSEC}$$

## COMMENTS:

- 1) SOURCE: SKIDMORE, I.C. AND MORRIS, E.  
THERMODYNAMICS OF NUCLEAR MATERIALS, P. 173 FF. (1962)  
INTERN. AT. ENERGY AGENCY, VIENNA  
ATOMIC WEAPONS RESEARCH ESTABLISHMENT, ALDERMASTON, ENGLAND
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION TECHNIQUE B  
THE SHOCK WAS PRODUCED BY AN EXPLOSIVELY ACCELERATED EN3 STEEL PLATE.  
THE SHOCK WAS TRANSMITTED THROUGH A STEEL PLATE INTO THE SAMPLE.
- 3) THE VELOCITY OF THE FLYING PLATE AND THE SHOCK AND SURFACE VELOCITY  
OF THE TARGET PLATE WERE MEASURED AS WELL AS THE SAMPLE SHOCK  
VELOCITY.
- 4) DATA SCATTER WAS ABOUT 0.03 MICROSEC.
- 5) CORRECTIONS WERE MADE FOR FLYING PLATE CURVATURE OF UP TO 1 MICROSEC.
- 6) THE HIGHER PRESSURES WERE OBTAINED BY A SPHERICALLY CONVERGING  
SYSTEM.
- 7) ALL PELLETS WERE SURROUNDED BY LEAD TO REDUCE LATERAL RAREFACTION.
- 8) V01 IS THE 20 DEGREES CENTIGRADE SPECIFIC VOLUME LISTED IN THE HAND-  
BOOK OF CHEMISTRY AND PHYSICS, 44TH EDITION, 1963.

TABLE 1

ETHYL ETHER (ETHER)  
23-2-1(4-10-1)---1



23-2-114-10-1)---2  
ETHYL ETHER (ETHER)

$\text{H}_3\text{-C-C(H}_2\text{)-O-C(H}_2\text{)-C-H}_3 = \text{C}_4\text{-H}_{10}\text{-O}$

$T_0 = 21\text{-}32$  DEG. CENTIGRADE  
 $V_0 = 1.407\text{-}1.433$  CC/G

$C_0 = 1.155$  KM/SEC.  
AT 20 DEG. CENTIGRADE

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURES IN KILOBARS, DENSITY IN G/CC AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| $T_0$ | $\rho_{00}$ | US   | UP    | P    | $V/V_0$ |
|-------|-------------|------|-------|------|---------|
| 32    | 0.6978      | 5.40 | 2.550 | 96.1 | 0.528   |
| 21    | 0.7107      | 3.88 | 1.517 | 41.8 | 0.609   |

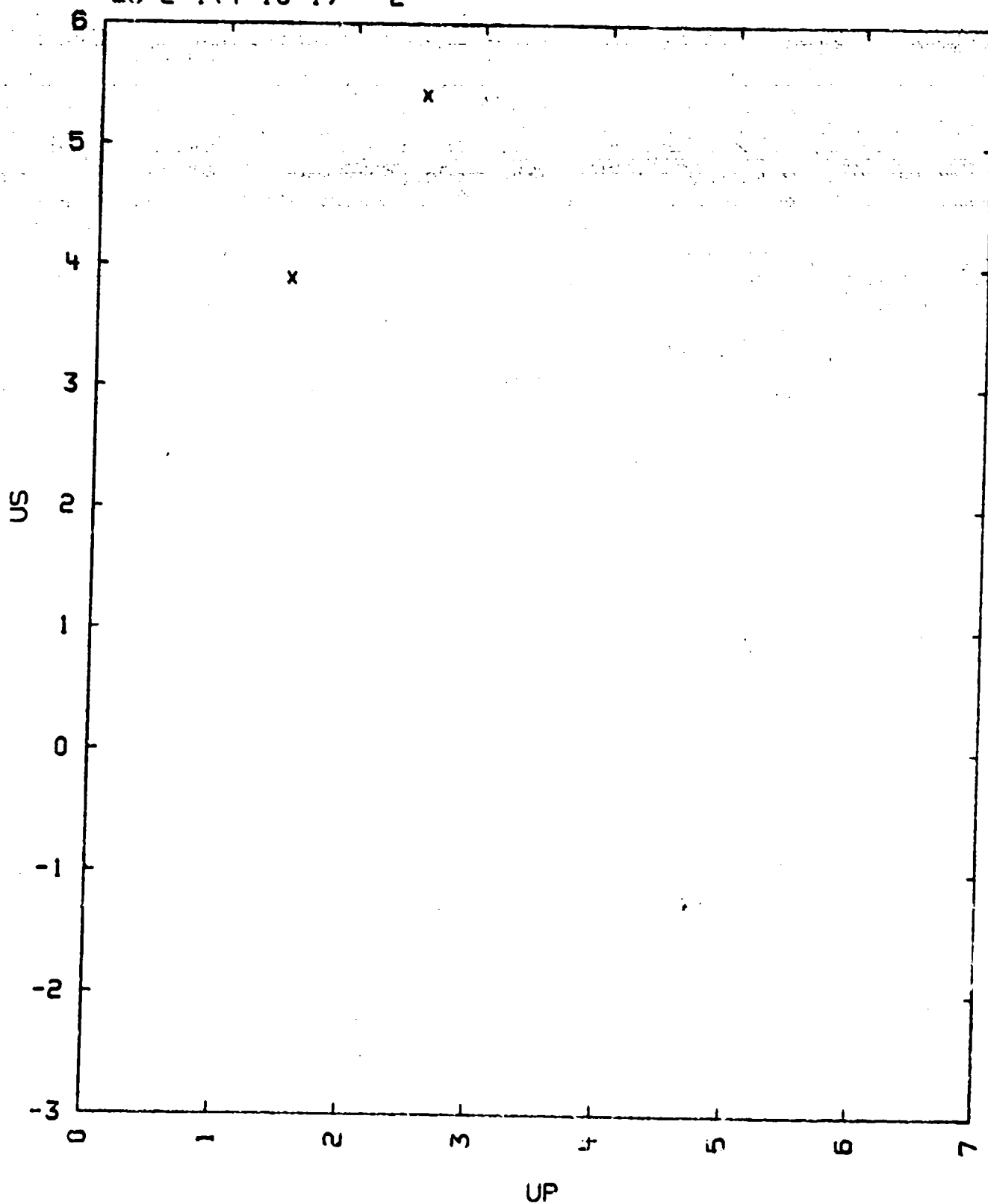
$$\text{US} = 1.65 + 1.47 \cdot \text{UP KM/SEC}$$

## COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 245T ALUMINUM
- 3)  $C_0$  WAS OBTAINED FROM L. BERGMANN, DER ULTRASCHALL (S. HIRZEL VERLAG, STUTTGART, 1954) 6TH ED., P. 376

TABLE I

ETHYL ETHER (ETHER)  
23-2-1(4-10-1)---2





23-2-1(5-8-2)---0

## POLYMETHYLMETHACRYLATE SUMMARY

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-O<sub>2</sub>-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)NV<sub>0</sub> = 0.8474 CC/G

CL = 2.72 KM/SEC

C<sub>0</sub> = 2.19 KM/SEC

CS = 1.40 KM/SEC

THE TABLE LISTS PLASTIC MASS HUGONIOT POINTS CALCULATED FROM THE FITS 1A, 2 AND 3A GIVEN BELOW. UNITS ARE: G/CC, KM/SEC, KBAR AND KBAR.CC/G FOR THE ENERGY DIFFERENCE. SER = SEMI ELASTIC REGION.

TABLE

| FIT | RHO0 | US     | UP   | P     | V/V0  | E-E0 | COMMENTS     |
|-----|------|--------|------|-------|-------|------|--------------|
| 1A  | 1.18 | 3.035  | .1   | 3.5   | 0.967 | .050 | SER          |
| -   | -    | 3.205  | .3   | 11.3  | 0.908 | .45  |              |
| -   | -    | 3.375  | .5   | 20.   | 0.852 | 1.25 |              |
| -   | -    | 3.488  | .633 | 26.   | 0.819 | 2.0  | INTERSECTION |
| 2A  | -    | 4.055  | 1.0  | 47.8  | .753  | 5.0  |              |
| -   | -    | 5.136  | 1.7  | 103.  | .609  | 14.4 |              |
| -   | -    | 6.218  | 2.4  | 176.  | .614  | 28.8 |              |
| -   | -    | -      | -    | -     | -     | -    | -            |
| 3A  | -    | 6.677  | 2.7  | 213.  | 0.596 | 36.4 |              |
| -   | -    | 7.717  | 3.5  | 319.  | 0.546 | 61.2 |              |
| -   | -    | 9.667  | 5.0  | 570.  | 0.483 | 125. |              |
| -   | -    | 12.267 | 7.0  | 1013. | 0.429 | 245. |              |
| -   | -    | 14.867 | 9.0  | 1579. | 0.395 | 405. |              |
| -   | -    | 17.467 | 11.0 | 2267. | 0.370 | 605. |              |

US = 2.95 + .85 \*UP, SIG.US = 7 (FOR PLEXIGLAS)  
 FOR UP BETWEEN .14 AND .46 KM/SEC  
 US = 2.510 + 1.545\*UP, SIG.US = .12 KM/SEC (FOR PLEXIGLAS)  
 FOR UP BETWEEN 1. AND 2.5 KM/SEC  
 US = 3.167 + 1.300\*UP, SIG.US = .14 KM/SEC (FOR PLEXIGLAS)  
 FOR UP BETWEEN 2.6 AND 10.2 KM/SEC  
 US = 2.280 + 1.782\*UP, SIG.US = .10 KM/SEC (FOR LUCITE)  
 FOR UP BETWEEN .8 AND 2.3 KM/SEC  
 US = 3.286 + 1.236\*UP, SIG.US = .08 KM/SEC (FOR LUCITE)  
 FOR UP BETWEEN 2.5 AND 4.3 KM/SEC

## COMMENTS:

## 1) SOURCE: COMPILER

FIT 1A FROM DATA OF 23-2-1(5-8-2)---12

- 2A AND 3A FROM DATA OF 23-2-1(5-8-2)---5 AND 10

FIT 1B AND 2B - - - 23-2-1(5-8-2)---3 AND 6.

- 2) NO SEPERATE ELASTIC WAVE HAS BEEN DETECTED BUT FIT NO 1 EXTRAPOLATES TO A POINT CLOSE TO CL INDICATING A LACK OF PLASTIC DEFORMATION AT LOW PRESSURES. SLOW YIELDING IS INDICATED BY THE ATTENUATION IN P SHOWN BY ENTRY 23-2-1(5-8-2)---13. AS INDICATED BY ---3, THE SLOPE OF 1A OBTAINED FROM THE ASSUMPTION UFS=2UP MAY BE TOO LARGE BY 15 TO

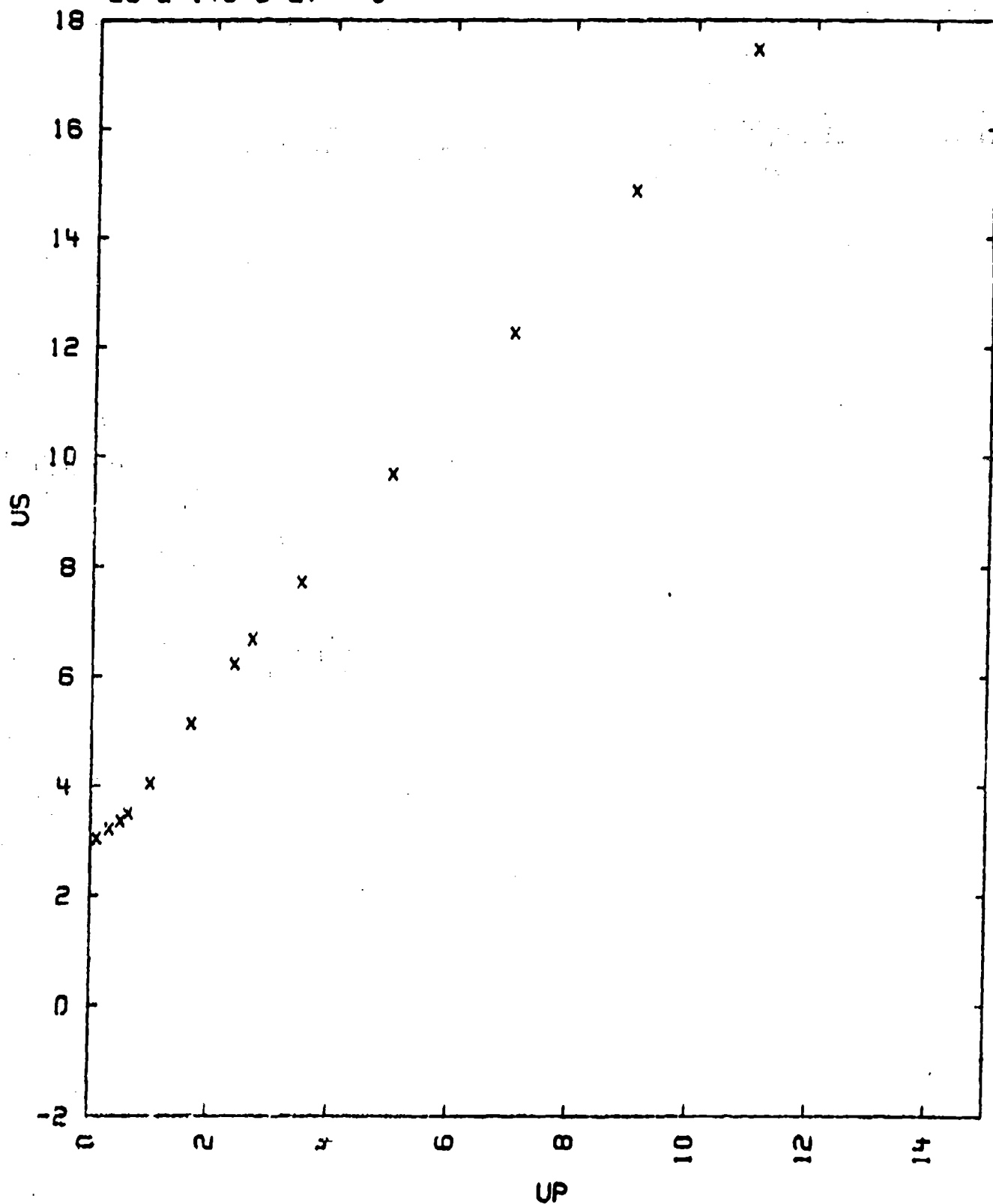
20 PERCENT.

- 3) POLYMETHYLMETHACRYLATE DATA VARY SOMEWHAT MORE THAN MONOMERIC MATERIALS FROM SOURCE TO SOURCE, INDICATING A SENSITIVITY TO THE METHOD OF PREPARATION.
  - 4) IN CONNECTION WITH COMMENT 3, THE DIFFERENCE BETWEEN FITS 2A AND 1B MAY BE THE MANUFACTURING PROCESS: FITS A ARE FOR PLEXIGLASS OF ROHM AND HAAS CO., WHILE FITS B ARE FOR DUPONT DE NEMOURS CO. LUCITE.
- ALSO:
- 23-2-1(5-8-2)---8 DATA SHOW THE CHANGE IN DUS/DUP AT 190 KBAR CLEARLY BUT SHOW A LOWER COMPRESSIBILITY THAN THE ABOVE.
- 23-2-1(5-8-2)---12 AND 15 LESS COMPRESSIBLE THAN THE ABOVE FITS
- 23-2-1(5-8-2)---9 QUITE SOFT COMPARED TO THE AMERICAN PRODUCTS
- 23-2-1(5-8-2)---11 IS IN GENERAL AGREEMENT
- OTHER DATA IS LESS ARE LESS ACCURATE.

TABLE I

POLYMETHYLMETHACRYLATE SUMMARY

23-2-1(5-8-2)---0



23-2-1(5-8-2)---1

PERSPEX (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-O<sub>2</sub>-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)NV<sub>0</sub> = 0.847 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,  
AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US    | UP   | P    | V/V <sub>0</sub> |
|------|-------|------|------|------------------|
| 1.18 | 7.11  | 3.34 | 282  | .530             |
| -    | 7.62  | 3.20 | 288  | .580             |
| -    | 7.43  | 3.26 | 288  | .563             |
| -    | 8.50  | 4.24 | 425  | .506             |
| -    | 8.50  | 4.34 | 435  | .493             |
| -    | 8.61  | 4.37 | 447  | .493             |
| -    | 8.67  | 4.40 | 450  | .491             |
| -    | 12.88 | 7.78 | 1180 | .396             |
| -    | 13.03 | 7.70 | 1190 | .409             |
| -    | 13.37 | 7.68 | 1210 | .426             |

US = 3.07 + 1.295 UP KM/SEC. SIG.US = 0.25 KM/SEC

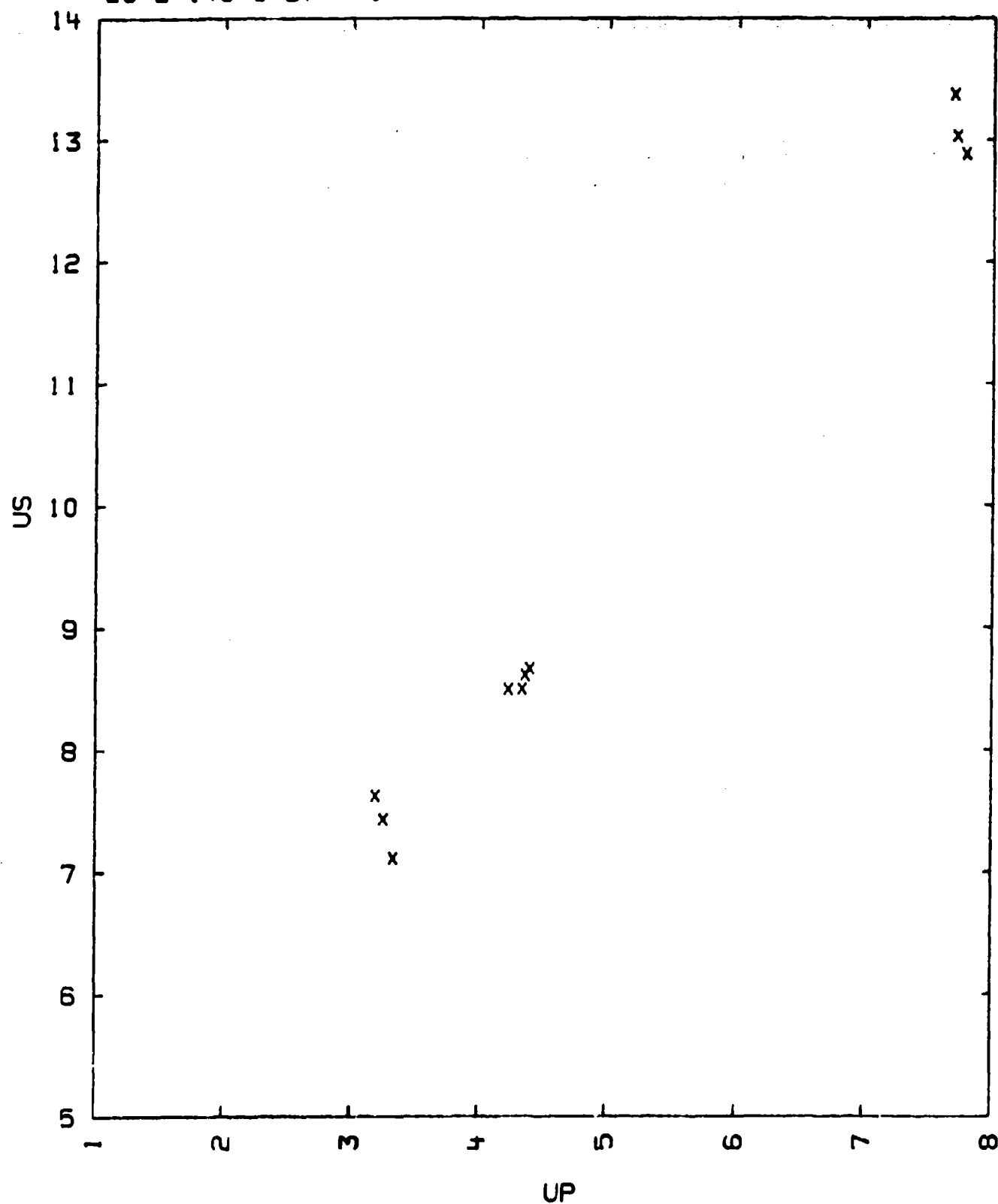
## COMMENTS:

- 1) SOURCE: SKIDMORE, I.C. AND MORRIS, E.  
THERMODYNAMICS OF NUCLEAR MATERIALS, P. 173 FF. (1962)  
INTERN. AT. ENERGY AGENCY, VIENNA  
ATOMIC WEAPONS RESEARCH ESTABLISHMENT, ALDERMASTON, ENGLAND
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION TECHNIQUE B  
THE SHOCK WAVE WAS PRODUCED BY AN EXPLOSIVELY ACCELERATED EN3 STEEL PLATE.  
THE SHOCK WAS TRANSMITTED THROUGH A STEEL PLATE INTO THE SAMPLE.
- 3) THE VELOCITY OF THE FLYING PLATE AND THE SHOCK AND SURFACE VELOCITY OF THE TARGET PLATE WERE MEASURED AS WELL AS THE SAMPLE SURFACE AND SHOCK VELOCITIES.
- 4) DATA SCATTER WAS ABOUT 0.03 MICROSEC.
- 5) CORRECTIONS WERE MADE FOR FLYING PLATE CURVATURE OF UP TO 1 MICROSEC.
- 6) THE HIGHER PRESSURES WERE OBTAINED BY A SPHERICALLY CONVERGING SYSTEM.
- 7) ALL PELLETS WERE SURROUNDED BY LEAD TO REDUCE LATERAL RAREFACTION.

TABLE 1

PERSPEX (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---1



23-2-1(5-8-2)---2  
 PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-O<sub>2</sub>-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)N

V<sub>0</sub> = .847 CC/O      CL = 2.670 KM/SEC      C<sub>0</sub> = 2.42 KM/SEC  
 CS = 1.121 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC. AND PRESSURE IN KILOBARS. U IS THE VELOCITY OF THE PROJECTILE PLATE.

TABLE

| RH00 | US   | UP    | P    | V/V <sub>0</sub> | U     |
|------|------|-------|------|------------------|-------|
| 1.18 | 3.23 | 0.150 | 5.69 | 0.9536           |       |
| -    | 3.22 | 0.210 | 7.88 | 0.9348           |       |
| -    | 3.92 | 0.665 | 30.7 | 0.8304           |       |
| -    | 3.93 | 0.900 | 41.6 | 0.7704           |       |
| -    | 4.35 | 1.20  | 61.3 | 0.6522           |       |
| -    | 4.39 | 1.34  | 69.4 | 0.6948           |       |
| 1.18 | 3.18 | 0.454 | 16.9 | 0.856            | 0.571 |
| -    | 3.26 | 0.590 | 22.7 | 0.819            | 0.745 |
| -    | 3.85 | 0.916 | 41.6 | 0.762            | 1.19  |
| -    | 4.17 | 1.17  | 57.6 | 0.720            | 1.54  |
| -    | 4.52 | 1.43  | 76.5 | 0.684            | 1.91  |
| -    | 5.97 | 2.28  | 160. | 0.618            | 3.18  |

US = 3.06 + 1.04\*UP KM/SEC (FIRST 6 PTS)

SIG.US = 0.1 KM/SEC

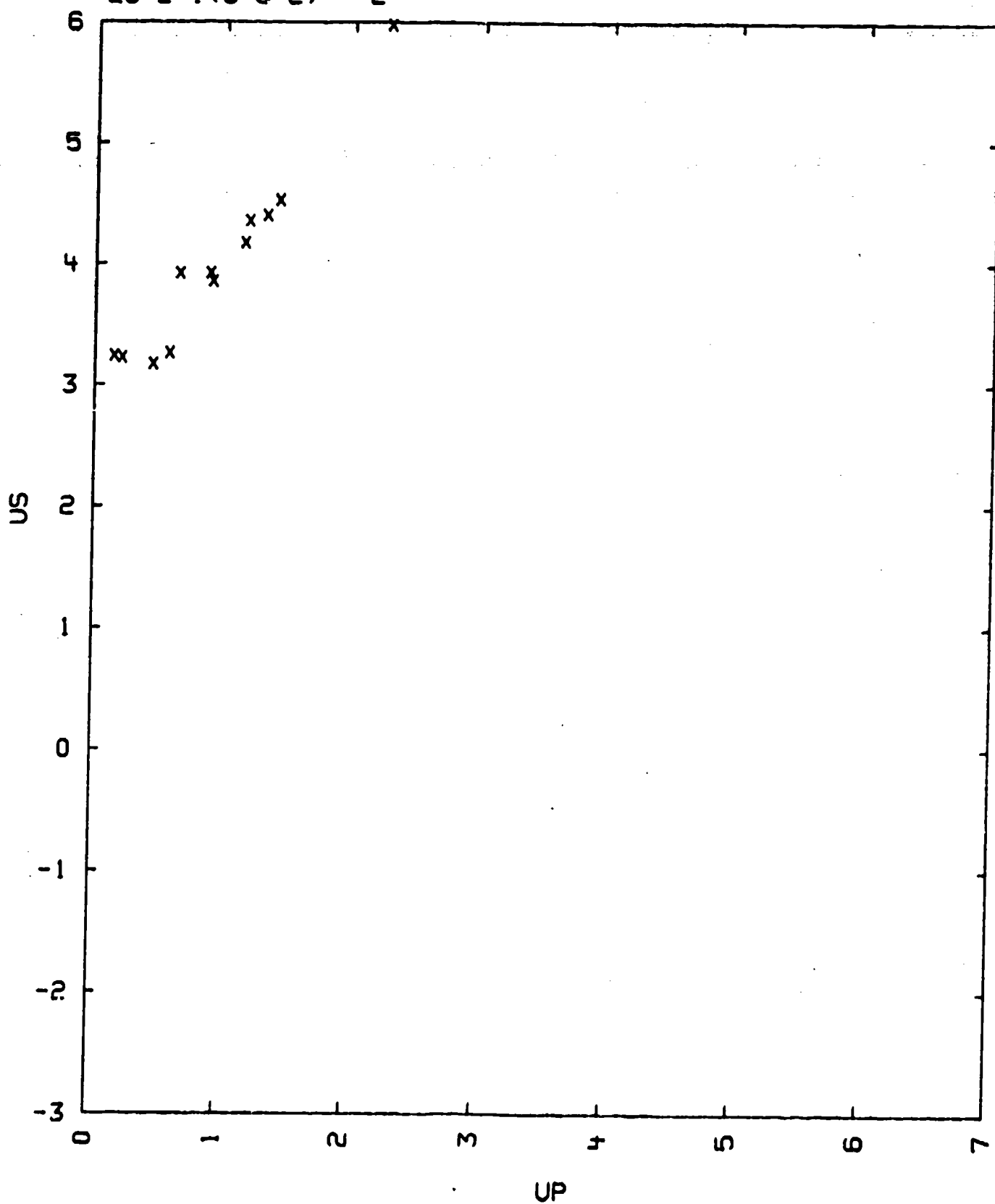
US = 2.35+1.57\*UP KM/SEC (LAST 6 PTS)

SIG.US = 0.06 KM/SEC

## COMMENTS:

- 1) SOURCE: WAGNER, M.H., WALDORF, W.F. AND LOUIE, N.A.  
 REPORT NO. AFSWC-TDR-62-66, VOL. 1 (1962)  
 WORK DONE AT DOWNEY, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE A  
 DATA REDUCTION TECHNIQUE: D, UP=1/2\*UFS FOR FIRST 6 POINTS ONLY  
 A, IMPACTOR MATERIAL 2024-T3 AL REST
- 3) ACCURACY IS LIMITED BECAUSE ASSEMBLY DIMENSIONS ALLOW RELATIVELY LARGE DEVIATIONS FROM ONE-DIMENSIONALITY.
- 4) CL AND CS FROM BERGMAN, L., DER ULTRASCHALL, S. HIRZEL VERLAG, STUTTGART, P 650 (1954)
- 5) THE 95 PERCENT CONFIDENCE RANGE OF THE MEASURED PARAMETERS IN THE LAST SET OF 6 POINTS IN THE ORDER OF THE LISTING IS GIVEN BY:  
 + OR - FDEL US = 11. 6.4 8.0 5.5 6.9 10.5 PERCENT  
 + OR - FDEL U = 1.8 2.1 2.9 5.0 2.1 7.1 -  
 HERE FDEL U = 100(DEL U)/U

TABLE I  
PLEXIGLAS (POLYMETHYLMETHACRYLATE)  
23-2-1(5-8-2)---2



23-2-1(5-8-2)---3  
LUCITE (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-02-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub> 2)N

V<sub>0</sub> = 0.845 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC  
AND PRESSURE IN KILOBARS.

| TABLE  |       |       |       |     |               |          |
|--------|-------|-------|-------|-----|---------------|----------|
| SAMPLE |       |       |       |     | AL BASE PLATE |          |
| RH00   | US    | UFS   | UP    | P   | V/V0          | PRESSURE |
| 1.182  | 8.55  | 8.15  | 4.19  | 422 | 0.510         | 796      |
| 1.184  | 7.84  | 7.25  | 3.76  | 348 | 0.520         | 670      |
| 1.183  | 5.31  | 3.21  | 1.75  | 110 | 0.670         | 231      |
| 1.183  | 6.43  | 5.12  | 2.52  | 192 | 0.608         | 381      |
| 1.184  | 7.35  | 6.04  | 3.30  | 287 | 0.551         | 553      |
| 1.184  | 8.50  |       | 4.23  | 426 | 0.502         | 804      |
| 1.186  | 5.83  | 3.94  | 1.99  | 138 | 0.659         | 277      |
| 1.184  | 4.45  | 2.24  | 1.21  | 64  | 0.728         | 143      |
| 1.183  | 3.66  | 1.42  | 0.88  | 38  | 0.761         | 94       |
| 1.186  | 5.00  | 2.907 | 1.615 | 96  | 0.6770        | 207      |
| 1.187  | 4.504 |       | 1.387 | 74  | 0.6921        | 168      |

US = 2.80 + 1.37 UP KM/SEC  
SIGMA US = 0.199 KM/SEC

#### COMMENTS:

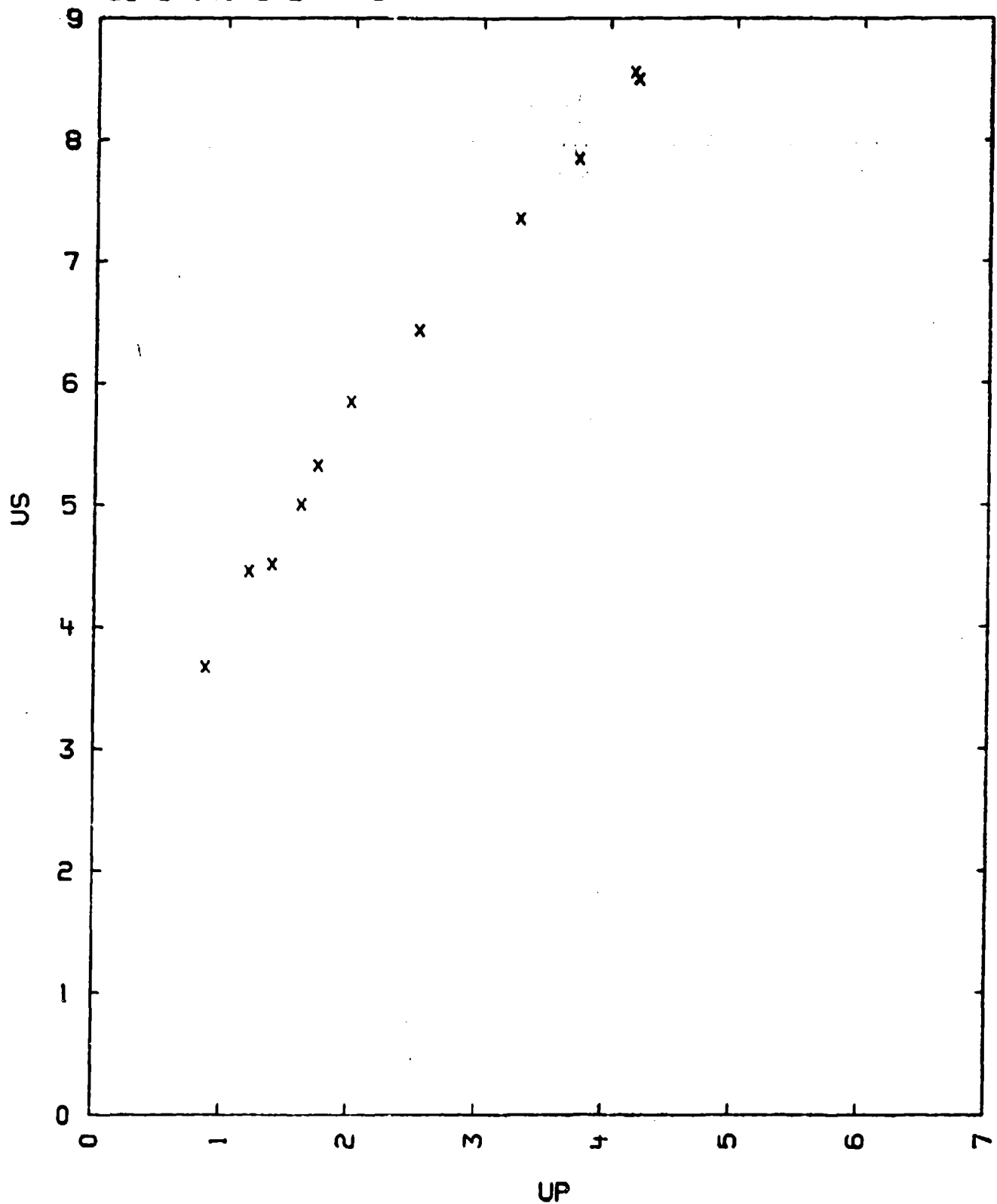
- 1) SOURCE: COMPILER  
L. R. L. EQUATION OF STATE FILE  
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)  
DATA REDUCTION TECHNIQUE B.
- 3) THE OBSERVATION IN THE TABLE THAT UP TENDS TO BE LESS THAN 1/2UFS  
SUGGESTS THAT PART OF THE SHOCK COMPRESSION IS IRREVERSIBLE ON THE  
TIME SCALE OF THE EXPERIMENT



TABLE 1

LUCITE (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---3



23-2-115-8-2)---4

PERSPEX (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-O<sub>2</sub>-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)NV<sub>0</sub> = 0.83 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,  
PRESSURE IN KILOBARS AND SAMPLE THICKNESS, D, IN MM.

TABLE

| RH00 | US   | UP   | UFS  | P    | V/V <sub>0</sub> | D     |
|------|------|------|------|------|------------------|-------|
| 1.2  | 5.37 | 2.2  | 4.3  | 141. | 0.59             | 3.22  |
| -    | 5.29 | 1.8  | 3.6  | 114. | 0.66             | 8.16  |
| -    | 5.12 | 1.64 | 3.28 | 101. | 0.680            | 12.42 |
| -    | 4.81 | 1.59 | 3.18 | 92.  | 0.670            | 24.88 |
| -    | 4.54 | 1.43 | 2.87 | 78.  | 0.685            | 37.5  |
| -    | 4.30 | 1.12 | 2.24 | 57.8 | 0.740            | 49.6  |
| -    | 4.08 | 0.95 | 1.89 | 46.5 | 0.767            | 62.3  |
| -    | 3.88 | 0.70 | 1.40 | 32.6 | 0.820            | 74.4  |

US = 3.07 + 1.12 UP KM/SEC

SIGMA US = 0.15 KM/SEC

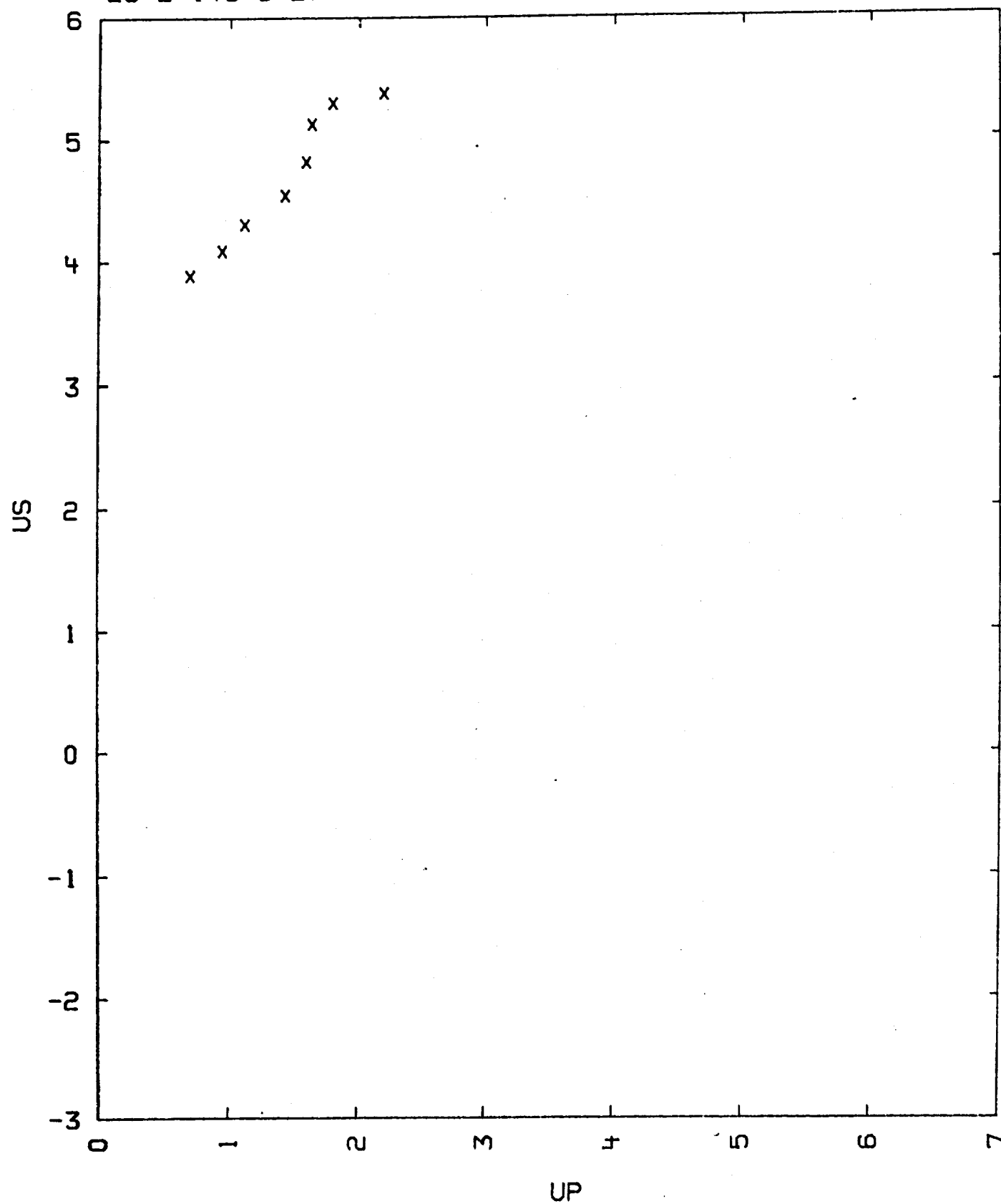
## COMMENTS

- 1) SOURCE: BUCHANAN, J. S., JAMES, H. J. AND TEAGUE, G. W.  
PHIL. MAG., VOL. 3, P. 1432, (1958)
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION TECHNIQUE D
- 3) NOTE FURTHER THAT THE SHOCK VELOCITIES WERE OBTAINED BY FIRST FITTING  
TIME-POSITION DATA FOR THE SHOCK IN LUCITE, GIVING:  
US = 1/(0.183 + 0.001\*D) KM/SEC., WHERE D IS IN MM  
THIS PRESMOOTHING OF THE US DATA REDUCED SIGMA US SLIGHTLY.
- 4) DEVIATIONS FROM ONE DIMENSIONALITY IN THESE EXPERIMENTS ARE RELATIVE-  
LY LARGE DUE TO THE SMALL EXPLOSIVE CHARGE USED: 7.5 CM.

TABLE I

PERSPEX (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---4



23-2-1(5-8-2)---5

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-02-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-02)NV<sub>0</sub> = 0.8474 CC/G

CL = 2.718 KM/SEC

C<sub>0</sub> = 2.188 KM/SEC

CS = 1.396 KM/SEC

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| RH00  | US    | UFS   | UP    | P     | V/V <sub>0</sub> |
|-------|-------|-------|-------|-------|------------------|
| 1.180 | 5.884 |       | 2.223 | 154.3 | 0.3222           |
| -     | 5.110 |       | 1.682 | 101.4 | 0.6708           |
| -     | 5.102 |       | 1.674 | 100.8 | 0.6719           |
| -     | 4.312 |       | 1.181 | 60.1  | 0.7261           |
| -     | 4.290 |       | 1.200 | 60.8  | 0.7203           |
| 1.182 | 4.336 |       | 1.198 | 61.4  | 0.7237           |
| 1.181 | 6.816 | 5.395 | 2.668 | 214.8 | 0.6086           |

US = 2.334 + 1.650 UP KM/SEC

SIGMA US = 0.067 KM/SEC

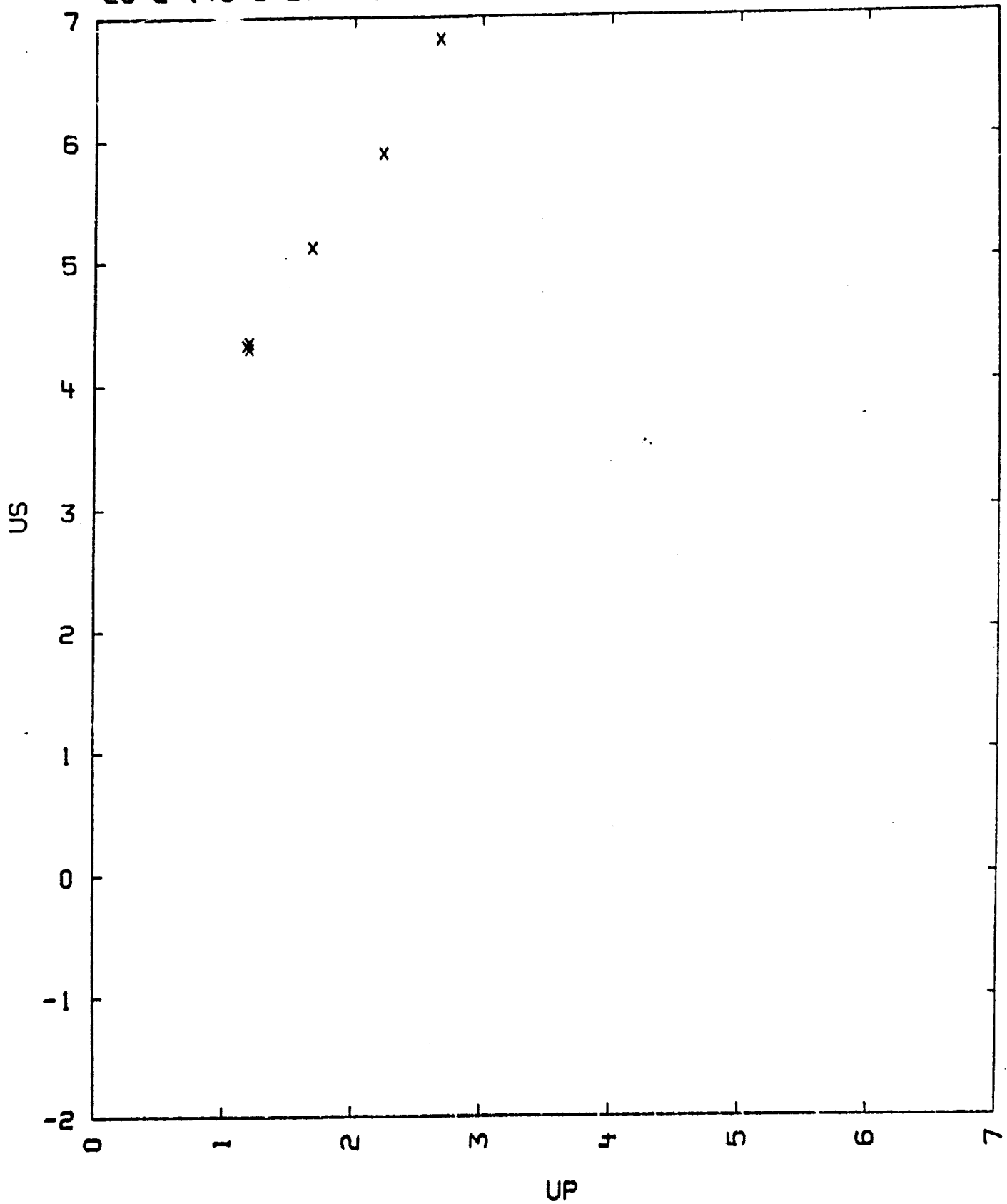
## COMMENTS:

- 1) SOURCE: DEAL, W. E.  
PRIVATE COMMUNICATION  
WALSH, J. M., YARGER, F. L., AND MCQUEEN, R. G.  
GMX-6 REPORTS 1954, 1955.  
GMX-6, LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS,  
NEW MEXICO
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B. STANDARD MATERIAL 2027 AL
- 3) ONLY THE LAST VALUE OF UP WAS OBTAINED BY SUBTRACTING FROM .5\*UFS THE  
EXTRAPOLATED QUANTITY 1/2(UFS-2UP) GIVEN BY THE MATERIAL
- 4) THE ABOVE SOUND VELOCITIES WERE OBTAINED ON A PLEXIGLAS TYPE G  
UNSHRUNK SHEET WITH RHO = 1.187 G/CC AT T = 23 DEGREES CENTIGRADE  
ALSO MEASURED BY DEAL AND MARSH:  
PLEXIGLAS TYPE II, UVT SHEETS, RHO = 1.185 G/CC, T = 23 DEGREES  
CENTIGRADE  
CL = 2.715, CS = 1.395, C<sub>0</sub> = 2.186 KM/SEC  
EVR-KLEER RHO = 1.184 G/CC T = 23 DEGREES  
CL = 2.691, CS = 1.376, C<sub>0</sub> = 2.172 KM/SEC  
BY RAMSAY, GMX-8, ABOVE ADDRESS  
EVR-KLEER  
CL = 2.713, CS = 1.367, C<sub>0</sub> = 2.206 KM/SEC  
'OLD' EVR-KLEER  
CL = 2.706, CS = 1.407, C<sub>0</sub> = 2.163 KM/SEC

TABLE I

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---5



23-2-1(5-8-2)---6

LUCITE (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-02-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-02)NV<sub>0</sub> = 0.8474 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC AND  
PRESSURE IN KILOBARS.

TABLE

| RH00  | US    | UP    | UFS   | P     | V/V <sub>0</sub> |
|-------|-------|-------|-------|-------|------------------|
| 1.180 | 6.257 | 2.244 | 4.522 | 165.7 | 0.6414           |
| -     | 6.078 | 2.153 |       | 154.4 | 0.6458           |
| -     | 5.263 | 1.689 | 3.396 | 104.9 | 0.6791           |
| -     | 4.705 | 1.310 | 2.592 | 72.7  | 0.7216           |
| -     | 4.695 | 1.310 | 2.609 | 72.6  | 0.7210           |
| -     | 4.719 | 1.299 | 2.580 | 72.3  | 0.7247           |
| -     | 5.409 | 1.722 |       | 109.9 | 0.6816           |

US = 2.556 + 1.637 UP KM/SEC

SIGMA US = 0.037 KM/SEC

## COMMENTS:

1) SOURCE: DEAL, W. E.

PRIVATE COMMUNICATION

GMX-6, LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS,

NEW MEXICO.

2) EXPERIMENTAL TECHNIQUE B

DATA REDUCTION TECHNIQUE B. STANDARD MATERIAL 2024 AL

3) THE LAST POINT HAS BEEN REPORTED BEFORE BY:

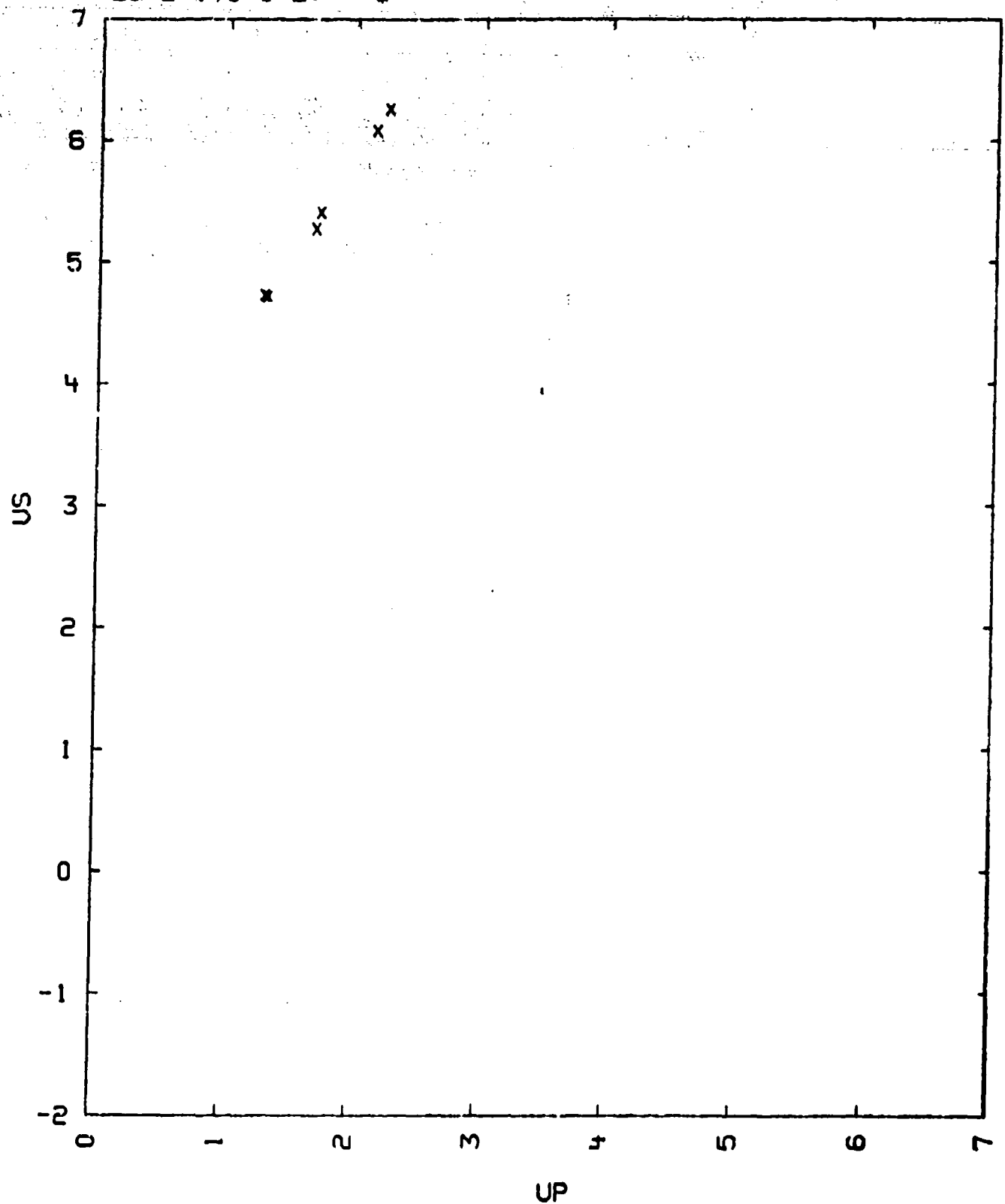
WALSH, J. M., YARGER, F. L., AND MCQUEEN, R. G.

GMX-6 REPORTS 1954, 1955.

TABLE 1

LUCITE (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---6



23-2-1(5-8-2)---7

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-O<sub>2</sub>-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)NV<sub>0</sub> = 0.847 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US    | UP    | P    | V/V <sub>0</sub> |
|------|-------|-------|------|------------------|
| 1.18 | 2.900 | 0.073 | 2.5  | 0.975            |
| -    | 2.940 | 0.077 | 2.7  | 0.974            |
| -    | 2.980 | 0.086 | 3.0  | 0.971            |
| -    | 3.025 | 0.098 | 3.5  | 0.967            |
| -    | 3.070 | 0.125 | 4.5  | 0.959            |
| -    | 3.101 | 0.150 | 5.5  | 0.952            |
| -    | 3.130 | 0.176 | 6.5  | 0.944            |
| -    | 3.157 | 0.202 | 7.5  | 0.936            |
| -    | 3.183 | 0.228 | 8.5  | 0.928            |
| -    | 3.080 | 0.176 | 6.5  | 0.943            |
| -    | 3.097 | 0.189 | 7.0  | 0.939            |
| -    | 3.121 | 0.215 | 8.0  | 0.931            |
| -    | 3.143 | 0.240 | 9.0  | 0.923            |
| -    | 3.177 | 0.291 | 11.0 | 0.908            |
| -    | 3.204 | 0.343 | 13.0 | 0.893            |
| -    | 3.228 | 0.394 | 15.0 | 0.879            |
| -    | 3.250 | 0.446 | 17.0 | 0.863            |
| -    | 3.270 | 0.488 | 19.0 | 0.851            |

US = NO SIMPLE POLYNOMIAL ADEQUATELY REPRESENTS THIS DATA

## COMMENTS

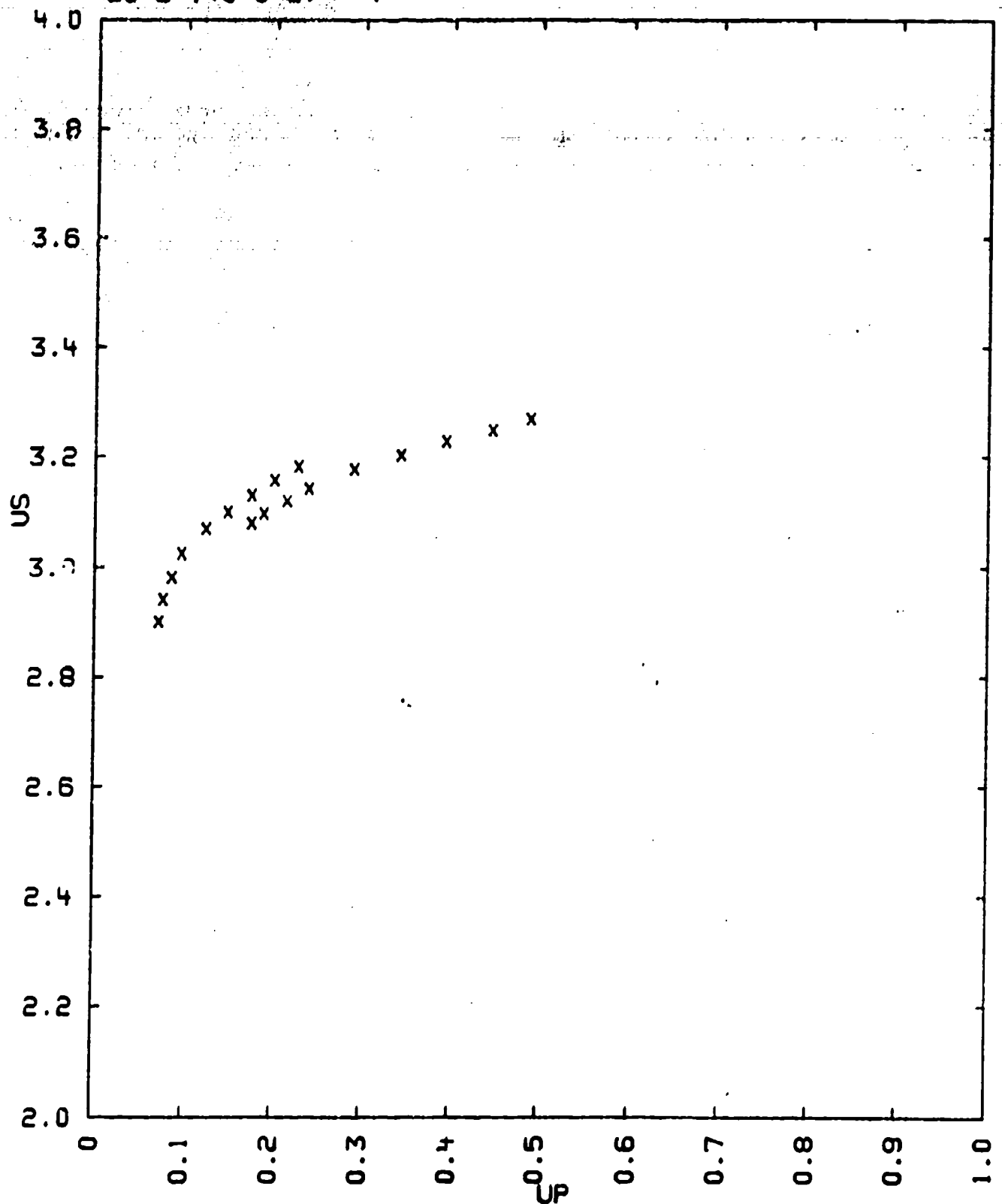
- 1) SOURCE: SCHMIDT, D. N. AND EVANS, M. W.  
PREPRINT  
STANFORD RES. INST., PALO ALTO, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE D  
DATA REDUCTION TECHNIQUE NOT SUMMARISED.  
A RELATIVELY ELABORATE CORRECTION MUST BE APPLIED TO THE OBSERVATIONS IN THESE TWO EXPERIMENTS SINCE THE WAVE HAS A DISTINCT TWO DIMENSIONAL CHARACTER AND IMPACTS THE SAMPLE SURFACE AT AN ANGLE.  
SEE: FOWLES, G. R., J. APPL. PHYS., VOL. 32, P. 1475, (1961)
- 3) THE DATA SHOW A STRONGLY CURVING US VS. UP LOC'S.



TABLE I

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---7



23-2-115-8-2)---8  
 PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C(O)-O-CH<sub>3</sub> N = C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>

V<sub>0</sub> = 0.847 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC. AND  
 PRESSURE IN KILOBARS

TABLE

| RH00 | US   | UP   | P     | V/V <sub>0</sub> |
|------|------|------|-------|------------------|
| 1.18 | 4.07 | 0.89 | 42.7  | 0.781            |
| -    | 4.58 | 1.17 | 63.2  | 0.744            |
| -    | 4.60 | 1.15 | 62.4  | 0.750            |
| -    | 5.45 | 1.75 | 112.5 | 0.678            |
| -    | 5.47 | 1.80 | 116.2 | 0.671            |
| -    | 5.52 | 1.71 | 111.4 | 0.690            |
| -    | 6.05 | 2.08 | 148   | 0.656            |
| -    | 6.07 | 2.11 | 151   | 0.652            |
| -    | 6.08 | 2.03 | 146   | 0.667            |
| -    | 6.08 | 2.16 | 155   | 0.644            |
| -    | 6.09 | 2.20 | 158   | 0.638            |
| -    | 6.15 | 2.10 | 152   | 0.658            |
| -    | 6.16 | 2.12 | 154   | 0.656            |
| -    | 6.46 | 2.34 | 178   | 0.637            |
| -    | 6.48 | 2.38 | 182   | 0.632            |
| -    | 6.78 | 2.48 | 198   | 0.634            |
| -    | 6.88 | 2.72 | 221   | 0.604            |
| -    | 6.93 | 2.65 | 217   | 0.617            |
| -    | 7.13 | 2.88 | 242   | 0.596            |
| -    | 7.33 | 3.08 | 266   | 0.579            |
| -    | 7.50 | 3.19 | 282   | 0.575            |
| -    | 7.54 | 3.24 | 288   | 0.570            |
| -    | 7.57 | 3.33 | 297   | 0.560            |
| -    | 7.58 | 3.28 | 293   | 0.568            |
| -    | 7.62 | 3.28 | 295   | 0.570            |
| -    | 7.62 | 3.32 | 298   | 0.564            |
| -    | 7.62 | 3.35 | 301   | 0.560            |
| -    | 7.64 | 3.28 | 296   | 0.571            |
| -    | 7.66 | 3.25 | 294   | 0.576            |
| -    | 7.67 | 3.36 | 304   | 0.562            |

US = 2.68 + 1.61 UP KM/SEC FROM UP = 0.8 TO 2.6 KM/SEC

SIGMA US = 0.08 KM/SEC

US = 3.51 + 1.25 UP KM/SEC FROM UP = 2.8 TO 3.5 KM/SEC

SIGMA US = 0.05 KM/SEC

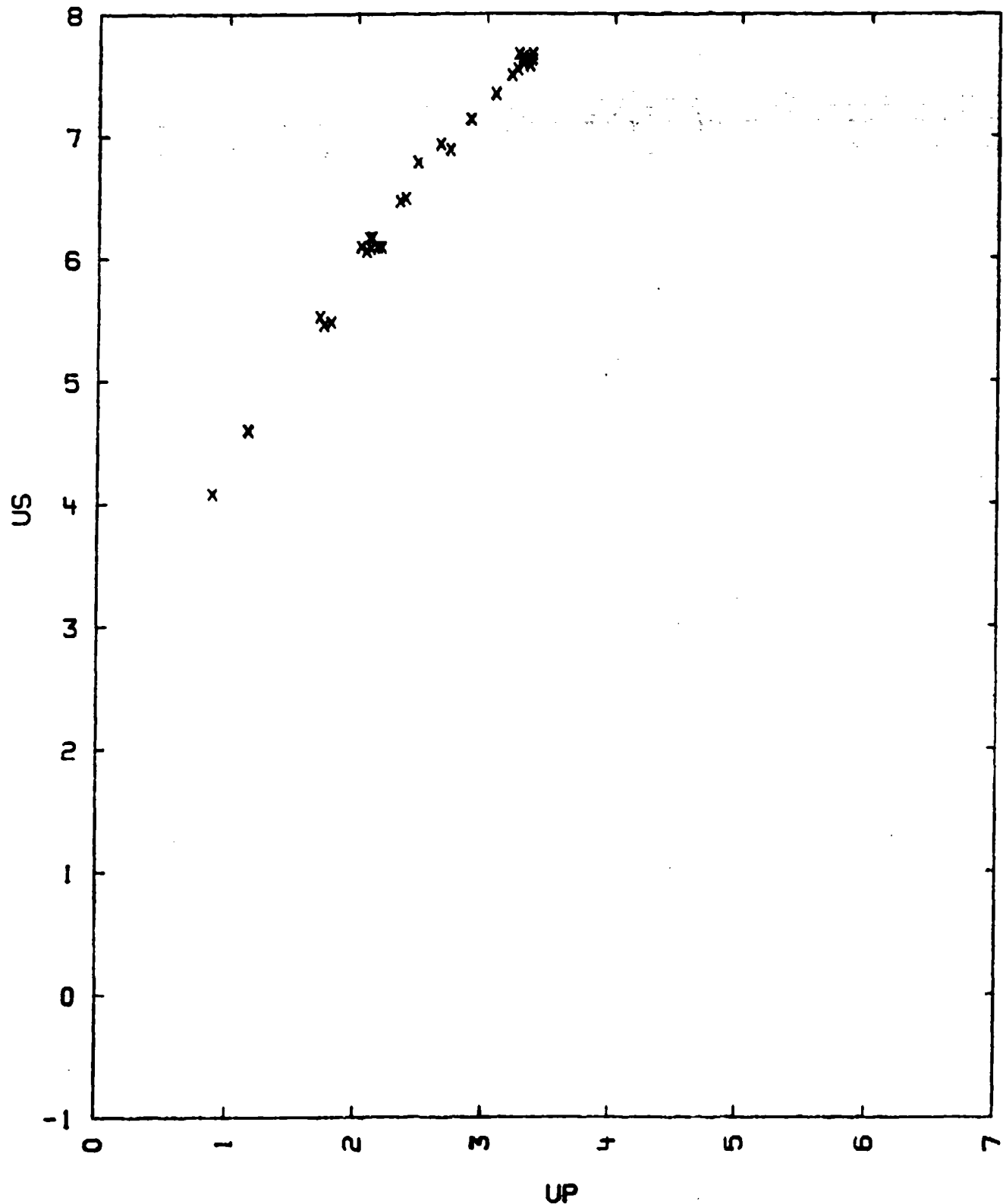
COMMENTS:

- 1) SOURCE: HAUVER, O.E. AND MELANI, A.  
B.R.L REPORT NO. 1259 (1964)  
BALLISTIC RES. LABS., ABERDEEN PROVING GROUNDS  
MARYLAND
- 2) EXPERIMENTAL TECHNIQUE H  
DATA REDUCTION METHOD B
- 3) THE ABOVE DATA SUGGEST A TRANSITION AT 200 KB WHICH IS SUPPORTED  
BY A RAPID CHANGE IN THE POLARIZATION SIGNAL ABOVE THIS PRESSURE
- 4) ALL POINTS WERE CORRECTED FOR SHOCK WAVE TILT

TABLE 1

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---8



23-2-1(5-8-2)---8

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-O<sub>2</sub>-C-H<sub>3</sub>)<sub>N</sub> = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)<sub>N</sub>

MANUFACTURED BY ROHM AND HAAS GMBH, DARMSTADT, GERMANY.

V<sub>0</sub> = 0.840 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,  
AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US   | UP   | P   | V/V <sub>0</sub> |
|------|------|------|-----|------------------|
| 1.19 | 4.17 | 1.31 | 65  | 0.686            |
| -    | 4.56 | 1.53 | 83  | 0.665            |
| -    | 5.28 | 2.05 | 128 | 0.611            |
| -    | 5.81 | 2.41 | 167 | 0.584            |
| -    | 5.78 | 2.44 | 168 | 0.577            |
| -    | 6.59 | 2.77 | 218 | 0.579            |

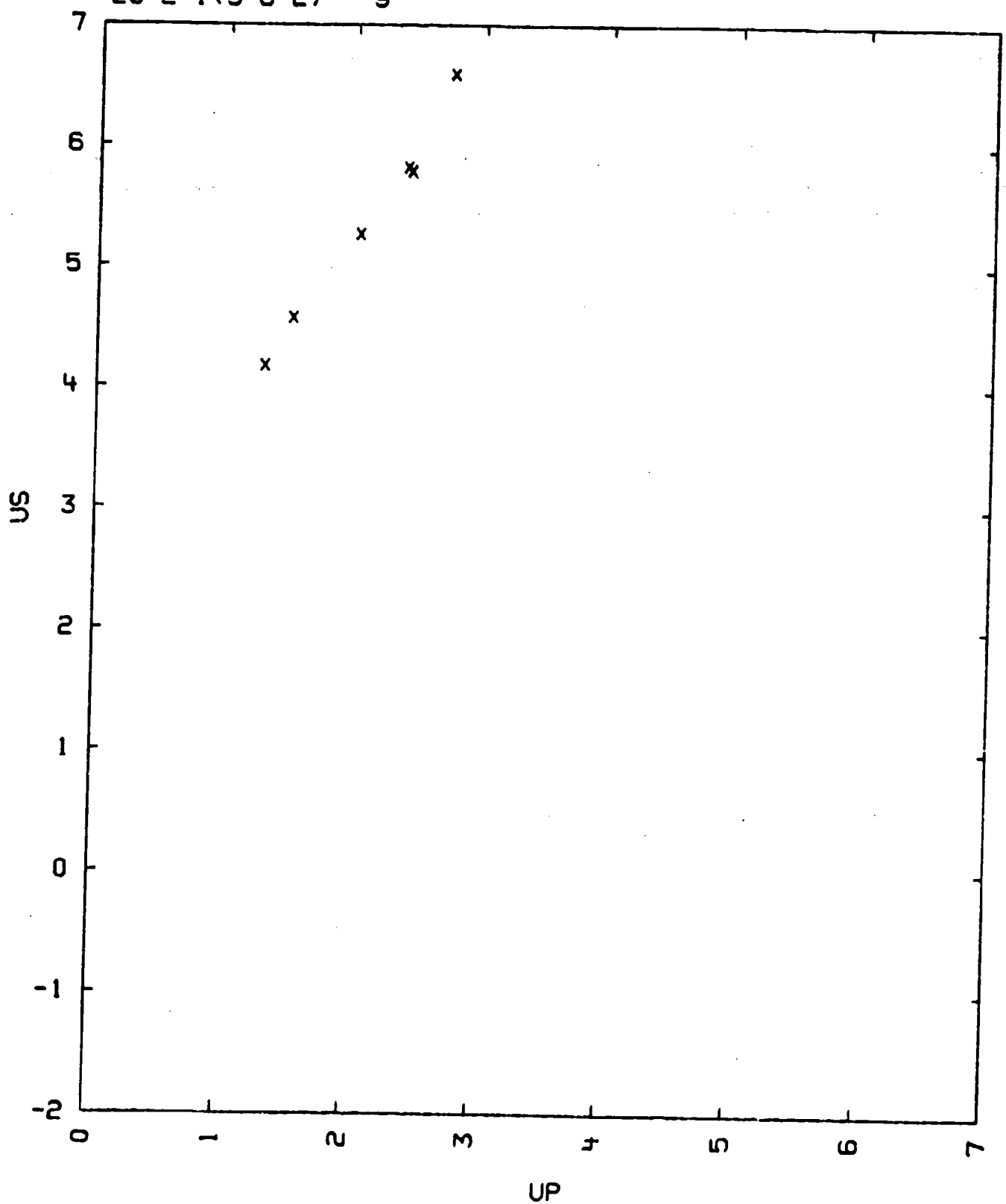
US = 2.12 + 1.56 UP KM/SEC

SIGMA US = 0.116 KM/SEC

## COMMENTS:

- 1) SOURCE: LUNDBERG, LENNART.  
PRIVATE COMMUNICATION  
RESEARCH INSTITUTE OF NATIONAL DEFENCE, STOCKHOLM, SWEDEN.
- 2) EXPERIMENTAL TECHNIQUE B.  
DATA REDUCTION TECHNIQUE B.

TABLE 1  
PLEXIGLAS (POLYMETHYLMETHACRYLATE)  
23-2-1(5-8-2)---9



23-2-1(5-8-2)---10

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-02-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-02)NV<sub>0</sub> = 0.847 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,  
AND PRESSURE IN KILOBARS.

TABLE

| SAMPLE |       |      |      |                  | BASE PLATE |      |
|--------|-------|------|------|------------------|------------|------|
| RH00   | US    | UP   | P    | V/V <sub>0</sub> | MATERIAL   | UP   |
| 1.18   | 4.24  | 1.04 | 52   | 0.734            | AL         | 0.69 |
| -      | 5.96  | 2.29 | 161  | 0.616            | AL         | 1.60 |
| -      | 6.42  | 2.44 | 185  | 0.620            | AL         | 1.74 |
| -      | 6.60  | 2.73 | 213  | 0.586            | PLEXIGLAS  | 2.73 |
| -      | 8.02  | 3.76 | 356  | 0.531            | AL         | 2.77 |
| -      | 8.96  | 4.52 | 477  | 0.495            | PLEXIGLAS  | 5.62 |
| -      | 9.72  | 4.97 | 570  | 0.488            | AL         | 3.70 |
| -      | 9.89  | 5.16 | 602  | 0.478            | PLEXIGLAS  | 6.46 |
| -      | 10.31 | 5.45 | 663  | 0.471            | PLEXIGLAS  | 6.85 |
| -      | 10.45 | 5.70 | 703  | 0.455            | PLEXIGLAS  | 7.16 |
| -      | 10.68 | 5.75 | 724  | 0.461            | PLEXIGLAS  | 7.24 |
| -      | 12.52 | 7.18 | 1060 | 0.427            | PLEXIGLAS  | 9.10 |

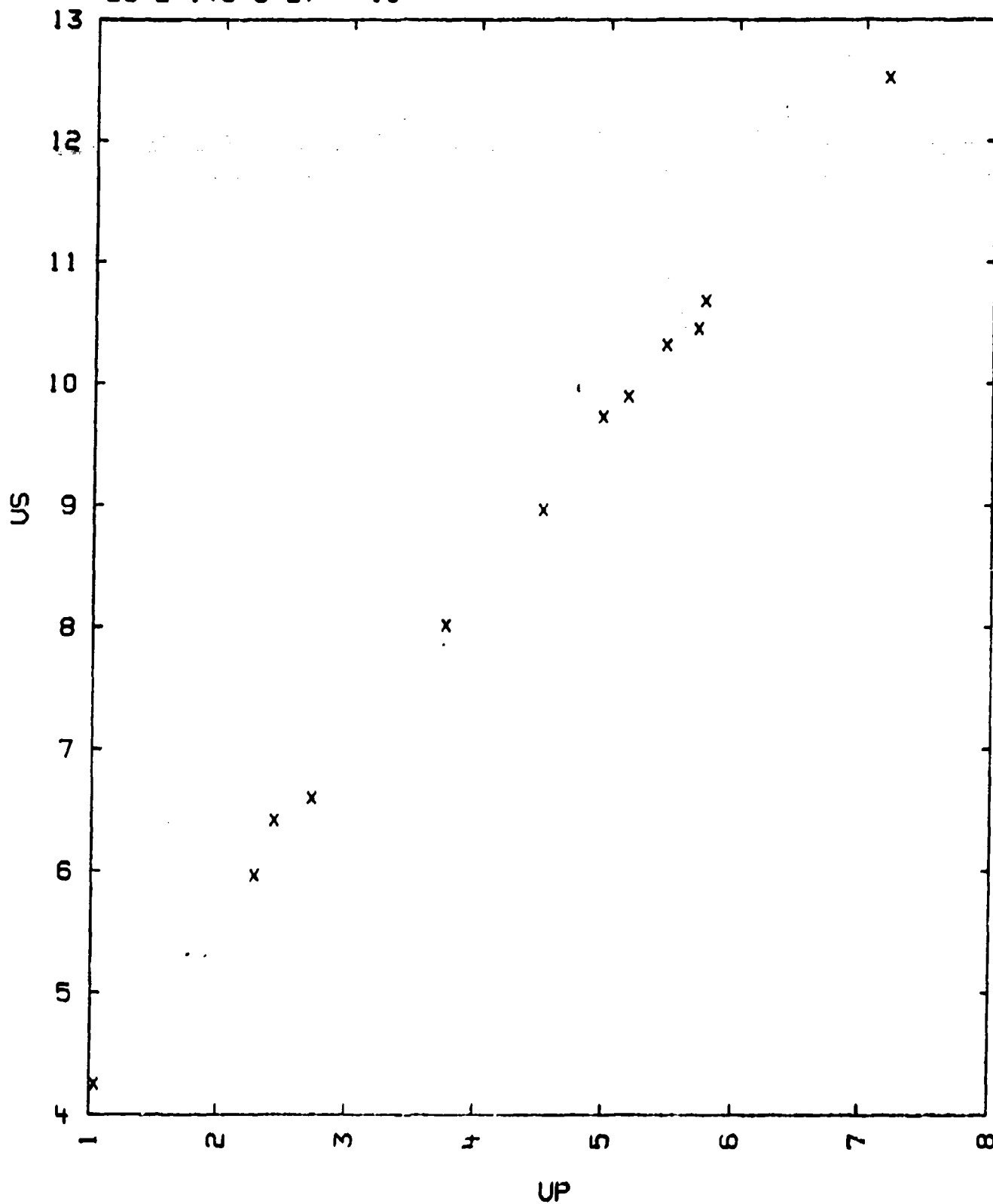
US = 2.96 + 1.34\*UP KM/SEC

SIGMA US = 0.098 KM/SEC

## COMMENTS:

- 1) SOURCE: BAKANOVA, A.A., DUDOLADOV, I.P. AND TRUNIN, R.F.  
FIZIKA TVERDOGO TELA, VOL. 7, NO. 6, PP. 1616 - 1622 (1965)
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION TECHNIQUE B.
- 3) THE FOLLOWING HUGONIOT RELATIONSHIPS FOR THE AL BASE PLATE WERE USED:  
US = 5.25 + 1.39 UP KM/SEC  
RH00 = 2.71 G/CC
- 4) THE ABOVE LINEAR US UP RELATIONSHIP SEEMS TO BREAK UP BELOW  
4.50 KM/SEC. BETWEEN UP = 2.0 AND 8.0 KM/SEC THIS SOURCE GIVES  
A FIT : US = 3.10 + 1.32\*UP KM/SEC .
- 5) A SINGLE POINT US = 16.5 UP = 10.2 P = 2000 V/V<sub>0</sub> = 0.382  
WAS REPORTED BY: ZELDOVICH ET AL  
DOKLADY AKAD. NAUK SSSR (PHYS), VOL. 122, P.48 (1958)  
OR  
SOVIET PHYS., DOKLADY, VOL. 3, P. 905, (1958)

TABLE 1  
PLEXIGLAS (POLYMETHYLMETHACRYLATE)  
23-2-1(5-8-2)---10





23-2-1(5-8-2)---11  
 PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C(O)-O-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)N

M33 PLASTIFIER

95 PERCENT  
 5 PERCENT

V<sub>0</sub> = 0.840 CC/G

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |       |       |       |       |                  | -STANDARD- |
|------------------|-------|-------|-------|-------|------------------|------------|
| RH00             | US    | UFS   | UP    | P     | V/V <sub>0</sub> | UFS        |
| 1.19             | 6.305 | 4.682 | 2.265 | 170   | 0.641            |            |
| -                | 6.305 | 4.744 | 2.290 | 172   | 0.637            |            |
| -                | 6.203 | 4.612 | 2.230 | 164.5 | 0.640            |            |
| -                | 6.289 | 4.409 | 2.140 | 160   | 0.660            |            |
| -                | 6.097 | 4.244 | 2.060 | 149.5 | 0.662            |            |
| -                | 6.068 | 4.394 | 2.135 | 154   | 0.648            |            |
| -                | 6.045 | 4.166 | 2.020 | 146.5 | 0.666            |            |
| -                | 6.105 | 4.251 | 2.060 | 148   | 0.669            |            |
| -                | 5.938 |       | 2.052 | 145   | 0.654            | 2.890      |
| -                | 5.708 |       | 2.037 | 138.5 | 0.643            | 2.840      |
| -                | 6.017 | 4.160 | 2.020 | 144.5 | 0.664            |            |
| -                | 6.017 | 4.150 | 1.995 | 143   | 0.668            |            |
| -                | 5.767 |       | 2.083 | 143   | 0.639            | 2.910      |
| -                | 5.980 |       | 2.002 | 142.5 | 0.665            | 2.820      |
| -                | 5.555 |       | 1.970 | 130   | 0.645            | 2.720      |
| -                | 5.695 |       | 1.948 | 132   | 0.658            | 2.720      |
| -                | 5.675 |       | 1.940 | 131   | 0.658            | 2.710      |
| -                | 5.675 |       | 1.881 | 127   | 0.669            | 2.640      |
| -                | 5.470 |       | 1.874 | 122   | 0.657            | 2.600      |
| -                | 5.543 |       | 1.850 | 122   | 0.668            | 2.570      |
| -                | 5.580 |       | 1.814 | 120.5 | 0.675            | 2.525      |
| -                | 5.562 |       | 1.828 | 121   | 0.671            | 2.545      |
| -                | 5.359 |       | 1.756 | 112   | 0.672            | 2.420      |
| -                | 5.537 |       | 1.723 | 113.5 | 0.689            | 2.400      |
| -                | 5.252 |       | 1.800 | 112   | 0.657            | 2.475      |
| -                | 5.336 |       | 1.771 | 112.5 | 0.668            | 2.445      |
| -                | 5.219 |       | 1.768 | 107   | 0.661            | 2.400      |
| -                | 5.279 |       | 1.780 | 109   | 0.663            | 2.440      |
| -                | 5.241 |       | 1.627 | 101.5 | 0.690            | 2.240      |
| -                | 5.219 |       | 1.642 | 102   | 0.685            | 2.260      |
| -                | 5.123 |       | 1.591 | 97    | 0.689            | 2.180      |
| -                | 5.068 |       | 1.592 | 96    | 0.686            | 2.175      |
| -                | 5.070 |       | 1.558 | 94    | 0.693            | 2.120      |
| -                | 5.070 |       | 1.566 | 95.5  | 0.691            | 2.130      |
| -                | 5.030 |       | 1.538 | 92    | 0.695            | 2.095      |
| -                | 4.975 |       | 1.571 | 93    | 0.684            | 2.145      |
| -                | 4.845 |       | 1.397 | 80.5  | 0.712            | 1.890      |
| -                | 4.757 |       | 1.413 | 80    | 0.703            | 1.910      |
| -                | 4.821 |       | 1.386 | 79.5  | 0.713            | 1.870      |

## PLEXIGLAS (POLYMETHYL METHACRYLATE)

| R/20 | US    | UFS | UP    | P    | V/V0  | UFS   |
|------|-------|-----|-------|------|-------|-------|
| -    | 4.734 |     | 1.402 | 78   | 0.704 | 1.880 |
| -    | 4.062 |     | 1.076 | 52   | 0.735 | 1.400 |
| -    | 4.175 |     | 1.107 | 55   | 0.735 | 1.450 |
| -    | 4.102 |     | 1.045 | 51   | 0.745 | 1.370 |
| -    | 4.128 |     | 1.099 | 54   | 0.734 | 1.450 |
| -    | 4.088 |     | 1.115 | 54   | 0.726 | 1.470 |
| -    | 4.068 |     | 1.053 | 51   | 0.741 | 1.370 |
| -    | 4.055 |     | 1.015 | 49   | 0.750 | 1.320 |
| -    | 4.146 |     | 1.034 | 51   | 0.751 | 1.340 |
| -    | 4.022 |     | 1.046 | 50   | 0.740 | 1.350 |
| -    | 4.071 |     | 1.043 | 50.5 | 0.744 | 1.370 |
| -    | 4.081 |     | 0.988 | 48   | 0.758 | 1.290 |
| -    | 4.158 |     | 0.991 | 49   | 0.762 | 1.300 |
| -    | 4.102 |     | 0.993 | 48   | 0.760 | 1.290 |
| -    | 4.088 |     | 0.977 | 47.5 | 0.761 | 1.280 |
| -    | 3.987 |     | 1.000 | 47.5 | 0.749 | 1.300 |
| -    | 3.987 |     | 1.012 | 48   | 0.746 | 1.305 |
| -    | 4.125 |     | 0.958 | 47   | 0.768 | 1.260 |
| -    | 4.062 |     | 0.956 | 46.5 | 0.766 | 1.257 |
| -    | 3.955 |     | 0.935 | 44   | 0.764 | 1.210 |
| -    | 3.897 |     | 0.917 | 42.5 | 0.765 | 1.190 |
| -    | 3.882 |     | 0.937 | 43   | 0.759 | 1.200 |
| -    | 3.903 |     | 0.930 | 43.5 | 0.760 | 1.220 |
| -    | 3.793 |     | 0.880 | 40   | 0.768 | 1.130 |
| -    | 3.770 |     | 0.858 | 38.5 | 0.772 | 1.110 |

US = 2.239 + 1.798 UP KM/SEC, SIG.US = 0.11 KM/SEC

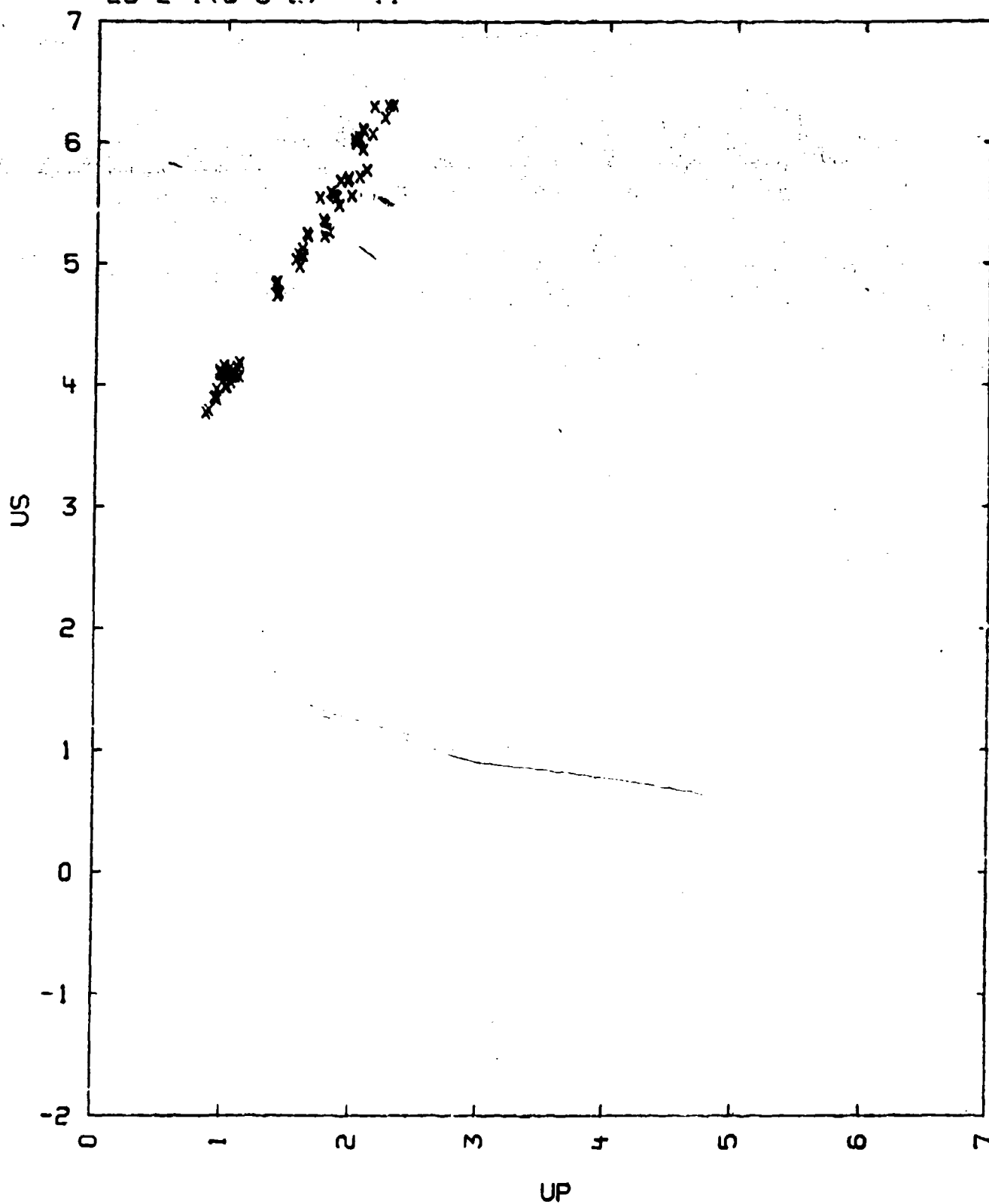
## COMMENTS:

- 1) SOURCE: BERGER J. AND FAUQUIGNON C.  
PRIVATE COMMUNICATION (1964), B.P. NO. 7, SEVRAN, FRANCE
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIALS ALUMINUM AU4G
3. SAMPLE DIMENSIONS FOR THE US MEASUREMENTS: 2.0 CM DIAMETER  
0.5 CM THICKNESS  
SAMPLE DIMENSIONS FOR THE UFS MEASUREMENTS: 2.0 CM DIAMETER  
0.25 CM THICKNESS

TABLE I

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---11



23-2-1(5-8-2)---12  
POLYMETHYL METHACRYLATE

(H<sub>2</sub>-C-C(H<sub>3</sub>)-C-CH<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)N

V<sub>0</sub> = 0.847 CC/G.

C<sub>0</sub> = 2.71 KM/SEC. SIGMA = 0.03 KM/SEC.

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS. X DESIGNATES THE SAMPLE THICKNESS WHICH IS GIVEN IN MM.

TABLE

| RH00 | US   | UP    | P    | V/V <sub>0</sub> | X   |
|------|------|-------|------|------------------|-----|
| 1.18 | 4.95 | 1.420 | 82.4 | 0.715            | 10  |
| -    | 4.62 | 1.210 | 66.0 | 0.738            | 15  |
| -    | 4.40 | 1.088 | 56.6 | 0.753            | 20  |
| -    | 4.21 | 0.990 | 49.2 | 0.765            | 25  |
| -    | 4.06 | 0.890 | 42.6 | 0.781            | 30  |
| -    | 3.88 | 0.780 | 35.7 | 0.799            | 35  |
| -    | 3.66 | 0.650 | 28.1 | 0.822            | 40  |
| -    | 3.46 | 0.538 | 22.0 | 0.845            | 45  |
| -    | 3.35 | 0.455 | 18.0 | 0.864            | 50  |
| -    | 3.30 | 0.383 | 14.9 | 0.884            | 55  |
| -    | 3.24 | 0.325 | 12.4 | 0.900            | 60  |
| -    | 3.21 | 0.283 | 10.7 | 0.912            | 65  |
| -    | 3.17 | 0.245 | 9.2  | 0.923            | 70  |
| -    | 3.14 | 0.225 | 8.3  | 0.928            | 75  |
| -    | 3.13 | 0.200 | 7.4  | 0.936            | 80  |
| -    | 3.10 | 0.145 | 5.3  | 0.953            | 100 |

US = 2.95 + 0.85 UP KM/SEC. FROM UP = 0.145 TO 0.455 KM/SEC.

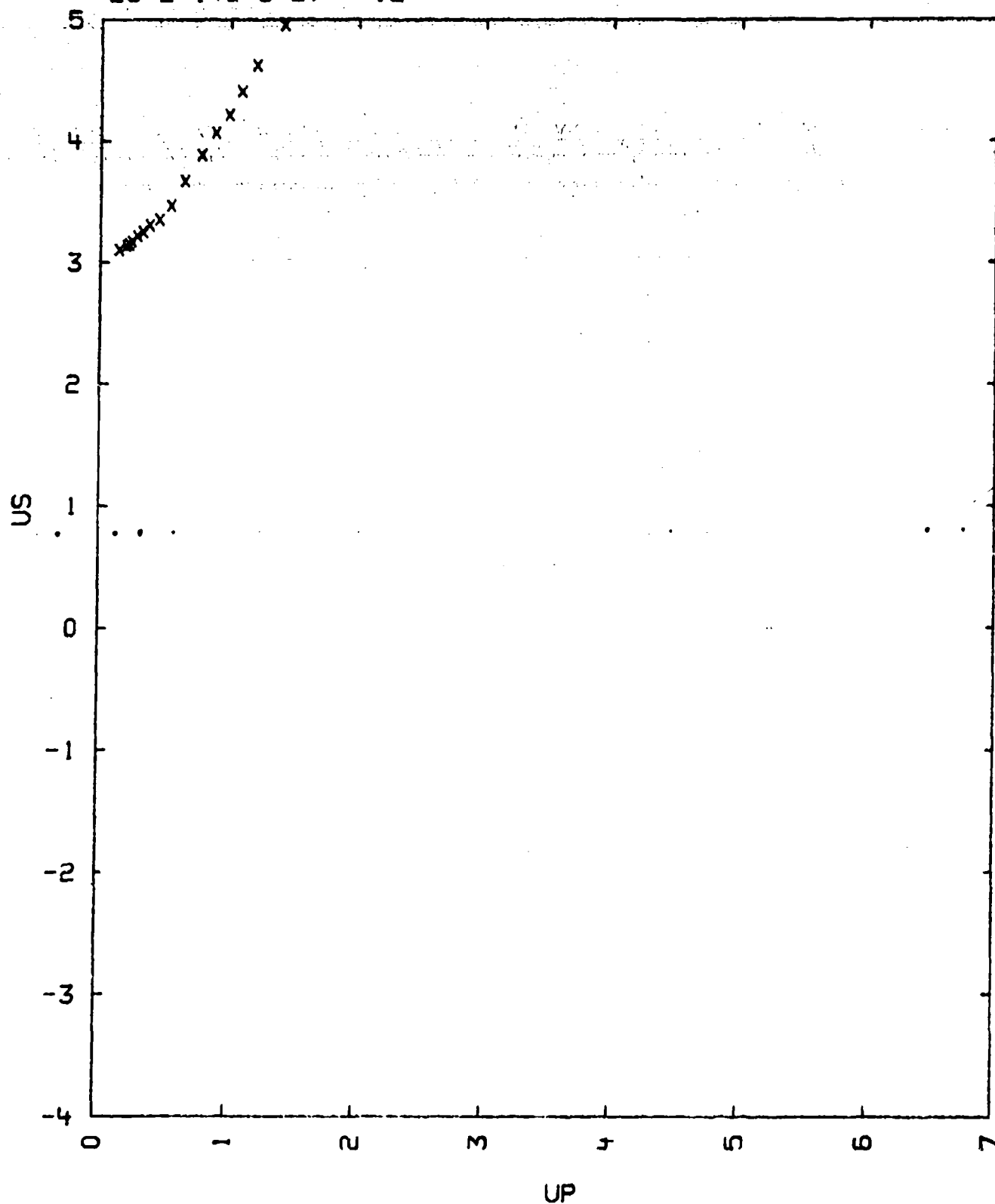
US = 2.56 + 1.69 UP KM/SEC. FROM UP = 0.538 TO 1.420 KM/SEC.

COMMENTS:

- 1) SOURCE: LIDDIAKD T. P.  
THE FOURTH SYMPOSIUM ON DETONATION, VOL. 1, 8-47 (1965)
- 2) EXPERIMENTAL TECHNIQUE: A TIME RESOLVED SHADOWGRAPH OF THE POSITION OF THE SHOCK FRONT AND A SMALL THIN FOIL WHICH IS ACCELERATED BY THE INITIAL PULSE REACHING THE FREE SURFACE, YIELDED US AND FOIL VELOCITY (UFS)  
DATA REDUCTION TECHNIQUE: D., WITH THE RELATIONSHIP  $2UP = UFS$ .
- 3, C<sub>0</sub> WAS MEASURED WITH PRESSURE WAVES PRODUCED IN THE SAMPLE BY AN EXPLODING WIRE.

TABLE I

POLYMETHYLMETHACRYLATE  
23-2-1(5-8-2)---12



23-2-1(5-B-2)---13  
 PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-O<sub>2</sub>-C-H<sub>3</sub>)<sub>N</sub> = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)<sub>N</sub>

V<sub>0</sub> = 0.849 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC.  
 PRESSURE IN KILOBARS, 1 REFERS TO IMPACT SURFACE OF SAMPLE, 2 REFERS TO  
 BACK SURFACE OF SAMPLE, AV REFERS TO THE AVERAGE VALUE ACROSS THE SAMPLE

TABLE

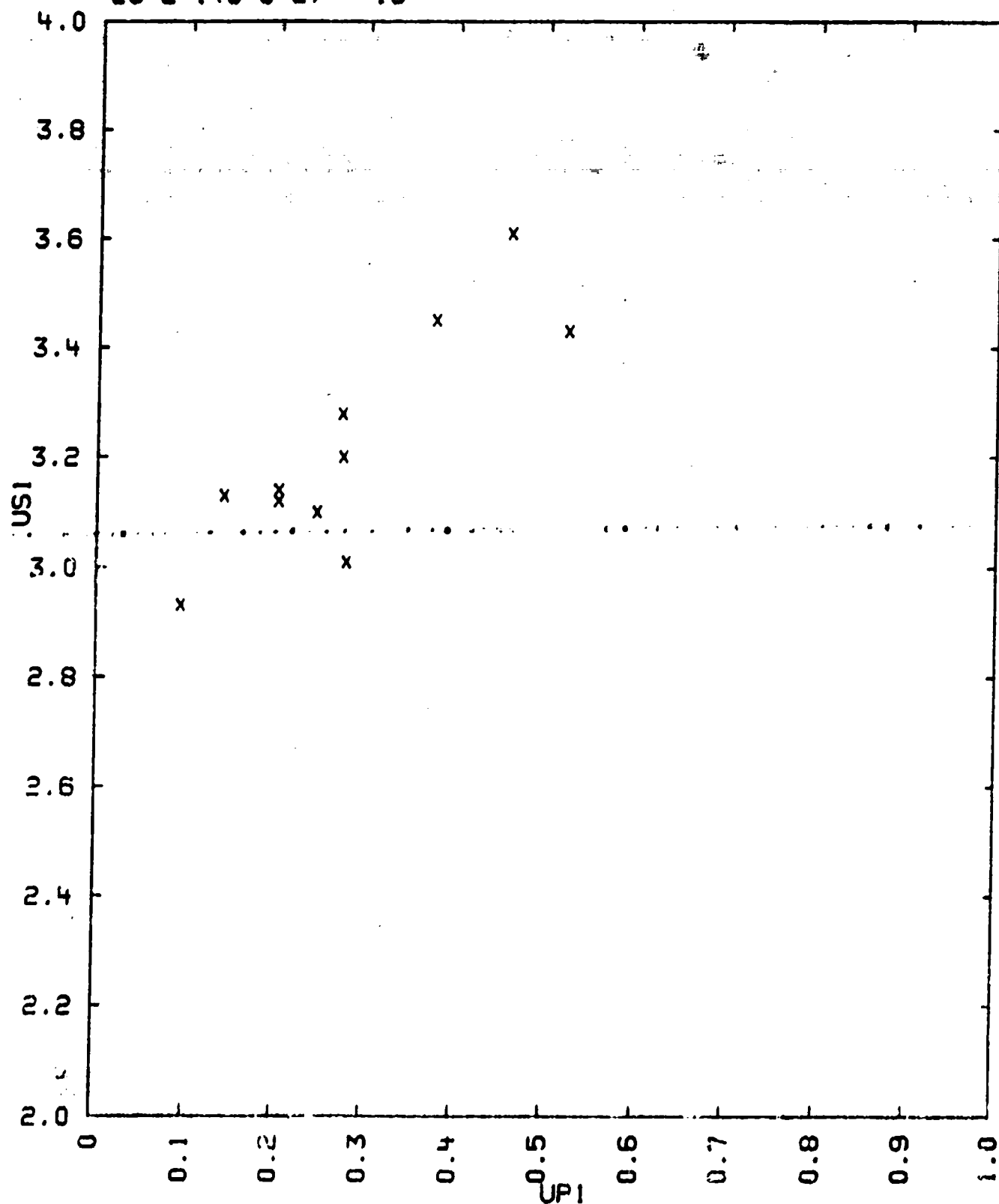
| RHO0  | U <sub>S1</sub> | U <sub>P1</sub> | P <sub>1</sub> | V <sub>1</sub> /V <sub>0</sub> | U <sub>SAV</sub> | P <sub>2</sub> |
|-------|-----------------|-----------------|----------------|--------------------------------|------------------|----------------|
| 1.178 | 2.93            | 0.0943          | 3.25           | 0.9678                         | 2.98             |                |
| -     | 3.13            | 0.142           | 5.24           | 0.9545                         | 3.00             | 4.9            |
| -     | 3.12            | 0.203           | 7.46           | 0.9348                         | 3.04             | 6.3            |
| -     | 3.14            | 0.203           | 7.50           | 0.9353                         | 3.06             | 6.4            |
| -     | 3.10            | 0.248           | 8.99           | 0.9207                         | 3.04             |                |
| -     | 3.01            | 0.280           | 9.94           | 0.9070                         | 3.16             | 8.9            |
| -     | 3.20            | 0.276           | 10.4           | 0.9138                         |                  |                |
| -     | 3.28            | 0.274           | 10.6           | 0.9168                         | 3.13             | 9.0            |
| -     | 3.45            | 0.377           | 15.3           | 0.8920                         |                  |                |
| -     | 3.61            | 0.459           | 19.5           | 0.8728                         |                  |                |
| -     | 3.43            | 0.524           | 21.2           | 0.8476                         |                  |                |

U<sub>S1</sub> = 2.84 + 1.38\*U<sub>P1</sub> KM/SEC FOR U<sub>P</sub> BETWEEN 0.09 AND 0.52 KM/SEC  
 SIGMA U<sub>S1</sub> = 0.11 KM/SEC

COMMENTS:

- 1) SOURCE: HALPIN, W. J. AND GRAHAM, R. A.  
 SHOCK WAVE COMPRESSION OF PLEXIGLAS FROM 3 TO 20 KBAR  
 PRESENTED AT THE FOURTH SYMPOSIUM ON DETONATION  
 P. 388, OCT. 1965. HELD AT THE U. S. NAVAL ORDNANCE  
 LABORATORY, WHITE OAK, SILVER SPRING MARYLAND.
- 2) EXPERIMENTAL TECHNIQUE I  
 DATA REDUCTION TECHNIQUE C
- 3) THE PRESSURE DIFFERENCE BETWEEN THE IMPACT SURFACE AND THE BACK  
 SURFACE OF THE SAMPLE SHOWS A DECREASE OF PRESSURE WHILE THE SHOCK  
 WAVE TRAVERSES THE SAMPLE.
- 4) THE PRESSURES MEASURED AT THE IMPACT AND BACK SURFACE SUGGEST  
 A PRESSURE ATTENUATION OF THE SHOCK WAVE.

TABLE 1  
PLEXIGLAS (POLYMETHYLMETHACRYLATE)  
23-2-1(5-8-2)---13



23-2-1(5-8-2)---14  
POLYMETHYLMETHACRYLATE

(H2-C-C(C-H3)-C-O2-C-H3)N = (C5-H8-O2)N

$V_0 = 0.862 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KBARS.

TABLE

| RH00 | US    | UP   | P    | V/V0  |
|------|-------|------|------|-------|
| 1.16 | 2.992 | 0.27 | 9.4  | 0.91  |
| -    | 3.50  | 0.40 | 16.2 | 0.894 |
| -    | 4.12  | 0.77 | 36.8 | 0.812 |
| -    | 4.45  | 1.06 | 54.5 | 0.762 |
| -    | 4.65  | 1.24 | 67.  | 0.735 |
| -    | 5.1   | 1.60 | 95.  | 0.69  |

$US = 2.47 + 2.49 \cdot UP - 0.54 \cdot UP^{0.2} \text{ KM/SEC.}$

$SIGMA US = 0.11 \text{ KM/SEC.}$

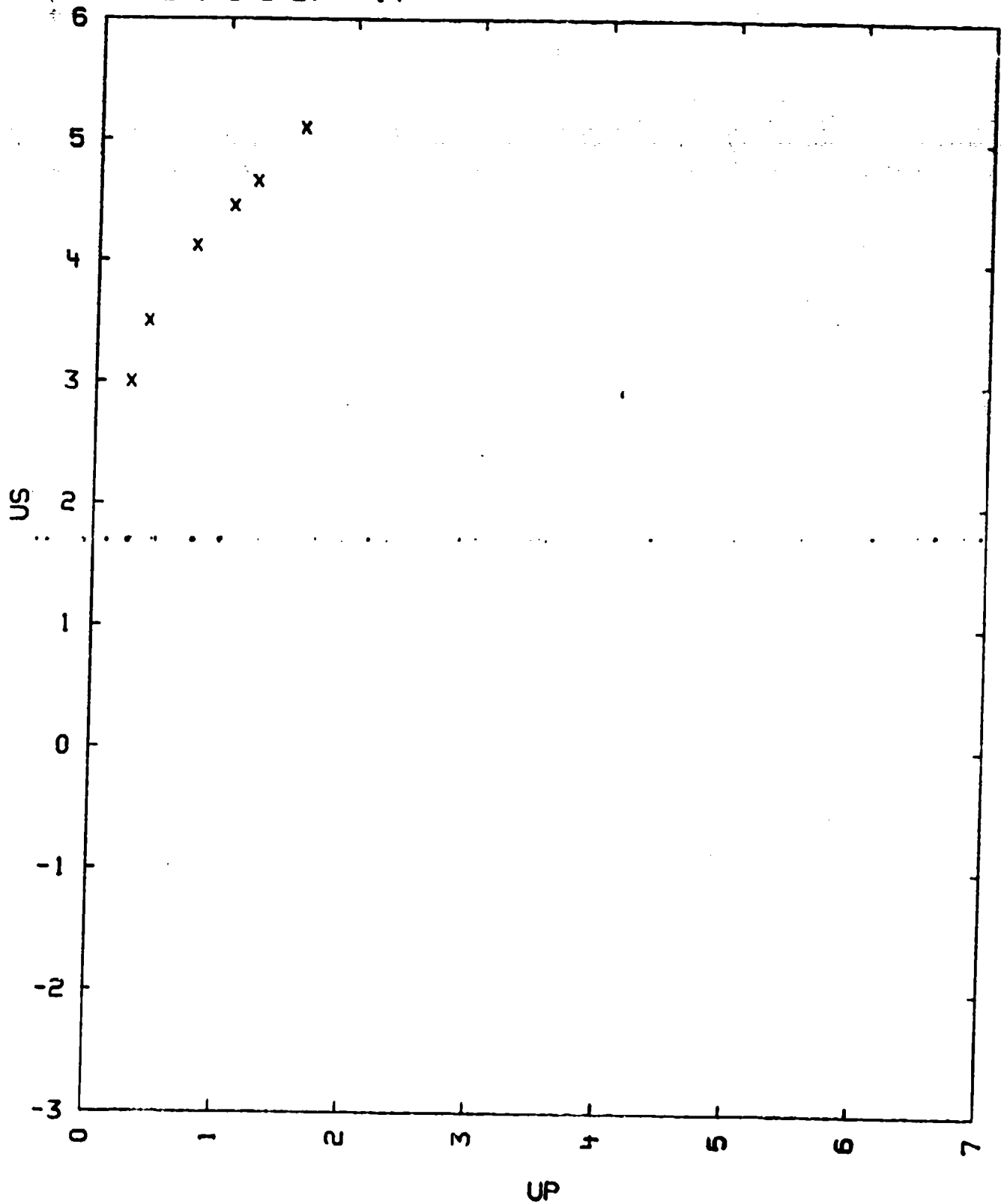
## COMMENTS:

- 1) SOURCE: DAPOIGNY, J., KIEFFER, J. AND VODAR, B.  
COMPTES RENDUS, VOL. 245, P. 1502 (1957)
- 2) EXPERIMENTAL TECHNIQUE J1  
DATA REDUCTION METHOD E (EXCEPT FOR THE 95 KBAR POINT WHICH WAS CALCULATED FROM THE MOTION OF THE EXPLOSIVE-SAMPLE INTERFACE.
- 3) THE DETONATION FRONT MOVED PARALLEL TO THE SAMPLE SURFACE GENERATING A STRONGLY ATTENUATING SHOCK WAVE AT SOME ANGLE TO THE SAMPLE-EXPLOSIVE INTERFACE. THE ABOVE POINTS WERE OBTAINED ON A SINGLE EXPERIMENT.
- 4) THE SHOCK-PARTICLE VELOCITY FUNCTION CURVES TOWARDS THE UP AXIS AS IN 23-2-1(5-8-2)---7, WHERE A SIMILAR SHOCK CONFIGURATION WAS USED.



TABLE 1

POLYMETHYLMETHACRYLATE  
23-2-1(5-8-2)---14



23-2-1(5-8-2)---18  
 PLEXIGLAS (POLYMETHYLMETHACRYLATE)

(H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C(O)-O-C-H<sub>3</sub>)N = (C<sub>5</sub>-H<sub>8</sub>-O<sub>2</sub>)N

V<sub>0</sub> = 0.847 CC/G.

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC.,  
 AND PRESSURE IN KILOBARS.

TABLE

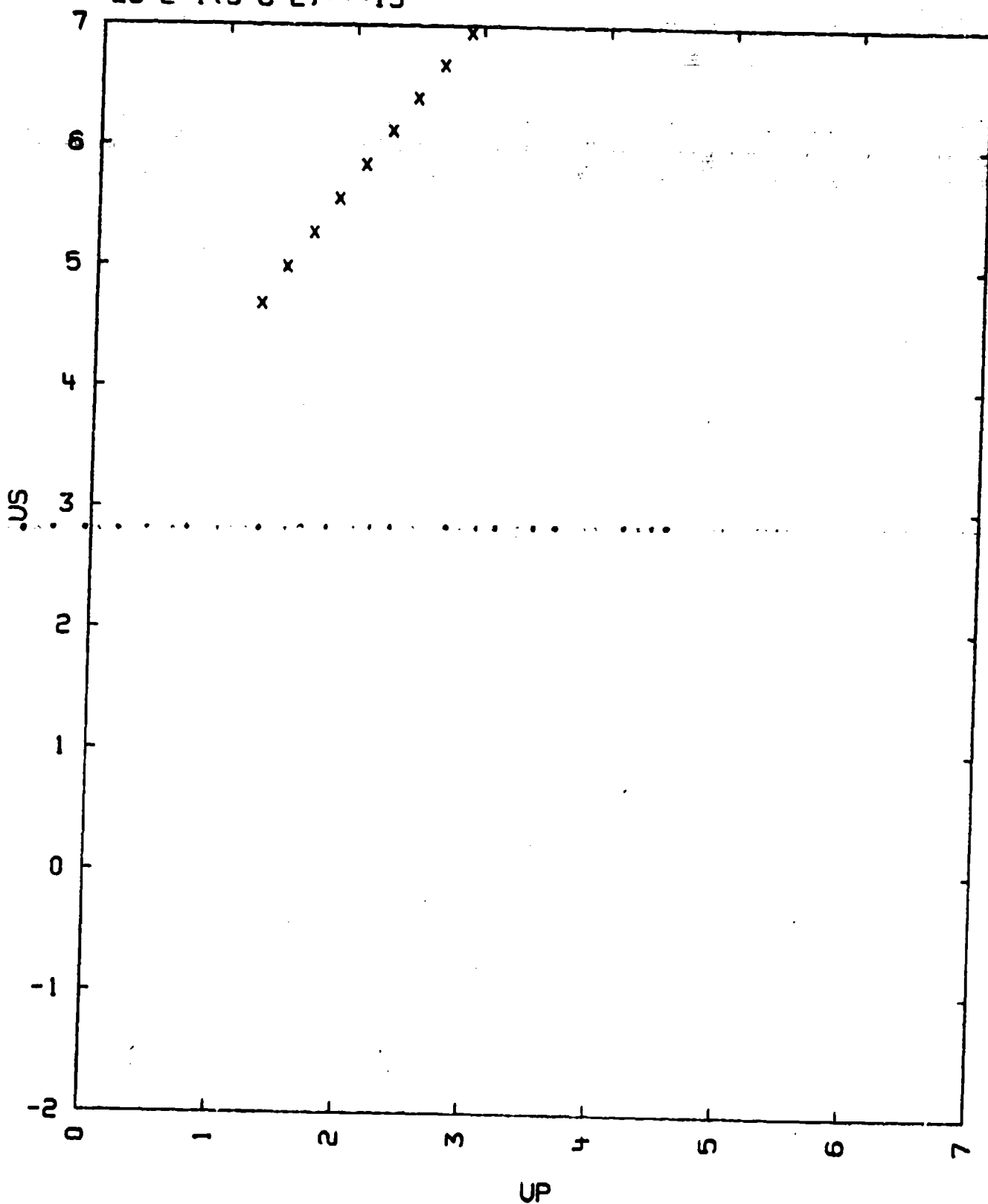
| RH00 | US   | UFS  | UP   | P     | V/V <sub>0</sub> |
|------|------|------|------|-------|------------------|
| 1.18 | 4.68 | 2.60 | 1.30 | 71.8  | 0.722            |
| -    | 4.98 | 3.00 | 1.50 | 88.0  | 0.699            |
| -    | 5.27 | 3.40 | 1.70 | 106.0 | 0.677            |
| -    | 5.55 | 3.80 | 1.90 | 124.0 | 0.658            |
| -    | 5.84 | 4.20 | 2.10 | 145.0 | 0.640            |
| -    | 6.12 | 4.60 | 2.30 | 166.0 | 0.624            |
| -    | 6.39 | 5.00 | 2.50 | 189.0 | 0.609            |
| -    | 6.67 | 5.40 | 2.70 | 213.0 | 0.595            |
| -    | 6.94 | 5.80 | 2.90 | 238.0 | 0.582            |

US = 2.87 + 1.41 UP KM/SEC. SIGMA US = 0.01 KM/SEC.

COMMENTS:

- 1) SOURCE: COLEBURN, N. L.  
 NAVHEPS REPORT 6026, 1960  
 U. S. NAVAL ORDNANCE LAB., WHITE OAK, MARYLAND.
- 2) EXPERIMENTAL TECHNIQUE C AND B.  
 DATA REDUCTION TECHNIQUE D, ASSUMING 2UP = UFS
- 3) EXPERIMENTAL ERROR IN THE FREE-SURFACE VELOCITY (UFS) IS 3 PERCENT.  
 A CORRECTION FOR SHOCK TILT WAS APPLIED, REDUCING THE MEASURED  
 ERROR IN US BY A FACTOR OF 10. THE ESTIMATED EXPERIMENTAL ERROR IN  
 US IS 0.5 PERCENT. THE SHOCK FRONT WAS TILTED WITH RESPECT TO THE  
 SURFACE BY 14 AND 22 DEGREES, UFS AND UP WERE ASSUMED PARALLEL TO  
 EACH OTHER AND PERPENDICULAR TO THE SHOCK FRONT.
4. THE VELOCITIES MEASURED WITH METHOD B WERE BE 10 PERCENT FASTER  
 THAN THOSE MEASURED WITH METHOD C, BECAUSE OF THE LARGE AMOUNT OF GAS  
 COMPRESSED IN THE FREE SURFACE GAP. EXPERIMENTS WITH METHOD B WERE  
 ACCORDINGLY CORRECTED BY THIS FACTOR.

TABLE I  
PLEXIGLAS (POLYMETHYLMETHACRYLATE)  
23-2-1(5-8-2)---15



23-2-1(5-8-2)---18  
LUCITE (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-O<sub>2</sub>-C-H<sub>3</sub>)N

V<sub>0</sub> = 0.845 CC/G

CL = 2.69 KM/SEC

C<sub>0</sub> = 2.17 KM/SEC

CS = 1.38 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |                  | -----STANDARD----- |        |
|------------------|------|------|------|------------------|--------------------|--------|
| RHOO             | US   | UP   | P    | V/V <sub>0</sub> | MATERIAL           | US(ST) |
| 1.180            | 4.88 | 1.25 | 69.  | 0.7318           | 2024 AL            | 6.44   |
| 1.180            | 4.65 | 1.28 | 70.  | 0.7247           | 2024 AL            | 6.47   |
| 1.180            | 4.64 | 1.28 | 70.  | 0.7241           | 2024 AL            | 6.47   |
| 1.180            | 5.20 | 1.64 | 101. | 0.6846           | 2024 AL            | 6.81   |
| 1.180            | 6.00 | 2.10 | 149. | 0.6500           | 2024 AL            | 7.28   |
| 1.180            | 6.18 | 2.19 | 160. | 0.6456           | 2024 AL            | 7.38   |
| 1.186            | 9.56 | 4.66 | 528. | 0.5126           | 2024 AL            | 9.95   |
| 1.186            | 9.74 | 5.09 | 588. | 0.4774           | 2024 AL            | 10.35  |

US = 2.551 + 1.645·UP KM/SEC FOR UP LESS THAN 3 KM/SEC  
SIG US = 0.039 KM/SEC

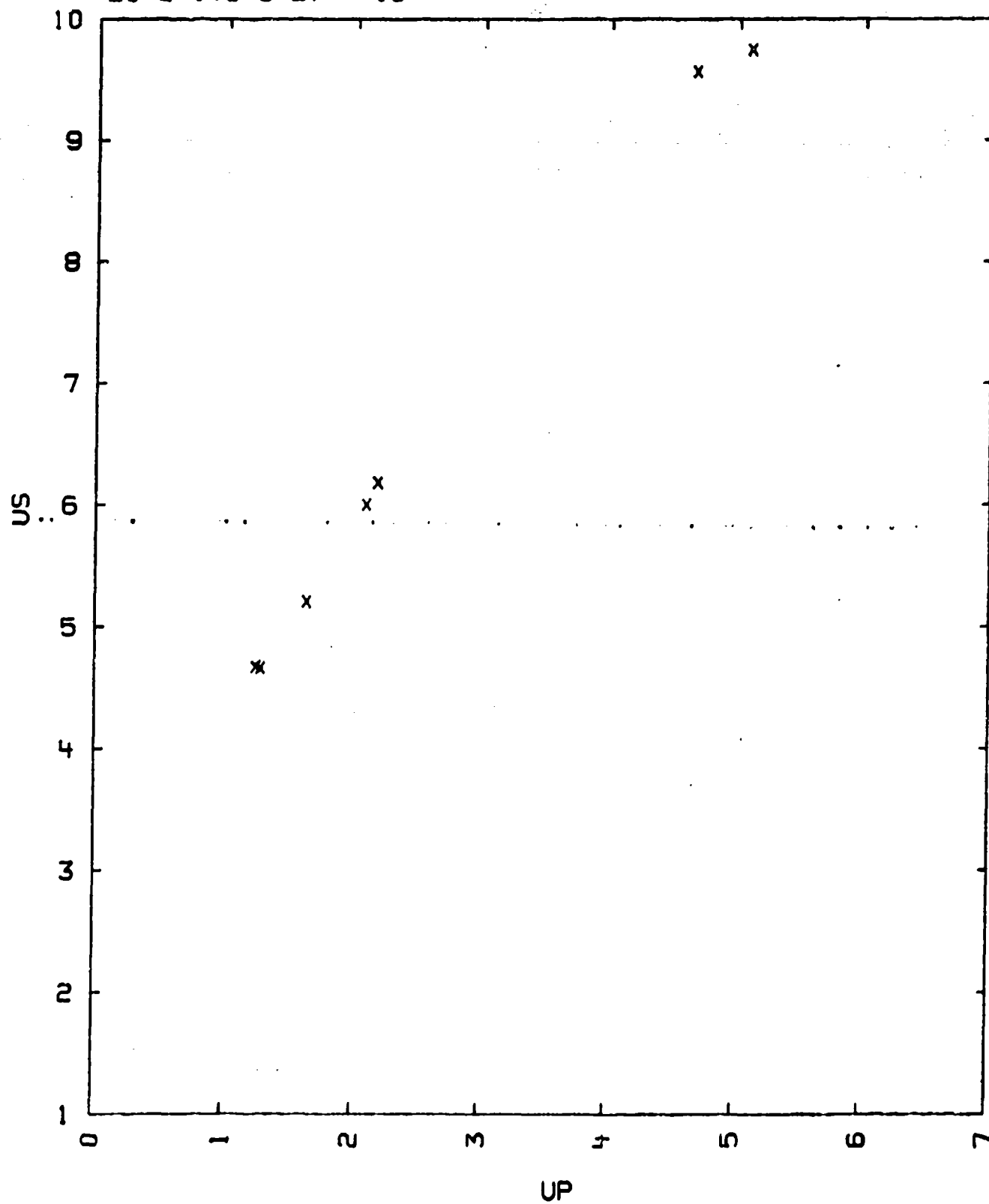
COMMENTS:

- 1) SOURCE: MCQUEEN, R.O., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE : B  
DATA REDUCTION TECHNIQUE : B

TABLE I

LUCITE (POLYMETHYLMETHACRYLATE)

23-2-1(5-8-2)---16



23-2-1(5-8-2)---17

PLEXIGLAS (POLYMETHYLMETHACRYLATE)

POLYMETHYLMETHACRYLATE (H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C-02-C-H<sub>3</sub>)NV<sub>0</sub> = 0.841 CC/G

CL = 2.72 KM/SEC

C<sub>0</sub> = 2.19 KM/SEC

CS = 1.40 -

CB = 2.18 -

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RHO0             | US   | UP   | P    | V/V0   | MATERIAL           | US(ST) |
| 1.186            | 3.45 | 0.54 | 22.  | 0.8435 | 2024 AL            | 5.79   |
| 1.186            | 3.70 | 0.72 | 32.  | 0.8054 | 2024 AL            | 5.94   |
| 1.189            | 3.76 | 0.76 | 34.  | 0.7979 | 2024 AL            | 5.98   |
| 1.186            | 3.72 | 0.76 | 34.  | 0.7957 | 2024 AL            | 5.98   |
| 1.189            | 3.74 | 0.79 | 35.  | 0.7888 | 921-T AL           | 5.76   |
| 1.186            | 4.04 | 0.97 | 46.  | 0.7599 | 2024 AL            | 6.17   |
| 1.186            | 4.05 | 0.98 | 47.  | 0.7580 | 2024 AL            | 6.18   |
| 1.180            | 4.26 | 1.13 | 57.  | 0.7347 | 2024 AL            | 6.32   |
| 1.182            | 4.28 | 1.15 | 58.  | 0.7313 | 2024 AL            | 6.33   |
| 1.180            | 4.24 | 1.15 | 58.  | 0.7288 | 2024 AL            | 6.33   |
| 1.186            | 4.78 | 1.34 | 76.  | 0.7197 | 2024 AL            | 6.53   |
| 1.186            | 4.78 | 1.34 | 76.  | 0.7197 | 2024 AL            | 6.53   |
| 1.189            | 4.67 | 1.34 | 74.  | 0.7131 | 2024 AL            | 6.53   |
| 1.186            | 4.66 | 1.36 | 75.  | 0.7082 | 2024 AL            | 6.54   |
| 1.184            | 4.59 | 1.37 | 74.  | 0.7015 | 2024 AL            | 6.55   |
| 1.189            | 4.70 | 1.46 | 82.  | 0.6894 | 921-T AL           | 6.43   |
| 1.180            | 5.04 | 1.62 | 96.  | 0.6786 | 2024 AL            | 6.79   |
| 1.180            | 5.05 | 1.63 | 97.  | 0.6772 | 2024 AL            | 6.80   |
| 1.186            | 5.33 | 1.69 | 107. | 0.6829 | 2024 AL            | 6.88   |
| 1.186            | 5.33 | 1.69 | 107. | 0.6829 | 2024 AL            | 6.88   |
| 1.189            | 5.14 | 1.74 | 106. | 0.6615 | 2024 AL            | 6.91   |
| 1.186            | 5.30 | 1.78 | 112. | 0.6642 | 2024 AL            | 6.95   |
| 1.189            | 5.30 | 1.87 | 118. | 0.6472 | 921-T A            | 6.86   |
| 1.189            | 5.30 | 1.87 | 118. | 0.6472 | 921-T AL           | 6.86   |
| 1.186            | 5.51 | 1.89 | 124. | 0.6570 | 2024 AL            | 7.07   |
| 1.180            | 5.81 | 2.17 | 149. | 0.6265 | 2024 AL            | 7.33   |
| 1.189            | 6.24 | 2.37 | 176. | 0.6202 | 2024 AL            | 7.55   |
| 1.186            | 6.24 | 2.39 | 176. | 0.6186 | 2024 AL            | 7.55   |
| 1.189            | 6.32 | 2.39 | 180. | 0.6218 | 921-T AL           | 7.43   |
| 1.186            | 6.32 | 2.40 | 180. | 0.6203 | 2024 AL            | 7.58   |
| 1.186            | 6.19 | 2.42 | 178. | 0.6090 | 2024 AL            | 7.58   |
| 1.186            | 6.44 | 2.47 | 189. | 0.6165 | 2024 AL            | 7.66   |
| 1.189            | 6.32 | 2.48 | 186. | 0.6076 | 921-T AL           | 7.52   |
| 1.186            | 6.69 | 2.64 | 209. | 0.6054 | 2024 AL            | 7.83   |
| 1.186            | 6.69 | 2.64 | 209. | 0.6054 | 2024 AL            | 7.83   |
| 1.186            | 6.84 | 2.79 | 226. | 0.5921 | 2024 AL            | 7.97   |
| 1.186            | 6.83 | 2.79 | 226. | 0.5915 | 2024 AL            | 7.97   |
| 1.186            | 6.83 | 2.83 | 229. | 0.5857 | 2024 AL            | 8.01   |

## PLEXIGLAS (POLYMETHYLMETHACRYLATE)

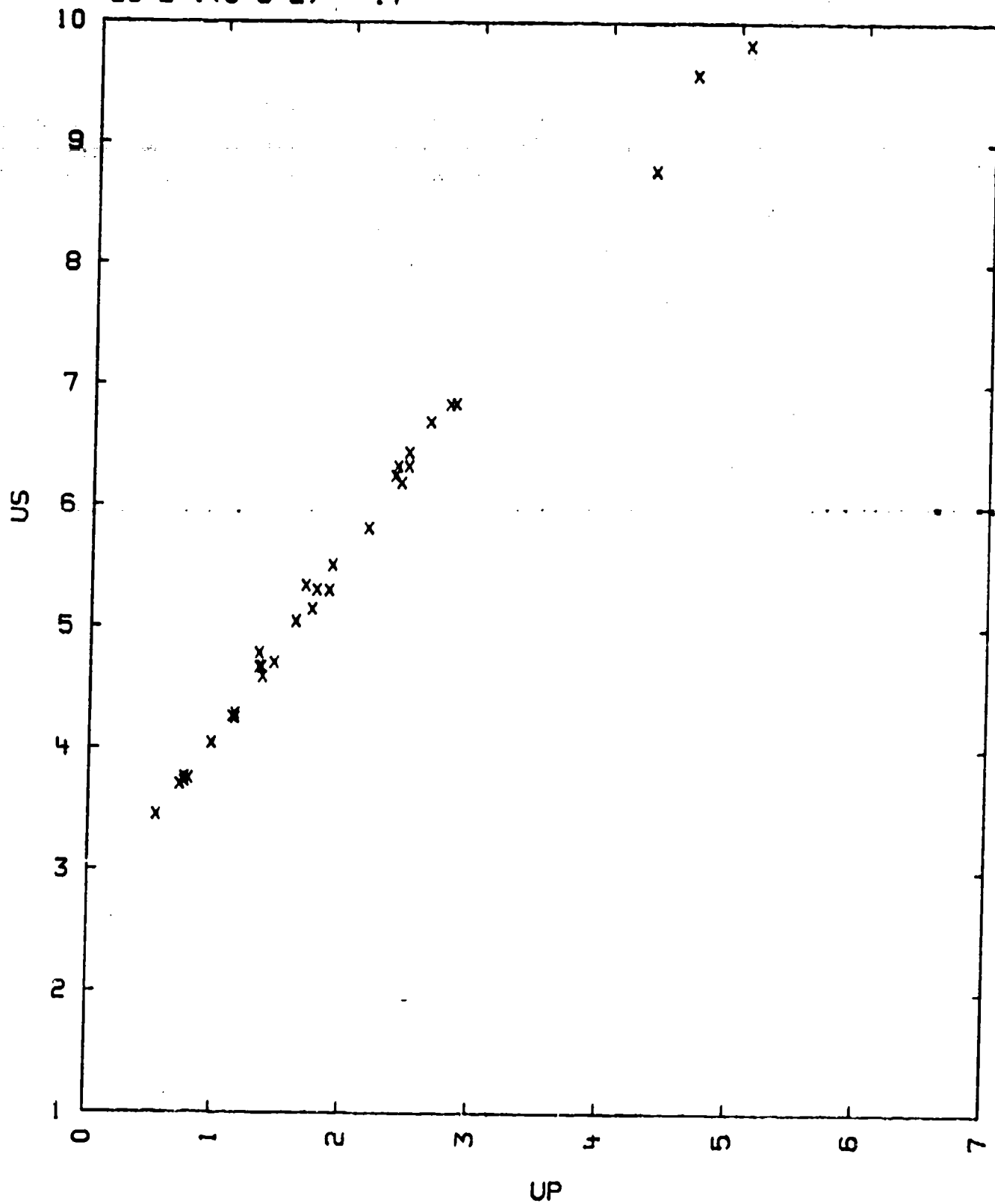
| RHOO  | US   | UP   | P    | V/VO   | MATERIAL | US(ST) |
|-------|------|------|------|--------|----------|--------|
| 1.188 | 6.82 | 2.83 | 229. | 0.5850 | 2024 AL  | 8.01   |
| 1.188 | 8.77 | 4.35 | 452. | 0.5040 | 2024 AL  | 9.57   |
| 1.188 | 8.76 | 4.35 | 452. | 0.5034 | 2024 AL  | 9.57   |
| 1.189 | 9.56 | 4.68 | 530. | 0.5126 | 2024 AL  | 9.95   |
| 1.189 | 9.81 | 5.07 | 591. | 0.4832 | 2024 AL  | 10.35  |

$US = 2.572 + 1.536 \cdot UP$  KM/SEC FOR UP BELOW 3 KM/SEC  
 $SIG US = 0.084$  KM/SEC

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE : B  
DATA REDUCTION TECHNIQUE : B

TABLE I  
PLEXIGLAS (POLYMETHYLMETHACRYLATE)  
23-2-1(5-8-2)---17





23-2-1(5-8-2)---18  
 PLEXIGLAS (POLYMETHYLMETHACRYLATE)

(H<sub>2</sub>-C-C(C-H<sub>3</sub>)-C(O)-O-C-H<sub>3</sub>)N

V<sub>0</sub> = 0.8475

THE TABLE LISTS RHOO IN G/CC, VELOCITIES IN KM/SEC AND P IN KBARS.  
 CU = COPPER, FS = FANSTEEL AND WF = WEIGHTING FACTOR.

TABLE

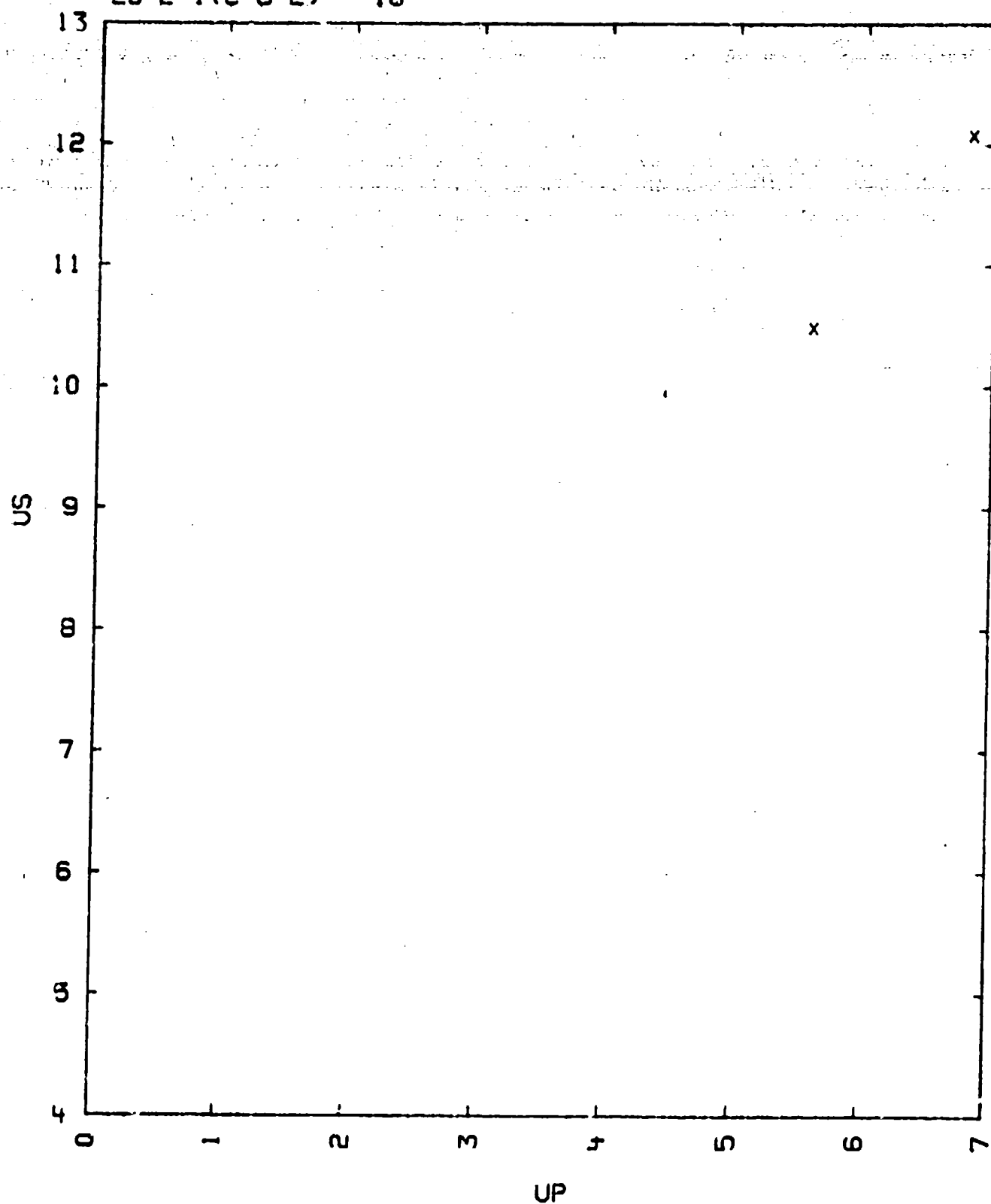
| - - - - - SAMPLE - - - - - |        |       |      |                  | - IMPACTOR - |       |
|----------------------------|--------|-------|------|------------------|--------------|-------|
| RHOO                       | US     | UP    | P    | V/V <sub>0</sub> | MAT          | U     |
| 1.180                      | 10.482 | 5.592 | 692. | .4666            | CU           | 6.907 |
| 1.180                      | 12.075 | 6.833 | 981. | .4300            | FS           | 7.902 |

US = 3.10 + 1.32\*UP KM/SEC (3.0 <UP< 8.0)

COMMENTS:

- 1) SOURCE: ISBELL W.M., SHIPMAN F.H. AND JONES A.H.  
 HUGONIOT EQUATION OF STATE OF ELEVEN MATERIALS TO FIVE MBARS.  
 MATERIALS SCIENCE LABORATORY REPORT: MSL-68-1
- 2) EXPERIMENTAL TECHNIQUE: A  
 DATA REDUCTION METHOD : A
- 3) NOMINAL UNCERTAINTIES ARE: (SIG.US)/US = .005 AND (SIG.U)/U = .005

TABLE 1  
PLEXIGLAS (POLYMETHYLMETHACRYLATE)  
23-2-1(5-8-2)---18



23-2-1(5-12-1)---1  
N-AMYL ALCOHOL

H3-C(H2)3-C(H2)-O-H = C5-H12-O

T0 = 19-23 DEG. CENTIGRADE  
V0 = 1.227-1.236 CC/G

CO(20 DEG. C) = 1.294 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| T0 | RH00   | US   | UP    | P     | V/V0  |
|----|--------|------|-------|-------|-------|
| 23 | 0.8091 | 5.81 | 2.465 | 115.9 | 0.576 |
| 19 | 0.8150 | 4.26 | 1.466 | 50.9  | 0.656 |

$$US = 1.98 + 1.55 \cdot UP \text{ KM/SEC}$$

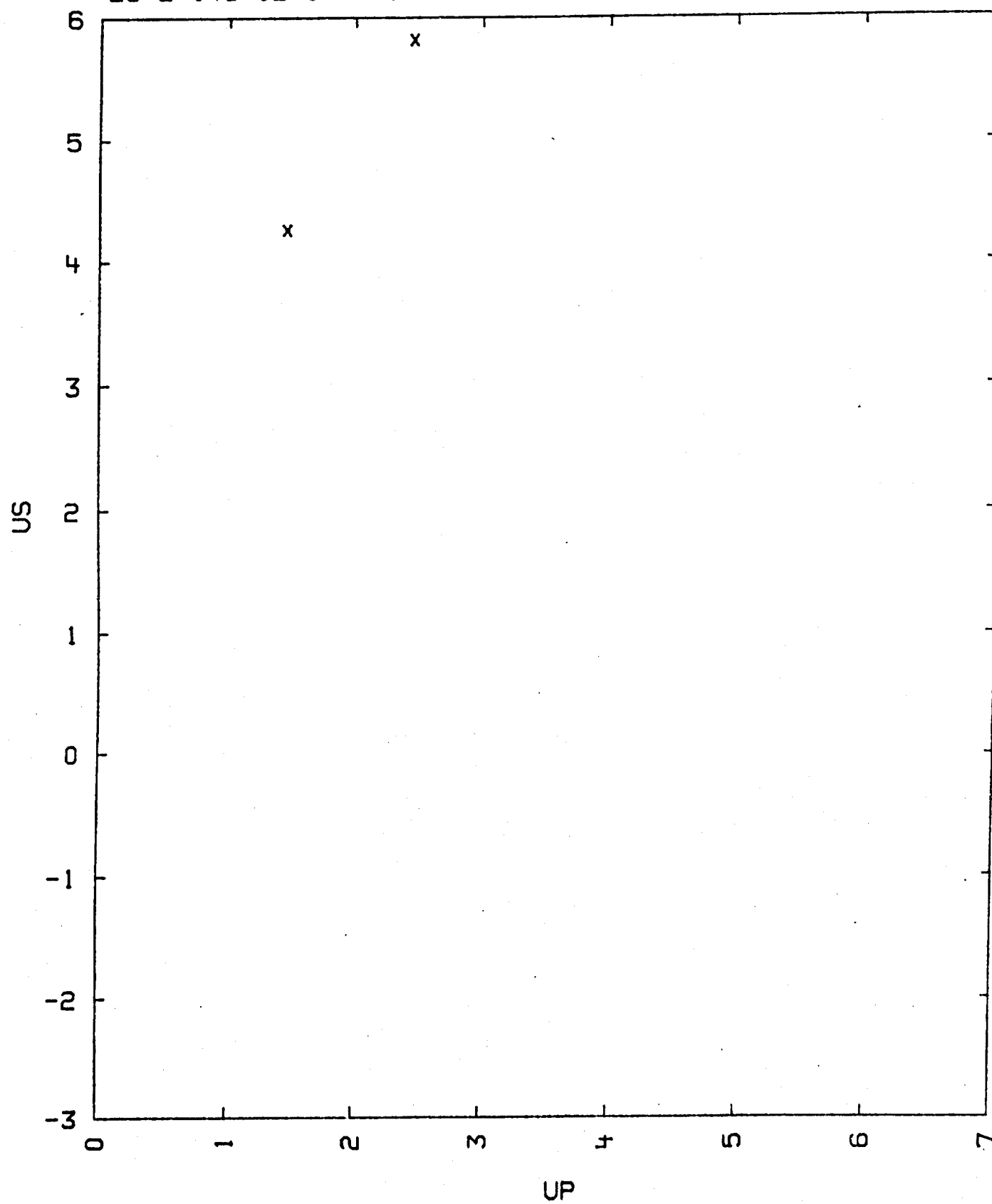
COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE ABOVE VALUE OF CO WAS OBTAINED FROM  
BERGMANN L., DER ULTRASCHALL (S.HIRZEL VERLAG, STUTTGART 1954)

TABLE I

N-AMYL ALCOHOL

23-2-1(5-12-1)---1



23-2-1(18-20-3)---1

PHENOXY

BISPHENOL-EPI RESIN (C18-H20-03)N

NOTE 3

VO = 0.849 CC/G      CL = 2.51 KM/SEC      CO = 2.18 KM/SEC  
 CS = 1.07 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
 AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RHO0             | US   | UP   | P    | V/VO   | MATERIAL           | US(ST) |
| 1.170            | 4.68 | 1.36 | 74.  | 0.7094 | 2024 AL            | 6.54   |
| 1.178            | 4.69 | 1.37 | 76.  | 0.7079 | 2024 AL            | 6.55   |
| 1.179            | 5.24 | 1.75 | 108. | 0.6660 | 2024 AL            | 6.92   |
| 1.178            | 5.27 | 1.77 | 110. | 0.6641 | 2024 AL            | 6.93   |
| 1.178            | 6.19 | 2.34 | 171. | 0.6220 | 2024 AL            | 7.51   |
| 1.179            | 6.17 | 2.35 | 171. | 0.6191 | 2024 AL            | 7.52   |
| 1.179            | 6.64 | 2.56 | 200. | 0.6145 | 2024 AL            | 7.75   |
| 1.178            | 7.03 | 3.05 | 253. | 0.5561 | 2024 AL            | 8.22   |
| 1.178            | 7.00 | 3.06 | 252. | 0.5629 | 2024 AL            | 8.23   |
| 1.178            | 7.46 | 3.59 | 315. | 0.5188 | 2024 AL            | 8.75   |
| 1.179            | 7.45 | 3.61 | 317. | 0.5154 | 2024 AL            | 8.76   |
| 1.178            | 8.88 | 4.62 | 483. | 0.4797 | 2024 AL            | 9.82   |
| 1.179            | 8.83 | 4.72 | 491. | 0.4655 | 2024 AL            | 9.91   |

US =  $2.486 + 1.591 \cdot UP$  KM/SEC FOR UP BELOW 2.9 KM/SEC

SIG US = 0.05 KM/SEC

US =  $3.398 + 1.159 \cdot UP$  KM/SEC FOR UP ABOVE 3.2 KM/SEC

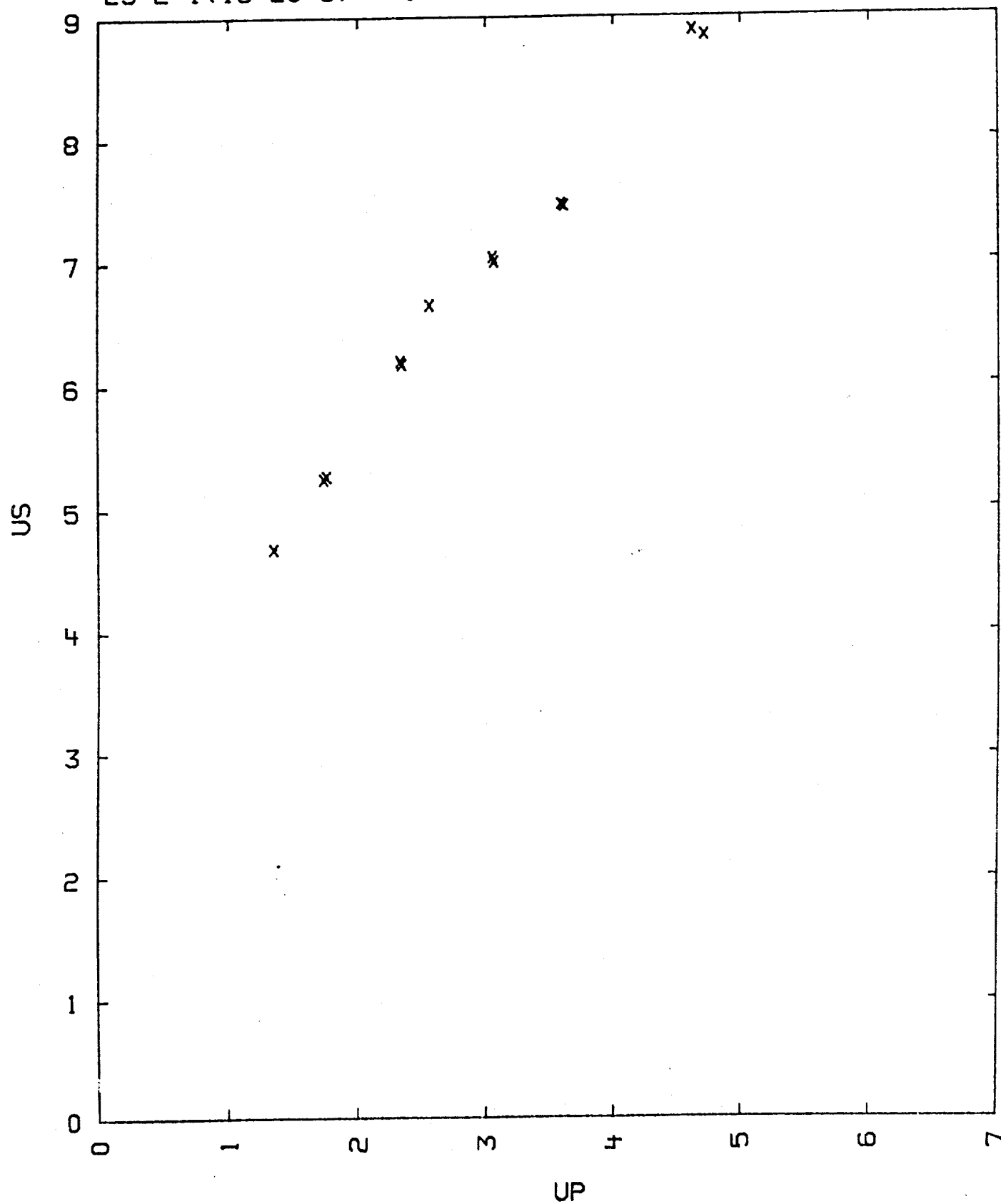
SIG US = 0.12 KM/SEC

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
 AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
 DATA REDUCTION TECHNIQUE: B
- 3) THE ABOVE COMPOSITION IS ONE GIVEN FOR UNION CARBIDES P.R.D.A. 8100  
 (JIM RINDE UCID 15815, LAWRENCE LIVERMORE LABORATORY, CALIF. 94550)  
 AND CONSISTENT WITH THE DESCRIPTION IN MODERN PLASTICS ENCYCLOPEDIA  
 (MC GRAW HILL, N.Y., 1975)

TABLE I

PHENOXY  
23-2-1(18-20-3)---1



23-2-1(7-8-1)---1

TOLUENE

C6(H5)-C-H3 = C7-H8-0

T0 = 4-15 DEG. C.

C0(20 DEG. C.) = 1.328 KM/SEC

V0 = 1.138-1.141 CC/G

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| T0 | RH00   | US   | UP    | P     | V/V0  |
|----|--------|------|-------|-------|-------|
| 4  | 0.8787 | 5.73 | 2.412 | 121.5 | 0.579 |
| 15 | 0.8764 | 4.12 | 1.443 | 52.1  | 0.650 |

$$US = 1.72 + 1.66 \cdot UP \text{ KM/SEC}$$

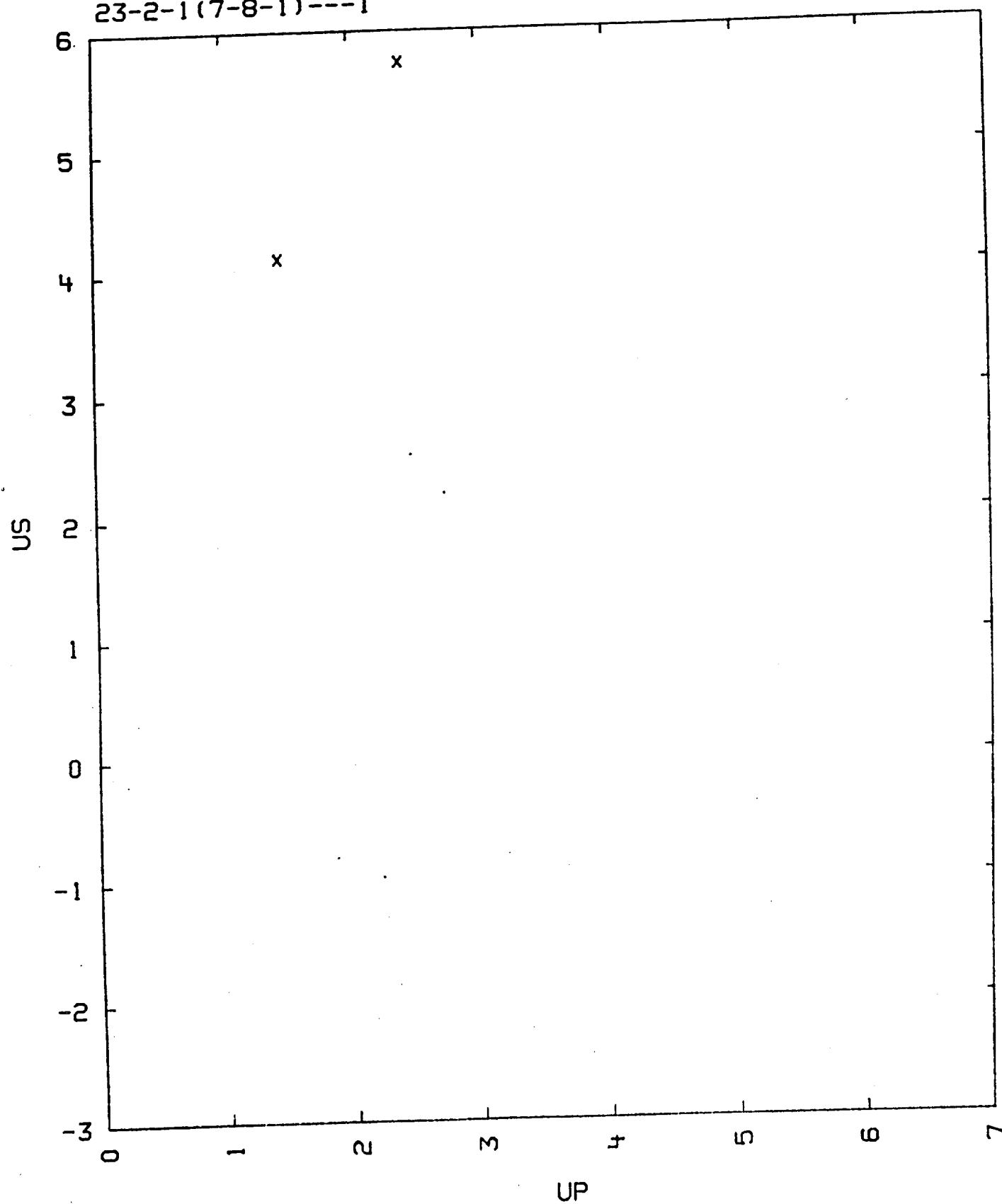
## COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE ABOVE VALUE OF C0 WAS OBTAINED FROM  
BERGMANN, DER ULTRASCHALL (S. HIRZEL VERLAG, STUTTGART 1954)

TABLE I

TOLUENE

23-2-1(7-8-1)---1





23-2-1(11-8-3)---1

DURITE

PHENOL-FURFURAL (C11-H8-O3)N

V0 = 0.725 CC/G

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL           | US(ST) |
| 1.379            | 4.62 | 1.30 | 83.  | 0.7186 | 2024 AL            | 6.53   |
| 1.378            | 7.02 | 2.94 | 284. | 0.5812 | 2024 AL            | 8.24   |
| 1.382            | 8.27 | 3.79 | 433. | 0.5417 | 2024 AL            | 9.16   |
| 1.382            | 9.63 | 4.89 | 651. | 0.4922 | 2024 AL            | 10.35  |

US = 2.847 + 1.404\*UP KM/SEC

SIGMA US = 0.105 KM/SEC

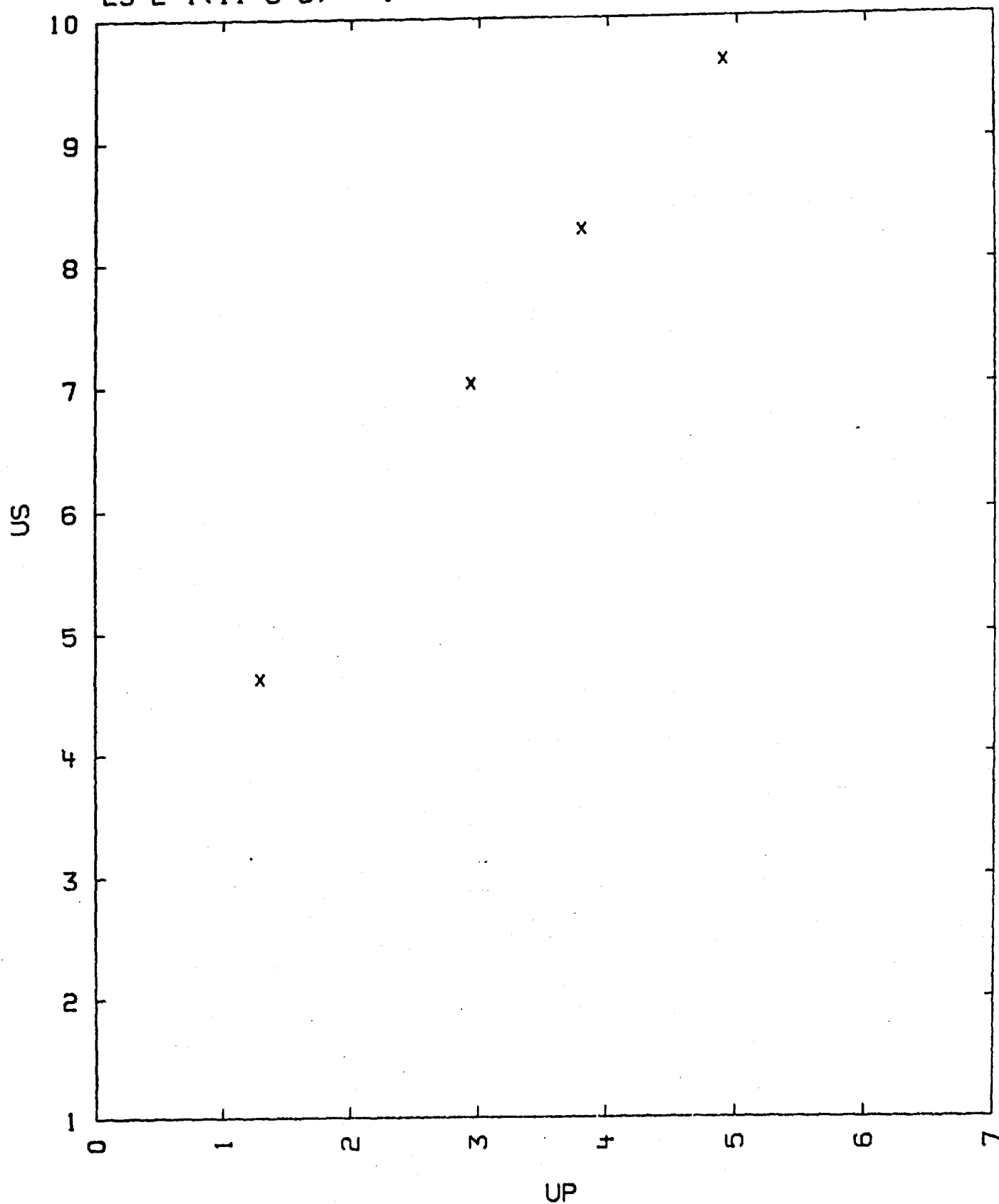
## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) DURITE IS A LINE OF PLASTICS, E.G., A CLASS OF FORMALDAHYDE OR  
PHENOLFURFURAL MOLDING COMPOUNDS SOLD BY DURITE PLASTICS DIVISION OF  
APPROXIMATELY EQUIMOLAR IN THE MONOMERS AND WITHOUT FILLER.  
CHEMICAL ANALYSIS NOT AVAILABLE

TABLE I

DURITE

23-2-1(11-8-3)---1



23-9(2-4)---0  
TEFLON SUMMARY

POLYTETRAFLUOROETHYLENE (F2-C-C-F2)N = (C2-F4)N

V0 = 0.459 - 1.023 CC/G

THE TABLE LISTS HUGONIOT POINTS CALCULATED FROM THE FIT GIVEN BELOW.  
UNITS ARE: G/CC, KM/SEC, KBAR, AND KBAR.CC/G FOR THE ENERGY DIFFERENCE.

TABLE

| RH00  | US    | UP  | P    | V/V0  | E-E0 |
|-------|-------|-----|------|-------|------|
| 2.170 | 2.681 | .5  | 29.1 | 0.813 | 1.25 |
| -     | 4.383 | 1.5 | 143. | 0.658 | 11.2 |
| -     | 6.087 | 2.5 | 330. | 0.589 | 31.2 |
| -     | 7.790 | 3.5 | 592. | 0.551 | 61.2 |
| 1.530 | 2.650 | 1.0 | 40.5 | 0.623 | 5.0  |
| -     | 4.161 | 2.0 | 127. | 0.519 | 20.0 |
| -     | 5.672 | 3.0 | 360. | 0.471 | 45.0 |
| -     | 7.183 | 4.0 | 440. | 0.443 | 80.  |
| 0.977 | 2.003 | 1.0 | 19.6 | 0.501 | 5.0  |
| -     | 3.348 | 2.0 | 65.4 | 0.403 | 20.0 |
| -     | 4.693 | 3.0 | 138. | 0.361 | 45.0 |
| 0.780 | 4.370 | 3.0 | 102. | 0.313 | 45.0 |
| -     | 5.656 | 4.0 | 176. | 0.293 | 80.  |
| -     | 6.942 | 5.0 | 271. | 0.280 | 125. |

$$US = 1.865 + 1.712 \cdot UP - 1.200(2.20 - RH00) - 0.300(2.20 - RH00)UP \\ 0.174(2.20 - RH00)^2$$

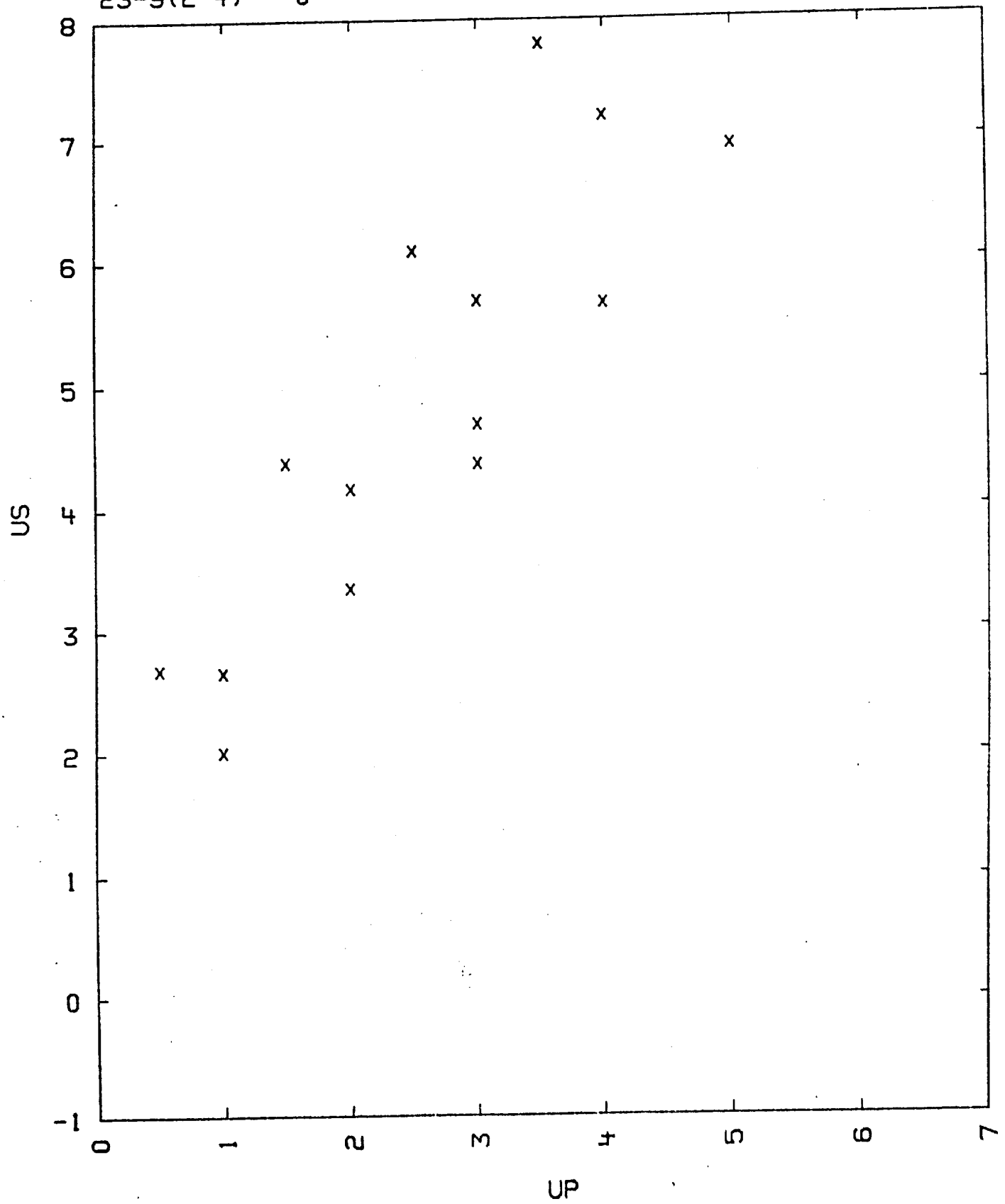
SIG.US = 0.14 KM/SEC. FOR UP IN THE LIMITS OF THE TABLE

COMMENTS:

- 1) SOURCE: COMPILER  
DATA FROM 23-9(2-4)---1,4, AND 5 WERE USED FOR THIS SUMMARY.
- 2) DATA OF 23-9(2-4)---2 IS OLDER AND LESS RELIABLE
- 3) SPECIAL HIGH DENSITY TEFLON WAS USED FOR THE DATA OF PAGE 23-9(2-4)---3. THESE DATA ARE LESS COMPRESSIBLE AT ALL BUT THE HIGHEST PRESSURE

TABLE 1

TEFLON SUMMARY  
23-9(2-4)---0



25 100-1  
TEFLON (POLYTETRAFLUOROETHYLENE)

$(F_2-C-C-F_2)_N = (C_2-F_4)_N$

$V_0 = 0.4655 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,  
AND PRESSURE IN KILOBARS.

TABLE

| RH00  | US    | UP    | P   | V/V0 |
|-------|-------|-------|-----|------|
| 2.148 | 5.150 | 1.960 | 217 | .619 |
|       | 4.372 | 1.513 | 142 | .654 |
|       | 3.800 | 1.176 | 96  | .691 |

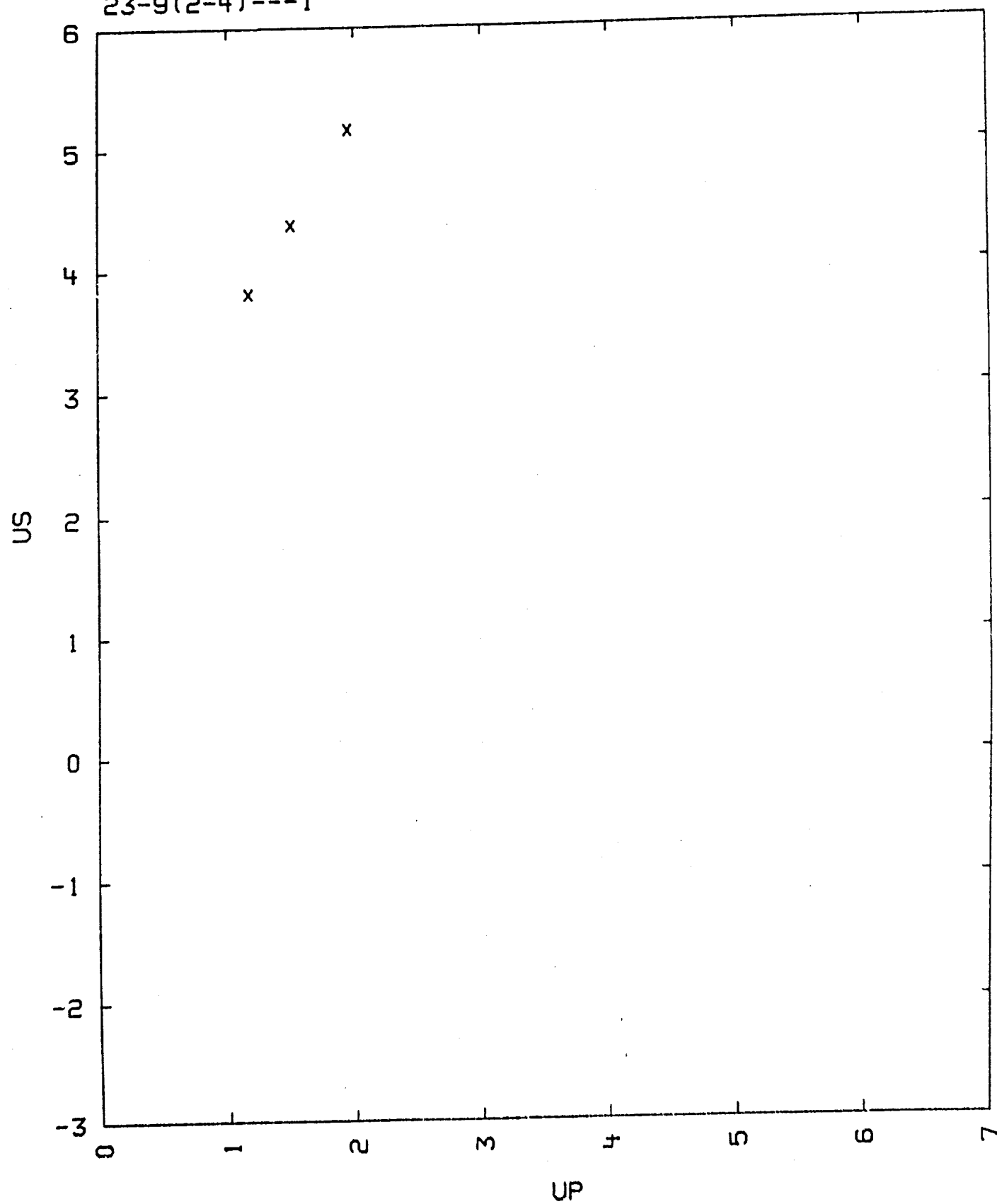
US =

COMMENTS:

- 1) SOURCE: DEAL, W. E.  
PRIVATE COMMUNICATION (1963)  
LOS ALAMOS SCIENTIFIC LABORATORY, GMX-6, LOS ALAMOS, N. MEX.
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B

TABLE I

TEFLON (POLYTETRAFLUOROETHYLENE)  
23-9(2-4)---1



23-9(2-4)---2  
TEFLON (POLYTETRAFLUOROETHYLENE)

$(F_2-C-C-F_2)_N = (C_2-F_4)_N$

$V_0 = .463 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC, AND PRESSURE IN KILOBARS. U IS THE VELOCITY OF THE PROJECTILE PLATE.

TABLE

| RH00 | US   | UP   | P    | V/V0  | U     |
|------|------|------|------|-------|-------|
| 2.16 | 1.85 | .263 | 10.5 | .8578 | 0.336 |
| -    | 2.08 | .410 | 18.4 | .8029 | 0.536 |
| -    | 2.49 | .578 | 31.1 | .7679 | 0.786 |
| -    | 3.03 | .837 | 54.8 | .7238 | 1.19  |
| -    | 3.32 | 1.06 | 76.4 | .6808 | 1.54  |

$US = 1.34 + 1.93 UP \text{ MM/MICROSEC.}$

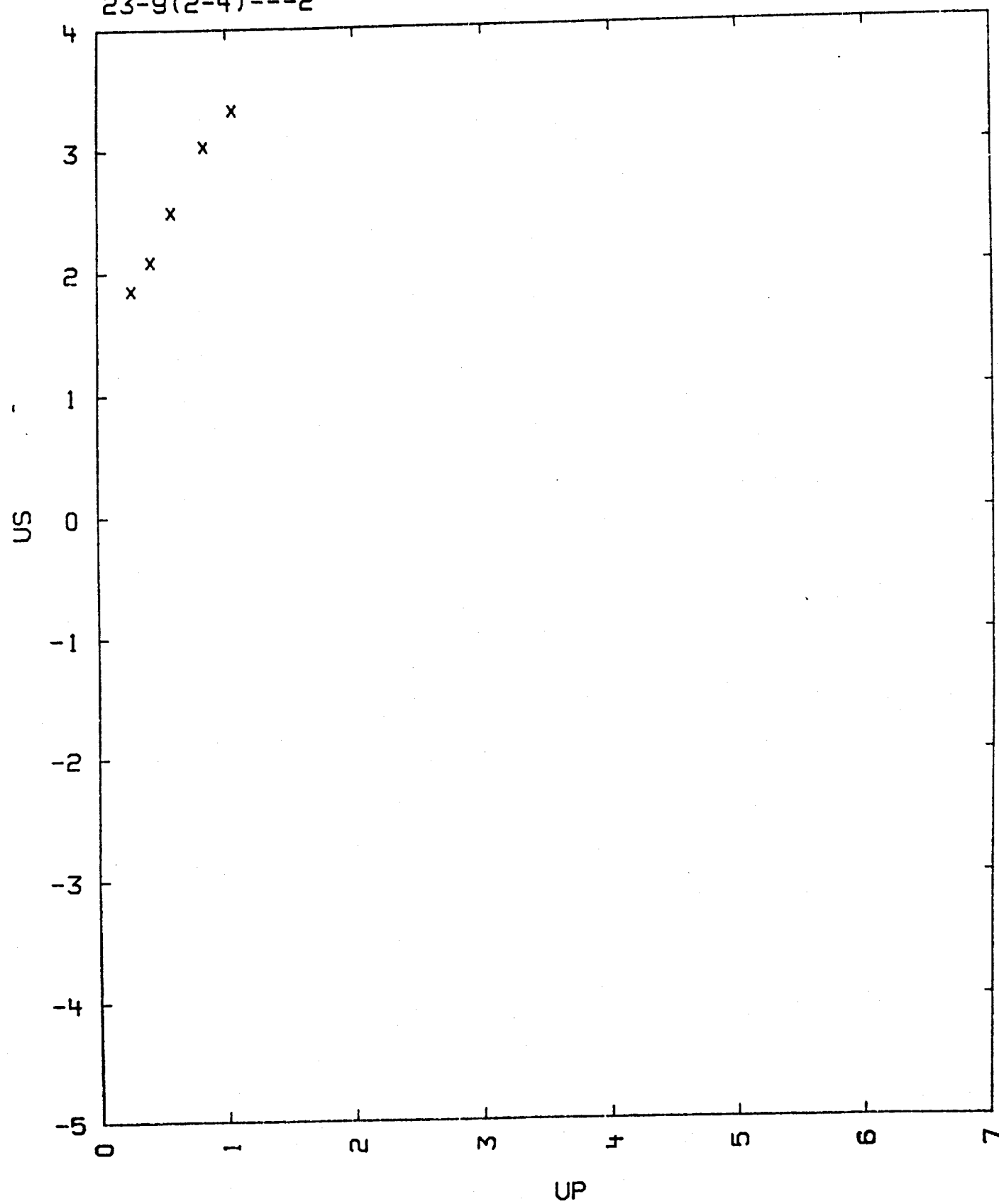
COMMENTS:

- 1) SOURCE: WAGNER, M.H., WALDORF, W.F. AND LOUIE, N.A.  
REPORT NO. AFSWC-TDR-62-66, VOL. 1  
WORK DONE AT DOWNEY, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE: A DRIVER PLATE: 2024-T3 AL  
DATA REDUCTION TECHNIQUE: A
- 3) ACCURACY IS LIMITED BECAUSE ASSEMBLY DIMENSIONS CAUSE DEVIATIONS FROM ONE DIMENSIONALITY.
- 4) THE 95 PERCENT CONFIDENCE LIMIT OF THE MEASURED VELOCITIES IN THE TABLE IS GIVEN IN ORDER OF THE LISTING BY THE UNCERTAINTIES:  
+ OR - FDEL US = 16. 8.6 7.2 6.1 7.2 PERCENT  
+ OR - FDEL U = 2.5 1.3 1.0 3.0 4.8 -  
HERE FDEL U =  $100(\text{DEL } U)/U$

TABLE I

TEFLON (POLYTETRAFLUOROETHYLENE)

23-9(2-4)---2





23-9(2-4)---3

TEFLON (POLYTETRAFLUOROETHYLENE)

(F2-C-C-F2)N = (C2-F4)N

V0 = 0.446 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US   | UP   | P     | V/V0  |
|------|------|------|-------|-------|
| 2.24 | 3.92 | 1.02 | 89.6  | 0.740 |
| -    | 3.93 | 1.03 | 90.7  | 0.736 |
| -    | 4.03 | 1.04 | 93.9  | 0.742 |
| -    | 4.41 | 1.27 | 125.5 | 0.712 |
| -    | 4.60 | 1.33 | 137.0 | 0.711 |
| -    | 4.87 | 1.50 | 163.6 | 0.692 |
| -    | 4.97 | 1.49 | 165.9 | 0.700 |
| -    | 5.18 | 1.69 | 196.1 | 0.674 |
| -    | 5.44 | 1.89 | 230.3 | 0.653 |
| -    | 5.46 | 1.83 | 223.8 | 0.665 |
| -    | 5.56 | 1.96 | 244.1 | 0.648 |
| -    | 5.79 | 2.08 | 269.8 | 0.641 |
| -    | 5.93 | 2.24 | 297.5 | 0.622 |
| -    | 6.25 | 2.43 | 340.2 | 0.611 |
| -    | 6.60 | 2.73 | 403.6 | 0.586 |
| -    | 7.24 | 3.19 | 517.4 | 0.559 |

US = 1.83 + 2.07 UP KM/SEC. FOR US BELOW 5 KM/SEC  
SIG.US = 0.05

US = 2.92 + 1.353 UP KM/SEC FOR US ABOVE 5 KM/SEC  
SIG.US = 0.04

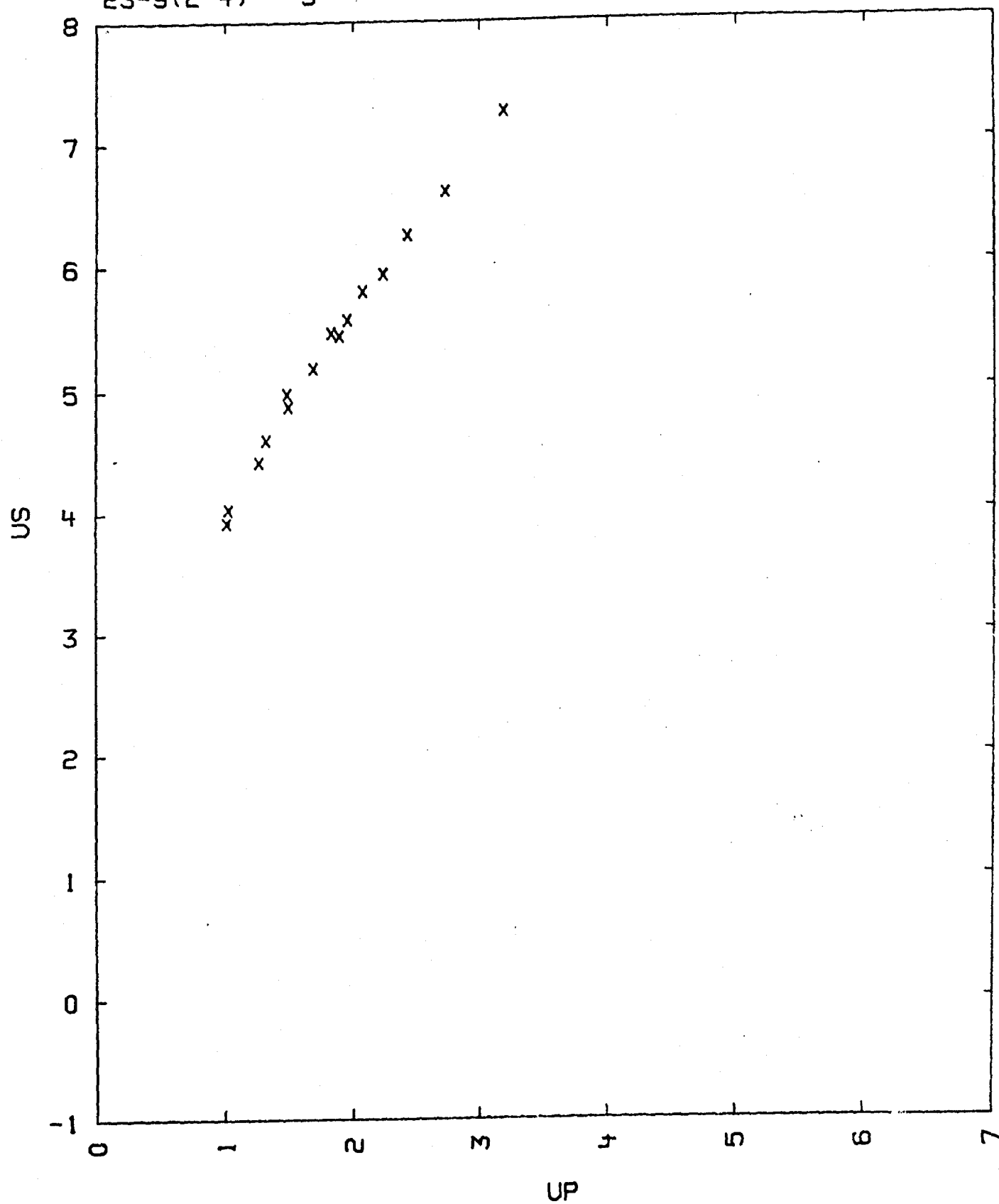
## COMMENTS:

- 1) SOURCE: NETHERWOOD, P. H.  
BRL MEMORANDUM REPORT NO. 1626 (DECEMBER, 1964)  
U. S. ARMY BALLISTIC RESEARCH LABORATORIES  
ABERDEEN PROVING GROUND, MARYLAND 21005
- 2) EXPERIMENTAL TECHNIQUE C1  
DATA REDUCTION TECHNIQUE B
- 3) PLATES OF ALUMINUM, BRASS, AND MAGNESIUM WITH KNOWN EQUATIONS OF STATE WERE USED. THE ADIABATIC UNLOADING PATHS IN THE P VS. UP PLANE WERE REPRESENTED BY THE REFLECTION OF THE HUGONIOT, SLIGHTLY ADJUSTED TO PASS THROUGH THE POINT (UFS+2UP)/2. SEE HAUVER, G. E., AND MELANI, A., BRL REPORT NO. 1259, AUGUST 1964.
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I

TEFLON (POLYTETRAFLUOROETHYLENE)

23-9(2-4)---3



23-9(2-4)---4  
TEFLON (POLYTETRAFLUOROETHYLENE)

$(-C(F_2)-C(F_2)-)_N = (C_2F_4)_N$

$V_0 = 0.4589-1.023 \text{ CC/G}$

THE TABLES LIST DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. U(ST) DESIGNATES THE VELOCITY OF THE 1100 ALUMINUM PROJECTILE

TABLE I

| RH00  | US   | UP    | P     | V/V0  | V(ST) |
|-------|------|-------|-------|-------|-------|
| 2.179 | 3.42 | 0.903 | 67.3  | 0.736 | 1.33  |
| -     | 3.73 | 1.073 | 87.2  | 0.712 | 1.61  |
| -     | 3.84 | 1.251 | 104.7 | 0.674 | 1.88  |
| -     | 4.33 | 1.477 | 139.4 | 0.659 | 2.28  |
| -     | 4.90 | 1.857 | 198.  | 0.621 | 2.93  |

$US = 2.00 + 1.55 \cdot UP \text{ KM/SEC}$

$SIGMA US = 0.074 \text{ KM/SEC}$

TABLE II

| RH00  | US   | UP    | P     | V/V0  | U(ST) |
|-------|------|-------|-------|-------|-------|
| 1.535 | 2.99 | 1.274 | 58.5  | 0.574 | 1.65  |
| -     | 3.10 | 1.249 | 59.4  | 0.597 | 1.63  |
| -     | 3.24 | 1.237 | 61.5  | 0.618 | 1.63  |
| -     | 3.52 | 1.498 | 80.9  | 0.575 | 2.00  |
| -     | 3.86 | 1.724 | 102.2 | 0.553 | 2.34  |
| -     | 4.10 | 2.101 | 132.3 | 0.488 | 2.87  |

$US = 1.61 + 1.23 \cdot UP \text{ KM/SEC}$

$SIGMA US = 0.14 \text{ KM/SEC}$

TABLE III

| RH00  | US   | UP    | P    | V/V0  | U(ST) |
|-------|------|-------|------|-------|-------|
| 0.977 | 2.41 | 1.434 | 33.8 | 0.405 | 1.66  |
| -     | 2.51 | 1.383 | 33.9 | 0.449 | 1.61  |
| -     | 2.66 | 1.691 | 44.0 | 0.364 | 1.98  |
| -     | 3.54 | 1.844 | 63.8 | 0.479 | 2.25  |
| -     | 3.86 | 2.379 | 89.8 | 0.384 | 2.93  |

$US = 3.38 + 1.52 \cdot UP \text{ KM/SEC}$

$SIGMA US = 0.29 \text{ KM/SEC}$

## COMMENTS

- 1) SOURCE: MORGAN D. T, ROCKOWITZ M., ATKINSON A. L.  
AVCO CORP. REPORT NO. AFWL-TR-65-117  
RESEARCH AND DEVELOPMENT DIVISION  
AVCO CORP., WILMINGTON, MASS., USA
- 2) EXPERIMENTAL TECHNIQUE: (SEE 3)  
DATA REDUCTION METHOD: B  
THE STANDARD MATERIAL WAS 1100 AL ALLOY WITH  
 $\rho_{00} = 2.70 \text{ G/CC}$ ,  $U_S = C + S \cdot U_P \text{ KM/SEC}$   
 $C = 5.144 \pm 0.093 \text{ KM/SEC}$   
 $S = 1.528 \pm 0.041$
- 3) THE PRESSURE WAS GENERATED WITH ALUMINUM 1100 ALLOY PROJECTILES  
THE PROJECTILE VELOCITY AND SAMPLE SURFACE MOTION WERE DETECTED BY  
REFLECTING A LASER BEAM OFF THESE SURFACES AND OBSERVING THE LIGHT  
PHOTOMETRICALLY THROUGH A SET OF SLITS. THESE MEASUREMENTS TOGETHER  
WITH THE OBSERVATION OF AN IMPACT FLASH GENERATED WHEN THE PROJECTILE  
AND SAMPLE COLLIDE, YIELD  $U_S$  AND  $U(ST)$
- 4) ACCURACY OF THE VELOCITY MEASUREMENTS WAS TYPICALLY 1 PERCENT

TABLE I

TEFLON (POLYTETRAFLUOROETHYLENE)

23-9(2-4)---4

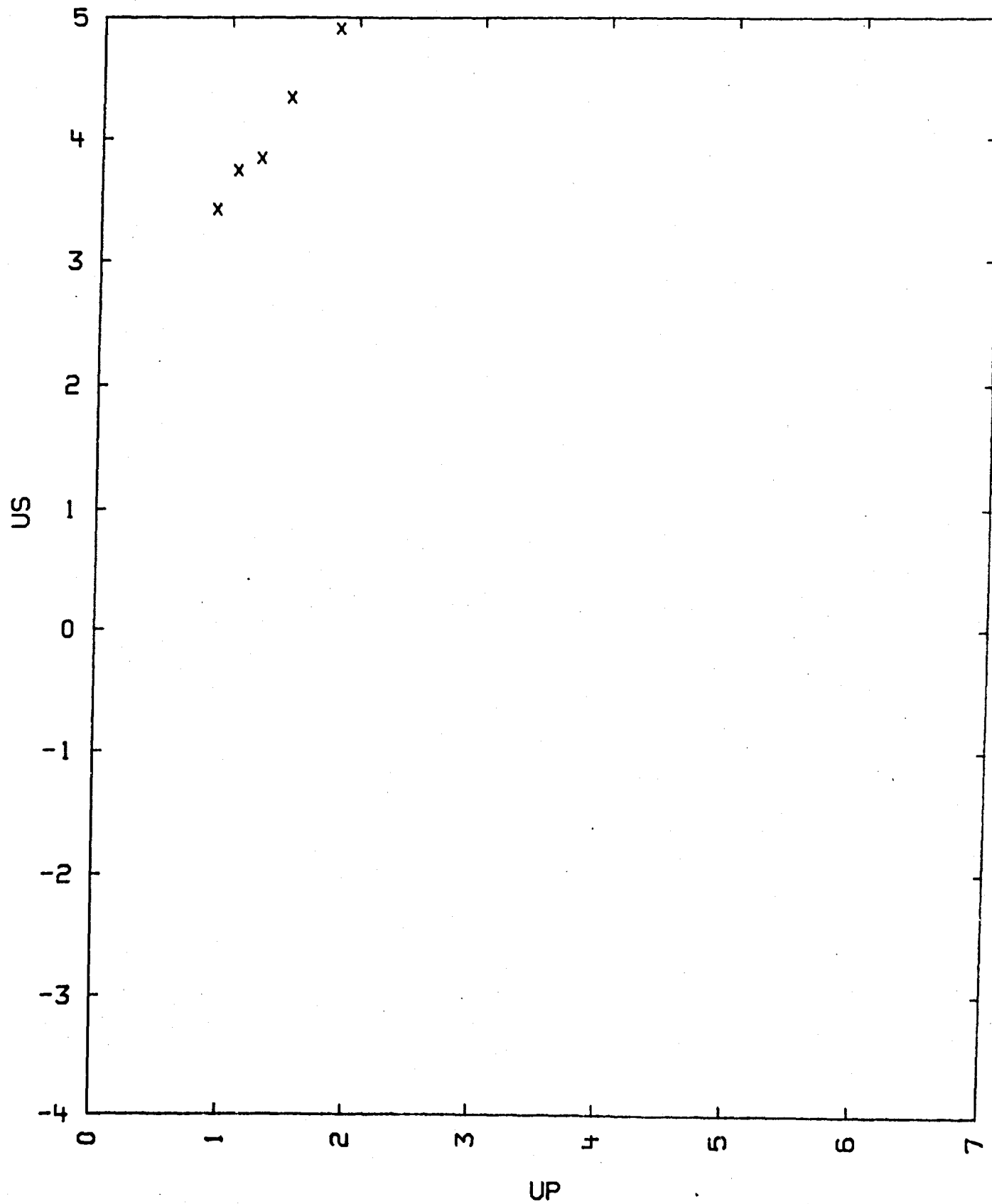


TABLE II

TEFLON (POLYTETRAFLUOROETHYLENE)

23-9(2-4)---4

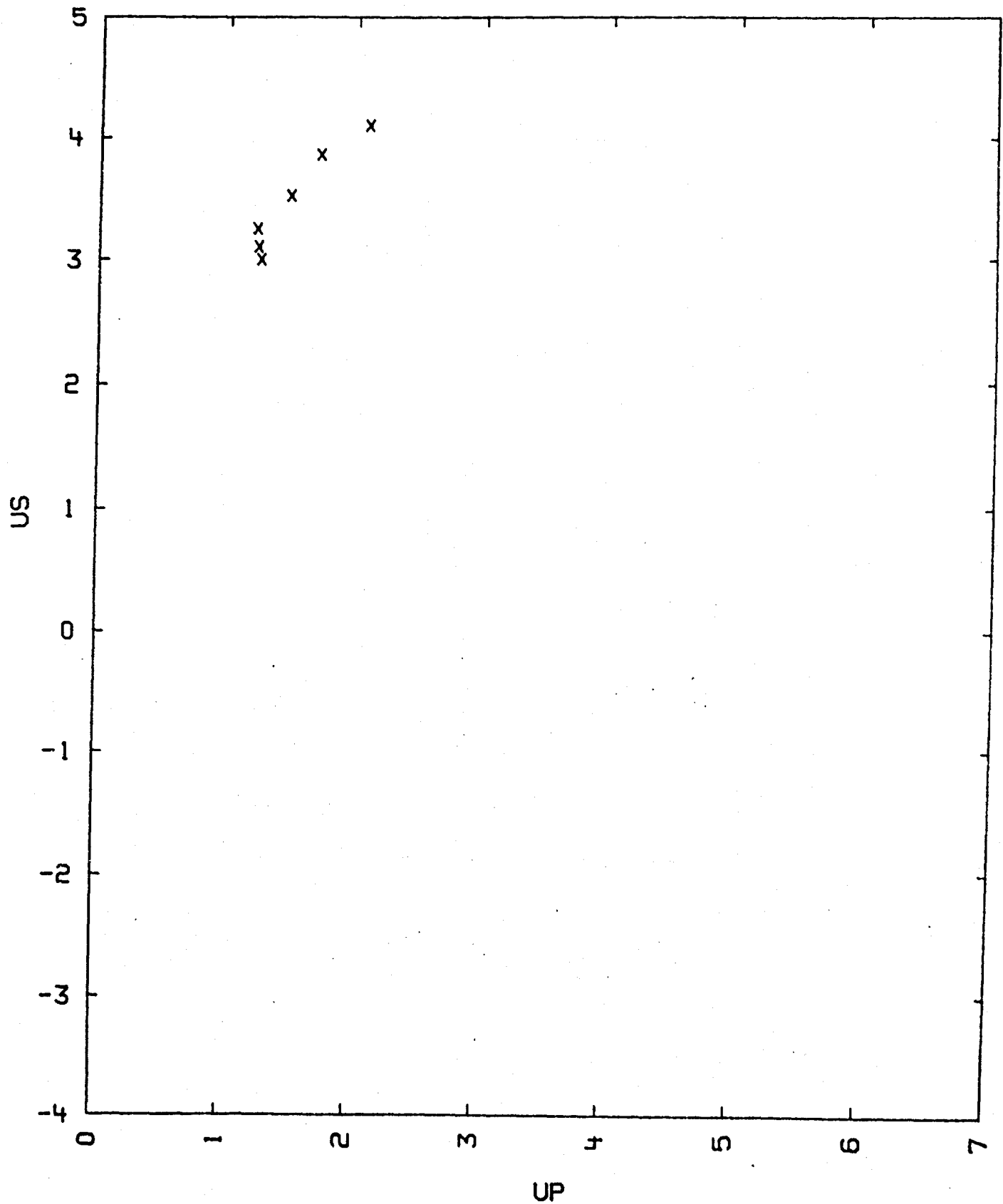
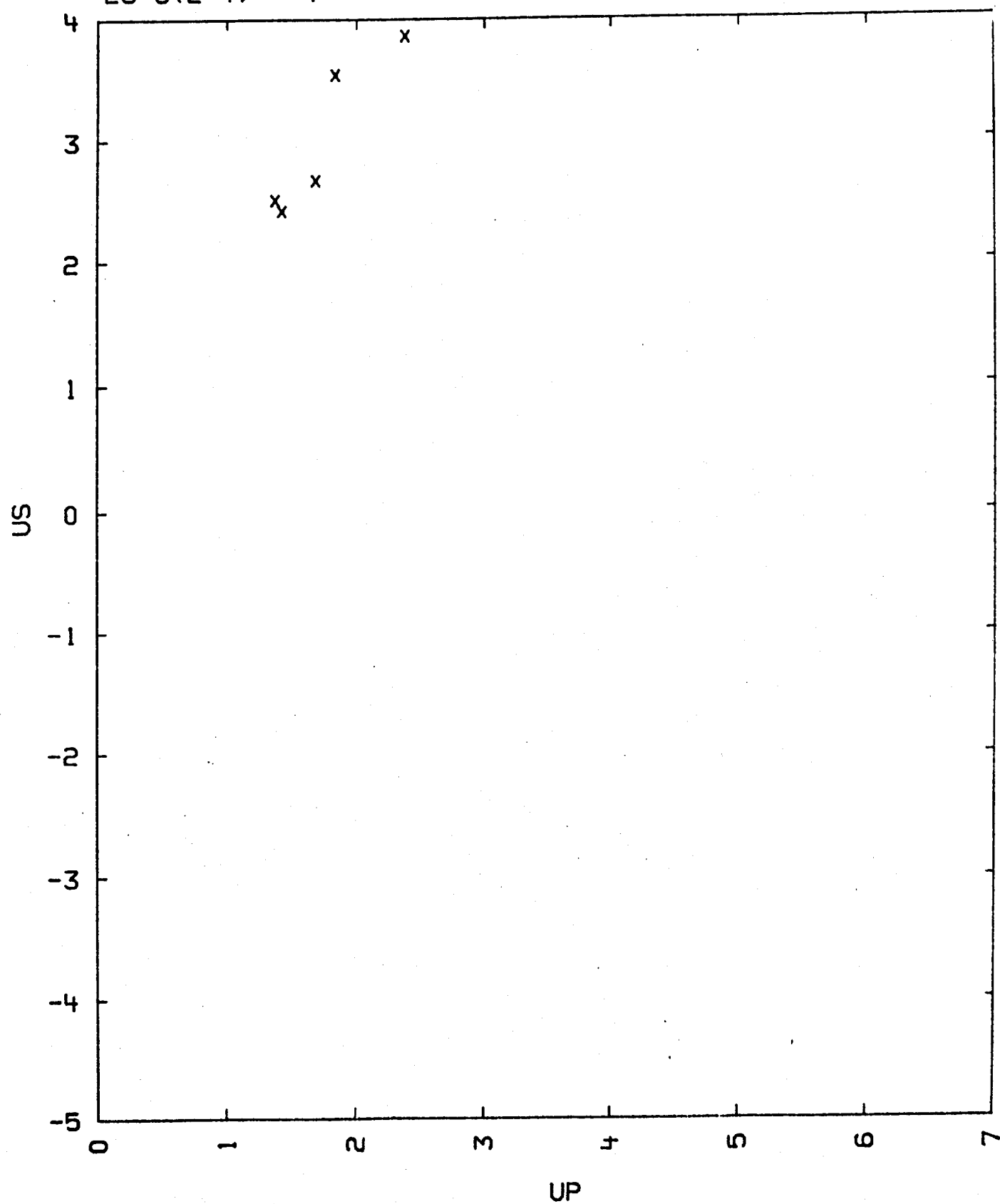


TABLE III

TEFLON (POLYTETRAFLUOROETHYLENE)

23-9(2-4)---4



23-9(2-4)---5

TEFLON (POLYTETRAFLUOROETHYLENE)

 $(-C(F_2)-C(F_2)-)_N = (C_2F_4)_N$ 

PARTICLE SIZE OF POROUS SAMPLES: SEE COMMENTS

 $V_0 = 0.4604 - 1.285 \text{ CC/G}$ 

THE TABLES LIST DENSITY IN G/CC, VELOCITIES IN KM/SEC AND P IN KILOBARS

TABLE I

| RH00   | US    | UP    | P     | V/V0   |
|--------|-------|-------|-------|--------|
| 0.7967 | 2.048 | 1.420 | 23.0  | 0.3066 |
| 0.7606 | 3.741 | 2.493 | 71.0  | 0.3336 |
| 0.7828 | 4.374 | 2.985 | 103.0 | 0.3175 |
| 0.7782 | 4.340 | 2.980 | 100.8 | 0.3134 |
| 0.7870 | 5.129 | 3.600 | 146.0 | 0.2981 |
| 0.7782 | 5.646 | 3.985 | 175.5 | 0.2941 |
| 0.7828 | 6.086 | 4.335 | 207.0 | 0.2877 |
| 0.7869 | 6.419 | 4.565 | 231.0 | 0.2888 |

 $US = -0.26 + 1.72 \cdot UP - 0.060 \cdot UP^2 \text{ KM/SEC}$  $SIG US = 0.047 \text{ KM/SEC}$ 

TABLE II

| RH00  | US    | UP    | P     | V/V0   |
|-------|-------|-------|-------|--------|
| 1.533 | 2.639 | 1.255 | 50.5  | 0.5244 |
| 1.524 | 4.354 | 2.120 | 140.5 | 0.5131 |
| 1.517 | 4.909 | 2.555 | 190.3 | 0.4795 |
| 1.525 | 4.952 | 2.535 | 191.5 | 0.4881 |
| 1.516 | 5.774 | 3.065 | 268.0 | 0.4692 |
| 1.524 | 6.207 | 3.373 | 319.0 | 0.4564 |
| 1.517 | 6.683 | 3.66  | 371.0 | 0.4522 |
| 1.516 | 6.992 | 3.855 | 408.5 | 0.4486 |

 $US = 0.14 + 2.14 \cdot UP - 0.096 \cdot UP^2 \text{ KM/SEC.}$  $SIG US = 0.07 \text{ KM/SEC.}$ 

TABLE III

| - - - - - SAMPLE - - - - - |      |       |      |     |       | - - BULLET - |       |
|----------------------------|------|-------|------|-----|-------|--------------|-------|
| RH00                       | US   | UP    | P    | PG  | V/V0  | MAT          | U     |
| 2.175                      | 1.92 | 0.208 | 8.7  | 8.4 | 0.892 | TEFLON       | 0.417 |
| 2.175                      | 2.00 | 0.247 | 10.8 | 9.0 | 0.876 | AL           | 0.311 |



## TEFLON (POLYTETRAFLUOROETHYLENE)

| RH00  | US    | UP    | P     | PG   | V/V0   | MAT    | U     |
|-------|-------|-------|-------|------|--------|--------|-------|
| 2.171 | 2.17  | 0.370 | 17.6  | 15.8 | 0.830  | TEFLON | 0.741 |
| 2.170 | 2.67  | 0.578 | 33.5  | 32.0 | 0.784  | AL     | 0.781 |
| 2.157 | 3.529 | 1.075 | 82.0  |      | 0.6954 |        |       |
| 2.168 | 5.120 | 1.835 | 203.0 |      | 0.6416 |        |       |
| 2.169 | 5.589 | 2.215 | 269.0 |      | 0.6037 |        |       |
| 2.175 | 5.628 | 2.205 | 269.5 |      | 0.6082 |        |       |
| 2.170 | 5.994 | 2.415 | 314.0 |      | 0.5971 |        |       |
| 2.169 | 6.360 | 2.665 | 368.0 |      | 0.5810 |        |       |
| 2.163 | 6.830 | 2.945 | 435.0 |      | 0.5688 |        |       |
| 2.172 | 7.105 | 3.080 | 476.0 |      | 0.5665 |        |       |
| 2.163 | 7.262 | 3.200 | 504.0 |      | 0.5593 |        |       |
| 2.169 | 7.543 | 3.375 | 552.5 |      | 0.5526 |        |       |

US =  $1.477 + 2.053 \cdot UP - 0.077 \cdot UP^2$ . KM/SEC

SIG US = 0.06 KM/SEC.

## COMMENTS

- 1) SOURCE: ANDERSON G. D., DORAN D. G. AND FAHRENBRUCH A. L.  
AIR FORCE WEAPONS LAB. REPORT AFWL-TR-65-147 (1965)  
- - - - - AFWL-TR-67-43  
STANFORD RES. INST., MENLO PARK, CALIFORNIA, USA.
- 2) EXPERIMENTAL METHOD: C  
DATA REDUCTION TECHNIQUE: B  
STANDARD MATERIAL 2024 AL ALLOY
- 3) THE POROUS SAMPLES IN TABLES II AND III WERE PREPARED BY PRESSING TOGETHER A MIXTURE OF DUPONTS TEFLON 7 POWDER (AVERAGE PARTICLE SIZE 35 MICRONS AND  $\rho = 0.25$  G/CC) AND AN APPROPRIATE AMOUNT OF LEACHABLE SALT. THE MIXTURE WAS PRESSED TO 200 ATMOSPHERE., SINTERED AT 22 DEG CENTIGRADE AND LEACHED FROM 11 TO 19 DAYS.  
D.T. MORGAN, M. ROCKOWITZ AND A. L. ATKINSON  
REPORT NUMBER: AFWL-TR-65-117 (1965)  
RES. AND DEVELOPMENT DIV., AVCO CORP., WILMINGTON, MASS., USA.

TABLE I

TEFLON (POLYTETRAFLUOROETHYLENE)

23-9(2-4)---5

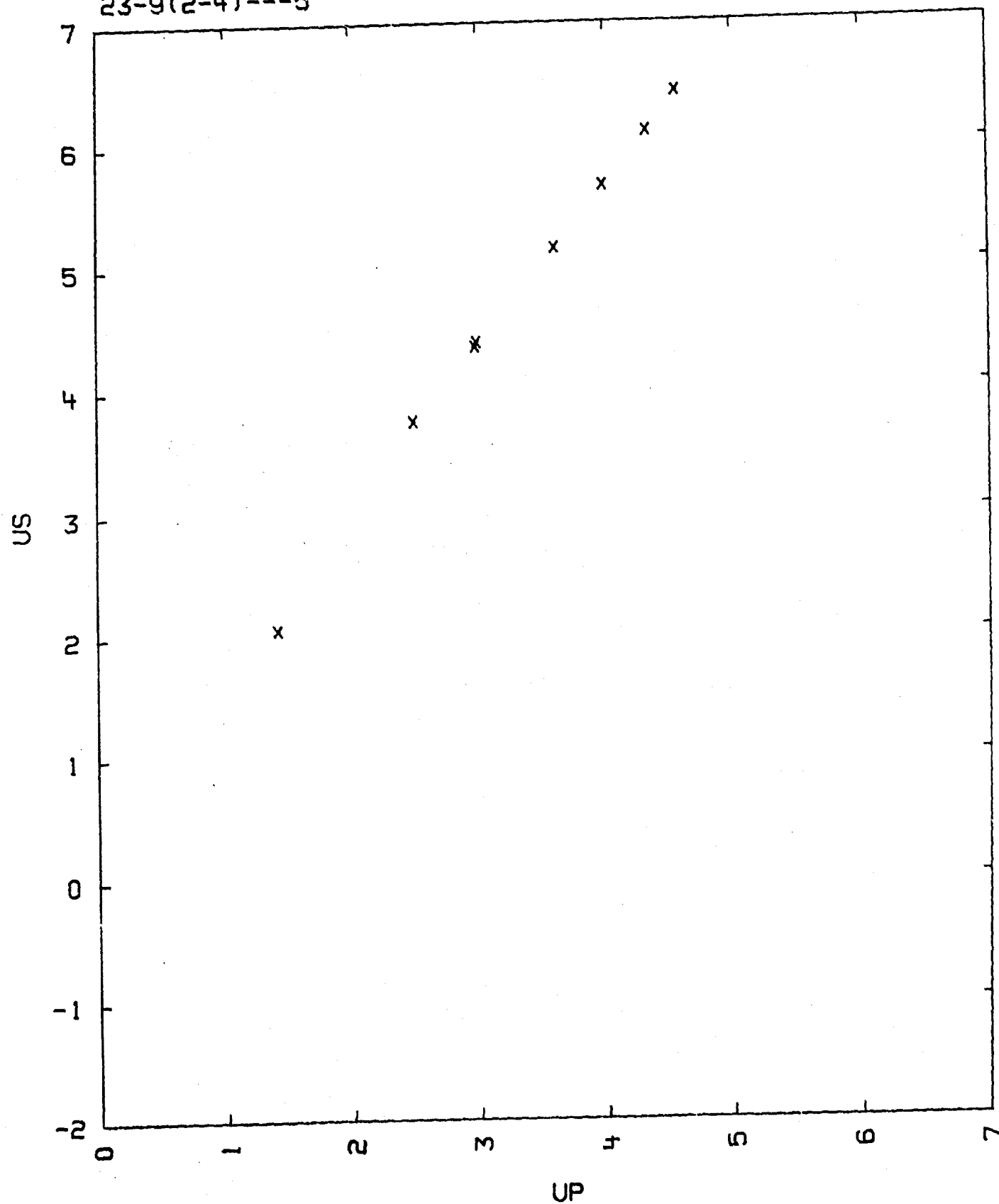


TABLE II

TEFLON (POLYTETRAFLUOROETHYLENE)

23-9(2-4)---5

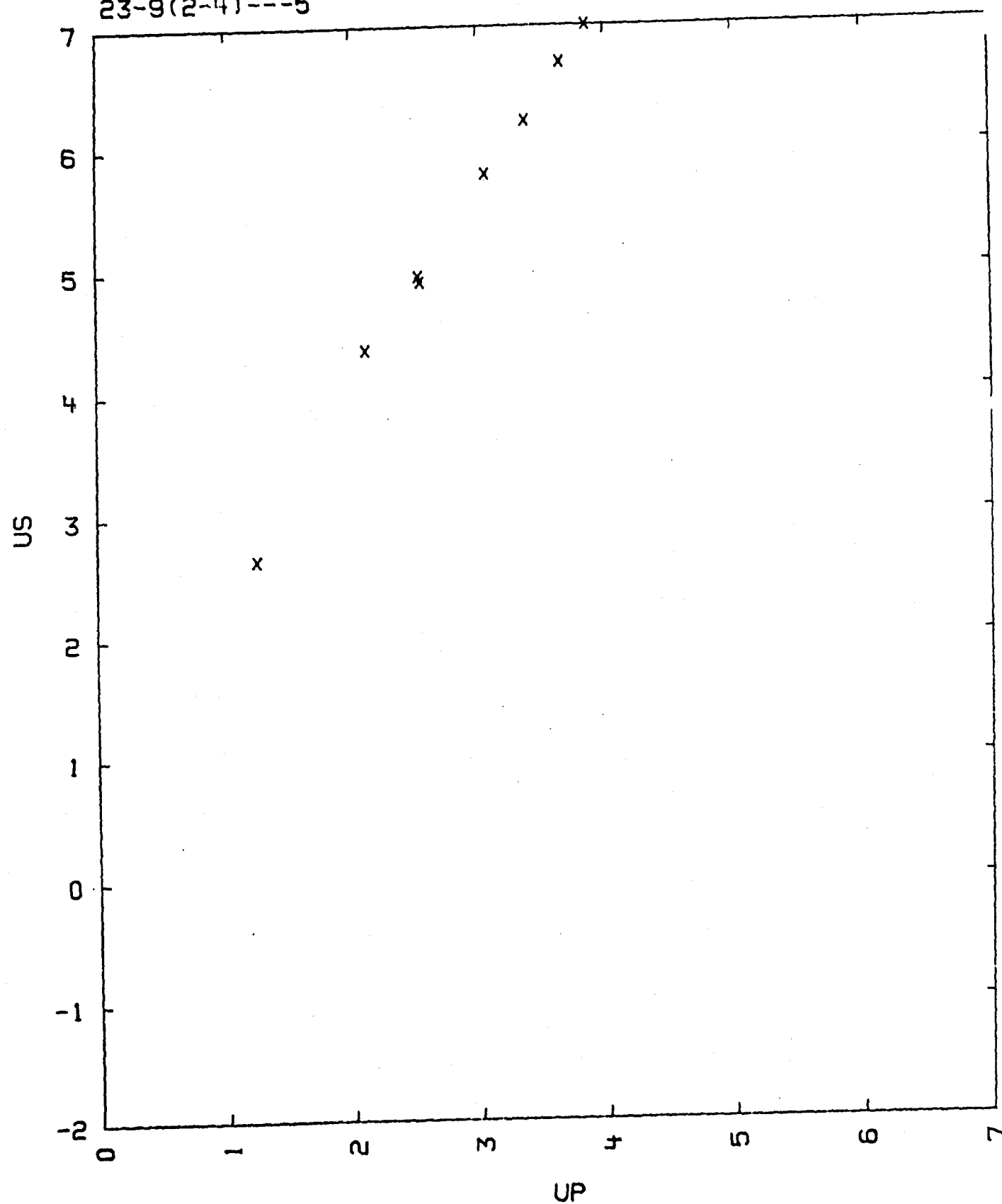
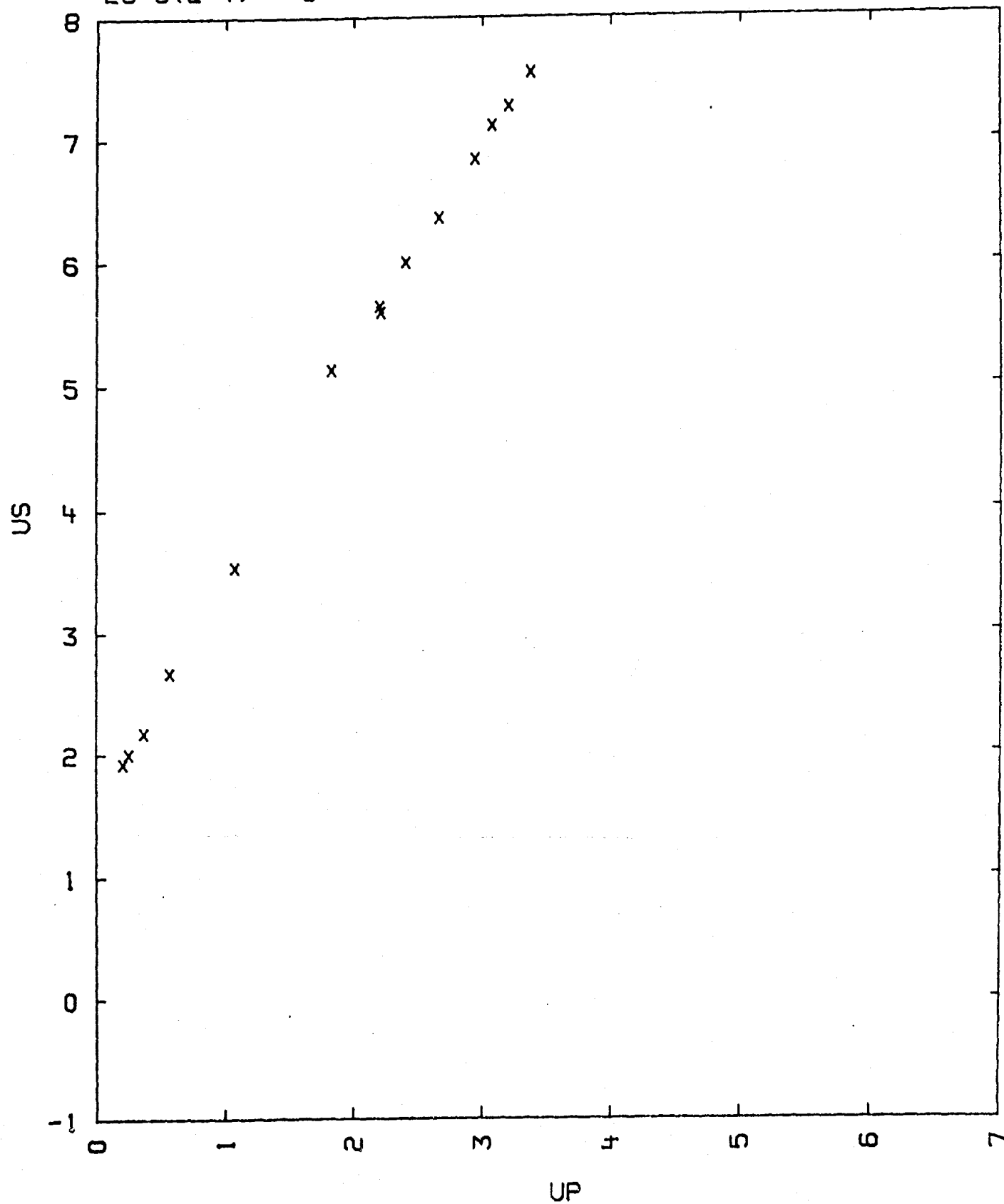


TABLE 111

TEFLON (POLYTETRAFLUOROETHYLENE)

23-9(2-4)---5



73-9(2-4) - 8

TEFLON

POLYTETRAFLUOROETHYLENE

(F2-C-C-F2)N

V0 = 0.465

C0 = 1.14 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL           | US(ST) |
| 2.152            | 2.89 | 0.66 | 41.  | 0.7716 | 2024 AL            | 5.94   |
| 2.152            | 3.25 | 0.85 | 59.  | 0.7385 | 2024 AL            | 6.14   |
| 2.152            | 3.71 | 1.09 | 87.  | 0.7062 | CU                 | 4.92   |
| 2.147            | 3.75 | 1.13 | 91.  | 0.6987 | 2024 AL            | 6.45   |
| 2.152            | 3.91 | 1.20 | 101. | 0.6931 | 2024 AL            | 6.53   |
| 2.147            | 4.32 | 1.47 | 136. | 0.6597 | 2024 AL            | 6.82   |
| 2.152            | 4.51 | 1.54 | 149. | 0.6585 | 2024 AL            | 6.91   |
| 2.152            | 4.64 | 1.69 | 169. | 0.6358 | CU                 | 5.50   |
| 2.147            | 5.15 | 1.89 | 209. | 0.6330 | 2024 AL            | 7.33   |
| 2.152            | 5.43 | 2.07 | 242. | 0.6188 | 2024 AL            | 7.54   |
| 2.152            | 5.77 | 2.32 | 288. | 0.5979 | CU                 | 6.15   |
| 2.152            | 5.99 | 2.41 | 311. | 0.5977 | 2024 AL            | 7.95   |
| 2.152            | 6.38 | 2.61 | 358. | 0.5909 | CU                 | 6.46   |
| 2.152            | 6.65 | 2.75 | 394. | 0.5865 | 2024 AL            | 8.38   |
| 2.152            | 6.72 | 2.90 | 419. | 0.5685 | CU                 | 6.75   |
| 2.152            | 7.08 | 3.06 | 466. | 0.5678 | 2024 AL            | 8.76   |
| 2.152            | 7.38 | 3.26 | 518. | 0.5583 | CU                 | 7.13   |
| 2.152            | 7.62 | 3.38 | 554. | 0.5564 | 2024 AL            | 9.16   |
| 2.152            | 8.13 | 3.53 | 618. | 0.5658 | 2024 AL            | 9.39   |
| 2.152            | 7.85 | 3.56 | 601. | 0.5465 | CU                 | 7.45   |
| 2.152            | 8.00 | 3.71 | 639. | 0.5362 | CU                 | 7.60   |
| 2.151            | 8.04 | 3.75 | 649. | 0.5336 | CU                 | 7.64   |
| 2.152            | 8.39 | 3.82 | 690. | 0.5447 | 2024 AL            | 9.72   |
| 2.152            | 8.95 | 4.39 | 846. | 0.5095 | 2024 AL            | 10.39  |

US =  $1.682 + 1.819 \cdot UP$  KM/SEC FOR UP BELOW 3.5 KM/SEC

SIG US 0.08 KM/SEC

US =  $3.47 + 1.25 \cdot UP$  KM/SEC FOR UP ABOVE 3.74 KM/SEC

SIG US = 0.18 KM/SEC

## COMMENTS:

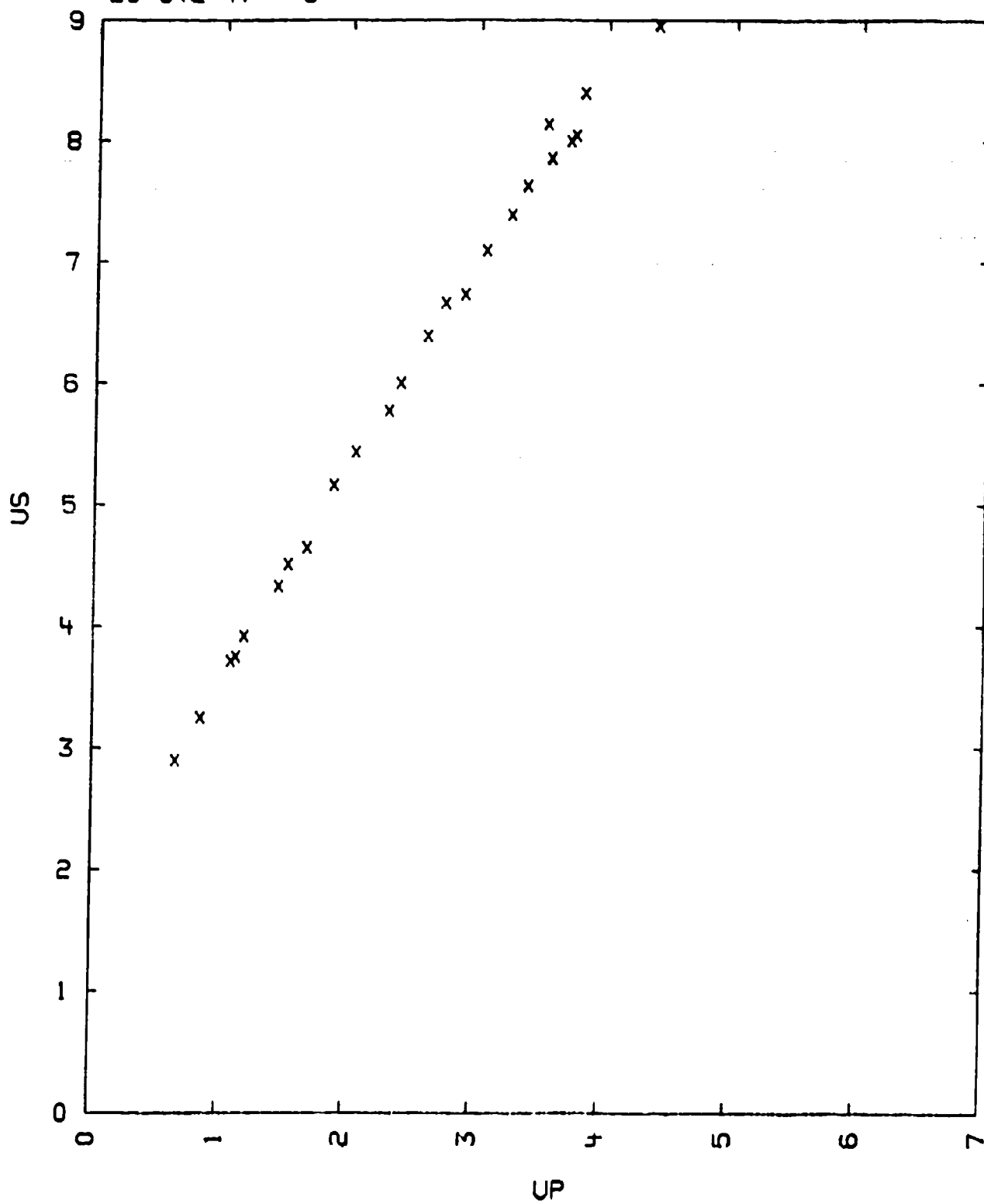
- 1) SOURCE: MCOUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B

DATA REDUCTION TECHNIQUE: B  
3)  $V(DP/DE) = 0.59$

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TABLE I

TEFLON  
23-9(2-4)---6

23-10-2(4-1-5)---1  
 NEOPRENE (POLY-2CHLORO-1,3 BUTADIENE)



$V_0 = 0.8949 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
 AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |      |
|------------------|------|------|------|--------|--------------------|------|
| RHOO             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |      |
| 1.439            | 4.37 | 1.14 | 72.  | 0.7391 | 2024 AL            | 6.38 |
| 1.438            | 5.01 | 1.53 | 110. | 0.6946 | 2024 AL            | 6.78 |
| 1.439            | 5.72 | 2.08 | 171. | 0.6364 | 2024 AL            | 7.34 |
| 1.440            | 5.76 | 2.09 | 173. | 0.6372 | 2024 AL            | 7.36 |
| 1.439            | 5.74 | 2.10 | 173. | 0.6341 | 2024 AL            | 7.36 |

$US = 2.785 + 1.419 \cdot UP \text{ KM/SEC}$

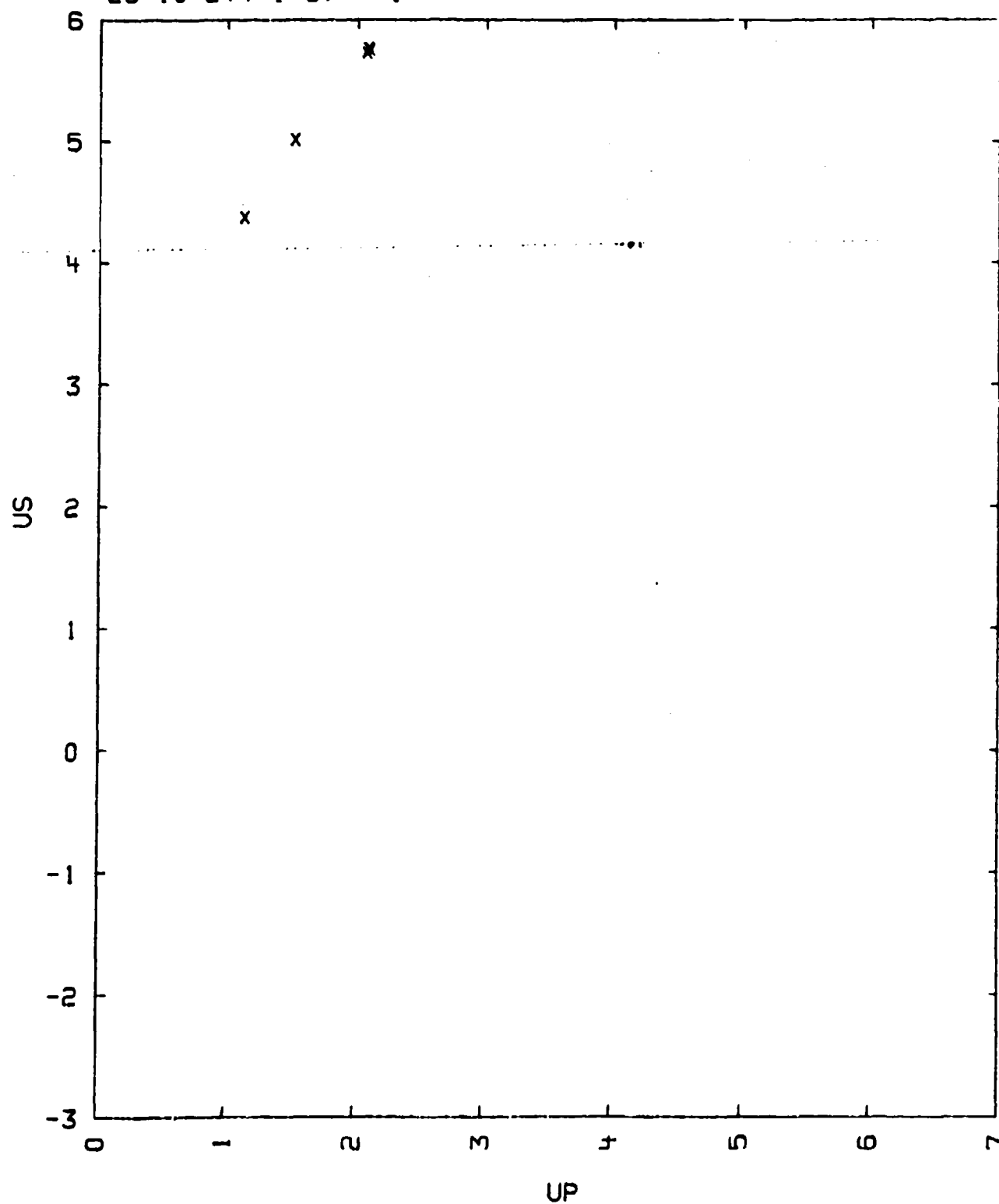
$SIGMA US = 0.041 \text{ KM/SEC}$

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
 AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES.  
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE:B  
 DATA REDUCTION TECHNIQUE:B (STANDARD BASE PLATE AS SHOWN)



TABLE 1  
NEOPRENE (POLY-2CHLORO-1,3 BUTADIENE)  
23-10-2(4-1-5)---1



23-10-9(2-1-3)---1  
 KEL F (POLYTRIFLUOROCHELOETHYLENE)

(CL-C(F)-C-F2)N = (C2-CL-F3)N

$V_0 = .48 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC, AND PRESSURE IN KILOBARS.

TABLE

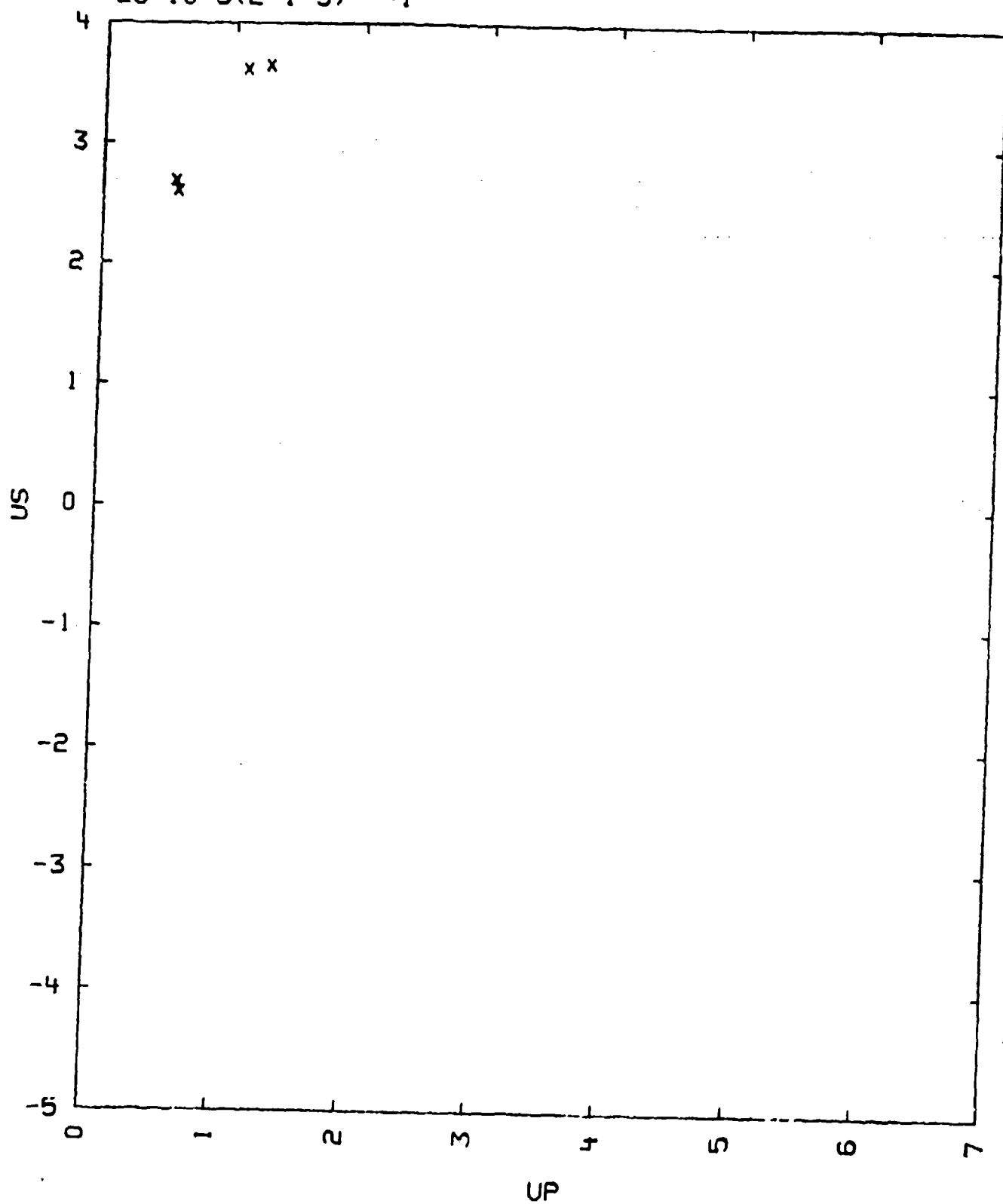
| RH00 | US   | UP    | P    | V/V0   |
|------|------|-------|------|--------|
| 2.10 | 2.60 | 0.580 | 31.7 | 0.7770 |
| -    | 2.68 | 0.565 | 31.9 | 0.7892 |
| -    | 3.61 | 1.10  | 83.1 | 0.6953 |
| -    | 3.64 | 1.27  | 96.8 | 0.6511 |

$US = 1.73 \pm 1.61 \text{ KM/SEC}$ ,  $SIG.US = 0.13 \text{ KM/SEC}$ .

COMMENTS:

- 1) SOURCE: WAGNER, M.H., WALDORF, W.F. AND LOUIE, N.A.  
 REPORT NO. AFSWC-TDR-62-66, VOL. 1 (1962)  
 WORK DONE AT DOWNEY, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE A  
 DATA REDUCTION TECHNIQUE D  
 IN THE TABLE UP = (1/2)UFS
- 3) ACCURACY IS LIMITED BECAUSE ASSEMBLY DIMENSIONS ALLOW RELATIVELY  
 LARGE DEVIATION FROM ONE-DIMENSIONALITY.

TABLE 1  
KEL F (POLYTRIFLUOROCHLOROETHYLENE)  
23-10-9(2-1-3)---1



23-10-9(12-8-18)---1

POLYTRIFLUOROCHLOROETHYLENE (HALOFLUOROCARBON OIL)

CL-(C-F<sub>2</sub>-C(F)-CL)<sub>16</sub>-CL = F18-CL8-C12

T0 = 15-30 DEG. C

V0 = 0.506 - 0.513 CC/G

C0 = 0.95 KM/SEC

IN THE TABLE BELOW, TEMPERATURE (T) IS GIVEN IN DEGREES CENTIGRADE,  
DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| T  | RHOD  | US    | UP    | P    | V/V0  |
|----|-------|-------|-------|------|-------|
| 30 | 1.948 | 4.814 | 1.86  | 175  | 0.613 |
| 30 | 1.948 | 3.500 | 1.07  | 72.5 | 0.694 |
| 20 | 1.965 | 4.779 | 1.89  | 178  | 0.604 |
| 15 | 1.975 | 3.108 | 0.875 | 54   | 0.718 |

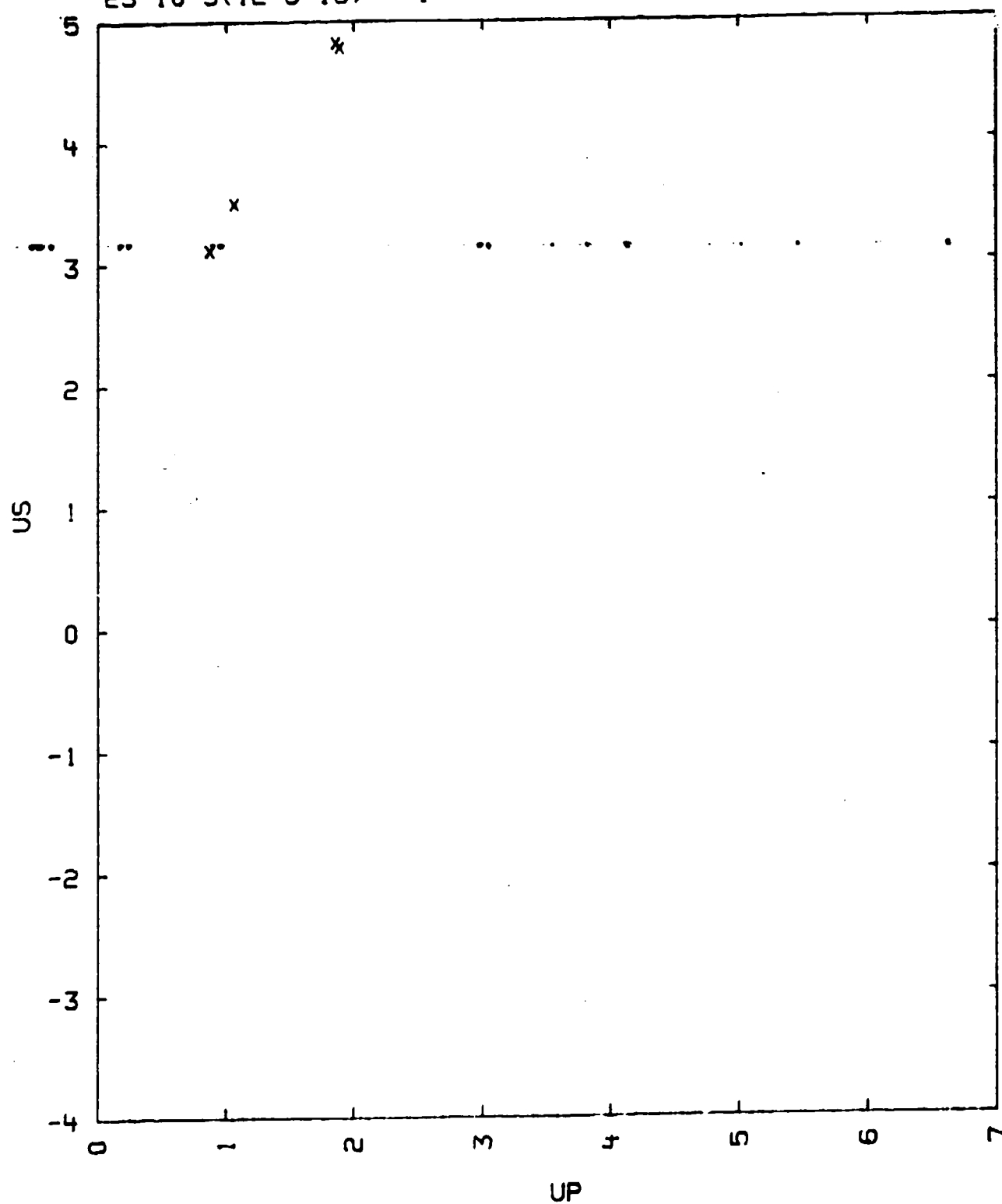
US = 1.69 + 1.66\*UP KM/SEC

SIGMA US = 0.05 KM/SEC

## COMMENTS:

- 1) SOURCE: RAMSAY, J. B.  
PRIVATE COMMUNICATION (1967)  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL ALUMINUM 2024.
- 3) THE MOLECULAR WEIGHT OF THIS POLYMER IS ABOUT 780 G.
- 4) C0 IS A ESTIMATED VALUE. BECAUSE OF HIGH ATTENUATION OF SOUND IN THE SAMPLE IT WAS NOT POSSIBLE TO MEASURE THE SOUND SPEED WITH THE USUAL PRECISION.

TABLE I  
POLYTRIFLUOROCHLOROETHYLENE (HALOFLUOROCARBON OIL)  
23-10-9(12-8-18) ---1



23-11-2(1-1-3)---1

BROMOFORM

C-H-BR3

DECOMPOSITION PRODUCTS

85 TO 95 PERCENT (ESTIMATED)

REMAINDER

T0 = 17-36 DEG. C

C0 = 0.93 KM/SEC

V0 = 0.356- 0.348 CC/G

IN THE TABLE, TEMPERATURE (T) IS GIVEN IN DEGREES CENTIGRADE, DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. M DENOTES THE SAMPLE MATERIAL (SEE COMMENT 4).

TABLE

| T  | RH00  | US   | UP   | P   | V/V0  | M |
|----|-------|------|------|-----|-------|---|
| 23 | 2.87  | 2.02 | 0.67 | 33  | 0.667 | D |
| 36 | 2.85  | 4.00 | 1.83 | 205 | 0.545 | C |
| 20 | 2.81  | 3.95 | 1.79 | 198 | 0.547 | A |
| 18 | 2.81  | 2.88 | 1.09 | 88  | 0.622 | A |
| 19 | 2.81  | 1.87 | 0.60 | 31  | 0.679 | A |
| 17 | 2.81  | 2.86 | 1.07 | 86  | 0.625 | A |
| 20 | 2.876 | 3.45 | 1.36 | 136 | 0.606 | B |
| 25 | 2.87  | 4.17 | 1.97 | 235 | 0.528 | B |
| 25 | 2.87  | 1.75 | 0.56 | 28  | 4.677 | C |
| 26 | 2.87  | 3.42 | 1.42 | 140 | 0.583 | C |
| 26 | 2.87  | 3.48 | 1.41 | 140 | 0.594 | C |
| 27 | 2.87  | 3.47 | 1.41 | 141 | 0.594 | C |

$$US = 0.210 + 3.061 \cdot UP + 0.433(2.876 - RH00) - 0.663(2.876 - RH00)UP - 0.53(2.876 - RH00)UP^2 \text{ KM/SEC} \quad \text{SIGMA US} = 0.04 \text{ KM/SEC}$$

## COMMENTS:

1) SOURCE: RAMSAY, J. B.

REPORTS NO. GMX-8-MR-62-6 AND GMX-8-MR-62-7 (1962)

LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA

2) EXPERIMENTAL TECHNIQUE : FOR THE FIRST ENTRY, TECHNIQUE E WAS USED.  
FOR ALL OTHER DATA POINTS TECHNIQUE B WAS USED.

## DATA REDUCTION TECHNIQUE B

STANDARD MATERIAL ALUMINUM 2024

3) ABSORPTION OF VISIBLE LIGHT AFTER ENTRY OF SHOCK INTO THE SAMPLE SUGGESTS DECOMPOSITION.

4) THE SAMPLE MATERIALS USED ARE LISTED BELOW:

A) PURITY NOT SPECIFIED, EASTMAN CHEMICAL CO., KINGSPORT, TENNESSEE USA.

B) STABILIZED WITH DIPHENYLAMINE, EASTMAN CHEMICAL CO., KINGSPORT, TENNESSEE, USA.

C) PRACTICAL GRADE, EASTMAN CHEMICAL CO., KINGSPORT, TENNESSEE, USA

D) PURITY NOT SPECIFIED, MATHESON, COLEMAN, AND BELL, EAST RUTHERFORD, NEW JERSEY, USA.

THE ABOVE VALUE OF PURITY WAS ESTIMATED. NO CHEMICAL ANALYSIS ON THE

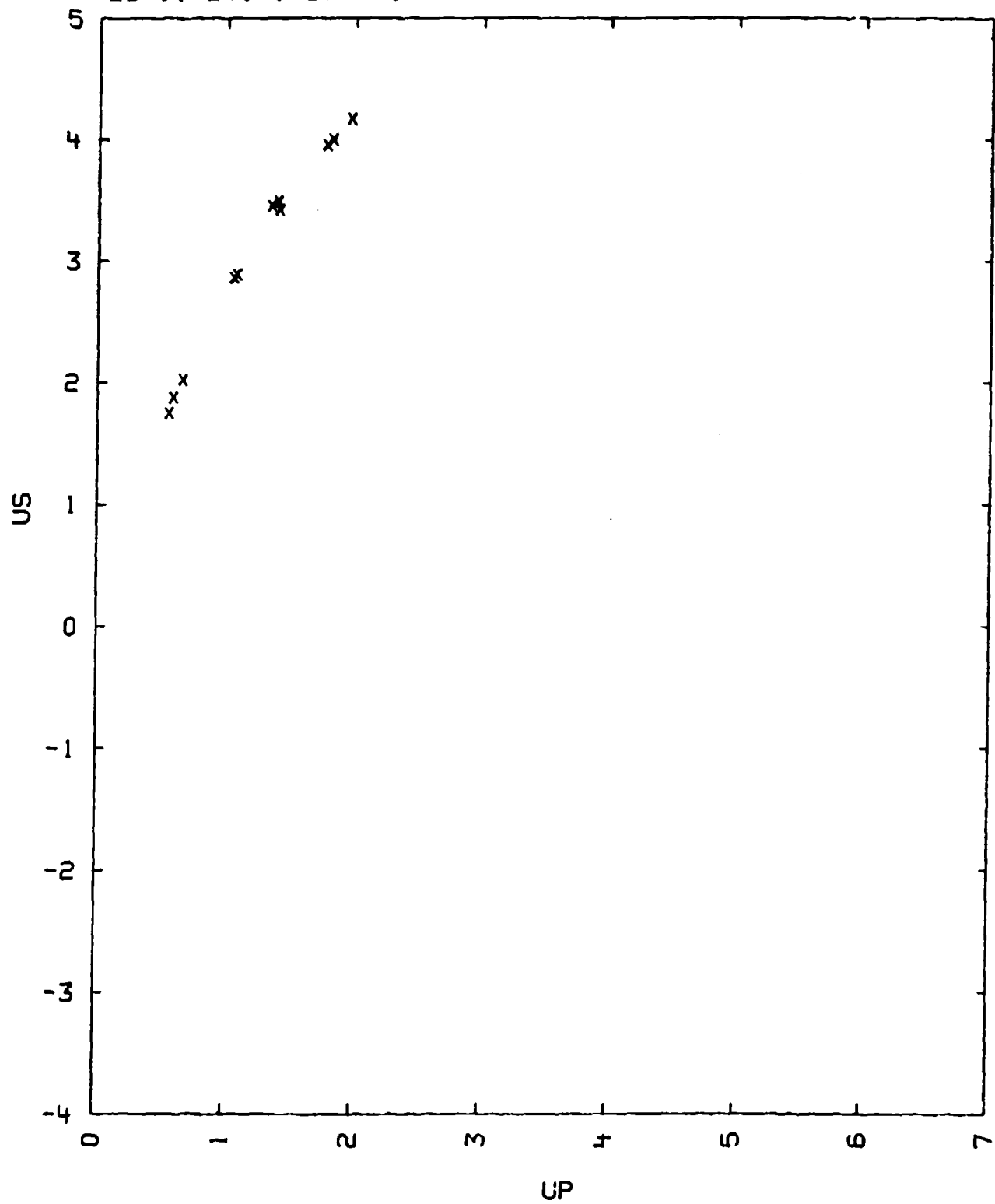
EXTENT OF DECOMPOSITION OF THIS LIGHT SENSITIVE MATERIAL HAS BEEN  
MADE.

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TABLE 1

BROMOFORM  
23-11-2(1-1-3)---1





23-11-2(2-5-1)---1

BROMOETHANE

H3-C-C(BR)H2 = C2-H5-BR

T0 = 16-19 DEG. CENTIGRADE

V0 = 0.682-0.685 CC/G.

CO(20 DEG.C) = 1.009 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN  
KILOBARS, DENSITY IN G/CC. AND TEMPERATURE IN DEG. CENTIGRADE

TABLE

| T0 | RH00  | US   | UP    | P     | V/V0  |
|----|-------|------|-------|-------|-------|
| 19 | 1.460 | 4.68 | 2.300 | 157.1 | 0.508 |
| 16 | 1.466 | 3.40 | 1.363 | 68.0  | 0.599 |

US =

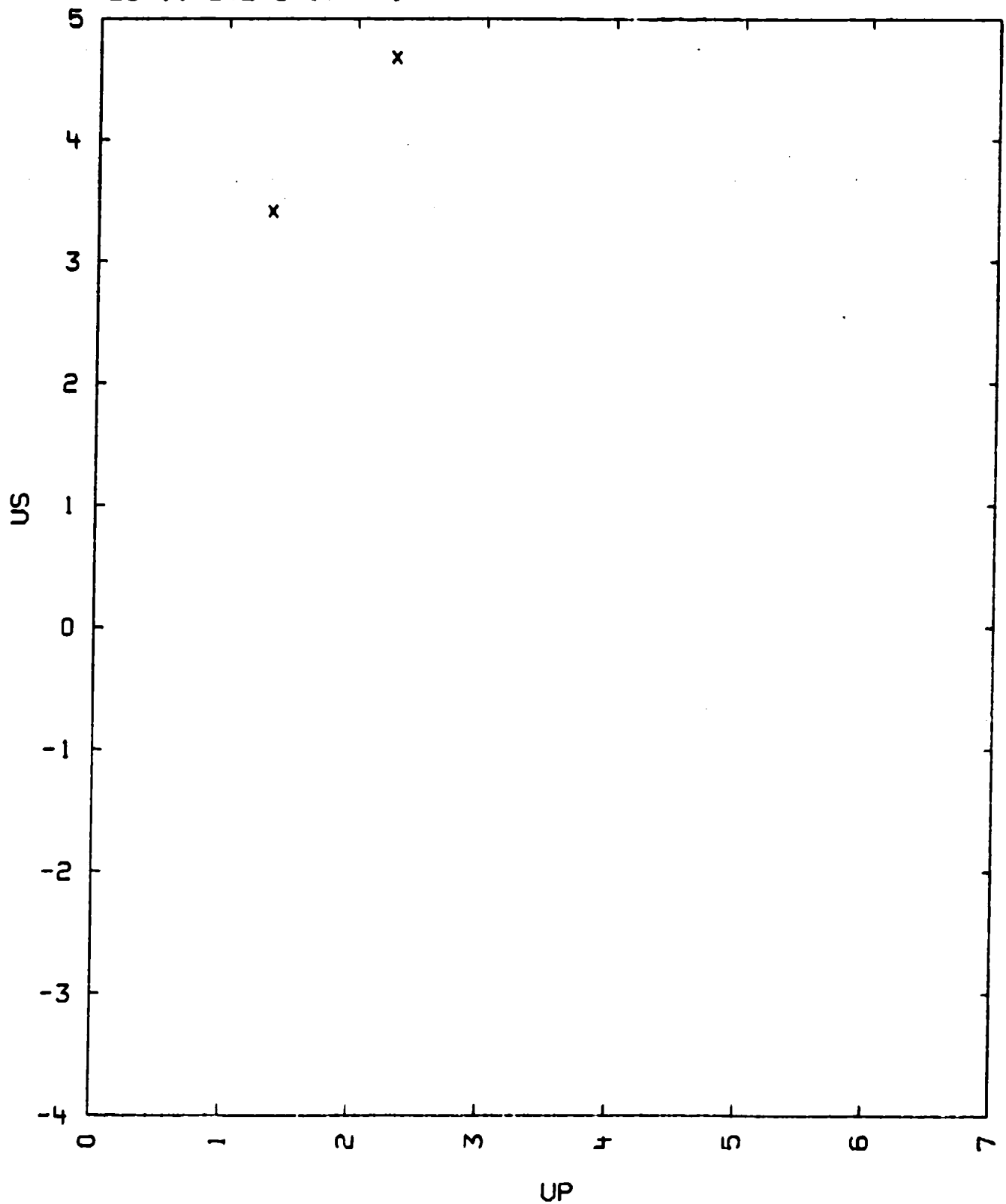
## COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 245T ALUMINUM
- 3) CO WAS OBTAINED FROM L. BERGMANN, DER ULTRASCHALL (S HIRZEL VERLAG,  
STUTTGART, 1954) 6TH ED., P. 375

TABLE I

BROMOETHANE

23-11-2(2-5-1)---1



23-18-2-1(1-1-3-3)---1  
NITROMETHANE

C(H3)-N-O3 = C-N-H3-O3

$V_0 = 0.884 \text{ CC/G}$

IN THE TABLE BELOW DENSITY IS IN G/CC, PRESSURE IN KBAR AND VELOCITIES IN KM/SEC.  $Z_0$  IS THE LENGTH NEEDED FOR BUILD-UP TO DETONATION IN MM. IN A 20 MM DIAMETER SAMPLE AND GT = GREATER THAN

TABLE

| RH00 | US   | UP   | P  | V/V0  | Z0   |
|------|------|------|----|-------|------|
| 1.13 | 4.40 | 1.76 | 86 | 0.602 | GT50 |
| -    | 4.15 | 1.55 | 73 | 0.628 | -    |
| -    | 3.78 | 1.27 | 54 | 0.667 | -    |
| -    | 3.50 | 1.08 | 43 | 0.690 | -    |
| -    | 3.37 | 0.90 | 35 | 0.730 | -    |
| -    | 2.83 | 0.62 | 20 | 0.782 | -    |

$US = 2.07 + 1.34 UP \text{ KM/SEC. } SIG.US = 0.06 \text{ KM/SEC.}$

COMMENTS:

1) SOURCE: ILYUKIN V. S., POKHIL P. F., ROZANOV O. K. AND SHVEDOVA N. S.  
DOKLADY AKAD NAUK SSSR VOL.131, P.793 (1960), OR  
SOVIET PHYS. DOKLADY VOL.5, P.337 (1960) (ENGLISH)

2) EXPERIMENTAL METHOD A

DATA REDUCTION METHOD B STANDARD MATERIAL, COPPER.

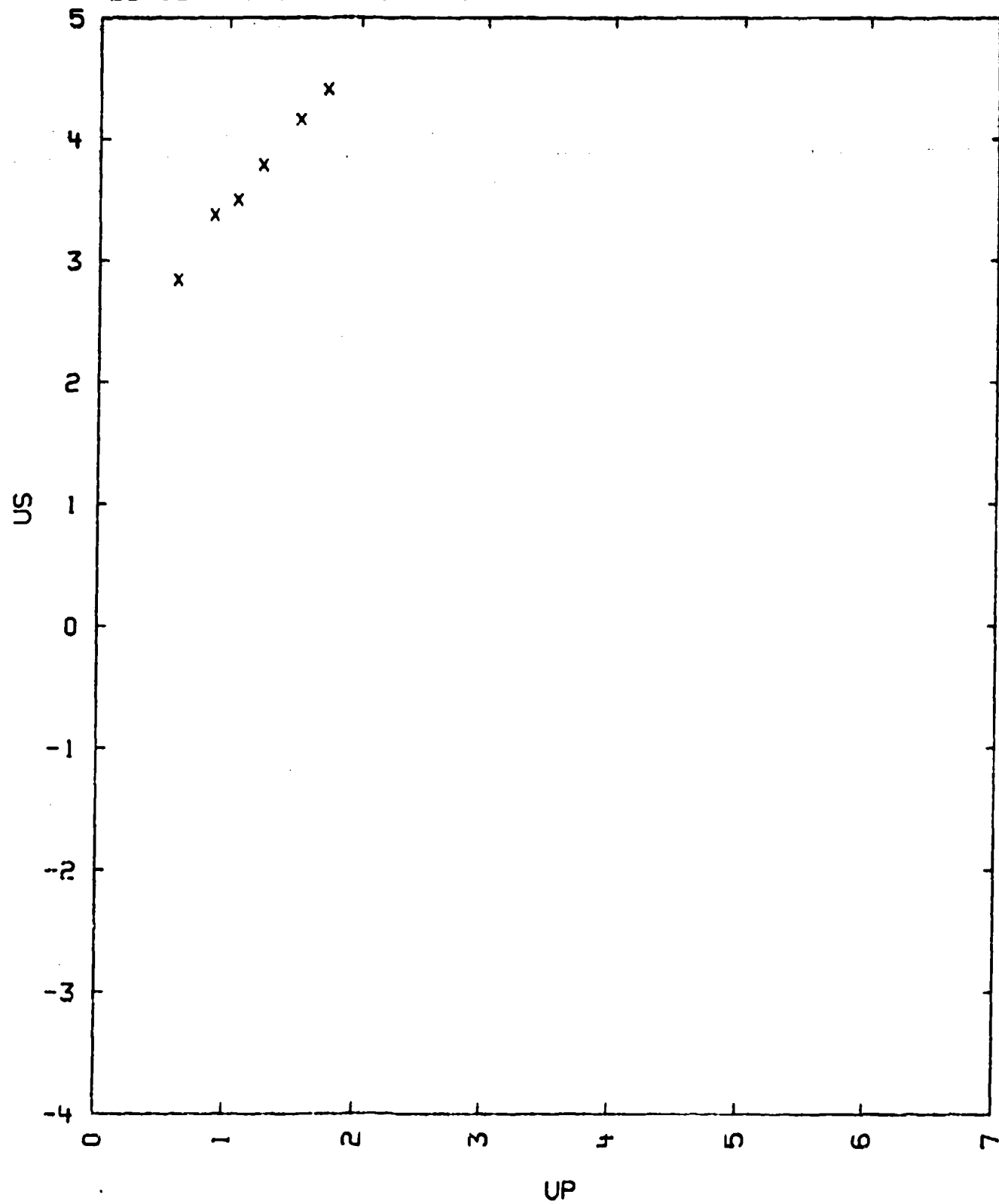
| US   | AND UP | OF COPPER |
|------|--------|-----------|
| 5.60 | 1.00   |           |
| 5.34 | 0.87   |           |
| 5.03 | 0.71   |           |
| 4.82 | 0.60   |           |
| 4.64 | 0.51   |           |
| 4.32 | 0.35   |           |

3) THE ABOVE FIT YIELDS A PRESSURE OF 209 KB AT THE DETONATION VELOCITY WHILE PCJ = 120 KBAR.

TABLE I

NITROMETHANE

23-18-2-1(1-1-3-3)---1



23-18-2-1(1-1-3-3)---2  
NITROMETHANE

C-113-N-03

T0 = 17.2-22.0 DEG. C  
V0 = 0.8865-0.8905 CC/G

IN THE TABLE BELOW, TEMPERATURE (T0) IS GIVEN IN DEGREES CENTIGRADE,  
DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| T0   | RH00  | US    | UP    | P    | V/V0  |
|------|-------|-------|-------|------|-------|
| 20.4 | 1.125 | 2.918 | 0.743 | 24.4 | 0.745 |
| 19.2 | 1.126 | 3.080 | 0.912 | 31.6 | 0.704 |
| 17.8 | 1.128 | 3.670 | 1.270 | 53.3 | 0.654 |
| 22.0 | 1.123 | 3.819 | 1.344 | 57.6 | 0.648 |
| 22.0 | 1.123 | 3.761 | 1.317 | 55.6 | 0.650 |
| 18.0 | 1.128 | 3.885 | 1.320 | 57.8 | 0.660 |
| 17.2 | 1.128 | 4.025 | 1.380 | 62.7 | 0.657 |
| 19.6 | 1.125 | 3.882 | 1.364 | 59.7 | 0.649 |
| 22.0 | 1.123 | 4.016 | 1.476 | 66.6 | 0.633 |
| 21.6 | 1.123 | 4.077 | 1.470 | 67.3 | 0.639 |
| 17.3 | 1.128 | 4.243 | 1.493 | 71.5 | 0.648 |
| 22.1 | 1.123 | 4.639 | 1.839 | 95.8 | 0.604 |
| 22.0 | 1.123 | 4.629 | 1.841 | 95.7 | 0.602 |

US =  $1.560 + 1.721 \cdot UP + 1.082(1.125 - RH00)$  KM/SEC  
SIGMA US = 0.05 KM/SEC

COMMENTS:

- 1) SOURCE: CRAIG, B. G.  
REPORT NO. GMX-8-MR-62-4 (1982)  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE E: THE SAMPLE WAS CONTAINED IN A WEDGE-SHAPED CELL MOUNTED ON THE BASE PLATE. THE FREE SURFACE OF THE BASE PLATE AND THE FREE SURFACE OF THE SAMPLE CELL WERE MEASURED. THUS, AN AVERAGE UP IS DETERMINED.

DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL ALUMINUM 2024

- 3) DETONATION OF THE SAMPLE OCCURRED WHEN UP WAS 1.839 KM/SEC. THE DIFFERENCE IN THE TWO PARTICLE VELOCITIES OF THE UNREACTED NITROMETHANE SAMPLE OBTAINED FROM THE BASE AND COVER PLATES WAS APPROXIMATELY  $\pm 0.05$  KM/SEC. SINCE THERE WAS NO CORRELATION OF THIS DIFFERENCE WITH PRESSURE IT SEEMS THAT NO SIGNIFICANT REACTION OR ATTENUATION OCCURRED BEHIND THE SHOCK FRONT, FOR ALL BUT THE HIGHEST PRESSURE.
- 4) THE EXPERIMENTAL HUGONIOT DATA WERE EXTRAPOLATED TO OBTAIN THE INTERSECTION WITH THE RAYLEIGH LINE ( $D \cdot RH00$ , WHERE D IS THE DETONATION VELOCITY). THIS INTERSECTION DETERMINES A VON NEUMANN SPIKE OF

199 KILOBARS, UP = 2.820 KM/SEC.

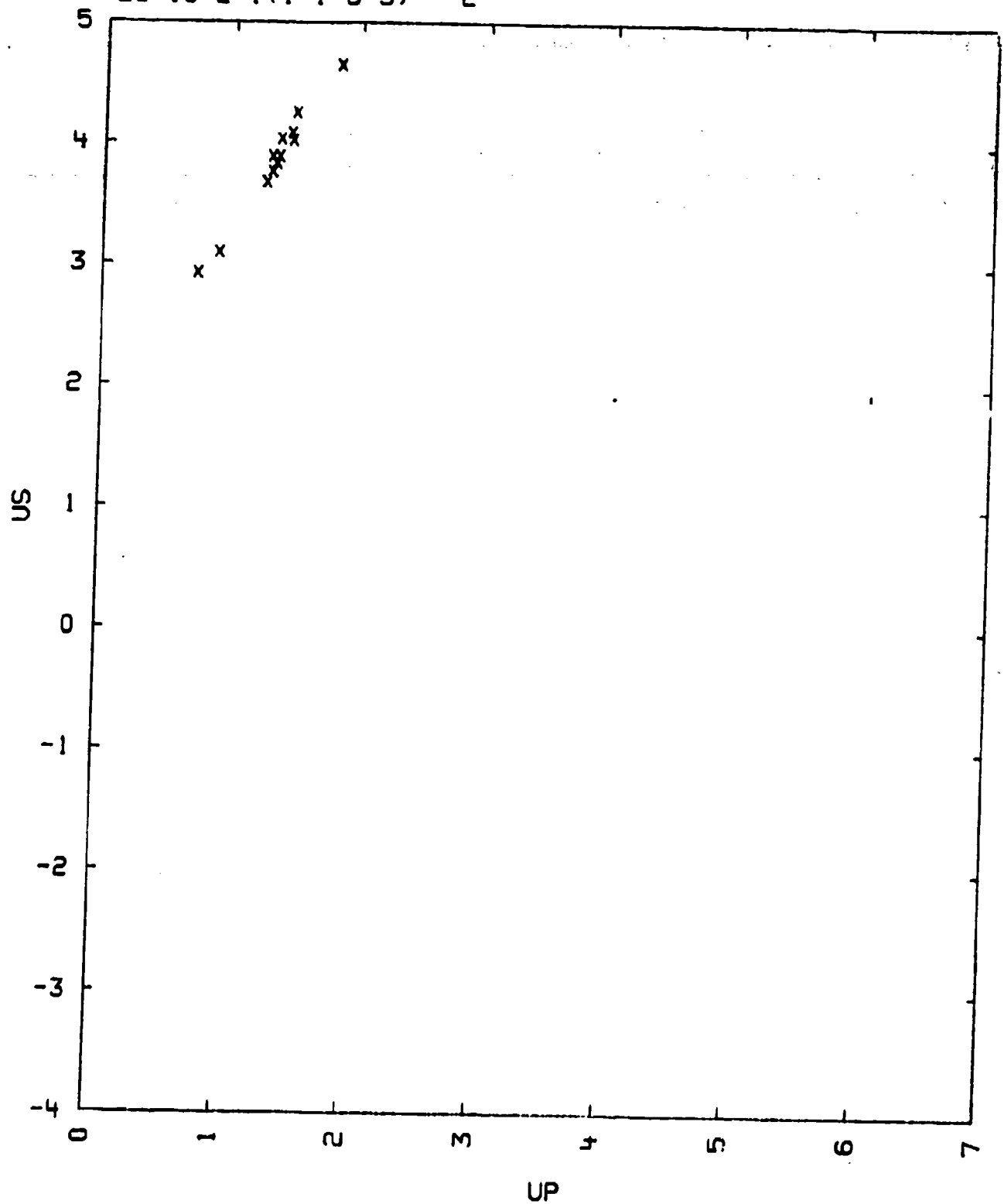
5) THE DENSITIES WERE CALCULATED USING THE THERMAL EXPANSION  
COEFFICIENT  $\beta_0$ :

$$\beta_0 = (1.159 \pm 0.01) \cdot 10^{-3}$$

MALIN, CAMPBELL, AND HOLLAND, JOURNAL OF APPLIED PHYSICS, VOL. 27,  
P 963 (1956).

TABLE 1

NITROMETHANE  
23-18-2-1(1-1-3-3)---2



23-18-2-1(2-X-Y-Z)---1  
 NYLON (POLYAMID)

C(2)N(X)H(Y)O(Z)

$V_0 = 0.877 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC, AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US   | UP    | P    | V/V0   |
|------|------|-------|------|--------|
| 1.14 | 2.40 | 0.135 | 3.64 | 0.9437 |
| -    | 2.38 | 0.165 | 4.50 | 0.9307 |
| -    | 3.52 | 0.505 | 20.2 | 0.8365 |
| -    | 3.51 | 0.665 | 26.6 | 0.8105 |
| -    | 4.56 | 1.55  | 80.2 | 0.6601 |

$US = 2.29 + 1.63 \text{ UP MM/MICROSEC}$

COMMENTS:

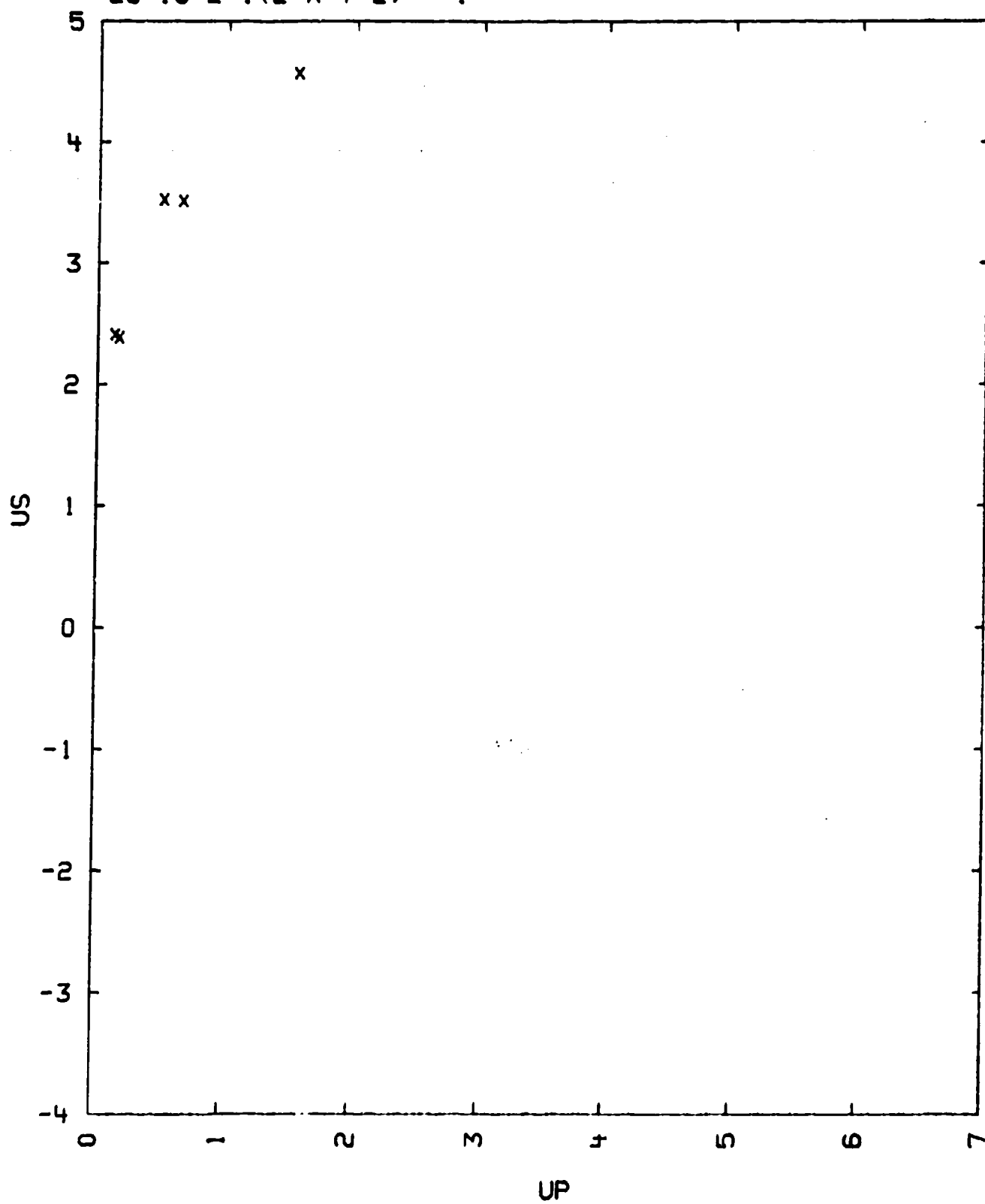
- 1) SOURCE: WAGNER, M.H., WALDORF, W.F. AND LOUIE, N.A.  
 REPORT NO. AFSWC-TDR-62-66, VOL. 1 (1962)  
 WORK DONE AT DOWNEY, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE A  
 DATA REDUCTION TECHNIQUE D  
 IN THE TABLE UP = (1/2)UFS
- 3) ACCURACY IS LIMITED BECAUSE ASSEMBLY DIMENSIONS ALLOW RELATIVELY LARGE DEVIATIONS FROM ONE-DIMENSIONALITY.



TABLE 1

NYLON (POLYAMID)

23-18-2-1(2-X-Y-Z)---1



23-18-2-1(2-X-Y-Z)---2  
 NYLON (POLYAMID)

C(2)N(X)H(Y)O(Z) WHERE X,Y,Z ARE RATIONAL NUMBERS

$V_0 = 0.8718 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/SEC. PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |       |       |       | -STANDARD- |       |
|------------------|-------|-------|-------|------------|-------|
| RH00             | US    | UP    | P     | V/V0       | UFS   |
| 1.147            | 5.924 | 1.973 | 134   | 0.667      | 2.765 |
| -                | 5.896 | 1.975 | 133.5 | 0.665      | 2.750 |
| -                | 6.105 | 2.057 | 144   | 0.663      | 2.910 |
| -                | 6.105 | 2.071 | 145   | 0.661      | 2.880 |
| -                | 5.834 | 1.913 | 128   | 0.672      | 2.650 |
| -                | 5.834 | 1.928 | 129   | 0.670      | 2.665 |
| -                | 5.924 | 1.959 | 133   | 0.669      | 2.740 |
| -                | 5.945 | 1.957 | 133.5 | 0.671      | 2.735 |
| -                | 5.624 | 1.753 | 114   | 0.688      | 2.440 |
| -                | 5.567 | 1.813 | 116   | 0.674      | 2.510 |
| -                | 5.682 | 1.763 | 115   | 0.690      | 2.445 |
| -                | 5.682 | 1.763 | 115   | 0.690      | 2.445 |
| -                | 5.242 | 1.592 | 95.5  | 0.696      | 2.175 |
| -                | 5.192 | 1.600 | 96    | 0.692      | 2.185 |
| -                | 5.236 | 1.567 | 94    | 0.701      | 2.142 |
| -                | 5.225 | 1.567 | 94    | 0.700      | 2.140 |
| -                | 4.980 | 1.395 | 79.5  | 0.720      | 1.980 |
| -                | 4.955 | 1.386 | 79    | 0.720      | 1.875 |
| -                | 4.897 | 1.335 | 75    | 0.727      | 1.790 |
| -                | 4.916 | 1.312 | 74    | 0.733      | 1.775 |
| -                | 4.812 | 1.309 | 72    | 0.728      | 1.760 |
| -                | 4.668 | 1.305 | 70.5  | 0.720      | 1.740 |
| -                | 4.716 | 1.250 | 67.5  | 0.735      | 1.670 |
| -                | 4.599 | 1.226 | 65    | 0.733      | 1.645 |
| -                | 4.421 | 1.045 | 53    | 0.764      | 1.335 |
| -                | 4.421 | 1.065 | 54    | 0.759      | 1.350 |
| -                | 4.252 | 1.065 | 52    | 0.750      | 1.392 |
| -                | 4.230 | 1.062 | 51.5  | 0.749      | 1.392 |
| -                | 4.058 | 0.925 | 43    | 0.772      | 1.185 |
| -                | 4.119 | 0.922 | 43.5  | 0.776      | 1.185 |
| -                | 4.125 | 0.909 | 43    | 0.780      | 1.777 |
| -                | 4.112 | 0.911 | 43    | 0.778      | 1.180 |
| -                | 4.156 | 0.996 | 47.5  | 0.760      | 1.297 |
| -                | 4.098 | 1.011 | 47.5  | 0.753      | 1.305 |
| -                | 4.378 | 1.016 | 51    | 0.768      | 1.325 |
| -                | 4.394 | 1.012 | 51    | 0.770      | 1.328 |

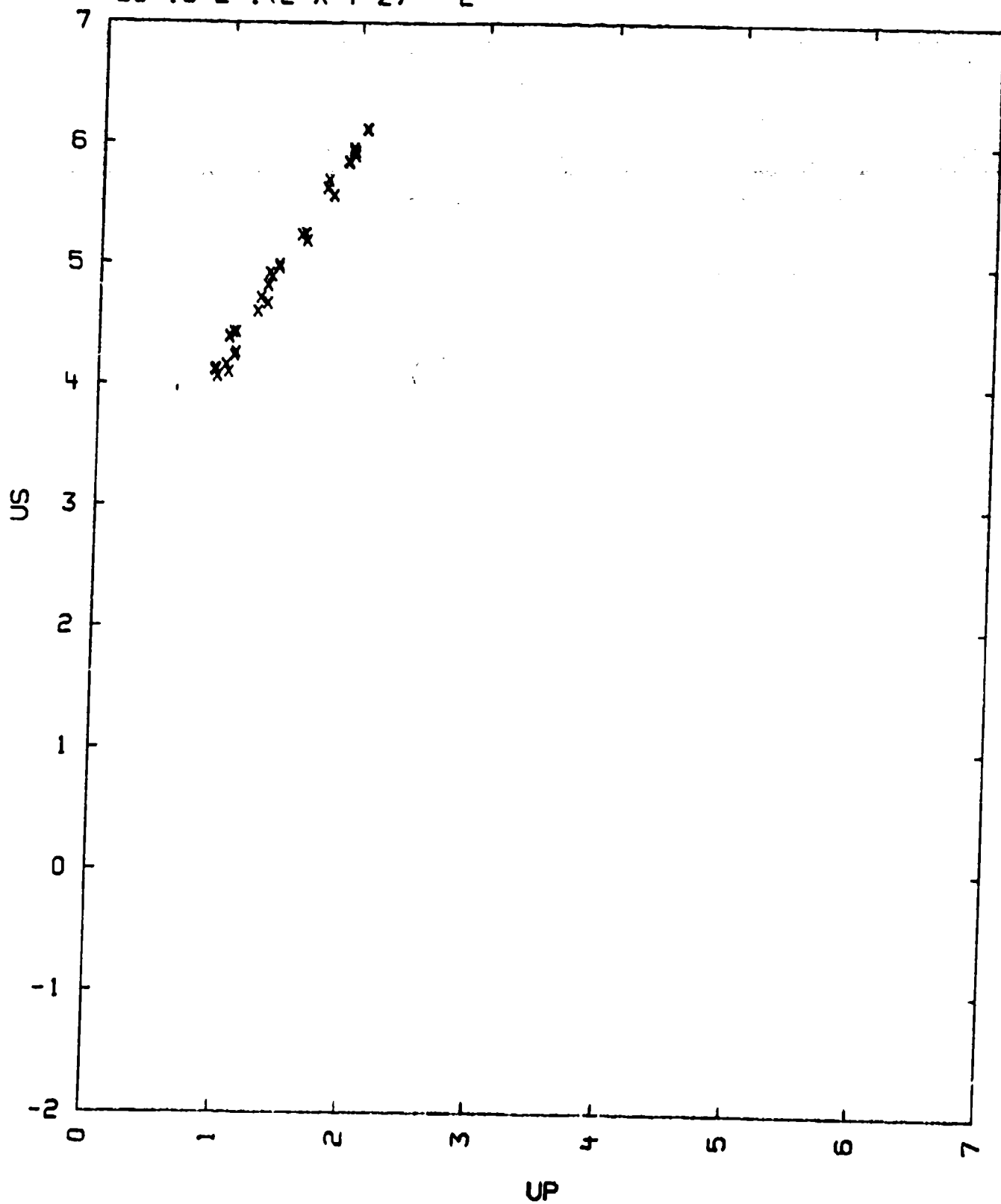
$US = 2.500 + 1.747 \text{ UP KM/SEC.}$

COMMENTS:

- 1) SOURCE: BERGER J. AND FAUQUIGNON C.  
PRIVATE COMMUNICATION (1964), B.P. NO. 7. SEVRAN, FRANCE
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIALS ALUMINUM AU40
- 3) SAMPLE DIMENSIONS WERE: 2.0 CM DIAMETER  
0.5 CM THICKNESS

TABLE I

NYLON (POLYAMID)  
23-18-2-1(2-X-Y-Z)---2



23-18-2-1(2-X-Y-Z)---3  
POLYURETHANE FOAM

C(2)N(X)H(Y)O(Z)

$V_0 = 3.125 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC.  
AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US    | UP   | P   | V/V0 |
|------|-------|------|-----|------|
| 0.32 | 5.51  | 3.79 | 70  | .312 |
| -    | 5.38  | 3.86 | 70  | .283 |
| -    | 5.55  | 3.91 | 70  | .296 |
| -    | 6.52  | 5.21 | 110 | .201 |
| -    | 6.90  | 5.01 | 110 | .274 |
| -    | 7.13  | 5.15 | 117 | .282 |
| -    | 7.35  | 5.10 | 120 | .306 |
| -    | 12.19 | 9.36 | 365 | .216 |
| -    | 11.27 | 8.76 | 316 | .223 |
| -    | 12.88 | 9.23 | 380 | .263 |

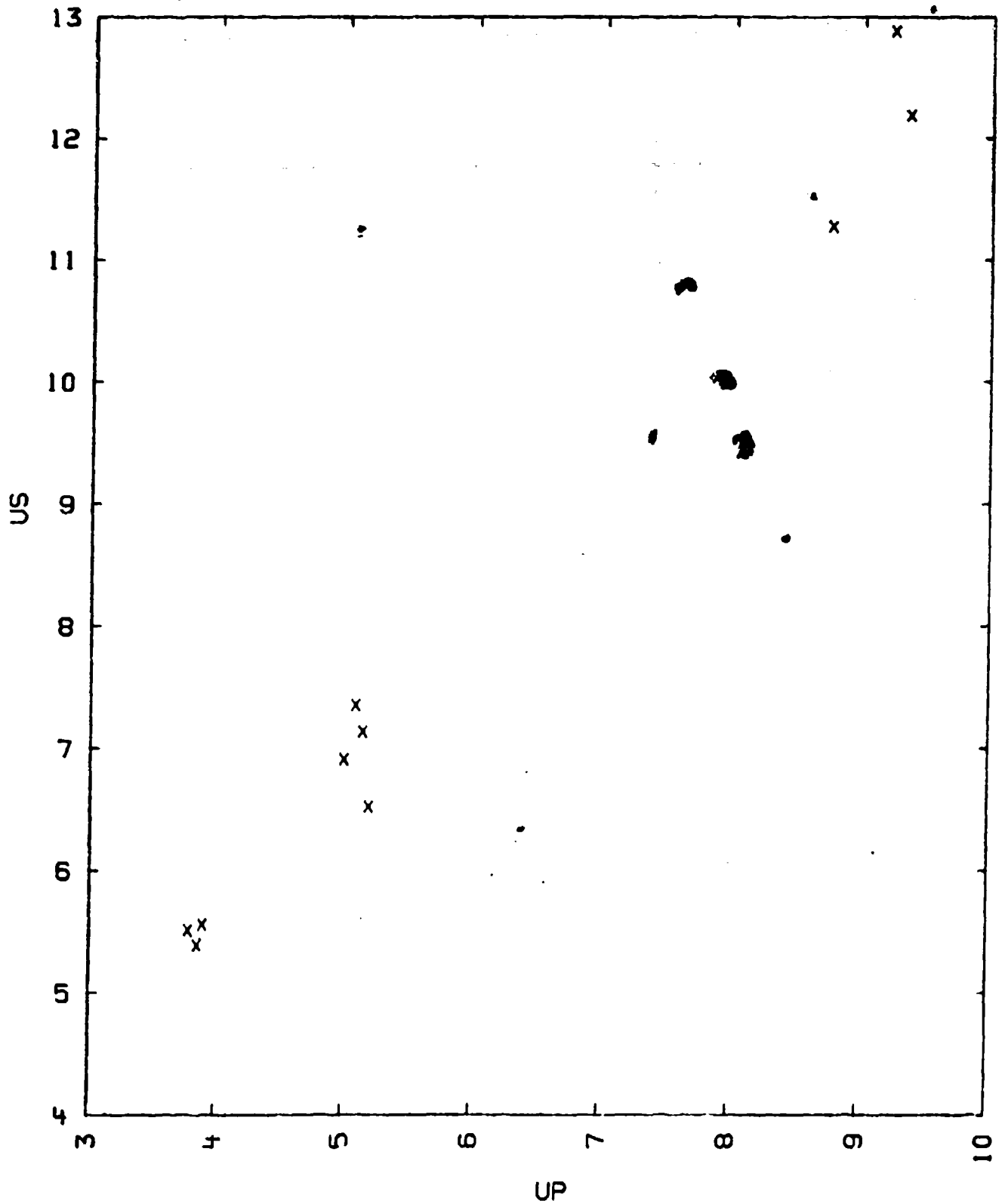
$US = 0.35 + 1.290 UP \text{ KM/SEC. SIG.US} = 0.38 \text{ KM/SEC.}$

COMMENTS:

- 1) SOURCE: SKIDMORE, I.C. AND MORRIS, E.  
THERMODYNAMICS OF NUCLEAR MATERIALS, P. 173 FF. (1962)  
INTERN. AT. ENERGY AGENCY, VIENNA  
ATOMIC WEAPONS RESEARCH ESTABLISHMENT, ALDERMASTON, ENGLAND
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION TECHNIQUE B  
THE SHOCK WAVE WAS PRODUCED BY AN EXPLOSIVELY ACCELERATED EN3 STEEL PLATE.  
THE SHOCK WAS TRANSMITTED THROUGH A STEEL PLATE INTO THE SAMPLE.
- 3) THE VELOCITY OF THE FLYING PLATE AND THE SHOCK AND SURFACE VELOCITY OF THE TARGET PLATE WERE MEASURED AS WELL AS THE SAMPLE SURFACE AND SHOCK VELOCITIES.
- 4) DATA SCATTER WAS ABOUT 0.03 MICROSEC.
- 5) CORRECTIONS WERE MADE FOR FLYING PLATE CURVATURE OF UP TO 1 MICROSEC.
- 6) THE HIGHER PRESSURES WERE OBTAINED BY A SPHERICALLY CONVERGING SYSTEM.
- 7) ALL PELLETS WERE SURROUNDED BY LEAD TO REDUCE LATERAL RAREFACTION.

TABLE I

POLYURETHANE FOAM  
23-18-2-1(2-X-Y-Z)---3



23-18-2-1(3-6-6-6)---1

CYCLOHEXANE, 1,3,5-TRINITRO, 1,3,5-TRIAZA (HEXOGEN) (CYCLONITE) (EXPLOSIVE)

(N(N-02)-C(H2)-)3 = C3-N6-H6-O6

V0 = 0.555 CC/G

V01 = 0.549 CC/G

IN THE TABLE BELOW DENSITY IS IN G/CC, PRESSURE IN KBAR AND VELOCITIES IN KM/SEC. Z0 IS THE LENGTH NEEDED FOR BUILD-UP TO DETONATION IN MM. IN A 20 MM DIAMETER SAMPLE AND GT = GREATER THAN

TABLE

| RHO0 | US   | UP   | P   | V/V0  | Z0   |
|------|------|------|-----|-------|------|
| 1.80 | 5.40 | 1.60 | 155 | 0.705 | 5    |
| -    | 5.22 | 1.40 | 131 | 0.731 | 9    |
| -    | 4.71 | 1.16 | 98  | 0.752 | 23   |
| -    | 4.42 | 0.98 | 78  | 0.782 | GT50 |
| -    | 4.30 | 0.83 | 64  | 0.807 | -    |

$$US = 2.87 + 1.61 \cdot UP \text{ KM/SEC.}$$

## COMMENTS:

1) SOURCE: ILYUKIN V. S., POKHIL P. F., ROZANOV O. K. AND SHVEDOVA N. S.  
DOKLADY AKAD NAUK SSSR VOL.131, P.793 (1960), OR  
SOVIET PHYS. DOKLADY VOL.5, P.337 (1960) (ENGLISH)

## 2) EXPERIMENTAL METHOD A

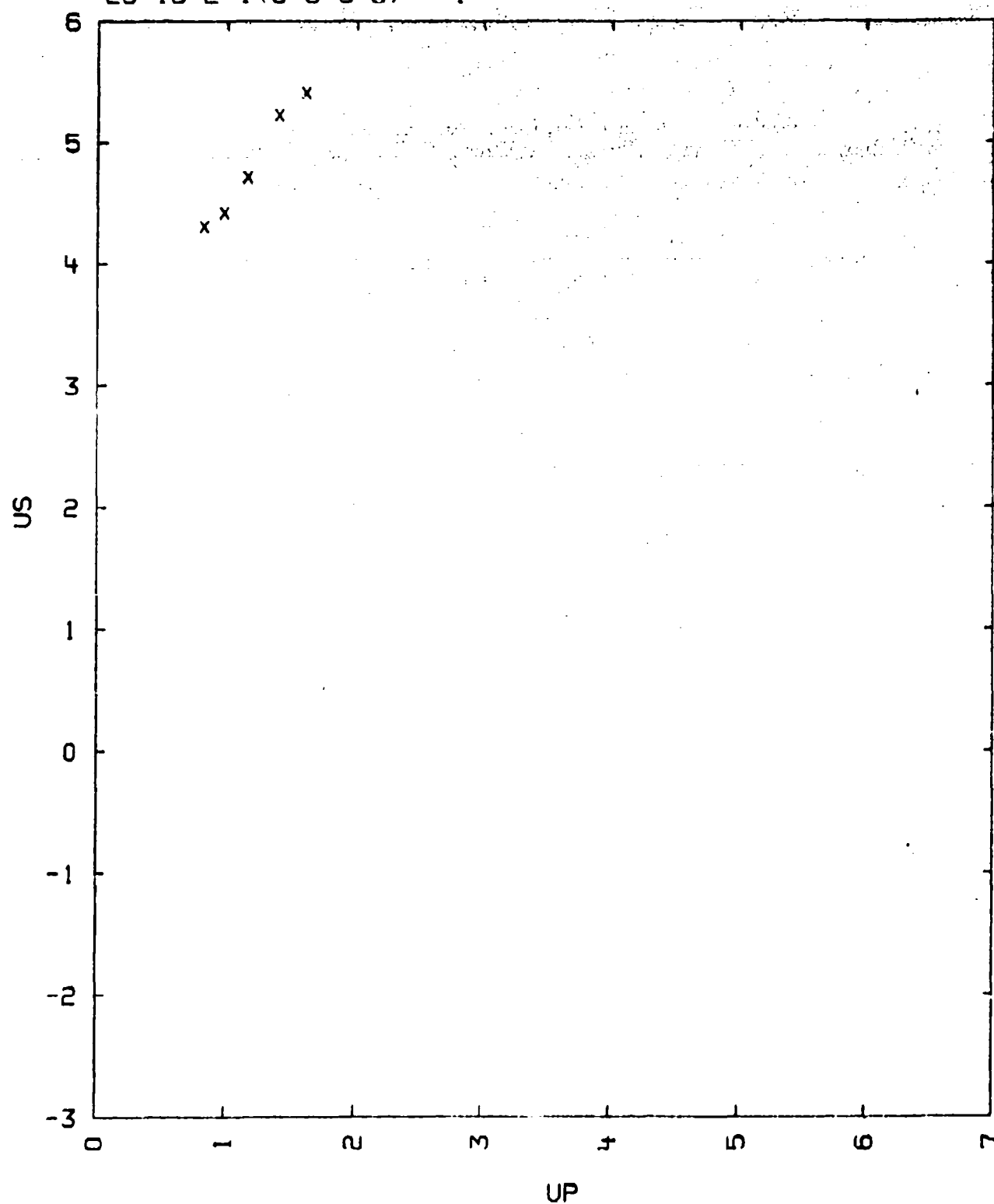
DATA REDUCTION METHOD B STANDARD MATERIAL COPPER.

| US   | AND UP | OF COPPER |
|------|--------|-----------|
| 5.60 | 1.00   |           |
| 5.34 | 0.87   |           |
| 5.03 | 0.71   |           |
| 4.82 | 0.60   |           |
| 4.64 | 0.51   |           |
| 4.32 | 0.35   |           |

3) THE ABOVE FIT YIELDS A PRESSURE OF 592 KB AT THE DETONATION VELOCITY WHILE PCJ = 390 KBARS.

4) V01 WAS OBTAINED FROM THE HANDBOOK OF CHEM. AND PHYS (CHEM RUBBER PUBL. CO. 1964) 45TH ED

TABLE 1  
CYCLOHEXANE, 1,3,5-TRINITRO, 1,3,5-TRIAZA (HEXOGEN) (  
23-18-2-1(3-6-6-6)---1





23-18-2-1(6-1-5-2)---1  
NITROBENZENE

C6(H5)-N-02

$V_0 = 0.834 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR.

TABLE

| RH00  | US   | UP   | P    | V/V0  |
|-------|------|------|------|-------|
| 1.199 | 5.72 | 2.33 | 160. | 0.593 |
| -     | 3.83 | 1.17 | 53.7 | 0.694 |
| -     | 3.30 | 0.79 | 31.2 | 0.761 |
| -     | 3.24 | 0.78 | 30.3 | 0.759 |
| -     | 3.28 | 0.80 | 31.5 | 0.756 |

$US = 2.01 + 1.59 \cdot UP \text{ KM/SEC.}$   
 $SIG US = 0.03 \text{ KM/SEC.}$

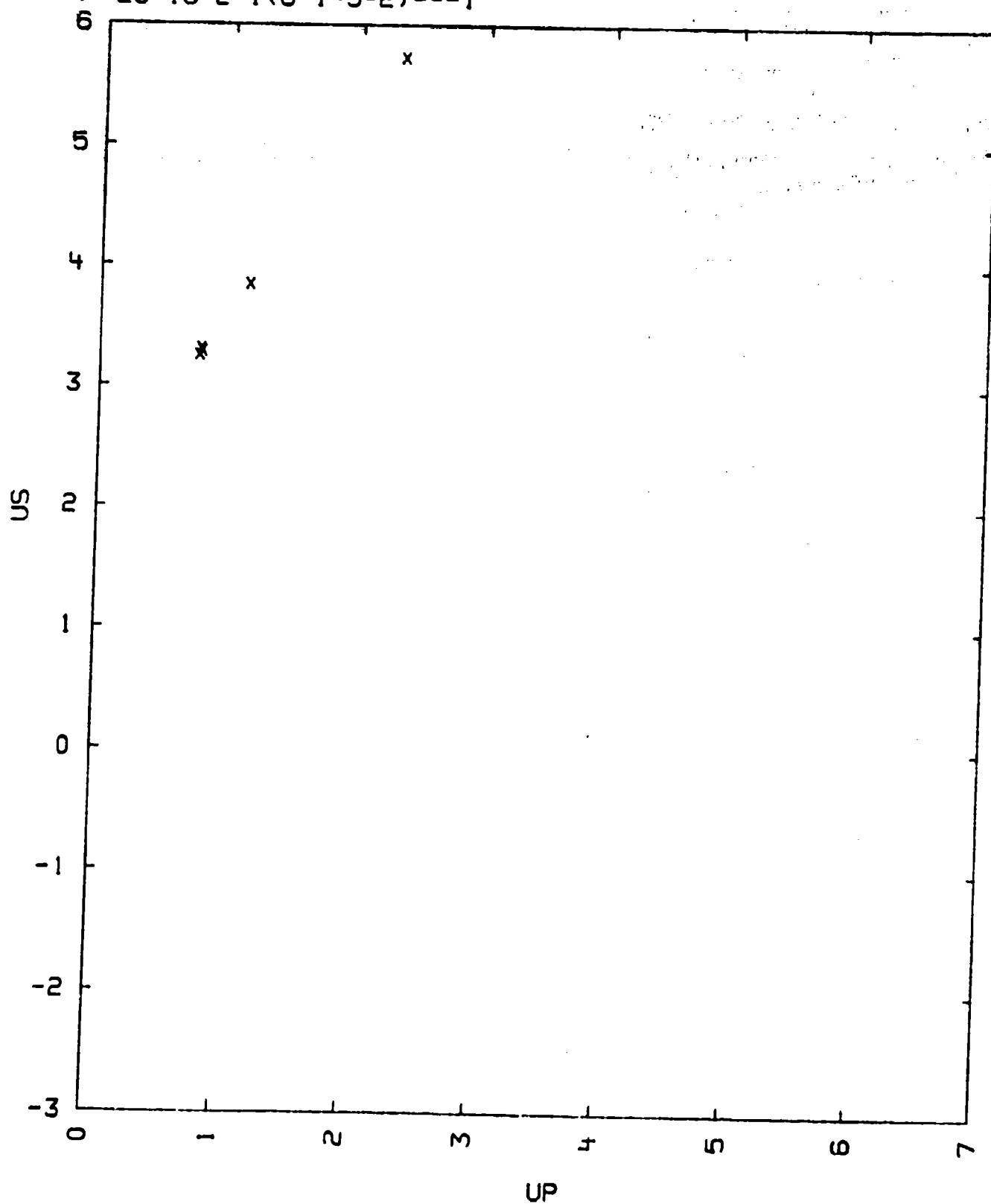
COMMENTS:

- 1) SOURCE: HAUVER, G. E. AND MELANI, A.  
 PRIVATE COMMUNICATION, JAN. 1969.  
 BALLISTICS RES. LAB., ABERDEEN PROVING GROUNDS  
 MARYLAND, USA.
- 2) EXPERIMENTAL TECHNIQUE: H  
 DATA REDUCTION TECHNIQUE: B  
 STANDARD MATERIALS: AL. BRASS, MG. AND  
 PLEXIGLAS WITH  $US=2.702+1.544 \cdot UP$  AND  $RH00=$   
 $=1.18 \text{ G/CC}$  DEFINING THE HUGONOT OF THE  
 LATTER.
- 3) THE RELEASE CURVES OF THE METAL WERE LOCATED FROM A MEASUREMENT OF  
 THE SHOCK VELOCITY OF THE PLEXIGLASS STANDARD

TABLE I

NITROBENZENE

23-18-2-1(6-1-5-2)---1



23-18-2-116-3-3-6)---]

TRINITROBENZENE, 1,3,5 (TNB) (EXPLOSIVE)

(C(H)-C(N-02)-13 = C6-N3-H3-06

V0 = 0.6097 CC/G

C0 = 2.358 KM/SEC

V01 = 0.5924 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS

TABLE

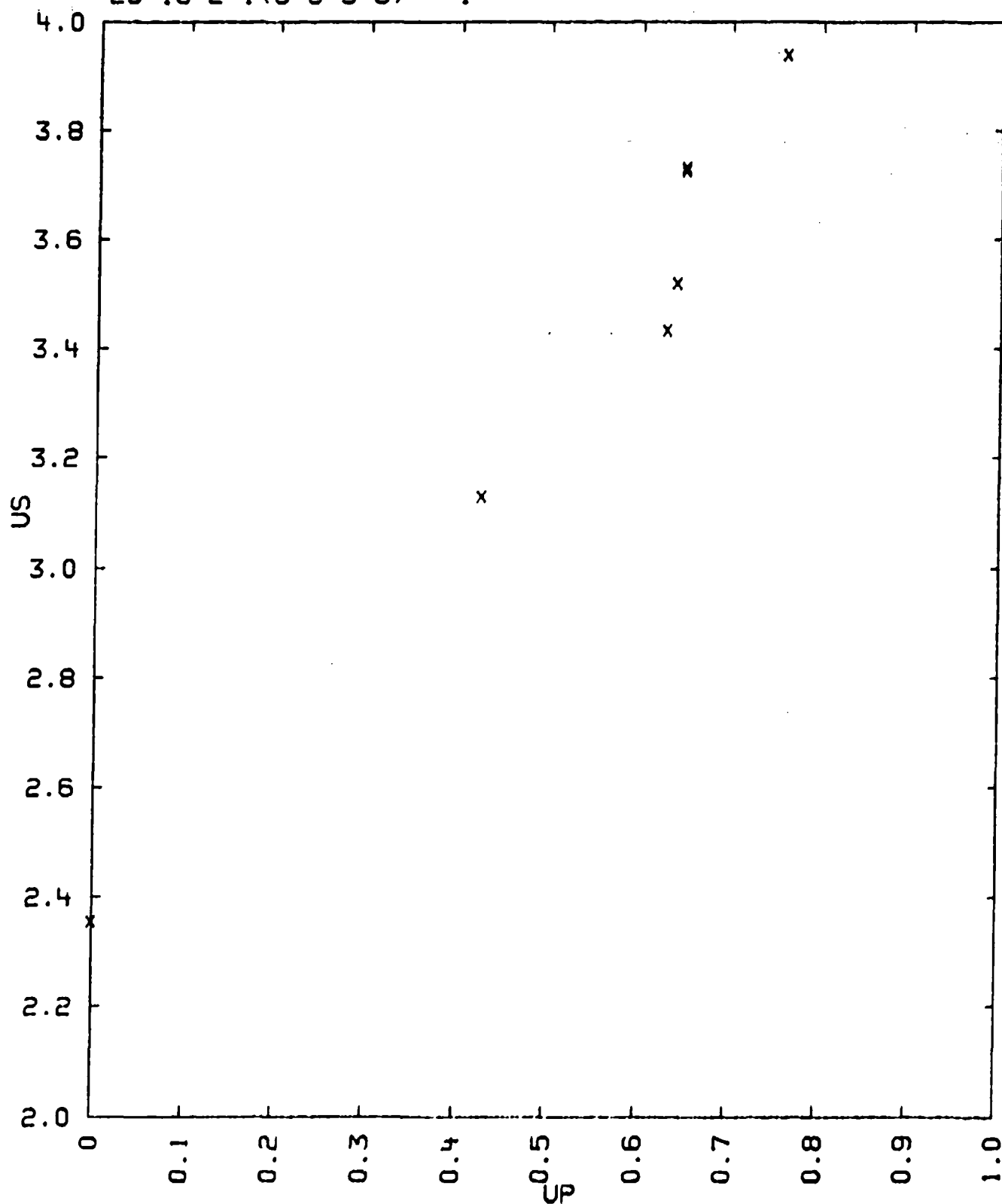
| RH00  | US    | UP    | P    | V/V0  |
|-------|-------|-------|------|-------|
| 1.640 | 3.129 | 0.426 | 21.8 | 0.663 |
| -     | 3.727 | 0.650 | 39.7 | 0.825 |
| -     | 3.730 | 0.650 | 39.7 | 0.825 |
| -     | 3.938 | 0.760 | 49.0 | 0.807 |
| -     | 3.432 | 0.630 | 35.4 | 0.816 |
| -     | 3.520 | 0.640 | 36.9 | 0.818 |
| -     | 2.356 | 0.000 | 0.0  | 1.00  |

US = A + B\*UP    A = 2.318 KM/SEC, SIGA = 0.072 KM/SEC  
 SIGUS = 0.11 KM/SEC    B = 2.025,    SIGB = 0.123

## COMMENTS:

- 1) SOURCE: COLEBURN N. L. AND LIDDIARD JR. T. P.  
 J. CHEM. PHYS., VOL. 44, P. 1929 (1965)  
 ALSO: PRIVATE COMMUNICATION
- 2) EXPERIMENTAL TECHNIQUE C1  
 DATA REDUCTION METHOD B:  $UP = 1/2 \cdot UP$  WAS ASSUMED FOR THE STANDARD MATERIALS BRASS AND PLEXIGLAS. SO THAT THE PRESSURE RELEASE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS UP HUGONIOT IN THE LINE  $UP = 1/2 \cdot UFS$
- 3) FOR BRASS  $US = 3.560 + 1.833 \cdot UP$  KM/SEC.  
 FOR PLEXIGLAS  $US = 2.710 + 1.568 \cdot UP - 0.037 \cdot UP^2$
- 4) THE GRUNEISEN COEFFICIENT  $\gamma = V(OP/OE) = 0.716$
- 5) V01 OBTAINED FROM: HANDBOOK OF CHEM. AND PHYS. (CHEM. RUBBER PUBL. CO., CLEVELAND, OHIO, 1963) 44TH ED.
- 6) C0 IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN UNCERTAINTY OF ABOUT 10 PERCENT

TABLE I  
TRINITROBENZENE, 1,3,5 (TNB) (EXPLOSIVE)  
23-18-2-1(6-3-3-6)---1



23-18-2-1(6-4-4-6)---1

BENZENE, 1-AMINO, 2,4,6-TRINITRO (TNA) (EXPLOSIVE)

-C(N-H2)-C(N-O2)(C(H)-C(N-O2))-12 = C6-N4-H4-O6  
NYLON95 PERCENT BY WT  
5 PERCENT BY WT.

V0 = 0.6250 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS

TABLE

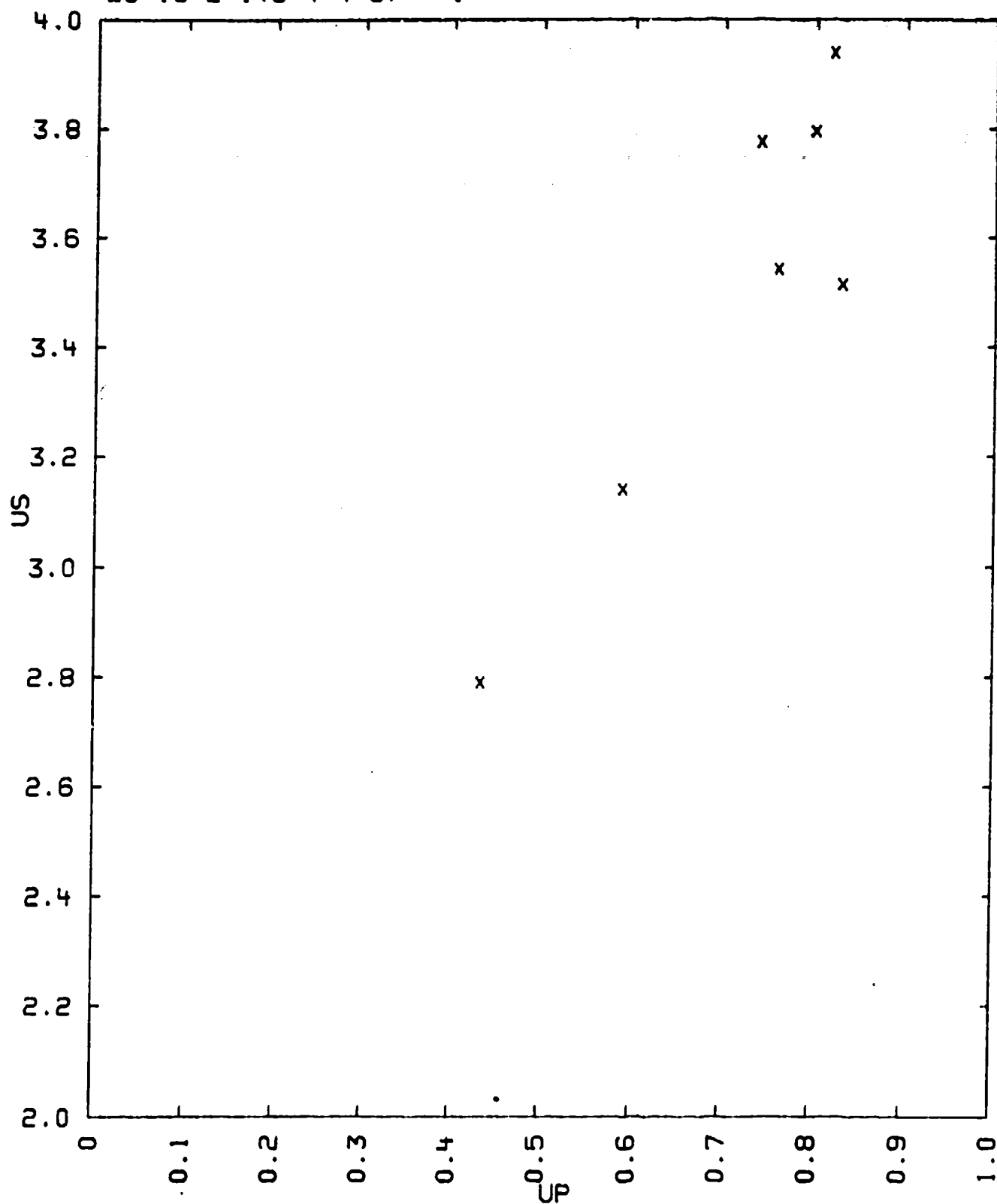
| RH00  | US    | UP    | P    | V/V0  |
|-------|-------|-------|------|-------|
| 1.600 | 3.140 | 0.590 | 29.6 | 0.812 |
| -     | 2.789 | 0.433 | 19.3 | 0.844 |
| -     | 3.938 | 0.820 | 51.6 | 0.791 |
| -     | 3.541 | 0.760 | 43.0 | 0.785 |
| -     | 3.774 | 0.740 | 44.6 | 0.803 |
| -     | 3.793 | 0.800 | 48.5 | 0.789 |
| -     | 3.515 | 0.830 | 46.6 | 0.763 |

US = A + B\*UP      A = 1.700 KM/SEC.    SIGA = 0.243 KM/SEC  
 SIG US = 0.18 KM/SEC    B = 2.531      SIGB = 0.337

## COMMENTS:

- 1) SOURCE: COLEBURN N. L. AND LIDDIARD JR. T. P.  
 J. CHEM. PHYS., VOL. 44, P. 1929 (1965)  
 ALSO: PRIVATE COMMUNICATION
- 2) EXPERIMENTAL TECHNIQUE C1  
 DATA REDUCTION METHOD B:  $UP = 1/2 * UP$  WAS ASSUMED FOR THE STANDARD MATERIALS BRASS AND PLEXIGLAS, SO THAT THE PRESSURE RELEASE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS UP HUGONIOT IN THE LINE  $UP = 1/2 * UFS$
- 3) FOR BRASS  $US = 3.560 + 1.833 * UP$  KM/SEC.  
 FOR PLEXIGLAS  $US = 2.710 + 1.568 * UP - 0.037 * UP^2$
- 4) C0 IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN UNCERTAINTY OF ABOUT 10 PERCENT

TABLE I  
BENZENE, 1-AMINO, 2,4,6-TRINITRO (TNA) (EXPLOSIVE)  
23-18-2-1 (6-4-4-6) ---1



23-18-2-1(6-5-5-6)---1

BENZENE, 1,3-DIAMINO, 2,4,6-TRINITRO (DATB) (EXPLOSIVE)

-C(H2)-C(N-O2)(C(N-H2)-C(N-O2)-)2 = C6-N5-H5-O8  
 NYLON IMPURITY 1. PERCENT BY WT.

V0 = 0.5618 CC/G

C0 = 2.660 KM/SEC

V01 = 0.5443 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS

TABLE

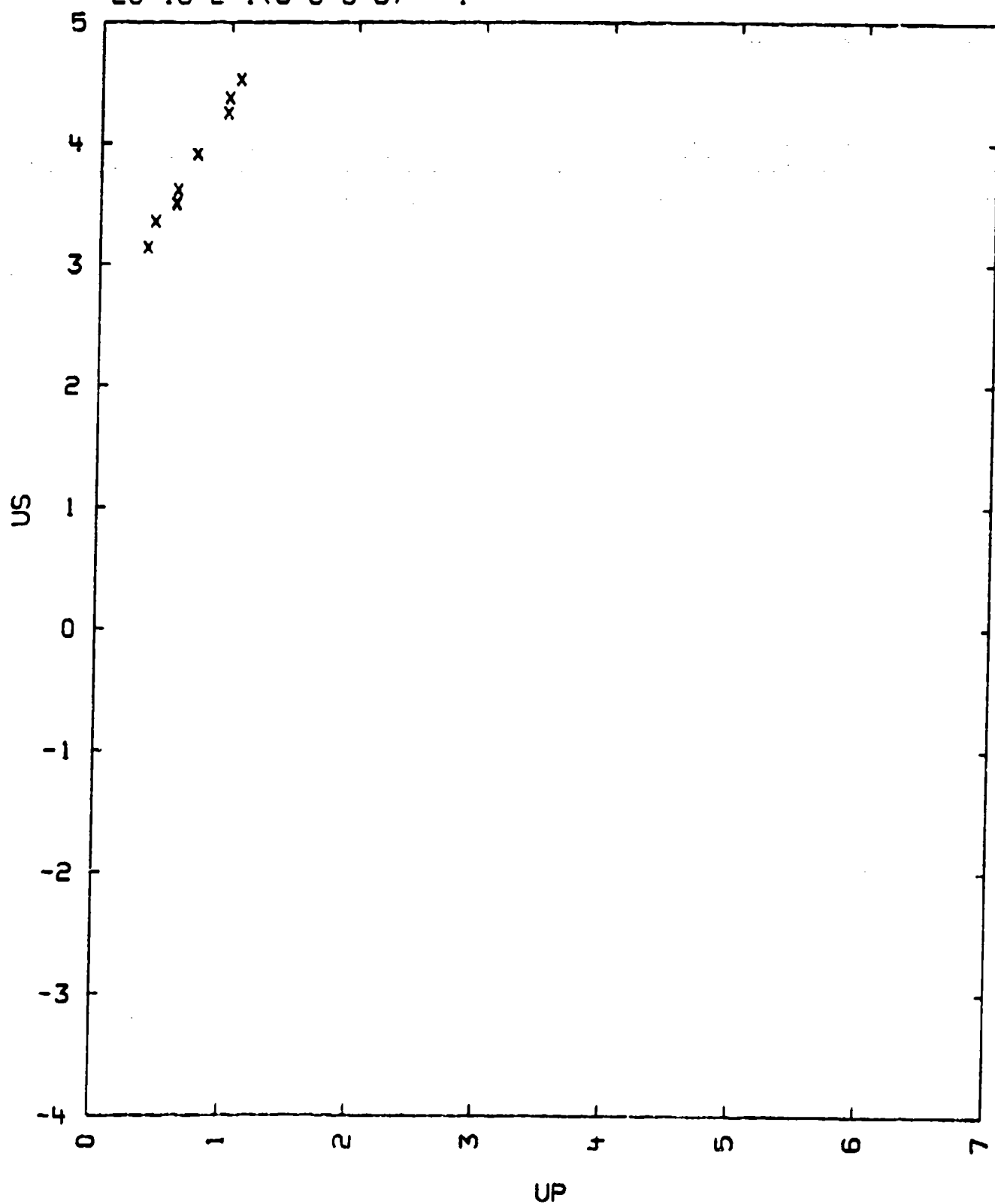
| RH00  | US    | UP    | P    | V/V0  |
|-------|-------|-------|------|-------|
| 1.780 | 3.132 | 0.375 | 20.9 | 0.880 |
| -     | 3.496 | 0.590 | 36.7 | 0.831 |
| -     | 3.350 | 0.421 | 25.1 | 0.874 |
| -     | 3.605 | 0.600 | 38.5 | 0.833 |
| -     | 3.498 | 0.590 | 36.7 | 0.831 |
| -     | 3.900 | 0.750 | 52.0 | 0.807 |
| -     | 4.247 | 0.980 | 74.0 | 0.769 |
| -     | 4.373 | 0.995 | 77.4 | 0.772 |
| -     | 4.517 | 1.080 | 86.8 | 0.760 |

US = A + B\*UP    A = 2.449 KM/SEC,    SIGA = 0.043 KM/SEC  
 SIGUS = 0.063 KM/SEC    B = 1.892,    SIGB = 0.058

## COMMENTS:

- 1) SOURCE: COLEBURN N. L. AND LIDDIARD JR. T. P.  
 J. CHEM. PHYS., VOL. 44, P. 1929 (1965)  
 ALSO: PRIVATE COMMUNICATION
- 2) EXPERIMENTAL TECHNIQUE C1  
 DATA REDUCTION METHOD B:  $UP = 1/2 \cdot UP$  WAS ASSUMED FOR THE STANDARD MATERIALS BRASS AND PLEXIGLAS, SO THAT THE PRESSURE RELEASE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS UP HUGONIOT IN THE LINE  $UP = 1/2 \cdot UFS$
- 3) FOR BRASS  $US = 3.560 + 1.833 \cdot UP$  KM/SEC.  
 FOR PLEXIGLAS  $US = 2.710 + 1.558 \cdot UP - 0.037 \cdot UP^2$
- 4) THE GRUNEISEN COEFFICIENT  $\gamma = V(DP/DE) = 1.76$
- 5) V01 WAS CALCULATED FROM THE LATTICE CONSTANTS A=7.30, B=5.20 AND C=11.63 ANGSTROM, WITH  $\beta = 95.9$  DEGREES OF THE MONOCLINIC UNIT CELL  
 NAVAL ORDNANCE LABORATORY REPORT NOLTR-62-46 (1962)  
 J. R. HOLDEN, USNOL, WHITE OAK, SILVER SPRING, MARYLAND, USA
- 6) C0 IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN UNCERTAINTY OF ABOUT 10 PERCENT

TABLE 1  
BENZENE, 1,3-DIAMINO, 2,4,6-TRINITRO (D/3) (EXPLOSI  
23-18-2-1(6-5-5-6)---1





23-18-2-1(6-6-6)---1

BENZENE, 1,3,5-TRIAMINO, 2,4,6-TRINITRO (TATB) (EXPLOSIVE)

(-C(N-H2)-C(N-O2)-)3 = C6-N6-H6-O6

V0 = 0.5414 CC/G

C0 = 2.050 KM/SEC.

V01 = 0.5160 CC/G

THE TABLE BELOW LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBARS.

TABLE

| RH00  | US    | UP    | P     | V/V0  |
|-------|-------|-------|-------|-------|
| 1.847 | 3.300 | 0.339 | 20.6  | 0.897 |
| -     | 3.220 | 0.413 | 24.5  | 0.871 |
| -     | 3.290 | 0.411 | 24.9  | 0.875 |
| -     | 3.400 | 0.441 | 27.6  | 0.870 |
| -     | 3.370 | 0.442 | 27.5  | 0.868 |
| -     | 3.390 | 0.452 | 28.3  | 0.868 |
| -     | 3.410 | 0.450 | 28.3  | 0.868 |
| -     | 3.510 | 0.514 | 33.3  | 0.853 |
| -     | 3.990 | 0.780 | 57.4  | 0.804 |
| -     | 4.130 | 0.818 | 62.3  | 0.801 |
| -     | 4.460 | 0.877 | 73.2  | 0.803 |
| -     | 4.660 | 0.969 | 83.4  | 0.792 |
| -     | 4.760 | 0.970 | 85.2  | 0.796 |
| -     | 4.480 | 0.993 | 82.1  | 0.778 |
| -     | 4.490 | 1.010 | 83.7  | 0.775 |
| -     | 4.440 | 1.033 | 84.7  | 0.767 |
| -     | 4.730 | 1.015 | 88.6  | 0.785 |
| -     | 4.690 | 1.017 | 88.0  | 0.783 |
| -     | 5.180 | 1.125 | 107.6 | 0.782 |
| -     | 5.140 | 1.128 | 107.0 | 0.780 |
| -     | 5.650 | 1.420 | 148.1 | 0.748 |

US = A + B\*UP      A = 2.340 KM/SEC, SIGA = 0.065 KM/SEC  
 SIG US = 0.14 KM/SEC      B = 2.318,      SIGB = 0.076

## COMMENTS:

- 1) SOURCE: COLEBURN N. L. AND LIDDIARD JR. T. P.  
 J. CHEM. PHYS., VOL. 44, P. 1929 (1965)  
 ALSO: PRIVATE COMMUNICATION

## 2) EXPERIMENTAL TECHNIQUE C1

DATA REDUCTION METHOD B: UP=1/2\*UP WAS ASSUMED FOR THE STANDARD MATERIALS BRASS AND PLEXIGLAS, SO THAT THE PRESSURE RELEASE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS UP HUGONIOR IN THE LINE UP = 1/2\*UFS

## 3) FOR BRASS US = 3.560 + 1.833\*UP KM/SEC.

FOR PLEXIGLAS US = 2.710 + 1.568\*UP - 0.037\*UP\*\*2

## 4) THE GRUNEISEN COEFFICIENT GAMMA = V(OP/DE) = 1.60

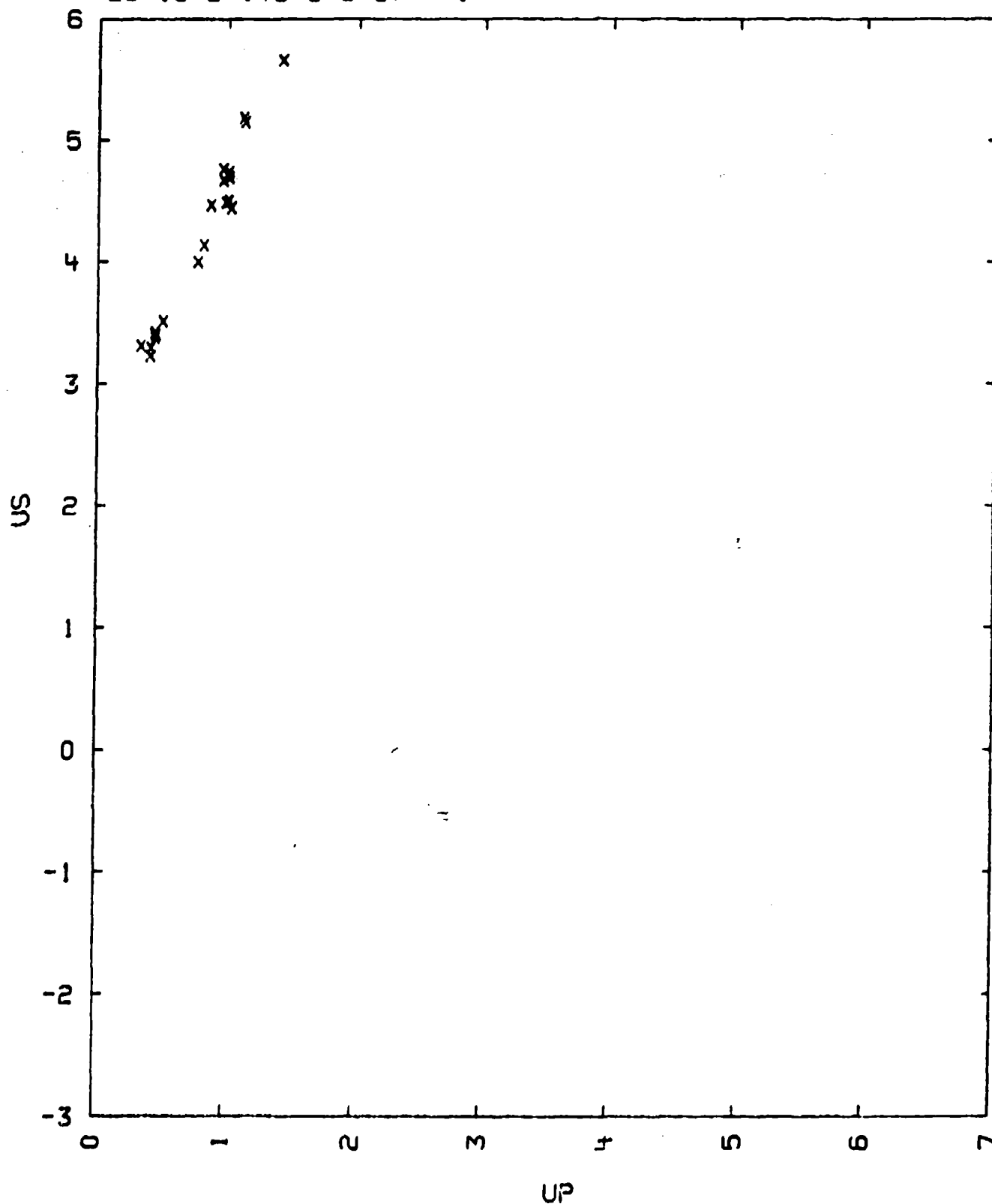
## 5) C0 IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN

UNCERTAINTY OF ABOUT 10 PERCENT

PAGE 584

U06/14/77

TABLE 1  
 BENZENE, 1,3,5-TRIAMINO, 2,4,6-TRINITRO (TATB) (EXPL  
 23-18-2-1(6-6-6-6)---1



23-18-2-1(7-1-7-2)---1  
MONONITROTOLUENE

02-N-C6(H4)-C-H3 = C7-H7-N-02

T0 = 12 DEG. CENTIGRADE  
V0 = 0.856 CC/G

C0 = 1.49 KM/SEC.  
AT 20 DEG. CENTIGRADE

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| RH00  | US   | UP    | P     | V/V0  |
|-------|------|-------|-------|-------|
| 1.168 | 5.64 | 2.300 | 151.5 | 0.592 |
| 1.168 | 4.20 | 1.340 | 65.8  | 0.681 |

US =

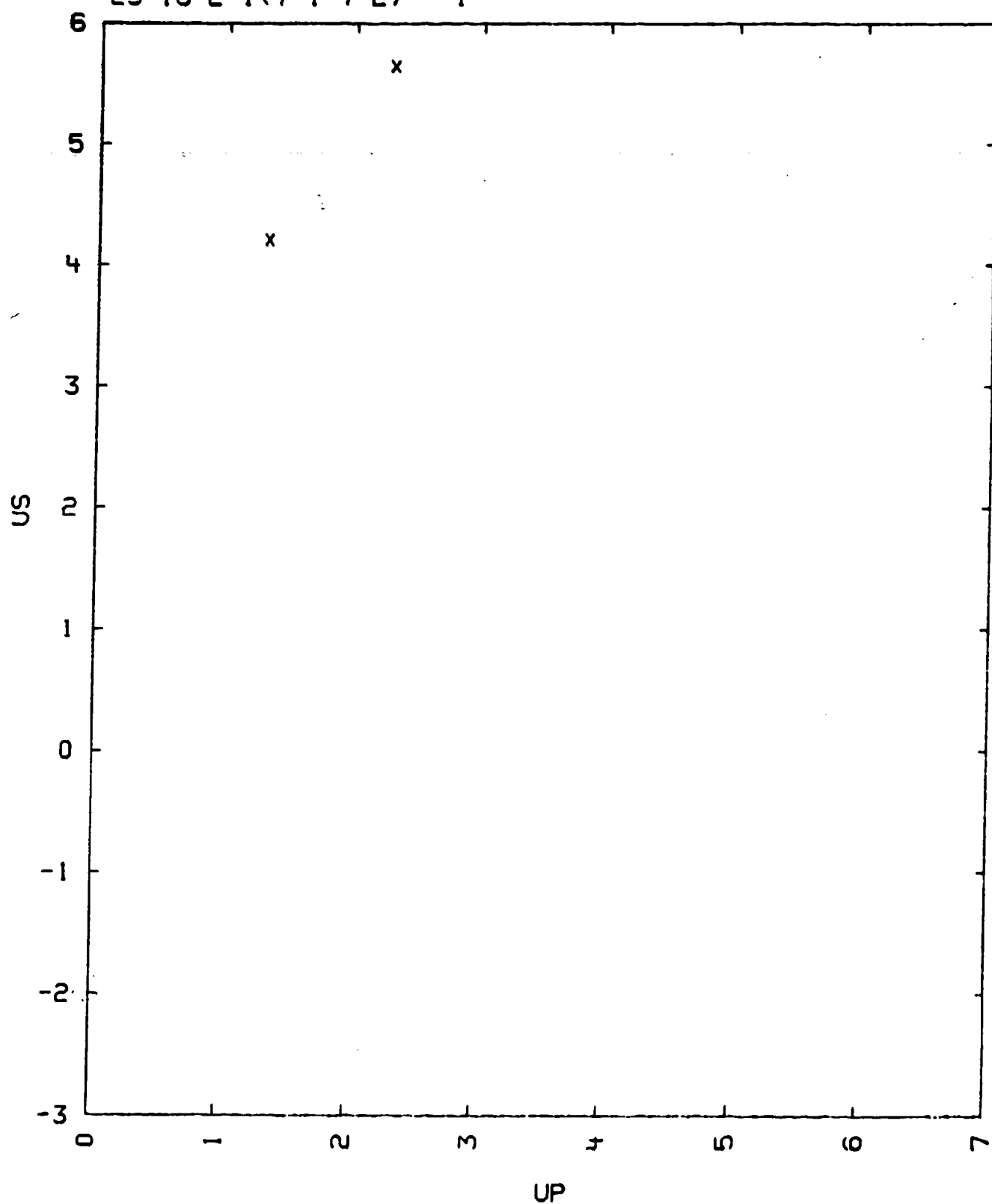
COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.  
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 24ST ALUMINUM
- 3) C0 WAS OBTAINED FROM L. BERGMANN, DER ULTRASCHALL, (S HIRZEL VERLAG, STUTTGART, 1954) 6TH ED., P. 379

TABLE I

MONONITROTOLUENE

23-18-2-1(7-1-7-2)---1



23-18-2-1(7-1-7-3)---1  
O-NITROANISOLE

H3-C-O-(C6-H4)-N-O2 = C7-N-H7-O3

$V_0 = 0.797 \text{ CC/G.}$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC AND PRESSURES IN KBAR.

TABLE

| RH00  | US   | UP   | P    | V/V0  |
|-------|------|------|------|-------|
| 1.225 | 4.96 | 1.68 | 104. | 0.661 |
| -     | 4.35 | 1.48 | 80.8 | 0.660 |
| -     | 4.33 | 1.42 | 77.2 | 0.672 |
| -     | 4.25 | 1.40 | 74.7 | 0.670 |
| -     | 4.70 | 1.62 | 95.5 | 0.655 |
| -     | 4.40 | 1.42 | 78.4 | 0.677 |
| -     | 4.86 | 1.80 | 110. | 0.630 |
| -     | 5.01 | 1.78 | 112. | 0.644 |
| -     | 5.97 | 2.59 | 194. | 0.566 |
| -     | 5.89 | 2.34 | 173. | 0.603 |
| -     | 5.39 | 2.10 | 142. | 0.610 |
| -     | 4.08 | 1.23 | 63.0 | 0.698 |
| -     | 4.14 | 1.23 | 63.9 | 0.703 |
| -     | 3.34 | 0.79 | 33.1 | 0.763 |
| -     | 2.91 | 0.34 | 12.4 | 0.883 |
| -     | 4.50 | 1.50 | 84.7 | 0.667 |
| -     | 4.54 | 1.50 | 85.5 | 0.670 |
| -     | 3.99 | 1.23 | 61.6 | 0.692 |
| -     | 3.50 | 0.82 | 36.0 | 0.766 |
| -     | 3.52 | 0.86 | 38.0 | 0.756 |
| -     | 3.48 | 0.86 | 37.6 | 0.753 |
| -     | 4.04 | 1.24 | 62.9 | 0.693 |
| -     | 6.07 | 2.53 | 193. | 0.583 |
| -     | 5.39 | 2.03 | 137. | 0.623 |
| -     | 4.09 | 1.22 | 62.6 | 0.702 |

$US = 2.244 + 1.502 \cdot UP \text{ KM/SEC.}$

$SIG US = 0.09 \text{ KM/SEC.}$

#### COMMENTS

1) SOURCE: HAUVER, G. E. AND MELANI, A.  
PRIVATE COMMUNICATION, JAN. 1969.  
BALLISTICS RES. LAB., ABERDEEN PROVING GROUNDS  
MARYLAND, USA.

2) EXPERIMENTAL TECHNIQUE: H  
DATA REDUCTION TECHNIQUE: B

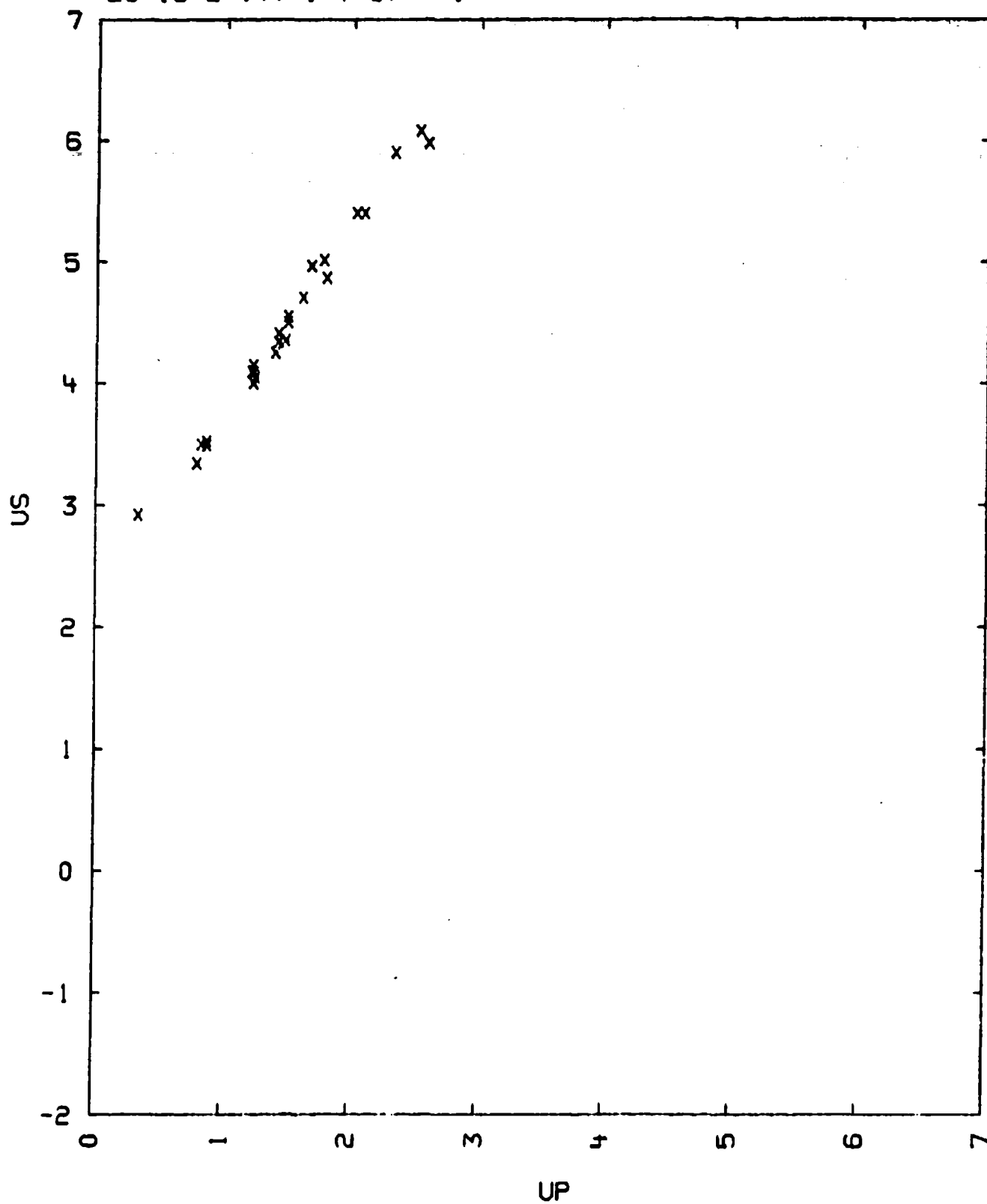
STANDARD MATERIALS: AL, BRASS, MG, AND  
PLEXIGLAS WITH  $US=2.702+1.544 \cdot UP$  AND  $RH00=$   
 $=1.18 \text{ G/CC}$  DEFINING THE HUGONOT OF THE

LATTER.

- 3) THE RELEASE CURVES OF THE METAL WERE LOCATED FROM A MEASUREMENT OF THE SHOCK VELOCITY OF THE PLEXIGLASS STANDARD

TABLE 1

O-NITROANISOLE  
23-18-2-1(7-1-7-3)---1





23-18-2-1(7-3-5-6)---1

TRINITROTOLUENE-2,4,6 (TNT) (EXPLOSIVE)

-C(C-H3)-C(N-O2)(-C(H)-C(N-O2))-12 = C7-N3-H5-O6

V0 = 0.6186 CC/G

V01 = 0.6046 CC/G

C0 = 2.572 KM/SEC

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. AL DENOTES ALUMINUM AND BR BRASS.

TABLE

| - - - - - SAMPLE - - - - - |       |       |       |        | - - HOLDER - - |       |
|----------------------------|-------|-------|-------|--------|----------------|-------|
| RH00                       | US    | UP    | P     | V/V0   | MATRL          | UP    |
| 1.614                      | 3.039 | 0.335 | 16.43 | 0.8897 | BR             | 0.194 |
| -                          | 3.137 | 0.314 | 15.89 | 0.8999 | BR             | 0.183 |
| -                          | 3.021 | 0.348 | 16.96 | .8848  | BR             | 0.201 |
| -                          | 3.054 | 0.347 | 17.10 | 0.8863 | BR             | 0.201 |
| -                          | 3.242 | 0.399 | 20.87 | 0.8769 | BR             | 0.233 |
| -                          | 3.394 | 0.419 | 22.95 | 0.8765 | BR             | 0.247 |
| -                          | 3.359 | 0.434 | 23.52 | 0.8707 | BR             | 0.255 |
| -                          | 3.152 | 0.476 | 24.21 | 0.8489 | BR             | 0.277 |
| -                          | 3.247 | 0.484 | 25.36 | 0.8509 | BR             | 0.283 |
| -                          | 3.441 | 0.491 | 27.26 | 0.8573 | BR             | 0.289 |
| -                          | 4.103 | 0.732 | 48.47 | 0.8215 | BR             | 0.441 |
| -                          | 4.137 | 0.831 | 55.48 | 0.7991 | BR             | 0.501 |
| -                          | 4.185 | 0.859 | 58.02 | 0.7947 | BR             | 0.518 |
| -                          | 4.033 | 0.793 | 51.61 | 0.8033 | BR             | 0.476 |
| -                          | 4.131 | 0.831 | 55.40 | 0.7988 | BR             | 0.501 |
| -                          | 4.157 | 0.885 | 59.37 | 0.7871 | BR             | 0.534 |
| -                          | 4.556 | 1.005 | 73.90 | 0.7794 | BR             | 0.614 |
| -                          | 4.489 | 1.009 | 73.10 | 0.7752 | BR             | 0.614 |
| -                          | 5.374 | 1.466 | 127.1 | 0.7272 | AL             | 1.095 |
| -                          | 5.311 | 1.475 | 126.4 | 0.7222 | AL             | 1.095 |

US = A + B\*UP

A = 2.390 KM/SEC

B = 2.050 KM/SEC

SIG US = 0.10

SIG A = 0.032 KM/SEC

SIG B = 0.034

## COMMENTS:

- 1) SOURCE: COLEBURN N. L. AND LIDDIARD JR. T. P.  
J. CHEM. PHYS., VOL. 44, P. 1929 (1965)  
ALSO: PRIVATE COMMUNICATION.

## 2) EXPERIMENTAL TECHNIQUE C1

## DATA REDUCTION METHOD B

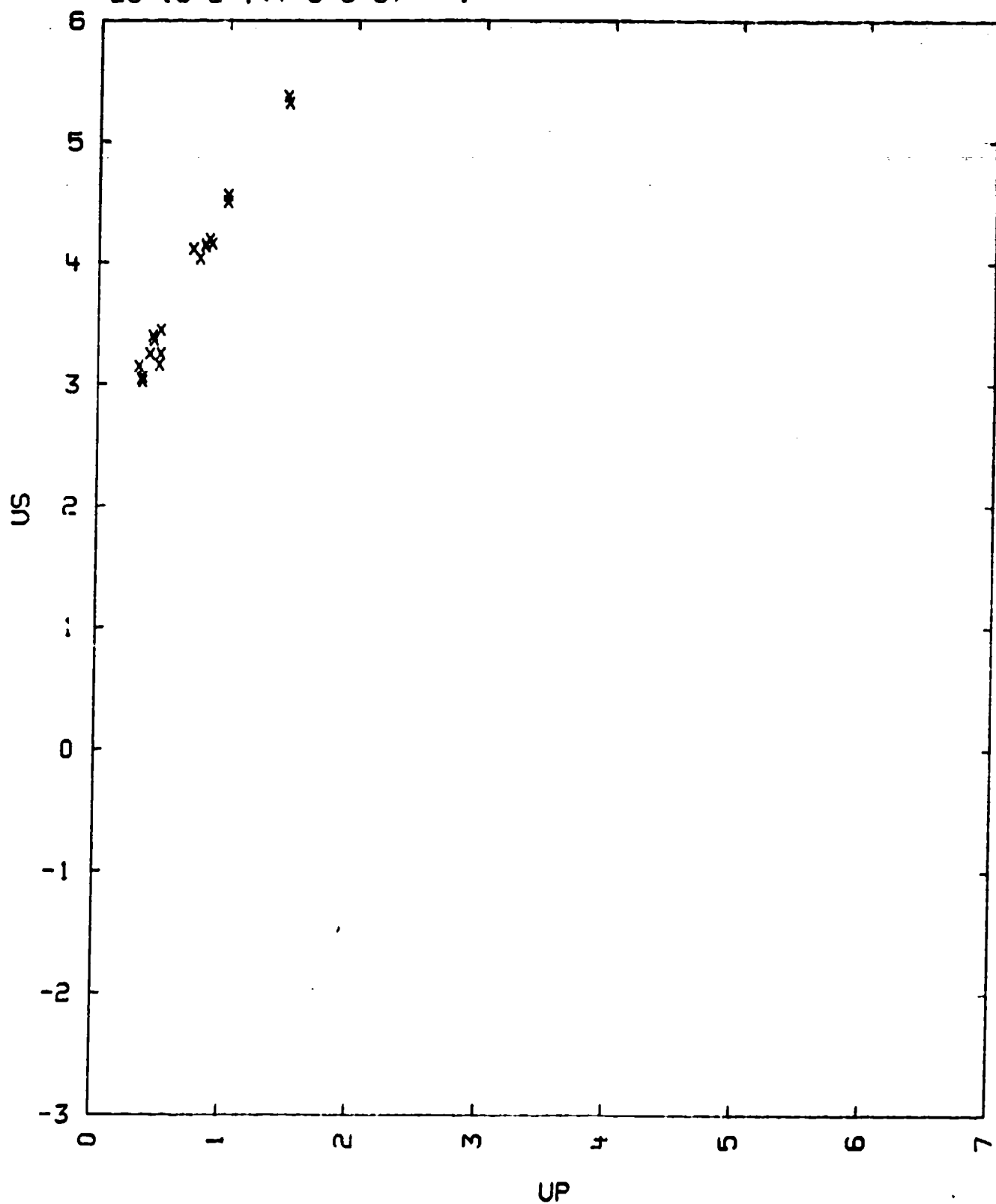
THE HUGONIOT AND RELEASE ISENTROPES OF THE SAMPLE HOLDER WERE TAKEN TO BE MIRROR IMAGES IN THE P VS. UP PLANE.

FOR BRASS US = 3.560 + 1.833\*UP KM/SEC WAS USED WITH RH00 = 8.37 G/CC.

FOR 245T ALUMINUM US = 5.35 + 1.34\*UP KM/SEC WAS USED.

- 3) AN ALUMINIZED MYLAR FILM WAS PLACED ON THE SAMPLE WITH A THIN LAYER OF SILICONE GREASE TO INCREASE THE REFLECTIVITY.
- 4) THE GRUNEISEN COEFFICIENT  $\gamma = V(DP/DE) = 0.737$ .
- 5)  $V_0$  WAS OBTAINED FROM THE HANDBOOK OF CHEMISTRY AND PHYSICS (CHEM RUBBER PUBLISHING CO. 1963) 44TH ED.
- 6)  $C_0$  IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN UNCERTAINTY OF ABOUT 10 PERCENT.

TABLE I  
TRINITROTOLUENE-2,4,6 (TNT) (EXPLOSIVE)  
23-18-2-1(7-3-5-6)---1



23-18-2-1(7-3-5-6)---2  
 TRINITROTOLUENE-2,4,6 (TNT) (EXPLOSIVE)

-C(C-H3)-C(N-O2)(-C(H)-C(N-O2))-12 = C7-N3-H5-O6

TO = 80.7 - 82.0 DEG. C.  
 VO = 0.679 - 0.680 CC/G

CO = 1.37 KM/SEC.

THE TABLE BELOW LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBARS.

TABLE

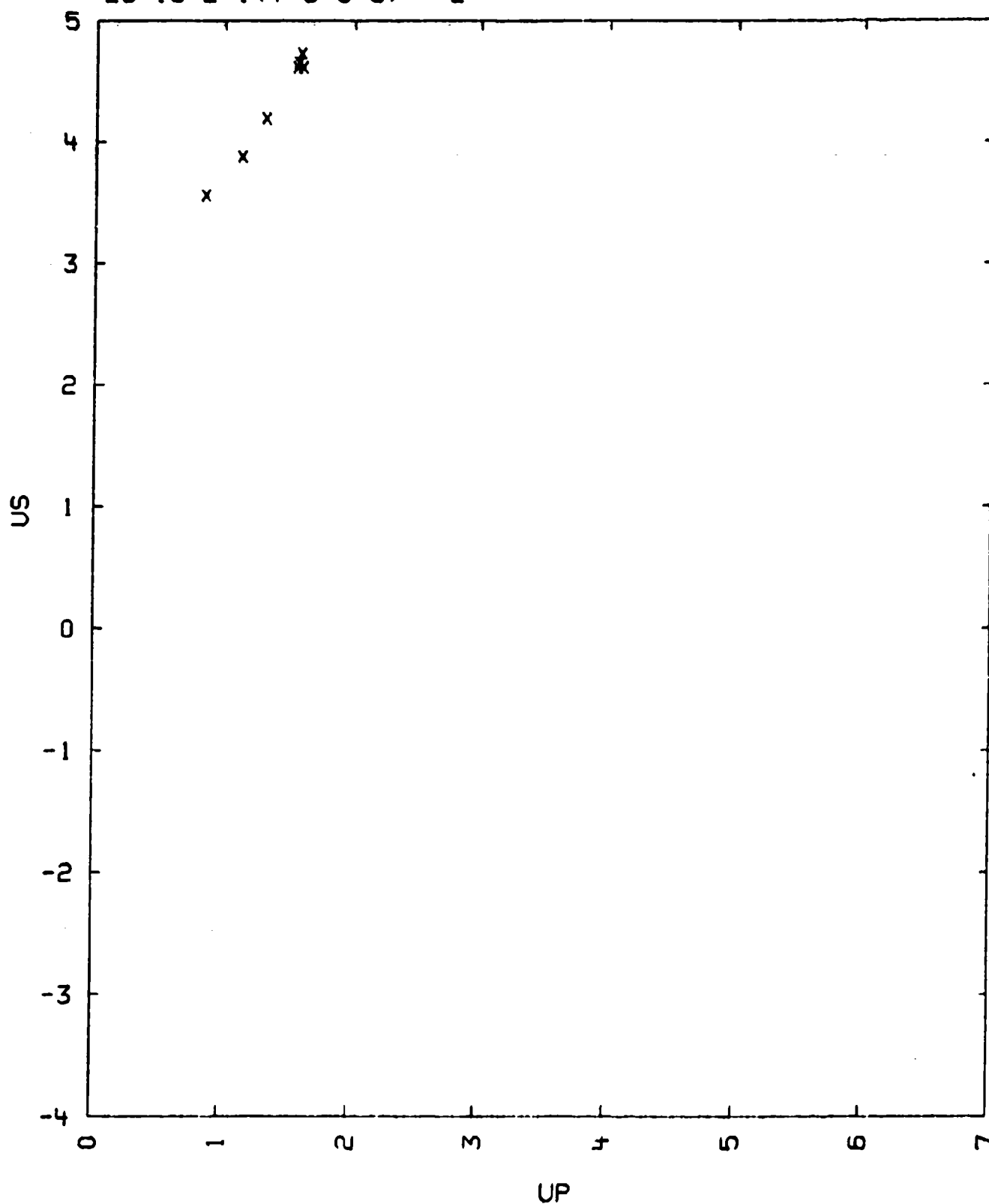
| TO   | RHOD  | US    | UP    | P     | V/VO  |
|------|-------|-------|-------|-------|-------|
| 80.7 | 1.473 | 3.552 | 0.860 | 44.5  | 0.758 |
| 82.0 | 1.470 | 3.872 | 1.141 | 65.2  | 0.705 |
| 80.7 | 1.473 | 4.183 | 1.328 | 81.7  | 0.683 |
| 80.7 | 1.473 | 4.603 | 1.601 | 108.5 | 0.652 |
| 81.0 | 1.473 | 4.607 | 1.561 | 105.8 | 0.661 |
| 82.3 | 1.470 | 4.640 | 1.569 | 106.8 | 0.662 |
| 80.7 | 1.473 | 4.727 | 1.596 | 111.3 | 0.662 |

US =  $2.14 + 1.57 \cdot UP$  KM/SEC  
 SIG US = 0.06 KM/SEC.

COMMENTS:

- 1) SOURCE: GARN W. B.  
 J. CHEM. PHYS. VOL. 30, P. 819 (1959)
  - 2) EXPERIMENTAL METHOD B  
 DATA REDUCTION METHOD B 24ST ALUMINUM STANDARD
  - 3) THE SPREAD OF THE US-UP POINTS IS TYPICALLY 2.5 PERCENT AND YIELD A PROBABLE ERROR OF 0.7 PERCENT.
  - 4) THE SAMPLE WAS IN LIQUID FORM NEAR THE FREEZING TEMPERATURE
  - 5) CO WAS OBTAINED BY J. B. RAMSAY AT 82 DEG. C. (GMX-8-MR-63-12)  
 LOS ALAMOS SCIENTIFIC LABORATORY  
 LOS ALAMOS, NEW MEXICO
- THIS VALUE IS MUCH SMALLER THAN THE ROOM TEMPERATURE VALUE OF THE SOLID: 2.08 KM/SEC AT A DENSITY OF 1.637 G/CC.  
 J. B. RAMSAY AND A. POPOLATO 4TH SYMP. DETONATIONS OCT 1965

TABLE 1  
TRINITROTOLUENE-2,4,6 (TNT) (EXPLOSIVE)  
23-18-2-1(7-3-5-6)---2



23-18-2-1(7-3-5-6)---3

TRINITROTOLUENE (TNT EXPLOSIVE) (EXPLOSIVE)

(C-H3)C-C(N-02)(-C(H)-C(N-02)-)2 = C7-H3-H5-06

V0 = 0.617 CC/G

V01 = 0.6046 CC/G

IN THE TABLE BELOW DENSITY IS IN G/CC, PRESSURE IN KBAR AND VELOCITIES  
IN KM/SEC, Z0 IS THE LENGTH NEEDED FOR BUILD-UP TO DETONATION IN MM. IN  
A 20 MM DIAMETER SAMPLE AND GT = GREATER THAN

TABLE

| RH00 | US   | UP   | P   | V/V0  | Z0   |
|------|------|------|-----|-------|------|
| 1.62 | 5.22 | 1.64 | 139 | 0.686 | 8    |
| -    | 4.93 | 1.44 | 115 | 0.710 | 13   |
| -    | 4.60 | 1.17 | 87  | 0.747 | GT50 |
| -    | 4.35 | 1.00 | 70  | 0.769 | GT50 |
| -    | 4.20 | 0.84 | 57  | 0.800 | GT50 |

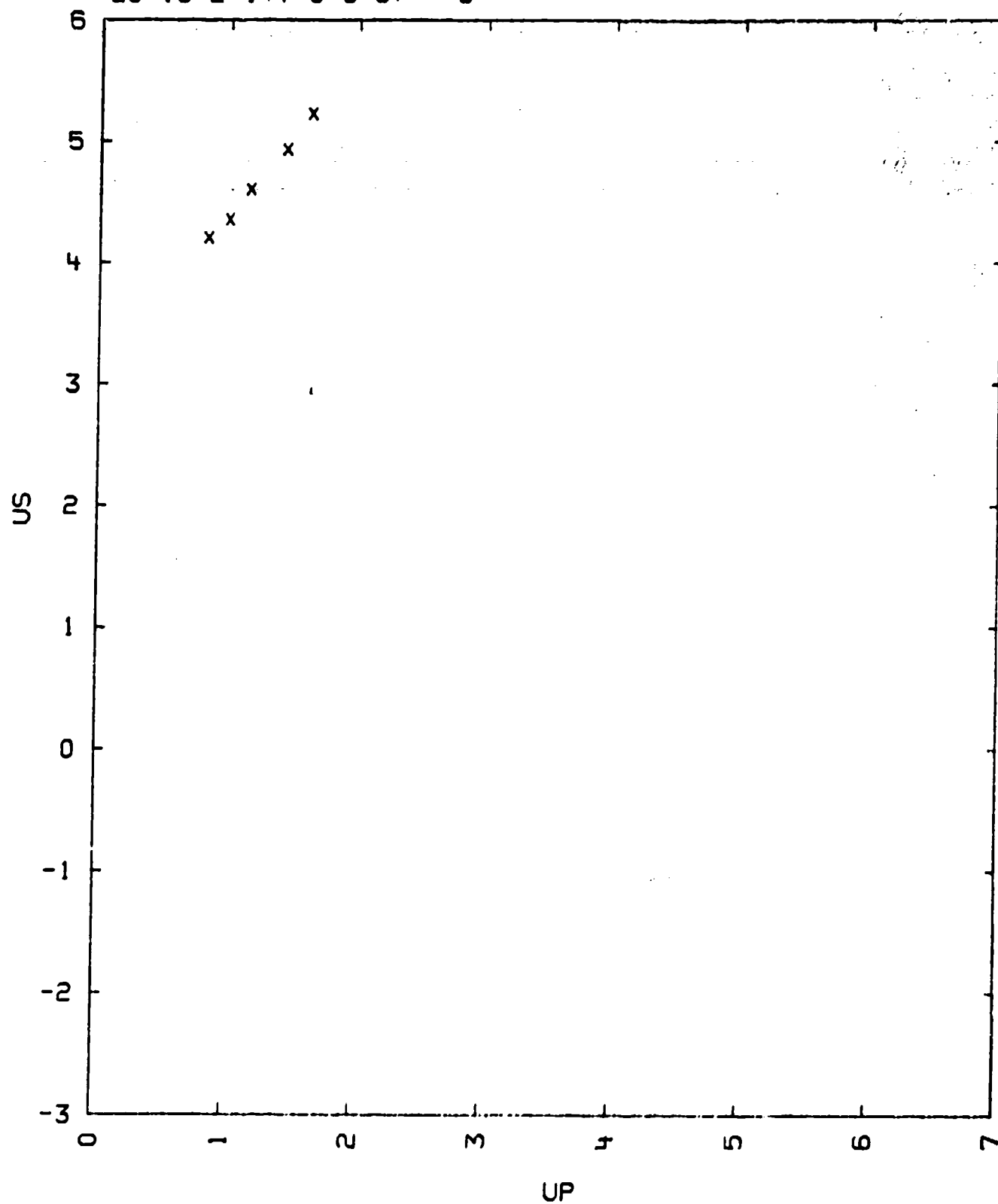
US = 3.09 + 1.29 UP KM/SEC, SIG.US = 0.26 KM/SEC

## COMMENTS:

- 1) SOURCE: ILYUKIN V. S., POKHIL P. F., ROZANOV O. K. AND SHVEDOVA N. S.  
DOKLADY AKAD NAUK SSSR VOL.131, P.793 (1960), OR  
SOVIET PHYS. DOKLADY VOL.5, P.337 (1960) (ENGLISH)
- 2) EXPERIMENTAL METHOD A  
DATA REDUCTION METHOD B STANDARD MATERIAL COPPER.  

| US   | AND UP | OF COPPER |
|------|--------|-----------|
| 5.60 | 1.00   |           |
| 5.34 | 0.87   |           |
| 5.03 | 0.71   |           |
| 4.82 | 0.60   |           |
| 4.64 | 0.51   |           |
| 4.32 | 0.35   |           |
- 3) THE ABOVE FIT YIELDS A PRESSURE OF 326 KB AT THE DETONATION VELOCITY  
WHILE PCJ = 210 KBARS
- 4) V01 WAS OBTAINED FROM THE HANDBOOK OF CHEM. AND PHYS. (CHEM. RUBBER  
PUBL. CO., CLEVELAND, OHIO, 1964) 45TH ED.

TABLE 1  
TRINITROTOLUENE (TNT EXPLOSIVE) (EXPLOSIVE)  
23-18-2-1(7-3-5-6)---3



23-18-2-117-3-5-6)---4  
 TRINITROTOLUENE (TNT) (EXPLOSIVE)

$C(C-H_3)-C(N-O_2)-(C(H)-C(N-O_2)-)_2 = C_7-H_3-N_3-O_6$

$V_0 = 0.6078 \text{ CC/G}$        $CL = 2.80 \text{ KM/SEC}$        $CO = 2.30 \text{ KM/SEC}$   
 $V_{01} = 0.6046 \text{ CC/G}$        $CS = 1.38 \text{ KM/SEC}$

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC. AND PRESSURE IN KILOBARS. L IS SAMPLE THICKNESS IN MM. AND  $P_0$  IS AN INDEPENDENT PRESSURE OBTAINED FROM A QUARTZ PRESSURE GAUGE (SEE COMMENTS).  $\Delta U$  IS THE DIFFERENCE IN AVERAGE VELOCITY OF THE FOOT OF THE WAVE AND THE WAVE POINT CORRESPONDING TO THE LISTED PRESSURE

TABLE

| RHO0  | US    | UP     | P     | V/V0   | L    | P0    | DELUS |
|-------|-------|--------|-------|--------|------|-------|-------|
| 1.647 | 2.732 | 0.0818 | 3.68  | 0.9701 | 6.2  | 3.40  | 0.41  |
| 1.643 | 2.496 | 0.0878 | 4.01  | 0.9608 | -    | 4.54  | 0.25  |
| 1.647 | 2.787 | 0.1009 | 4.63  | 0.9638 | -    | 4.33  | 0.20  |
| 1.645 | 2.345 | 0.1239 | 4.78  | 0.9472 | -    | 4.91  | 0.23  |
| 1.647 | 2.778 | 0.1284 | 5.08  | 0.9539 | -    | 5.75  | 0.10  |
| 1.644 | 2.405 | 0.1472 | 5.82  | 0.9388 | -    | 6.74  | 0.21  |
| 1.648 | 2.733 | 0.1623 | 7.31  | 0.9406 | -    | 8.22  | 0.16  |
| 1.645 | 2.805 | 0.1808 | 8.34  | 0.9356 | 12.7 | 8.68  | 0.12  |
| 1.647 | 2.919 | 0.2030 | 9.76  | 0.9305 | 6.2  | 10.85 | 0.11  |
| 1.644 | 2.844 | 0.2082 | 9.73  | 0.9288 | -    | 9.28  | 0.12  |
| 1.645 | 2.751 | 0.2109 | 9.55  | 0.9234 | -    | 9.58  | 0.13  |
| 1.645 | 2.903 | 0.2541 | 12.14 | 0.9125 | -    | 12.47 | 0.10  |
| 1.645 | 2.997 | 0.3001 | 14.79 | 0.8999 | 6.2  | 14.26 | 0.04  |
| 1.646 | 3.038 | 0.3076 | 15.37 | 0.8987 | -    | 14.67 | 0.05  |
| 1.646 | 3.141 | 0.3723 | 19.24 | 0.8815 | -    | 20.20 | 0.06  |
| 1.645 | 3.150 | 0.3909 | 20.25 | 0.8759 | -    | 19.61 | 0.10  |
| 1.646 | 3.375 | 0.4218 | 23.43 | 0.8750 | 12.7 | 23.21 | 0.06  |
| 1.647 | 3.344 | 0.4400 | 24.23 | 0.8684 | 12.7 | 24.70 | 0.07  |

$US = 2.372 + 2.16 \cdot UP$  ABOVE  $UP = 0.19 \text{ KM/SEC.}$   
 $SIGMA US = 0.084 \text{ KM/SEC.}$

## COMMENTS:

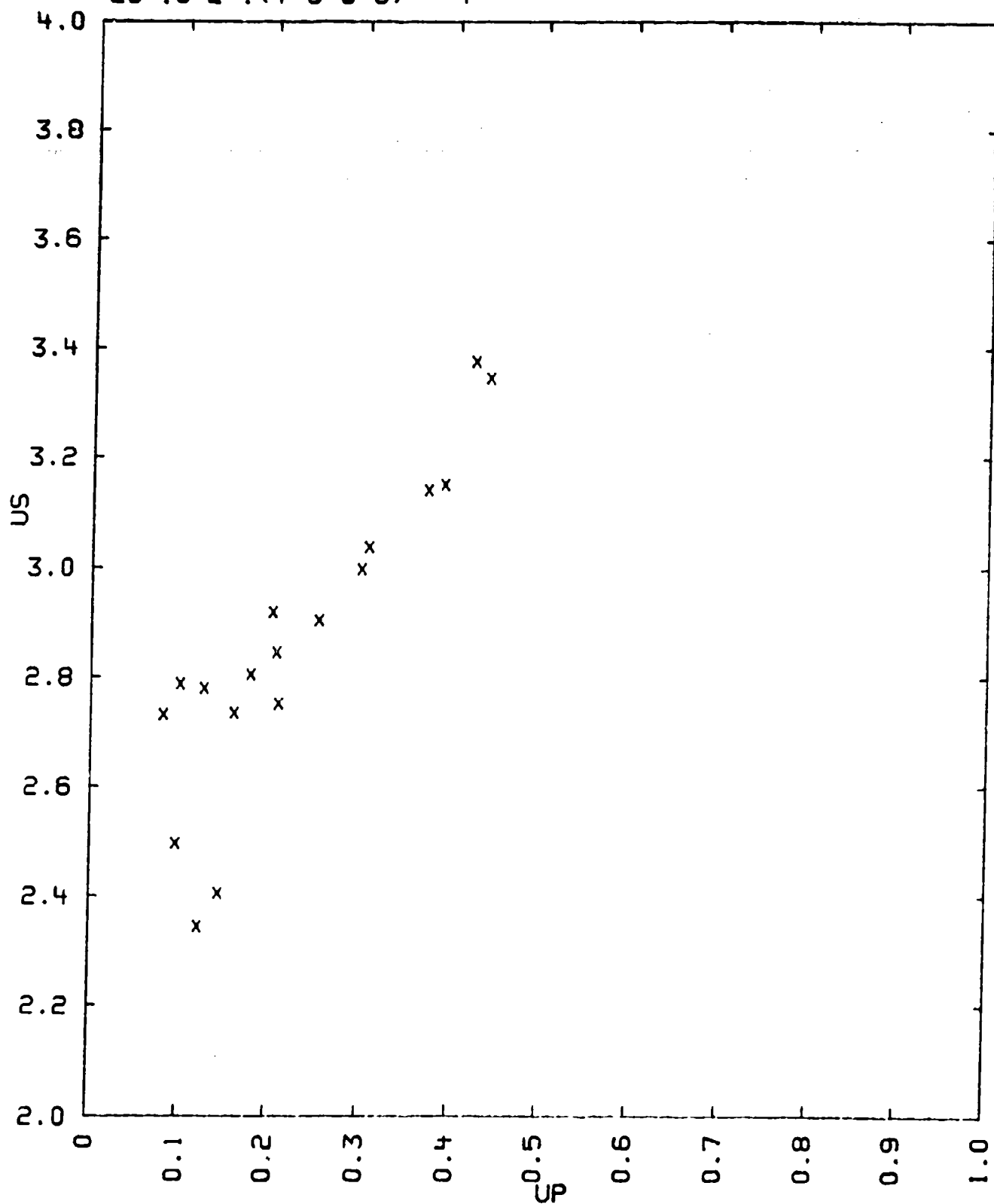
- 1) SOURCE: WASLEY R. J. AND OBRIEN J. F.  
 PRIVATE COMMUNICATION (1966)  
 LAWRENCE RAD. LAB., LIVERMORE, CALIFORNIA, U. S. A.
- 2) EXPERIMENTAL METHOD: A AND 12  
 DATA REDUCTION METHOD: A  
 THE PRESSURE WAS PRODUCED BY IMPACTING TWO SAMPLES OF TNT, SO THAT  $UP = 1/2$  PROJECTILE VELOCITY.
- 3) FURTHER WORK IS IN PROGRESS ON THIS MATERIAL
- 4) THE WIDTH OF MOST SHOCK FRONTS MAKES CHOICE OF THE APPROPRIATE SHOCK VELOCITY TO BE USED IN THIS SIMPLE ANALYSIS UNCERTAIN. THE VALUE OF  $US$  USED CORRESPONDS TO THE TIME AT WHICH THE QUARTZ GAUGE READS



1/2 OF PEAK VOLTAGE. IN THE OPINION OF THE COMPILER THIS DOES NOT MAKE THE VALUE OF  $\Delta S$  UNCERTAIN BY MORE THAN 5 PERCENT FOR THE WIDEST SHOCK IN THE TABLE. THE ACCURACY OF  $P_0$  IS 5 PERCENT

- 5) THE RELATIVELY LARGE DISCREPANCY OF THE THREE POINTS AT 4.10, 4.78 AND 5.82 KBARS IS AS YET NOT EXPLAINED. HOWEVER, NONE OF THE POINTS BELOW 9 KILOBARS WERE USED SINCE THE EFFECT OF THE POORLY DEFINED ELASTIC WAVE ON THESE EXPERIMENTS ADDS A FURTHER UNCERTAINTY
- 6)  $V_0$  WAS OBTAINED FROM THE HANDBOOK OF CHEM. AND PHYS. (CHEM. RUBBER PUBL. CO., CLEVELAND, OHIO, 1964) 45TH ED.

TABLE I  
 TRINITROTOLUENE (TNT) (EXPLOSIVE)  
 23-18-2-1(7-3-5-6)---4



23-10-2-1(7-3-5-8)---5  
TNT (EXPLOSIVE)

TRINITROTOLUENE  
(N-02)3-C6(H2)-C-H3 = C7-N3-H5-O6

V0 = 0.6321 CC/G  
V01 = 0.6046 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND  
PRESSURE IN KILOBARS. X DENOTES BRASS STANDARD THICKNESS IN CM.

TABLE

| RH00  | X     | US   | UP    | P     | V/V0  |
|-------|-------|------|-------|-------|-------|
| 1.582 | 1.270 | 4.89 | 1.395 | 107.9 | 0.715 |
| -     | 2.492 | 4.65 | 1.275 | 93.8  | 0.726 |
| -     | 3.762 | 4.47 | 1.145 | 81.1  | 0.744 |

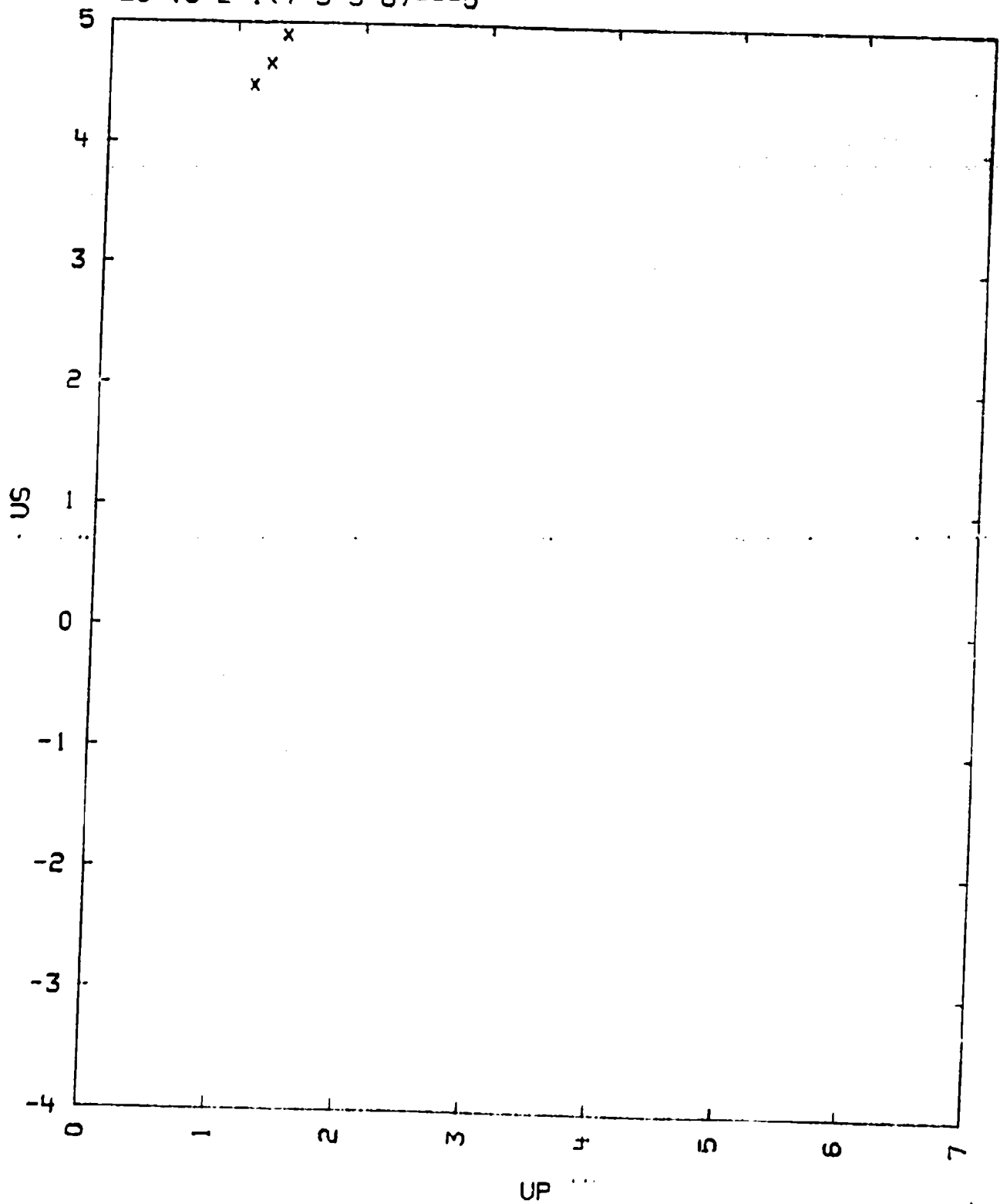
US = 2.52 + 1.69\*UP +OR- 0.06 KM/SEC

## COMMENTS:

- 1) SOURCE: MAJOWICZ, M. J. AND JACOBS, S. J.  
NAVORD REPORT NO. 5700, 1958  
U.S. NAVAL ORDNANCE LAB., WHITE OAK, MARYLAND, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE C  
DATA REDUCTION TECHNIQUE B. WHERE  $UP = 1/2(US)$ . IT WAS ASSUMED THE  
RELEASE ISENTROPE WAS A STRAIGHT LINE WITH SLOPE  $RH00(US)$ .  
STANDARD MATERIAL BRASS
- 3) US IS THE VELOCITY AT ZERO THICKNESS OF THE EXPLOSIVE OBTAINED BY  
EXTRAPOLATING THE VELOCITY VERSUS THICKNESS CURVE OBTAINED FROM A  
WEDGE OF EXPLOSIVE.
- 4) THE DETONATION VELOCITY IS 5.23 KM/SEC.,  $SIGMA = 0.015$  KM/SEC  
THIS VELOCITY WAS REACHED AT THICKNESS BETWEEN 4.3-10.7 MM DEPENDING  
ON INPUT PRESSURE.
- 5) V01 WAS CALCULATED BY USING THE WEIGHT PERCENT OF THE ELEMENTS.

TABLE I

TNT (EXPLOSIVE)  
23-18-2-1(7-3-5-6)---5



23-18-2-1(7-3-5-6)---8  
TRINITROTOLUENE (TNT) (EXPLOSIVE)

-C(C-H3)-C(N-O2)(-C(H)-C(N-O2))-12 = C7-N3-H5-O6

V0 = 0.621 CC/G

VOI = 0.6046 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND  
PRESSURE IN KILOBARS.

TABLE

| RH00  | US   | UP   | P     | V/V0  |
|-------|------|------|-------|-------|
| 1.610 | 3.83 | 0.77 | 47.5  | 0.799 |
| -     | 3.84 | 0.76 | 47.0  | 0.802 |
| -     | 4.63 | 1.10 | 82.0  | 0.762 |
| -     | 4.49 | 1.12 | 80.9  | 0.751 |
| -     | 4.60 | 1.11 | 82.2  | 0.759 |
| -     | 3.78 | 0.76 | 46.3  | 0.799 |
| -     | 3.46 | 0.56 | 31.2  | 0.838 |
| -     | 3.59 | 0.55 | 31.8  | 0.847 |
| -     | 3.31 | 0.49 | 26.1  | 0.852 |
| -     | 3.36 | 0.49 | 26.5  | 0.854 |
| -     | 3.65 | 0.54 | 31.7  | 0.852 |
| -     | 3.45 | 0.56 | 31.1  | 0.838 |
| -     | 4.42 | 1.06 | 75.4  | 0.760 |
| -     | 4.22 | 1.04 | 70.7  | 0.754 |
| -     | 4.53 | 1.02 | 74.4  | 0.775 |
| -     | 4.15 | 0.79 | 52.8  | 0.809 |
| -     | 3.51 | 0.56 | 31.6  | 0.840 |
| -     | 3.36 | 0.57 | 30.8  | 0.830 |
| -     | 4.53 | 1.04 | 75.9  | 0.770 |
| -     | 4.42 | 1.05 | 74.7  | 0.762 |
| -     | 4.39 | 1.05 | 74.2  | 0.761 |
| -     | 4.40 | 1.06 | 75.1  | 0.759 |
| -     | 3.51 | 0.56 | 31.6  | 0.840 |
| -     | 4.01 | 0.80 | 51.6  | 0.800 |
| -     | 4.94 | 1.28 | 101.8 | 0.741 |
| -     | 3.39 | 0.57 | 31.1  | 0.832 |
| -     | 3.99 | 0.85 | 54.6  | 0.787 |
| -     | 5.25 | 1.31 | 110.7 | 0.750 |
| -     | 3.52 | 0.56 | 31.7  | 0.841 |
| -     | 4.04 | 0.85 | 55.3  | 0.789 |
| -     | 5.13 | 1.33 | 109.8 | 0.741 |
| -     | 3.71 | 0.84 | 50.2  | 0.774 |
| -     | 3.99 | 0.83 | 53.3  | 0.792 |
| -     | 4.73 | 1.15 | 87.6  | 0.757 |
| -     | 4.11 | 0.82 | 54.3  | 0.800 |
| -     | 4.61 | 1.16 | 86.1  | 0.748 |
| -     | 4.80 | 1.17 | 90.4  | 0.756 |
| -     | 4.77 | 1.17 | 89.9  | 0.755 |
| -     | 4.63 | 1.19 | 88.7  | 0.743 |
| -     | 4.24 | 0.83 | 56.7  | 0.804 |
| -     | 4.15 | 0.84 | 56.1  | 0.798 |

## TRINITROTOLUENE (TNT) (EXPLOSIVE)

| RHO | US   | UP   | P    | V/VO  |
|-----|------|------|------|-------|
| -   | 4.08 | 0.84 | 55.2 | 0.794 |
| -   | 3.93 | 0.85 | 53.8 | 0.784 |

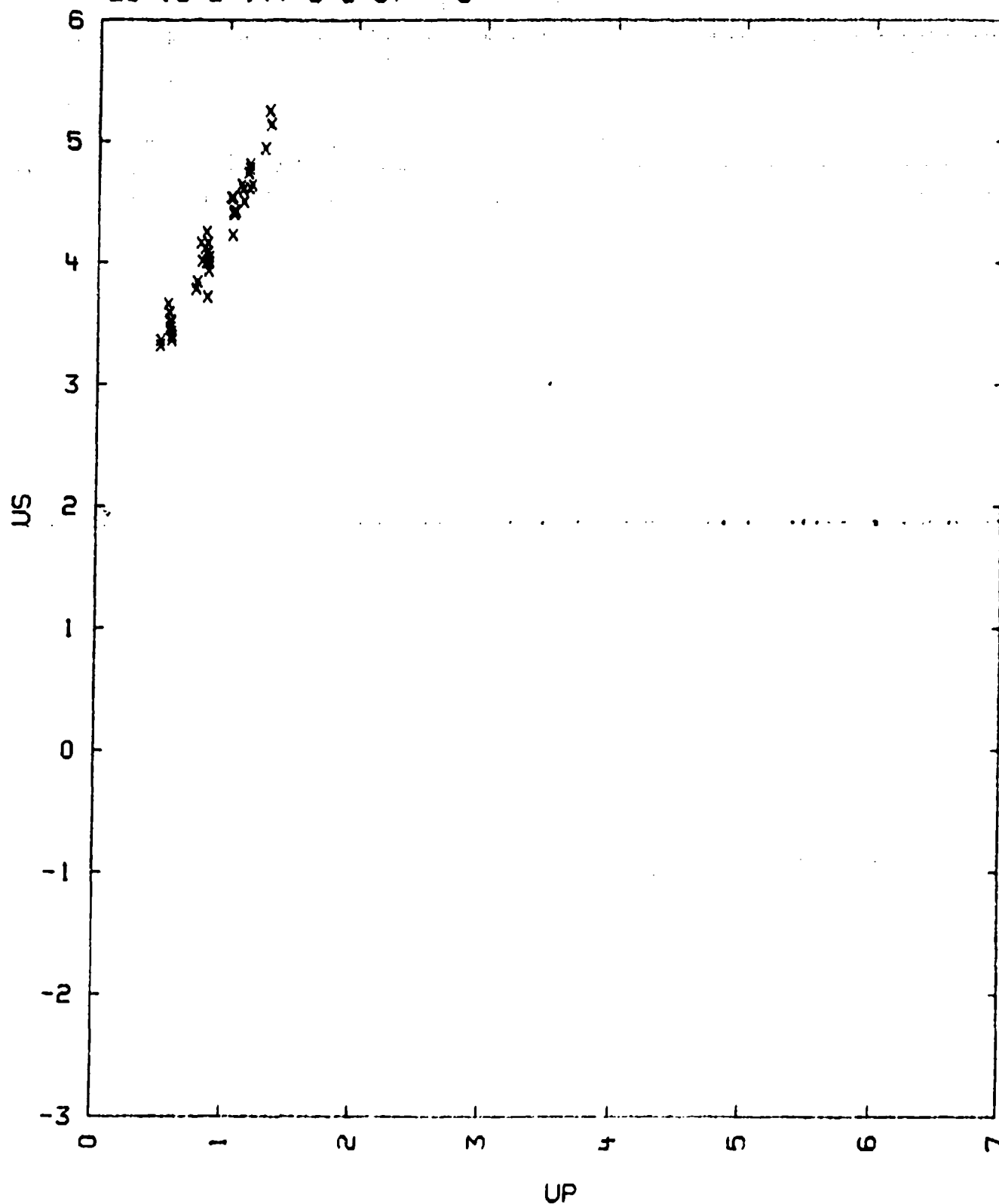
$$US = 2.34 + 2.03 \cdot UP \text{ KM/SEC}$$

$$SIGMA US = 0.12 \text{ KM/SEC}$$

## COMMENTS:

- 1) SOURCE: BOYLE, V. M. AND ERVIN, L. H.  
BRL MEMO. REPORT NO. 1814, JANUARY 1967  
BALLISTIC RESEARCH LABORATORIES. AMXBR-TD  
ABERDEEN PROVING GROUND, MARYLAND 21005.
- 2) EXPERIMENTAL TECHNIQUE: THE SHOCK VELOCITY IN THE SAMPLE WAS MEASURED BY A SMEAR CAMERA THAT SWEEPED THE SHADOWGRAPH OF A TRANSPARENT CHANNEL IN THE SAMPLE ACROSS THE FILM PLANE. THE CHANNEL WAS MADE BY SPLITTING THE SAMPLE IN TWO ALONG THE SHOCK DIRECTION AND SEPARATING THE TWO HALVES BY A THIN (0.127 MM) TRANSPARENT PLASTIC SHEET (EXTRUDED ACETATE).  
DATA REDUCTION TECHNIQUE: B  
STANDARD MATERIALS USED:  
ALUMINUM, 2024-T4,  $US = 5.360 + 1.351 \cdot UP \text{ KM/SEC}$   
 $RHO = 2.785 \text{ G/CC}$   
PLEXIGLASS,  $US = 2.702 + 1.544 \cdot UP, \text{ KM/SEC}, RHO = 1.184 \text{ G/CC}$   
 $UP = 1/2 \text{ UFS}$  WAS ASSUMED FOR THE STANDARD MATERIALS SO THAT THE PRESSURE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS. UP HUGONIOT IN THE LINE  $UP = 1/2 \text{ UFS}$ .
- 3) THE DEGREE TO WHICH THE RESULTS MAY BE AFFECTED BY CHEMICAL REACTION OF THE SHOCKED EXPLOSIVE SAMPLE HAS NOT BEEN DETERMINED AT THIS TIME.
- 4) VOI WAS OBTAINED FROM THE HANDBOOK OF CHEM. AND PHYS. (CHEM. RUBBER PUBL. CO. 1963) 44TH ED.

TABLE 1  
TRINITROTOLUENE (TNT) (EXPLOSIVE)  
23-18-2-1(7-3-5-6)---6



23-18-2-1(7-3-5-8)---7

TRINITROTOLUENE (TNT) (EXPLOSIVE)

-C(C-H3)-C(N-O2)-(-C(H)-C(N-O2))-12 = C7-N3-H5-O6

V0 = 0.77 - 1.02 CC/O

V01 = 0.6046

THE TABLES LIST DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBAR. FOR UNCERTAINTIES SEE COMMENTS. D IS STANDARD THICKNESS IN MM.

TABLE I

| SAMPLE |       |       |      |       | STANDARD |      |      |
|--------|-------|-------|------|-------|----------|------|------|
| RH00   | US    | UP    | P    | VIV0  | UP       | P    | D    |
| 1.30   | 2.198 | 0.581 | 16.6 | 0.736 | 0.507    | 20.3 | 50.8 |
| -      | 2.097 | 0.609 | 16.6 | 0.710 | 0.517    | 20.7 | 50.8 |
| -      | 2.845 | 0.730 | 27.0 | 0.742 | 0.682    | 29.4 | 43.4 |

$$US = -1.00 + 5.27 \cdot UP \text{ KM/SEC}$$

TABLE II

| SAMPLE |      |       |      |       | STANDARD |      |      |
|--------|------|-------|------|-------|----------|------|------|
| RH00   | US   | UP    | P    | VIV0  | UP       | P    | D    |
| 0.98   | 1.05 | 0.35  | 3.6  | 0.666 | 0.228    | 8.7  | 76.2 |
| -      | 1.97 | 0.435 | 8.4  | 0.779 | 0.333    | 12.9 | 63.5 |
| -      | 1.99 | 0.440 | 8.6  | 0.779 | 0.333    | 12.9 | 63.5 |
| -      | 1.80 | 0.680 | 12.0 | 0.622 | 0.517    | 20.7 | 50.8 |
| -      | 1.68 | 0.700 | 11.5 | 0.583 | 0.517    | 20.7 | 50.8 |
| -      | 1.46 | 0.725 | 10.4 | 0.503 | 0.517    | 20.7 | 50.8 |
| -      | 1.74 | 0.772 | 13.2 | 0.540 | 0.560    | 22.9 | 46.8 |
| -      | 1.63 | 0.793 | 12.7 | 0.514 | 0.578    | 23.8 | 47.7 |
| -      | 1.63 | 0.794 | 12.7 | 0.514 | 0.578    | 23.8 | 47.7 |
| -      | 1.80 | 0.960 | 17.0 | 0.468 | 0.654    | 27.9 | 44.5 |
| -      | 2.17 | 1.080 | 23.0 | 0.503 | 0.837    | 38.6 | 38.2 |
| -      | 2.60 | 1.030 | 26.3 | 0.605 | 0.840    | 38.8 | 38.1 |
| -      | 3.11 | 1.330 | 40.5 | 0.571 | 1.111    | 56.9 | 25.4 |
| -      | 3.06 | 1.340 | 40.0 | 0.562 | 1.111    | 56.9 | 25.4 |
| -      | 3.05 | 1.340 | 40.0 | 0.560 | 1.111    | 56.9 | 25.4 |
| -      | 3.26 | 1.720 | 55.0 | 0.472 | 1.413    | 80.4 | 12.7 |
| -      | 3.26 | 1.720 | 55.0 | 0.472 | 1.413    | 80.4 | 12.7 |

$$US = 0.749 + 1.513 \cdot UP \text{ KM/SEC}$$

$$SIG \text{ US} = 0.33 \text{ KM/SEC}$$

COMMENTS:

1J06/14/77



- 1) SOURCE: ERKMAN J.O. AND EDWARDS D.J.  
 NAVAL ORDINANCE LABORATORY TECH. REP. NO. NOLTR 74-213 (1974)  
 NAVAL ORDINANCE LABORATORY, WHITE OAK, SILVER SPRING,  
 MD. 20910, USA.

- 2) EXPERIMENTAL TECHNIQUE: K1  
 DATA REDUCTION METHOD: B

THE POLYMETHYLMETHACRYLATE STANDARD IS A CYLINDER OF DIAMETER 50.8 MM., LENGTH D, SHOCK HUGONIOTS  $U_S = 2.561 + 1.595 \cdot U_P$  ( $U_P$  AT OR ABOVE 0.536 KM/SEC.) AND  $U_S = 2.7228 + 4.0667 \cdot U_P - 10.9051 \cdot U_P^2 + 10.691 \cdot U_P^3$  KM/SEC ( $U_P$  LESS THAN 0.536),  $\rho_{H00} = 1.185$  G/CC. DATA OF BARKER L.M. AND HOLLENBACH (J. APPL. PHYS. V.41, 4208 (1970)) AND OF SCHULER K.W. AND MUNZIATO J.W. (SIXTH INTERNATIONAL CONGRES OF RHEOLOGY, LYON FRANCE (1972)) ON THE RELEASE CURVES WERE FITTED TO A FUNCTION  $F(\rho_{H0}/\rho_{H00})$  AND CONVERTED TO THE P U-P PLANE USING THE RIEMAN INTEGRAL AND THE CONDITION THAT U=U-P ON THE HUGONIOT. THE HUGONIOT U-P VALUES ARE GIVEN BY

$$U_P = 1.7735 \cdot \exp(-0.01841 \cdot D) + 0.8765 \cdot \exp(-0.3495 \cdot D) \quad (D < 36 \text{ MM})$$

$$U_P = 0.0905 + 4.0877 \cdot \exp(-0.04451 \cdot D) \quad (D > 36 \text{ MM})$$

FOR THE 50.8 MM LONG CYLINDER OF 50/50 PENTOLITE BOOSTER CHARGE USED.

- 3) THE EXPERIMENTAL ERROR IN U-P IS 3 PERCENT AND REFLECTS ITSELF IN A 12 PERCENT UNCERTAINTY IN P AND A 0.05 TO 0.06 CC/G UNCERTAINTY IN V.
- 4) THE DATA AGREES WITH THE HUGONIOT CALCULATED FROM THE IDEAL DENSITY TNT SHOCK LOCUS ASSUMING EQUILIBRIUM THERMODYNAMICS. A GRUNEISEN EOS WITH  $\gamma = 0.737$  AND A NONPOROUS ( $\rho_{H00} = 1.614$  G/CC) HUGONIOT ( $U_S = 2.39 + 2.05 \cdot U_P$  KM/SEC) WAS USED IN THESE CALCULATIONS
- 5) V01 IS TAKEN FROM THE HANDBOOK OF CHEM. AND PHYS (CHEMICAL RUBBER CO., CLEVELAND, OHIO. (1969-70)) 50TH ED.

TABLE I

TRINITROTOLUENE (TNT) (EXPLOSIVE)

23-18-2-1(7-3-5-6)---7

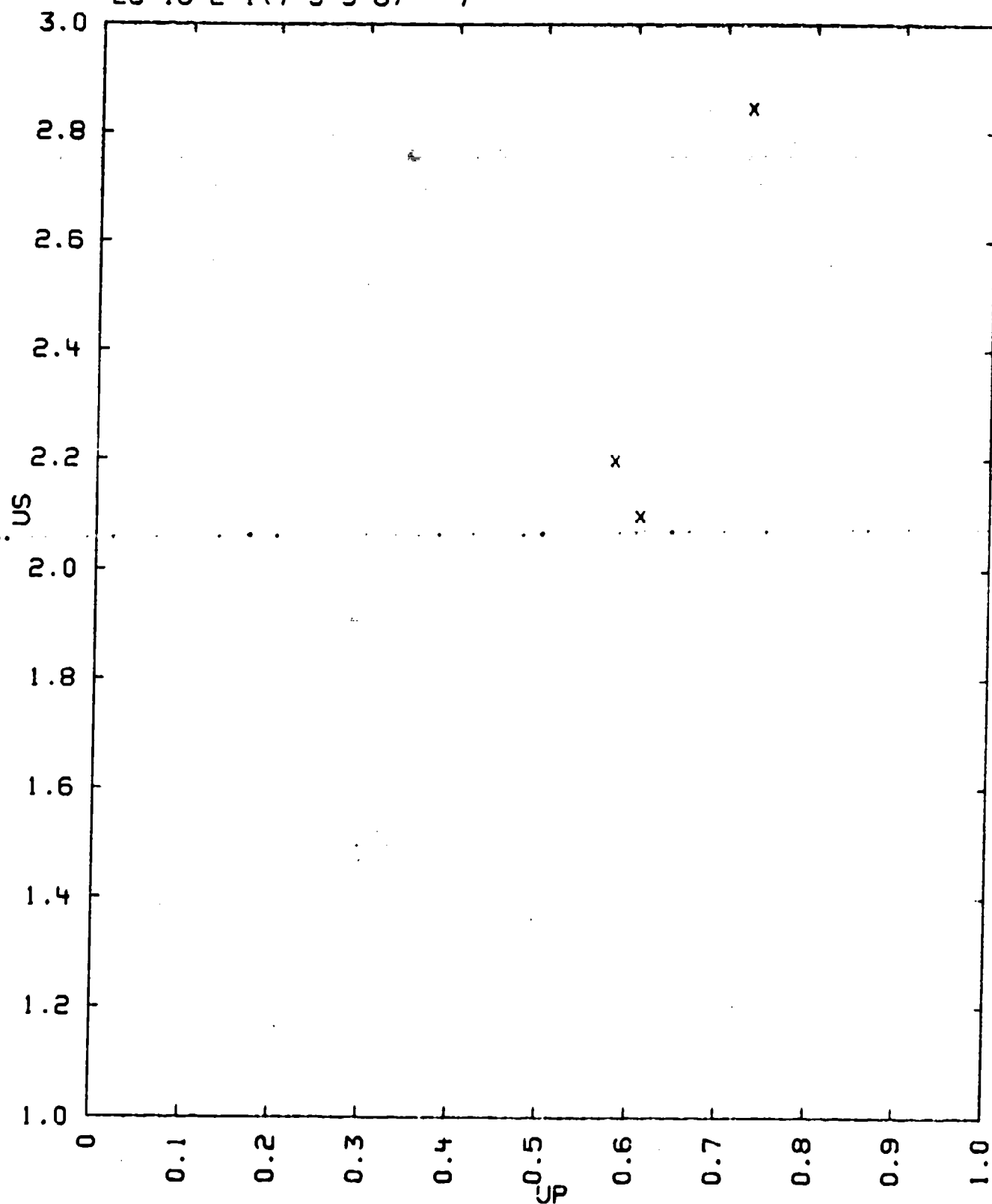
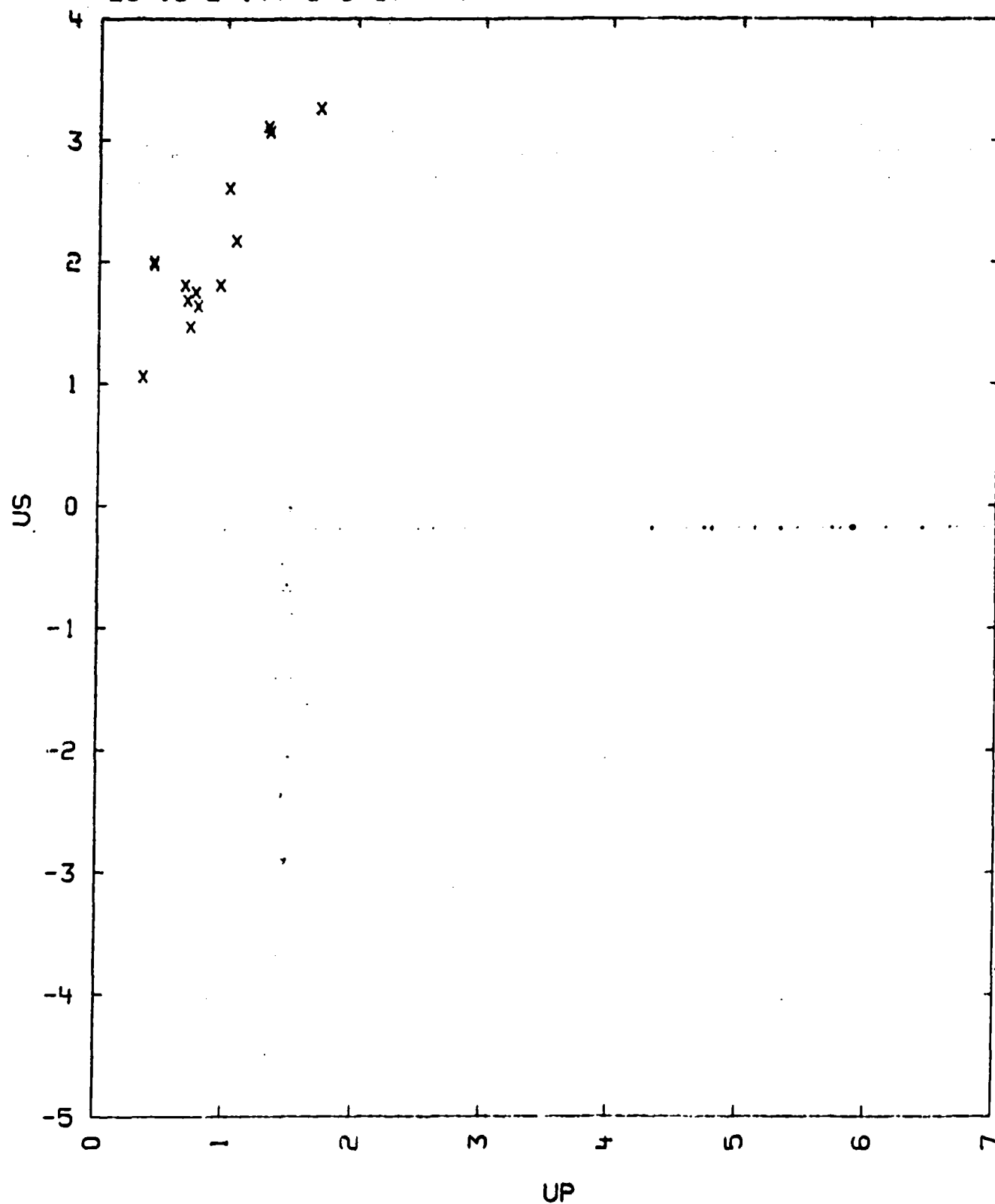


TABLE II

TRINITROTOLUENE (TNT) (EXPLOSIVE)

23-18-2-1(7-3-5-6)---7



23-18-2-1(200-6-224-28)---1  
EPOXY RESIN (EPON 828)

|                                                   |                          |                  |
|---------------------------------------------------|--------------------------|------------------|
| BISPHENOL-A -EPICHLOROHYDRIN RESIN: C200-H222-034 |                          | 83.3 WT. PERCENT |
| CURING AGENT :                                    |                          | 16.7 - -         |
| METAPHENYLENEDIAMINE                              | C6(H4)-(N(H2))2          | 17 - -           |
| METHYLENEDIANILINE                                | ((H2)N-C6(H4)-C(H2)-)2   | 81 - -           |
| PHENYLGlyCIDylether                               | C6(H5)-O-C(H2)-C2(H3)-O2 | 2 - -            |

V0 = 0.833 CC/G

CL = 2.70 KM/SEC.

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR. M.T. IS THE MEASURING TECHNIQUE FURTHER DELINIATED IN COMMENT 2.

TABLE

| RH00 | US   | UP    | P     | V/V0  | M.T. |
|------|------|-------|-------|-------|------|
| 1.20 | 2.76 | 0.065 | 2.15  | 0.976 | DI   |
| 1.20 | 2.78 | 0.089 | 2.95  | 0.968 | DI   |
| 1.20 | 2.84 | 0.111 | 3.78  | 0.961 | DI   |
| 1.20 | 3.00 | 0.185 | 6.67  | 0.938 | DI   |
| 1.20 | 3.01 | 0.238 | 8.59  | 0.921 | DI   |
| 1.20 | 3.18 | 0.307 | 11.70 | 0.903 | DI   |
| 1.20 | 3.24 | 0.371 | 14.40 | 0.885 | DI   |
| 1.20 | 3.39 | 0.467 | 18.90 | 0.862 | DI   |
| 1.20 | 2.83 | 0.106 | 3.61  | 0.962 | TR   |
| 1.20 | 2.83 | 0.110 | 3.74  | 0.961 | TR   |
| 1.20 | 3.04 | 0.234 | 8.55  | 0.923 | TR   |
| 1.20 | 3.04 | 0.246 | 8.96  | 0.919 | TR   |
| 1.20 | 3.24 | 0.372 | 14.45 | 0.885 | TR   |
| 1.20 | 3.24 | 0.391 | 15.19 | 0.879 | TR   |

US = 2.67 + 1.55\*UP KM/SEC

SIG.US = 0.03 KM/SEC.

#### COMMENTS:

#### 1) SOURCE: GUESS, T. R.

SANDIA LABORATORY REPORT, SC-DR-60-343 (1968)

SANDIA LABORATORY, ALBUQUERQUE, NEW MEXICO, U.S.A.

#### 2) EXPERIMENTAL TECHNIQUE: 12 AND A

IN THE TABLE DI LABELS EXPERIMENTS IN WHICH THE SAMPLE WAS IMPACTED BY AN X-CUT QUARTZ CRYSTAL. HERE P AND US WERE MEASURED

TR LABELS EXPERIMENTS WHERE A HARDENED STEEL (ALLOY 4340 RC-54) PROJECTILE WAS USED. HERE P,US AND BULLET VELOCITY WERE MEASURED

WITH THIS REDUNDANCY OF INFORMATION AND THE STEEL HUGONIOT TWO P,V,UP POINTS WERE DETERMINED PER EXPERIMENT, INDICATING THE ACCURACY

DATA REDUCTION TECHNIQUE: A AND C

#### 3) UNCERTAINTIES IN THE MEASURED PARAMETERS ARE:

SIG US = 2 PERCENT

SIG P = 3.4 -

SIG U = 1 -

U IS THE BULLET VELOCITY.

NO WAVE ATTENUATION WAS OBSERVED, UNLIKE IN PLEXIGLAS

- 4) THIS POLYMER IS A CONDENSATION PRODUCT OF BISPHENOL-A AND EPICHLOROHYDRIN HARDENED WITH THE LISTED CURING AGENT. THE MOLECULAR COMPOSITION OF THE UNHARDENED RESIN IS OBTAINED BY TAKING 10 TO 20 MONOMER UNITS IN THE CHAIN. THE CURING AGENT COMPOSITION WAS OBTAINED USING THE ABOVE MOLECULAR CONTENT (SANDIA STANDARD 4604085, P.2) AND A CHEMICAL ANALYSIS:

C - 78.7, H - 5.4, N - 15.4 AND O - 0.5 WT. PERCENT

THE CURED PLASTIC CONSISTING OF 100 PARTS RESIN AND 20 PARTS CURING AGENT YIELDED:

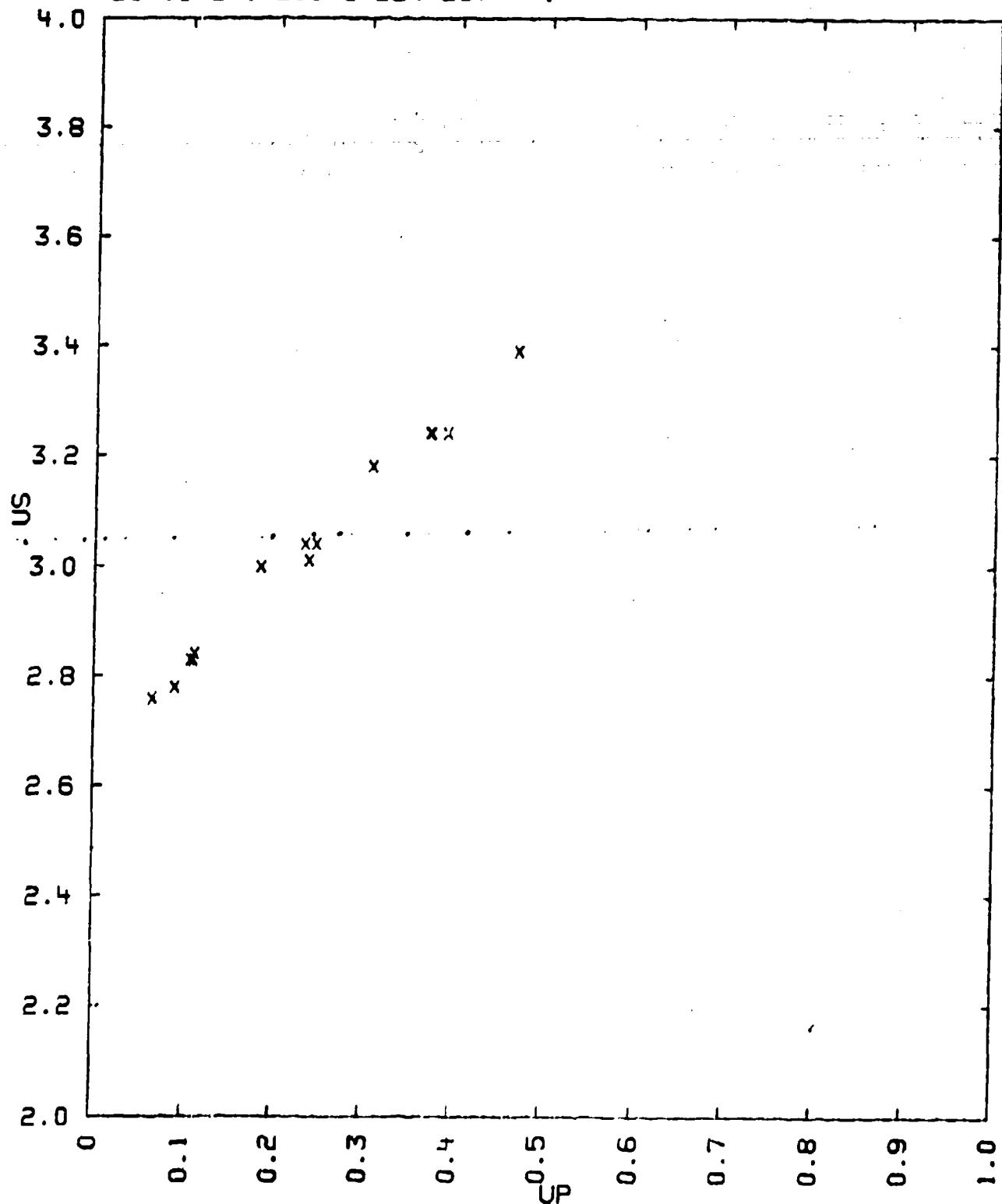
C - 75.3, H - 6.7, N - 2.6 AND O - 15.5 WT. PERCENT

KEN WISHMANN, SANDIA LABORATORY.

THE RESIN STRUCTURE IS DESCRIBED BY I SKEIST, HANDBOOK OF ADHESIVES (REINHOLD PUBL. CORP., N.Y., 1962) P. 323 FF.

TABLE I

EPOXY RESIN (EPON 828)  
23-18-2-1 (200-6-224-28) ---1



EPON 815: NOTE 3

BPA-EPI RESIN (C18-H22-O3)N  
BUTYLOXYCIDYL ETHER C7-H14-O2  
DIETHYLENETRIAMINE H-N(-C(H2)-CCH2)-N-H2/2

79.2 WT PERCENT  
10.8 WT PERCENT  
10. WT PERCENT

V0 = 0.8446 CC/G CL = 2.87 KM/SEC CO = 2.30 - 2.19 KM/SEC  
CS = 1.48 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL           | US(ST) |
| 1.184            | 3.26 | 0.37 | 14.  | 0.8865 | CU                 | 4.24   |
| 1.184            | 3.35 | 0.41 | 16.  | 0.8776 | 2024 AL            | 5.67   |
| 1.184            | 3.42 | 0.49 | 20.  | 0.8567 | 2024 AL            | 5.75   |
| 1.184            | 3.80 | 0.64 | 29.  | 0.8316 | CU                 | 4.47   |
| 1.184            | 3.71 | 0.70 | 31.  | 0.8113 | 2024 AL            | 5.93   |
| 1.184            | 3.80 | 0.72 | 32.  | 0.8105 | 2024 AL            | 5.94   |
| 1.184            | 3.70 | 0.74 | 32.  | 0.8000 | 2024 AL            | 5.96   |
| 1.184            | 3.72 | 0.78 | 34.  | 0.7903 | 2024 AL            | 6.00   |
| 1.184            | 4.31 | 0.92 | 47.  | 0.7865 | CU                 | 4.72   |
| 1.184            | 4.17 | 0.93 | 46.  | 0.7770 | 2024 AL            | 6.14   |
| 1.184            | 4.22 | 0.96 | 48.  | 0.7725 | CU                 | 4.75   |
| 1.184            | 4.19 | 0.96 | 48.  | 0.7709 | CU                 | 4.75   |
| 1.184            | 4.09 | 0.99 | 48.  | 0.7579 | 2024 AL            | 6.19   |
| 1.184            | 4.48 | 1.15 | 61.  | 0.7433 | CU                 | 4.92   |
| 1.184            | 4.56 | 1.19 | 64.  | 0.7390 | CU                 | 4.96   |
| 1.184            | 4.57 | 1.19 | 64.  | 0.7395 | CU                 | 4.96   |
| 1.198            | 4.54 | 1.21 | 66.  | 0.7335 | 2024 AL            | 6.41   |
| 1.198            | 4.53 | 1.22 | 66.  | 0.7307 | 2024 AL            | 6.41   |
| 1.184            | 4.74 | 1.34 | 75.  | 0.7173 | 2024 AL            | 6.53   |
| 1.184            | 4.74 | 1.36 | 76.  | 0.7131 | 2024 AL            | 6.55   |
| 1.184            | 4.68 | 1.42 | 79.  | 0.6966 | 2024 AL            | 6.60   |
| 1.198            | 5.24 | 1.70 | 107. | 0.6756 | 2024 AL            | 6.88   |
| 1.198            | 5.24 | 1.70 | 107. | 0.6756 | 2024 AL            | 6.88   |
| 1.198            | 5.24 | 1.70 | 107. | 0.6756 | 2024 AL            | 6.88   |
| 1.184            | 5.30 | 1.70 | 107. | 0.6792 | CU                 | 5.41   |
| 1.184            | 5.37 | 1.72 | 109. | 0.6797 | CU                 | 5.42   |
| 1.184            | 5.36 | 1.73 | 110. | 0.6772 | 2024 AL            | 6.91   |
| 1.184            | 5.33 | 1.75 | 110. | 0.6717 | 2024 AL            | 6.92   |
| 1.184            | 5.35 | 1.80 | 114. | 0.6636 | 2024 AL            | 6.97   |
| 1.184            | 5.33 | 1.81 | 114. | 0.6604 | CU                 | 5.50   |
| 1.184            | 5.63 | 1.89 | 126. | 0.6643 | CU                 | 5.58   |
| 1.198            | 6.12 | 2.25 | 165. | 0.6324 | 2024 AL            | 7.43   |
| 1.198            | 6.09 | 2.25 | 164. | 0.6305 | 2024 AL            | 7.43   |
| 1.184            | 6.34 | 2.36 | 177. | 0.6278 | 2024 AL            | 7.54   |
| 1.184            | 6.28 | 2.39 | 178. | 0.6194 | 2024 AL            | 7.57   |

## EPOXY

| RH00  | US   | UP   | P    | V/VO   | MATERIAL | US(ST) |
|-------|------|------|------|--------|----------|--------|
| 1.184 | 6.38 | 2.40 | 181. | 0.6238 | 2024 AL  | 7.58   |
| 1.184 | 6.63 | 2.41 | 189. | 0.6365 | 2024 AL  | 7.61   |
| 1.184 | 6.43 | 2.52 | 192. | 0.6081 | CU       | 6.15   |
| 1.184 | 6.60 | 2.58 | 202. | 0.6091 | 2024 AL  | 7.76   |
| 1.184 | 6.88 | 2.76 | 225. | 0.5988 | 2024 AL  | 7.95   |
| 1.184 | 7.17 | 2.84 | 241. | 0.6039 | CU       | 6.46   |
| 1.184 | 7.21 | 3.18 | 271. | 0.5589 | CU       | 6.75   |
| 1.184 | 7.34 | 3.19 | 277. | 0.5654 | 2024 AL  | 8.38   |
| 1.184 | 7.61 | 3.56 | 321. | 0.5322 | 2024 AL  | 8.74   |
| 1.184 | 7.65 | 3.58 | 324. | 0.5320 | 2024 AL  | 8.76   |
| 1.184 | 7.62 | 3.61 | 326. | 0.5262 | CU       | 7.13   |
| 1.184 | 7.95 | 3.78 | 356. | 0.5245 | CU       | 7.30   |
| 1.184 | 8.39 | 3.89 | 386. | 0.5364 | CU       | 7.42   |
| 1.184 | 8.24 | 3.95 | 385. | 0.5206 | 2024 AL  | 9.16   |
| 1.184 | 8.06 | 3.95 | 377. | 0.5099 | CU       | 7.45   |
| 1.181 | 8.26 | 4.12 | 402. | 0.5012 | CU       | 7.60   |
| 1.181 | 8.48 | 4.14 | 415. | 0.5118 | CU       | 7.64   |
| 1.184 | 8.73 | 4.15 | 429. | 0.5246 | 2024 AL  | 9.39   |
| 1.184 | 8.90 | 4.49 | 473. | 0.4955 | 2024 AL  | 9.72   |
| 1.184 | 8.82 | 4.65 | 486. | 0.4728 | CU       | 8.13   |
| 1.184 | 9.16 | 4.68 | 508. | 0.4891 | CU       | 8.14   |
| 1.198 | 9.25 | 4.86 | 539. | 0.4746 | 2024 AL  | 10.10  |
| 1.198 | 9.23 | 4.86 | 537. | 0.4735 | 2024 AL  | 10.10  |
| 1.184 | 9.74 | 5.10 | 588. | 0.4764 | 2024 AL  | 10.36  |
| 1.184 | 9.76 | 5.13 | 593. | 0.4744 | 2024 AL  | 10.39  |

US =  $2.632 + 1.664 \cdot UP - 0.060 \cdot UP^2$  KM/SEC

SIG US = 0.13 KM/SEC

OR

US =  $2.682 + 1.532 \cdot UP$  KM/SEC FOR UP BELOW 3 KM/SEC

SIG US = 0.09 KM/SEC

AND

US =  $3.221 + 1.258 \cdot UP$  KM/SEC FOR UP ABOVE 3 KM/SEC

SIG US 0.14 KM/SEC

## COMMENTS:

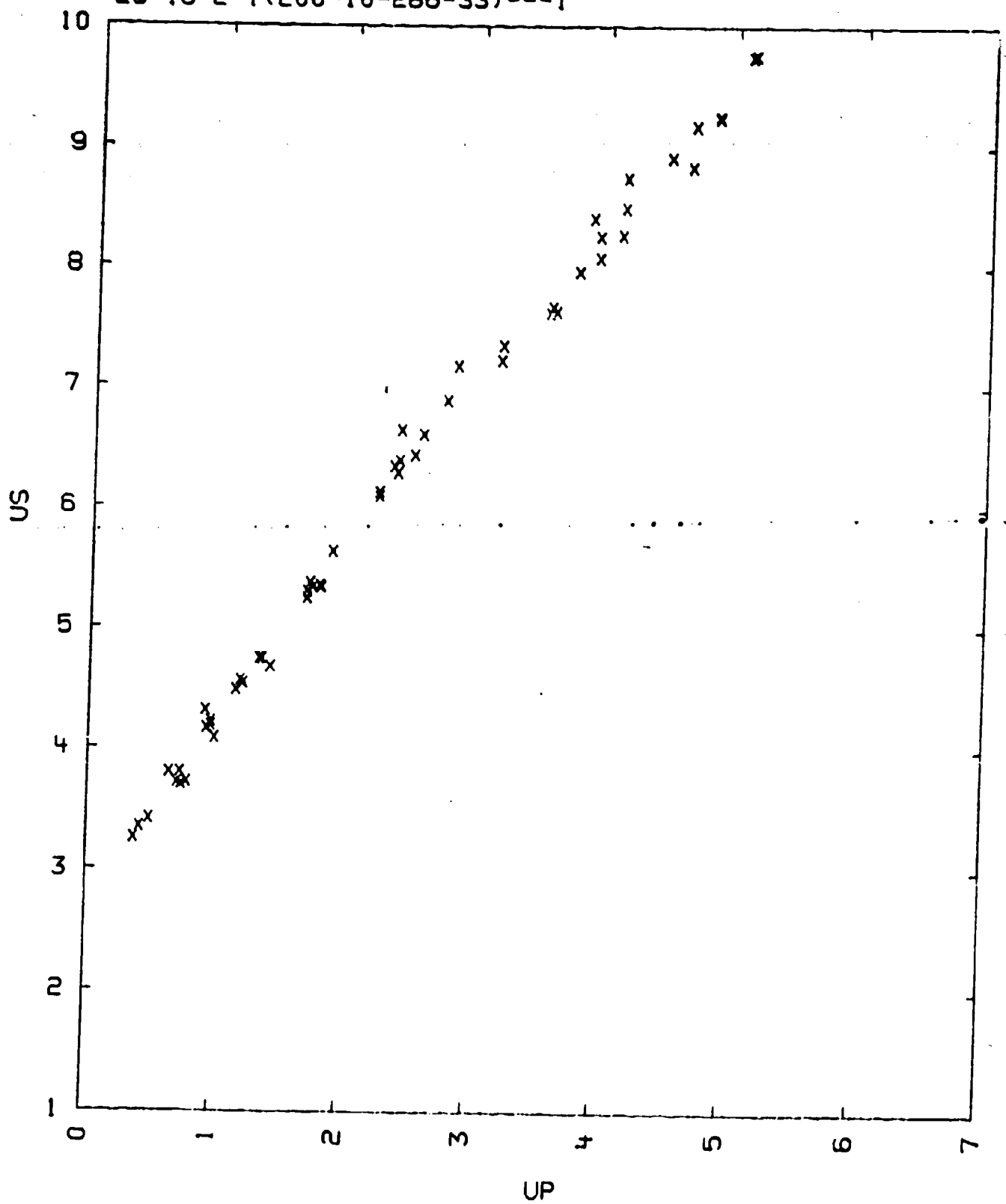
- 1) SOURCE: MCOQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES, HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) THE COMPOSITION WAS ASSUMED TO BE THE SAME AS THAT GIVEN FOR THE EPOXY RESIN IN THE MIXTURE CU-0--EPOXY = 36-1--23-18-2-1 (200-10-286-33)---1 GIVEN BY THIS SOURCE. NOTE SIMILARITY TO THE OTHER EPOXY LISTED ABOVE: 23-18-2-1(200-6-224-28)---1 SEE ALSO MODERN PLASTICS ENCYCLOPEDIA (MC GRAW HILL, N.Y., 1975) VOL. 51, NO. 10A
- 4) V(OP/DE) = 1.13



TABLE 1

EPOXY

23-18-2-1(200-10-286-33)---1



23-18-2-1(200-16-286-79)---1  
POLYURETHANE

(C200-N16-H286-079)N

99.9 WT PERCENT

VO = 0.7905 CC/G

CO = 2.07 KM/SEC

IN THE TABLE BELOW, DENSITY IS GIVEN G/CC, VELOCITIES IN KM/SEC, AND  
PRESSURE IN KILOBARS.

TABLE

| RH00  | US    | UP    | P     | V/VO   |
|-------|-------|-------|-------|--------|
| 1.265 | 4.215 | 1.119 | 596.7 | 0.7345 |
| -     | 4.198 | 1.120 | 594.8 | 0.7332 |
| -     | 4.562 | 1.345 | 776.2 | 0.7052 |
| -     | 4.549 | 1.346 | 774.6 | 0.7041 |
| -     | 5.278 | 1.786 | 119.3 | 0.6616 |
| -     | 5.279 | 1.786 | 119.3 | 0.6617 |
| -     | 6.033 | 2.246 | 171.4 | 0.6277 |
| -     | 5.986 | 2.251 | 170.5 | 0.6270 |
| -     | 6.430 | 2.505 | 203.8 | 0.6104 |
| -     | 6.409 | 2.507 | 203.3 | 0.6088 |
| -     | 6.551 | 2.606 | 216.0 | 0.6022 |
| -     | 6.539 | 2.607 | 215.7 | 0.6013 |
| -     | 6.776 | 2.761 | 236.7 | 0.5925 |
| -     | 6.749 | 2.764 | 234.0 | 0.5905 |
| -     | 6.844 | 2.824 | 244.5 | 0.5874 |
| -     | 7.719 | 3.483 | 340.1 | 0.5488 |
| -     | 7.698 | 3.485 | 339.4 | 0.5473 |
| -     | 8.543 | 4.335 | 468.5 | 0.4926 |
| -     | 8.534 | 4.337 | 468.2 | 0.4918 |

US = 1.989 + 2.101\*UP - 1.351\*UP\*\*2 +OR- 0.05 KM/SEC

## COMMENTS:

- 1) SOURCE: CARTER, W. J., MARSH, S. P. AND MCQUEEN, R. G.  
PRIVATE COMMUNICATION (1967)  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B  
STANDARD MATERIAL 2024 ALUMINUM.
- 3) CO WAS GIVEN BY THE AUTHORS.
- 4) THE POLYMER WAS MADE BY MIXING TWO PARTIALLY POLYMERISED MIXTURES:  
R MIXTURE: ADIPIC ACID H-O2-C(=O)-H214-C-O2-H  
DIETHYLENE GLYCOL (H-O-C(H2)-C(H2)12-O  
TRYMETHYLOL PROPANE H3-C(H2)-C(=O)(H2)-O-H  
ACID NO.: 1.2 +OR-0.2  
OH NO.: 320 +OR-10  
WEIGHT RATIO : C/H/O = 55.9/8.3/35.8  
WATER : LESS THAN 0.05 PERCENT  
T MIXTURE: TOLUENEDIISOCYANATE : H3-C(=O)-H31(N-C-O)2

## RESIN

AMENE EQUIVALENT : 129 +OR- 2 GRAMS

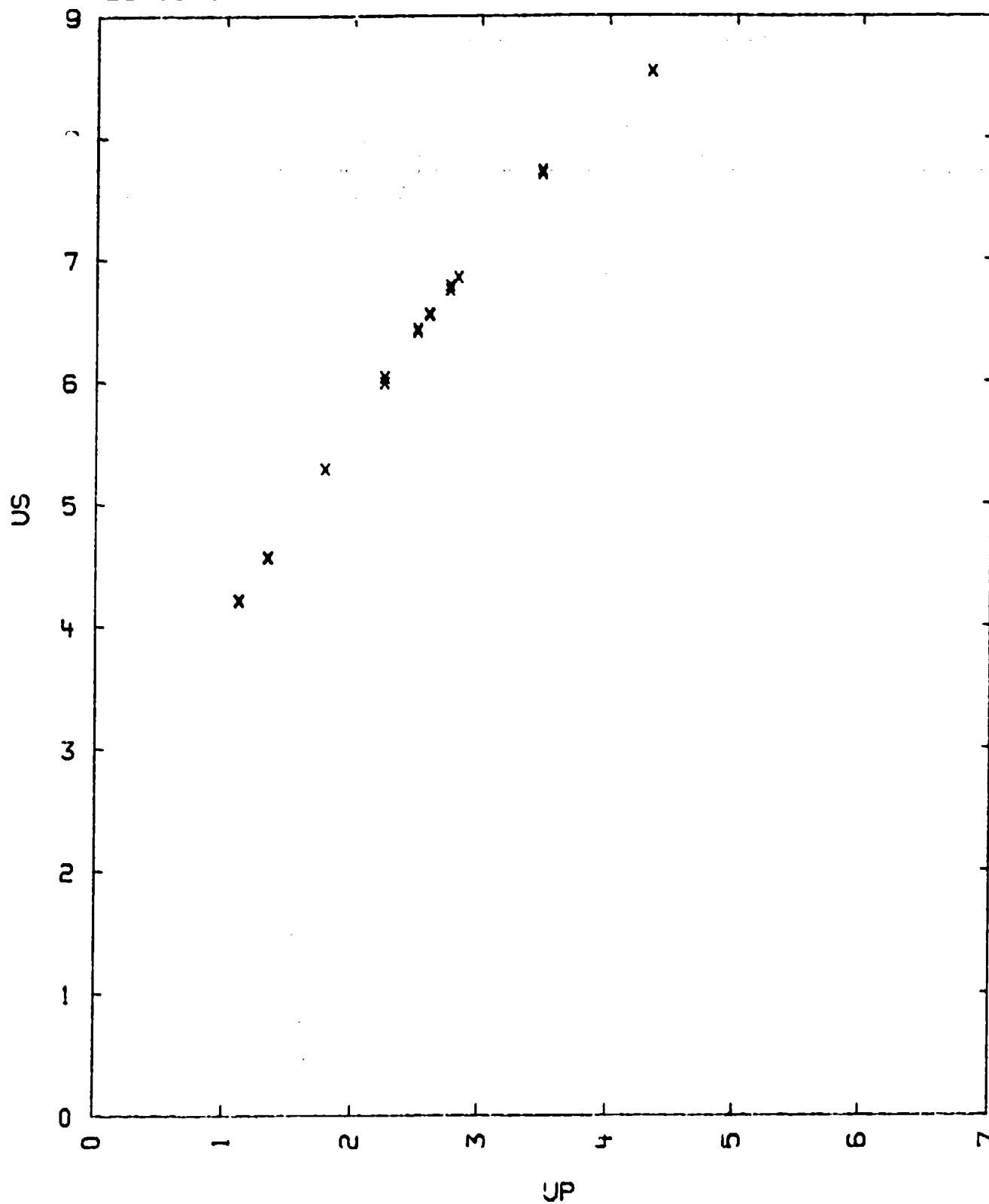
WEIGHT RATIO : C/H/N/O = 60.2/4.5/12.6/22.7

POLYMER : WEIGHT RATIO : C/H/N/O/(ASH+CL) = 57.44/6.90/5.43/30.10/0.1

TABLE 1

POLYURETHANE

23-18-2-1(200-16-286-79)---1



23-18-2-1(200-16-286-79)---2  
POLYURETHANE

C200-N16-H286-079

$V_0 = 0.7805$

$CL = 2.39 \text{ KM/SEC}$   $CO = 2.07 \text{ KM/SEC}$   
 $CS = 1.03 \text{ KM/SEC}$

IN THE TABLES BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBAR  
AND DENSITY IN G/CC.

TABLE I

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RHO0             | US   | UP   | P    | V/V0   | MATERIAL           | US(ST) |
| 1.265            | 4.15 | 1.05 | 55.  | 0.7470 | 2024 AL            | 6.26   |
| 1.265            | 4.14 | 1.05 | 55.  | 0.7464 | 2024 AL            | 6.26   |
| 1.265            | 4.50 | 1.28 | 73.  | 0.7156 | 2024 AL            | 6.48   |
| 1.265            | 4.48 | 1.28 | 73.  | 0.7143 | 2024 AL            | 6.48   |
| 1.265            | 5.20 | 1.71 | 112. | 0.6712 | 2024 AL            | 6.91   |
| 1.265            | 5.20 | 1.71 | 112. | 0.6712 | 2024 AL            | 6.91   |
| 1.265            | 5.95 | 2.17 | 163. | 0.6353 | 2024 AL            | 7.38   |
| 1.265            | 5.90 | 2.18 | 163. | 0.6305 | 2024 AL            | 7.38   |
| 1.265            | 6.34 | 2.43 | 195. | 0.6167 | 2024 AL            | 7.64   |
| 1.265            | 6.32 | 2.43 | 194. | 0.6155 | 2024 AL            | 7.64   |
| 1.265            | 6.46 | 2.53 | 207. | 0.6084 | 2024 AL            | 7.74   |
| 1.265            | 6.44 | 2.53 | 206. | 0.6071 | 2024 AL            | 7.74   |
| 1.265            | 6.68 | 2.68 | 226. | 0.5988 | 2024 AL            | 7.90   |
| 1.265            | 6.65 | 2.68 | 225. | 0.5970 | 2024 AL            | 7.90   |
| 1.265            | 6.75 | 2.74 | 234. | 0.5941 | 2024 AL            | 7.97   |
| 1.265            | 7.61 | 3.39 | 326. | 0.5545 | 2024 AL            | 8.64   |
| 1.265            | 7.59 | 3.40 | 326. | 0.5520 | 2024 AL            | 8.64   |
| 1.265            | 8.42 | 4.15 | 442. | 0.5071 | 2024 AL            | 9.42   |
| 1.265            | 8.42 | 4.15 | 442. | 0.5071 | 2024 AL            | 9.42   |
| 1.265            | 9.28 | 4.76 | 559. | 0.4871 | 2024 AL            | 10.08  |
| 1.265            | 9.20 | 4.78 | 556. | 0.4804 | 2024 AL            | 10.08  |

$US = 2.486 + 1.577 \cdot UP \text{ KM/SEC}$  FOR UP BELOW 2.6

$SIG US = 0.024 \text{ KM/SEC}$

$US = 3.423 + 1.216 \cdot UP \text{ KM/SEC}$  FOR UP ABOVE 2.6 KM/SEC

$SIG US = 0.05 \text{ KM/SEC}$

TABLE II

| -----SAMPLE----- |      |      |     |        | -----STANDARD----- |        |
|------------------|------|------|-----|--------|--------------------|--------|
| RHO0             | US   | UP   | P   | V/V0   | MATERIAL           | US(ST) |
| 0.476            | 2.34 | 1.62 | 18. | 0.3077 | 2024 AL            | 6.48   |
| 0.381            | 2.55 | 1.62 | 18. | 0.3647 | 2024 AL            | 6.48   |
| 0.355            | 3.13 | 2.15 | 24. | 0.3131 | 2024 AL            | 6.86   |

$US = 0.351 + 1.292 \cdot UP \text{ KM/SEC}$

## POLYURETHANE

RH00      US      UP      P      V/VO      MATERIAL US(ST)  
 SIGMA US = 0.148    KM/SEC

TABLE III

| -----SAMPLE----- |      |      |     |        | -----STANDARD----- |      |
|------------------|------|------|-----|--------|--------------------|------|
| RH00             | US   | UP   | P   | V/VO   | MATERIAL US(ST)    |      |
| 0.310            | 2.52 | 1.68 | 13. | 0.3333 | 2024 AL            | 6.51 |
| 0.339            | 3.12 | 2.15 | 23. | 0.3109 | 2024 AL            | 6.86 |
| 0.308            | 3.21 | 2.16 | 21. | 0.3271 | 2024 AL            | 6.86 |
| 0.333            | 3.25 | 2.16 | 23. | 0.3354 | 2024 AL            | 6.87 |
| 0.319            | 3.88 | 2.72 | 34. | 0.2990 | 2024 AL            | 7.29 |
| 0.320            | 3.68 | 2.74 | 32. | 0.2554 | 2024 AL            | 7.29 |
| 0.315            | 3.75 | 2.74 | 32. | 0.2693 | 2024 AL            | 7.29 |

US = 0.712 + 1.127\*UP    KM/SEC  
 SIGMA US = 0.100    KM/SEC

TABLE IV

| -----SAMPLE----- |      |      |     |        | -----STANDARD----- |      |
|------------------|------|------|-----|--------|--------------------|------|
| RH00             | US   | UP   | P   | V/VO   | MATERIAL US(ST)    |      |
| 0.289            | 3.33 | 2.19 | 21. | 0.3423 | 2024 AL            | 6.88 |
| 0.267            | 3.08 | 2.21 | 18. | 0.2825 | 2024 AL            | 6.88 |
| 0.250            | 3.05 | 2.22 | 17. | 0.2721 | 2024 AL            | 6.88 |
| 0.296            | 3.79 | 2.75 | 31. | 0.2744 | 2024 AL            | 7.29 |
| 0.286            | 3.75 | 2.85 | 31. | 0.2400 | 2024 AL            | 7.36 |
| 0.285            | 3.78 | 2.86 | 31. | 0.2434 | 2024 AL            | 7.36 |
| 0.282            | 3.78 | 2.86 | 30. | 0.2434 | 2024 AL            | 7.36 |
| 0.273            | 3.68 | 2.87 | 29. | 0.2201 | 2024 AL            | 7.36 |
| 0.285            | 4.00 | 2.87 | 33. | 0.2825 | 2024 AL            | 7.38 |
| 0.289            | 4.00 | 2.87 | 33. | 0.2825 | 2024 AL            | 7.38 |

US = 0.868 + 1.038\*UP    KM/SEC  
 SIGMA US = 0.136    KM/SEC

TABLE V

| -----SAMPLE----- |      |      |    |        | -----STANDARD----- |      |
|------------------|------|------|----|--------|--------------------|------|
| RH00             | US   | UP   | P  | V/VO   | MATERIAL US(ST)    |      |
| 0.145            | 2.23 | 1.73 | 6. | 0.2242 | 2024 AL            | 6.51 |
| 0.150            | 2.26 | 1.74 | 6. | 0.2301 | 2024 AL            | 6.51 |
| 0.149            | 2.26 | 1.74 | 6. | 0.2301 | 2024 AL            | 6.51 |
| 0.147            | 2.23 | 1.74 | 6. | 0.2197 | 2024 AL            | 6.52 |
| 0.145            | 2.24 | 1.75 | 6. | 0.2187 | 2024 AL            | 6.52 |

## POLYURETHANE

| RH00  | US   | UP   | P   | V/V0   | MATERIAL | US(ST) |
|-------|------|------|-----|--------|----------|--------|
| 0.159 | 2.95 | 2.21 | 10. | 0.2508 | 2024 AL  | 6.85   |
| 0.159 | 3.06 | 2.22 | 11. | 0.2745 | 2024 AL  | 6.86   |
| 0.157 | 3.01 | 2.22 | 10. | 0.2625 | 2024 AL  | 6.86   |
| 0.149 | 2.94 | 2.23 | 10. | 0.2415 | 2024 AL  | 6.86   |
| 0.202 | 3.06 | 2.23 | 14. | 0.2712 | 2024 AL  | 6.88   |
| 0.178 | 3.75 | 2.88 | 19. | 0.2320 | 2024 AL  | 7.33   |
| 0.158 | 3.74 | 2.88 | 17. | 0.2299 | 2024 AL  | 7.32   |
| 0.160 | 3.78 | 2.98 | 18. | 0.2116 | 2024 AL  | 7.39   |
| 0.175 | 3.66 | 2.98 | 19. | 0.1858 | 2024 AL  | 7.39   |
| 0.156 | 3.63 | 2.98 | 17. | 0.1791 | 2024 AL  | 7.39   |
| 0.159 | 3.68 | 3.00 | 18. | 0.1848 | 2024 AL  | 7.40   |
| 0.159 | 3.61 | 3.01 | 17. | 0.1662 | 2024 AL  | 7.40   |

$$US = 0.328 + 1.148 \cdot UP \quad \text{KM/SEC}$$

$$SIGMA US = 0.119 \quad \text{KM/SEC}$$

TABLE VI

| -----SAMPLE----- |      |      |     |        | -----STANDARD----- |        |
|------------------|------|------|-----|--------|--------------------|--------|
| RH00             | US   | UP   | P   | V/V0   | MATERIAL           | US(ST) |
| 0.107            | 2.30 | 1.73 | 4.  | 0.2478 | 2024 AL            | 6.50   |
| 0.107            | 2.32 | 1.77 | 4.  | 0.2371 | 2024 AL            | 6.53   |
| 0.093            | 2.97 | 2.26 | 6.  | 0.2391 | 2024 AL            | 6.86   |
| 0.098            | 3.00 | 2.26 | 7.  | 0.2467 | 2024 AL            | 6.87   |
| 0.095            | 2.87 | 2.27 | 6.  | 0.2091 | 2024 AL            | 6.87   |
| 0.091            | 2.92 | 2.29 | 6.  | 0.2158 | 2024 AL            | 6.88   |
| 0.099            | 3.41 | 3.05 | 10. | 0.1056 | 2024 AL            | 7.40   |
| 0.094            | 3.37 | 3.05 | 10. | 0.0950 | 2024 AL            | 7.40   |
| 0.077            | 3.36 | 3.07 | 8.  | 0.0863 | 2024 AL            | 7.40   |
| 0.081            | 3.49 | 3.07 | 9.  | 0.1203 | 2024 AL            | 7.41   |
| 0.077            | 3.39 | 3.08 | 8.  | 0.0914 | 2024 AL            | 7.41   |

$$US = 1.109 + 0.760 \cdot UP \quad \text{KM/SEC}$$

$$SIGMA US = 0.109 \quad \text{KM/SEC}$$

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.O., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES, HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B (STANDARD BASE PLATE AS SHOWN)
- 3) THE NONPOROUS SAMPLES WERE FROM THE C.P.R. INTERNATIONAL CORP. THE FOAMS WERE PRODUCED AT THE LOS ALAMOS LABORATORY IN NEW MEXICO
- 4)  $V(DP/DE) = 1.5\%$

TABLE I

POLYURETHANE

23-18-2-1(200-16-286-79)---2

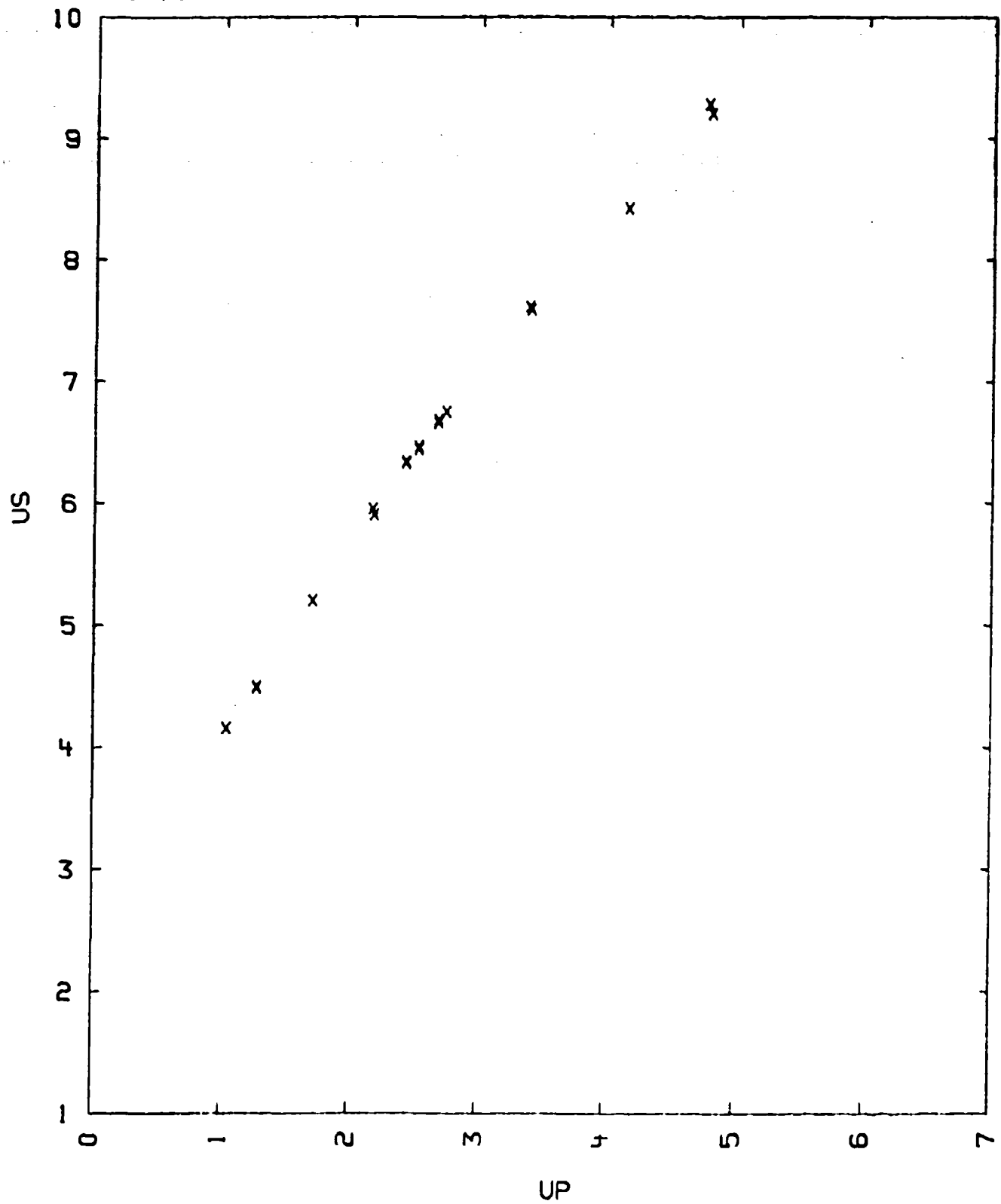




TABLE 11

POLYURETHANE

23-18-2-1(200-16-286-79)---2

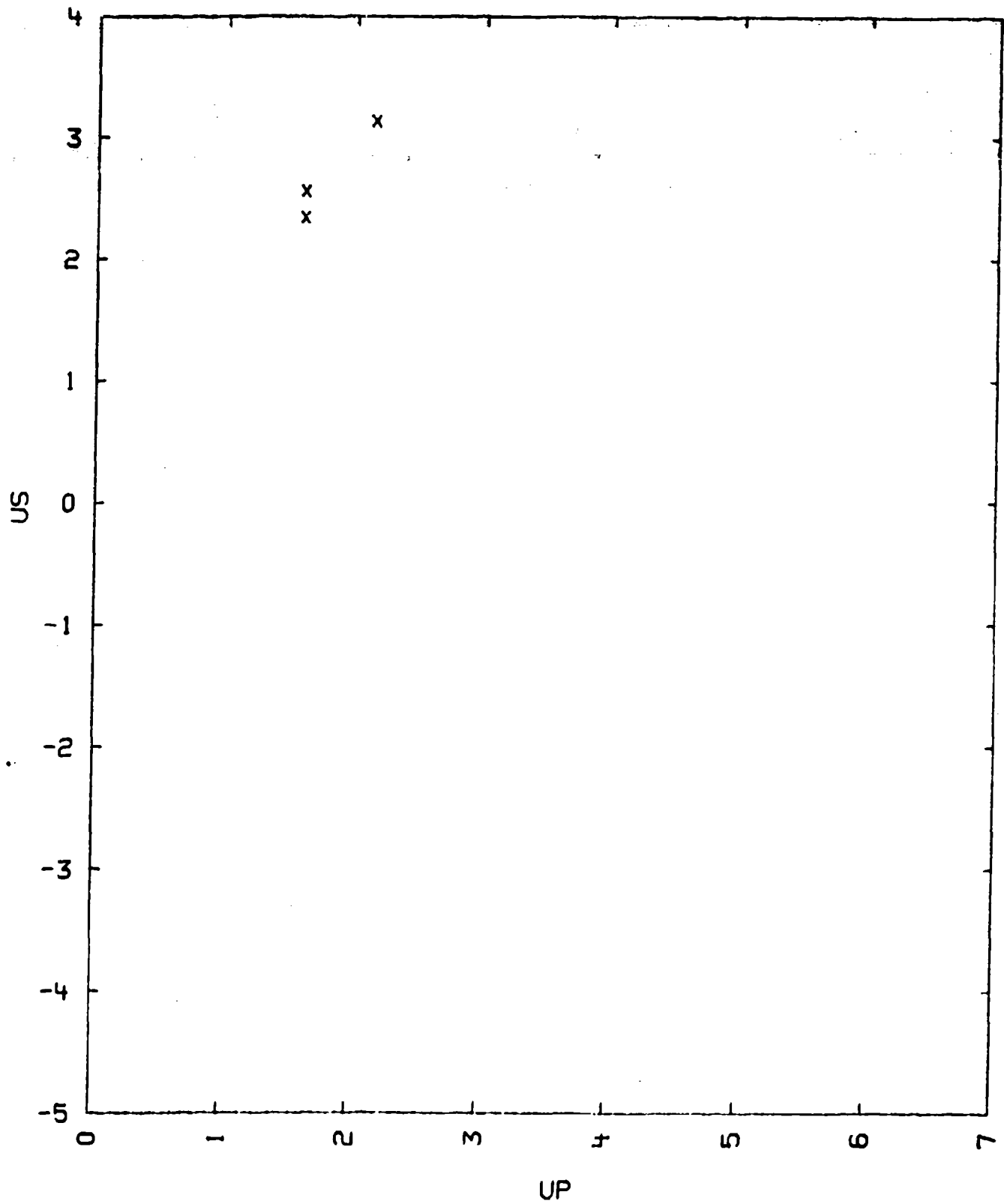


TABLE III

POLYURETHANE

23-18-2-1 (200-16-286-79) ---2

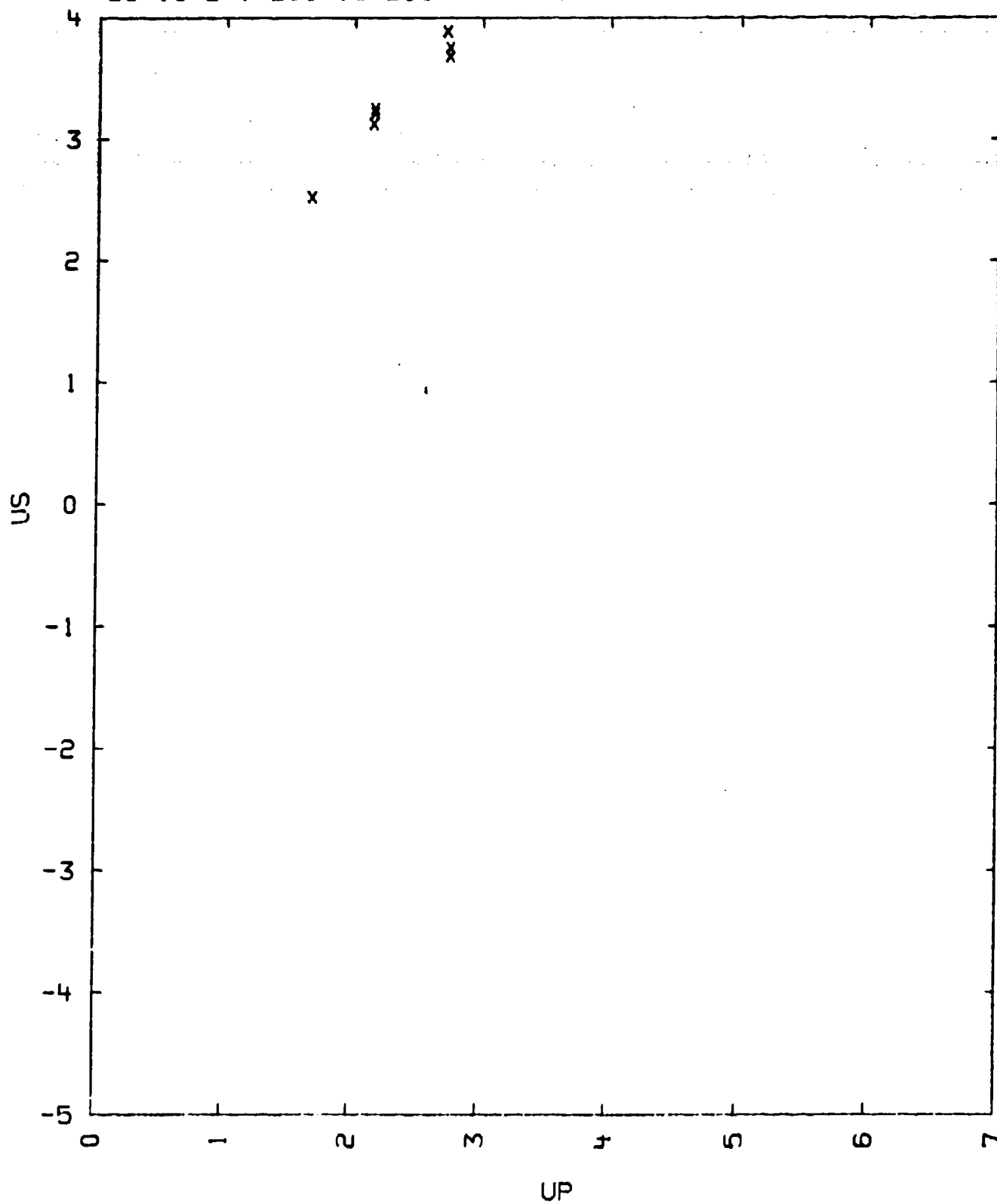


TABLE IV

POLYURETHANE

23-18-2-1(200-16-286-79)---2

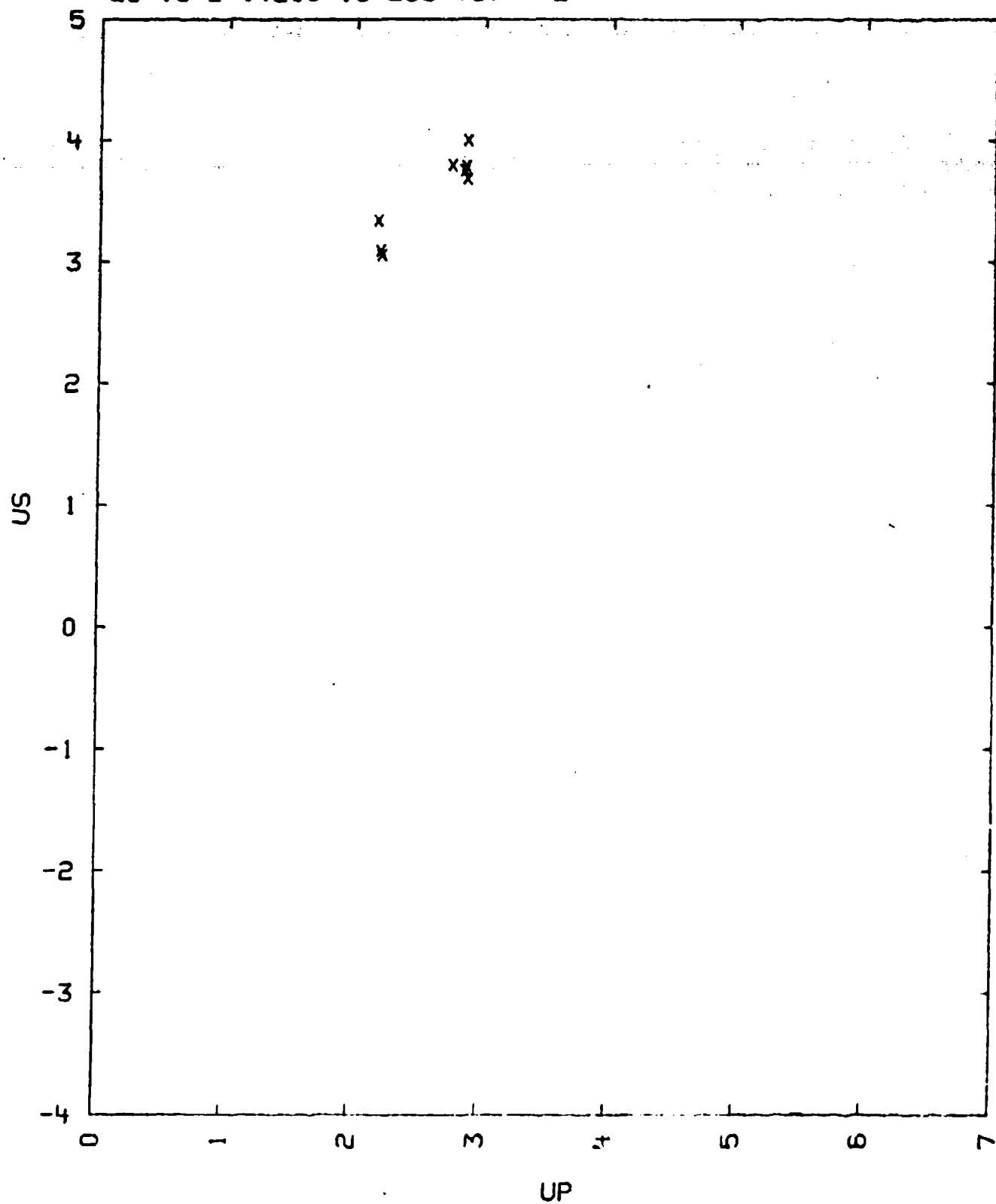


TABLE V

POLYURETHANE

23-18-2-1 (200-16-286-79) ---2

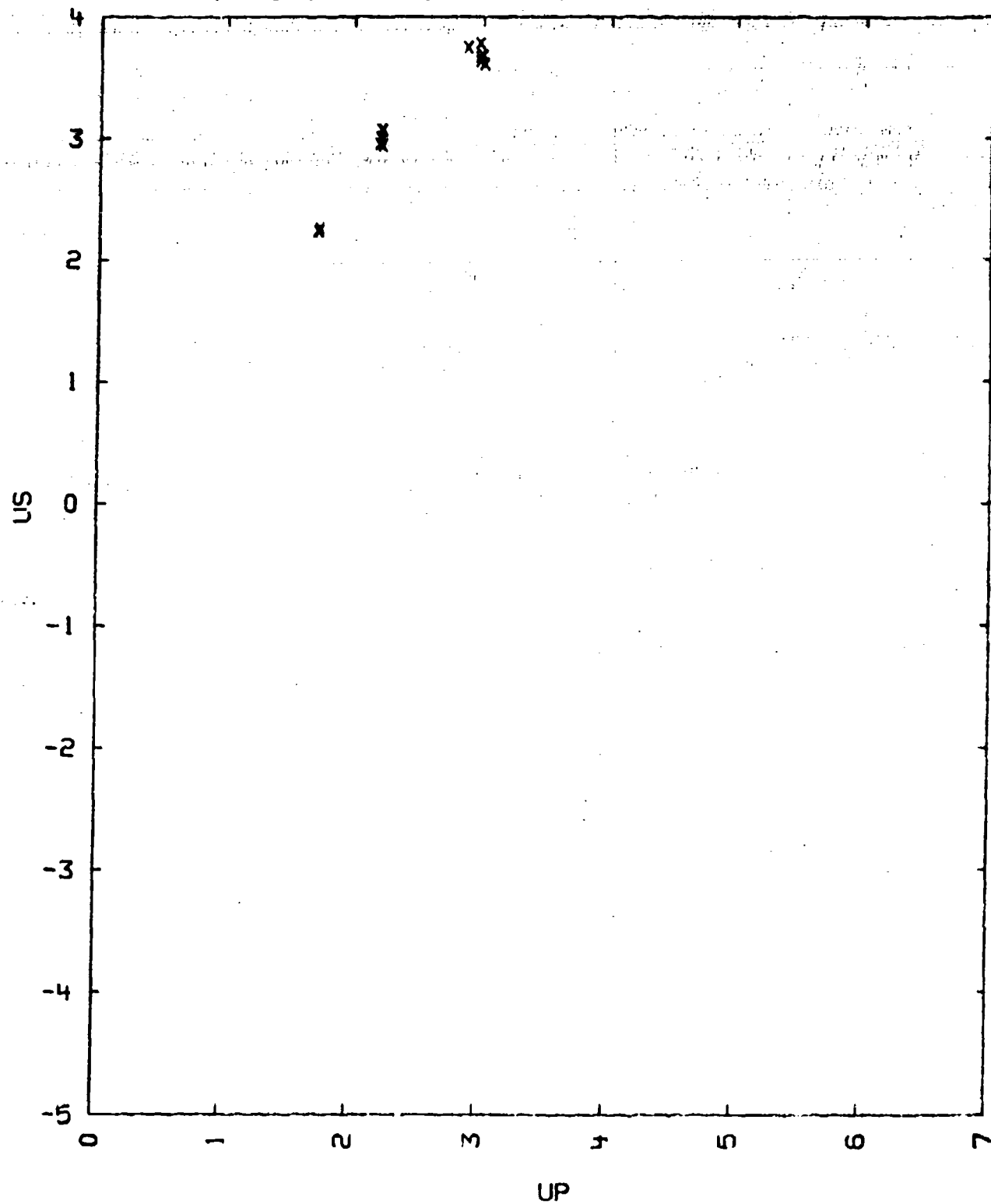
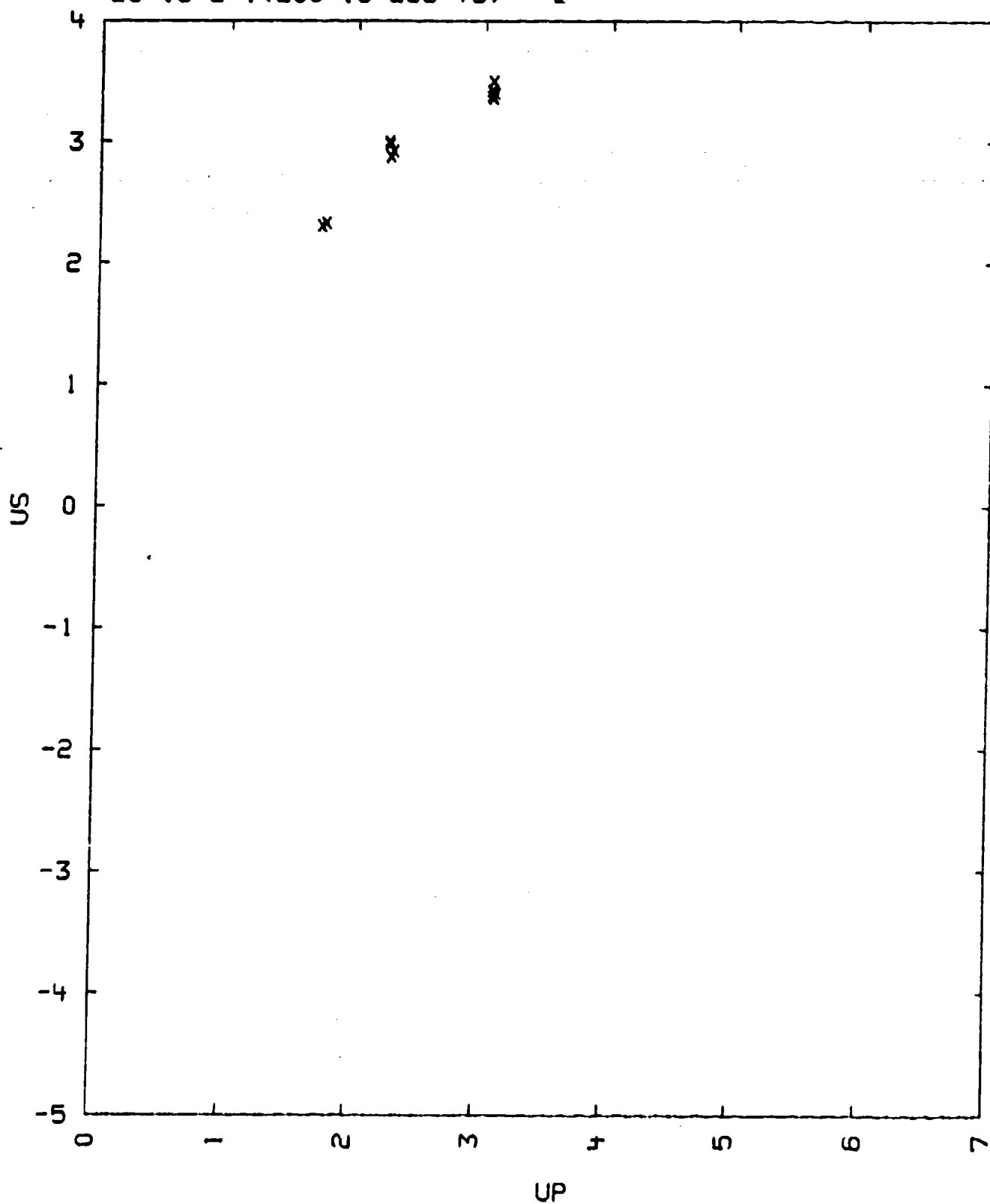


TABLE VI

POLYURETHANE

23-18-2-1 (200-16-286-79) ---2



23-18-10-2-1(200-8-3-349-46)---1  
ADIPRENE RUBBER L-100

(C140-N6-CL2-H245-032)N

$V_0 = .917 - .912 \text{ CC/G}$

$C_0 = .75 - .91 \text{ KM/SEC.}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC.,  
AND PRESSURE IN KILOBARS.

TABLE

| - - - - - SAMPLE - - - - - |      |      |      |       | - - STANDARD - - |        |
|----------------------------|------|------|------|-------|------------------|--------|
| RH00                       | US   | UP   | P    | V/V0  | MATERIAL         | US(ST) |
| 1.096                      | 4.56 | 1.42 | 71.  | .6886 | 2024 AL          | 6.56   |
| 1.095                      | 4.99 | 1.74 | 95.  | .6513 | 2024 AL          | 6.86   |
| 1.091                      | 6.24 | 2.61 | 178. | .5817 | 2024 AL          | 7.71   |
| 1.094                      | 7.93 | 3.61 | 313. | .5448 | 2024 AL          | 8.75   |

$US = 2.279 + 1.542 \cdot UP \text{ KM/SEC}$

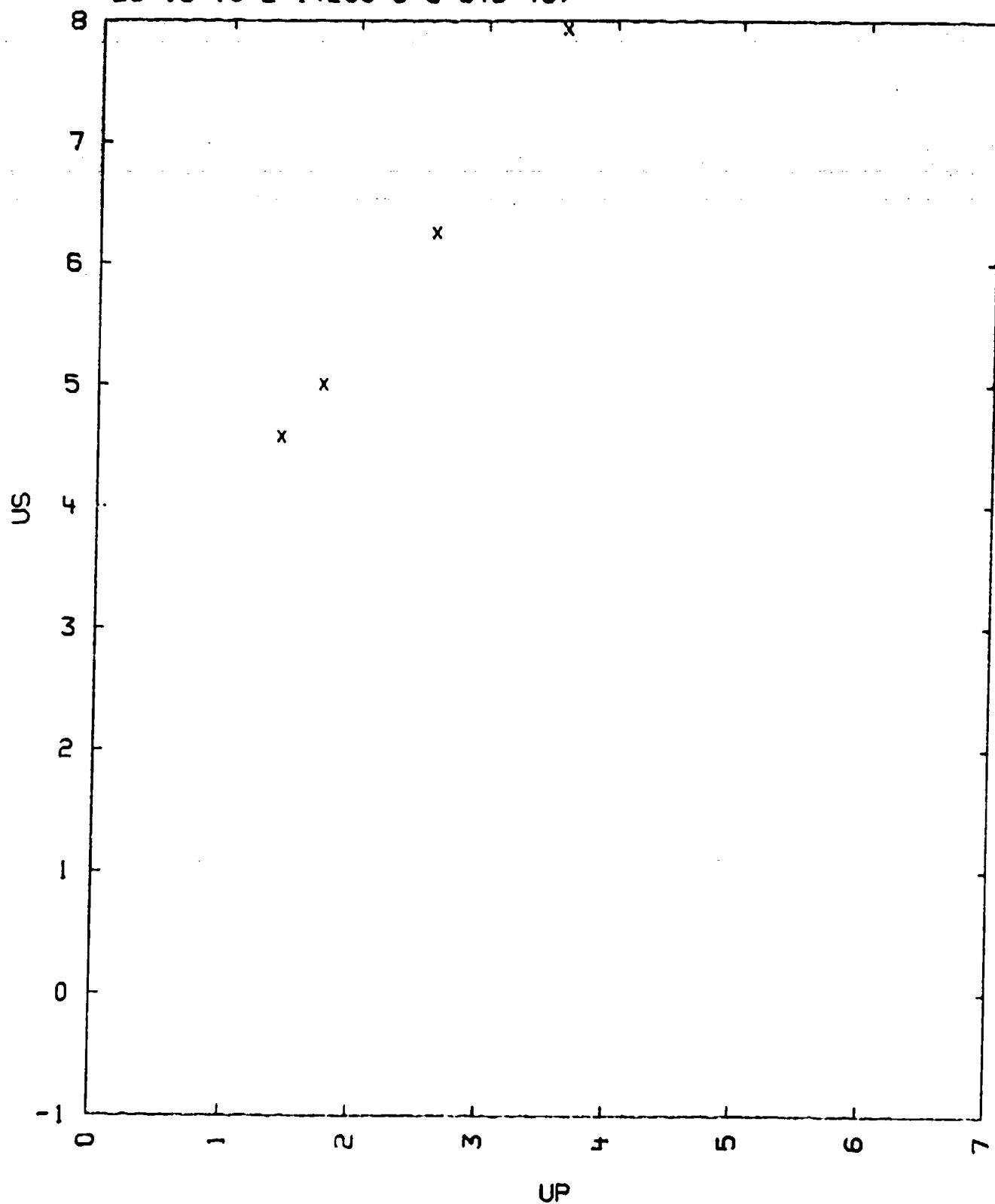
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B (STANDARD BASE PLATE AS SHOWN)
- 3) ADIPRENE L-100 IS A CONDENSATION PRODUCT OF 2,4-TOLYLENEDIISO-  
CYANATE AND 1,4-BUTYLENEOXIDE POLYGLOL (WITH 27-28 BUTYLENE GROUPS  
IN THE POLYMER). THIS LIQUID IS HARDENED WITH ABOUT 11 PERCENT BY  
WEIGHT OF 4,4-DIAMINO-3,3-DICHLORODIPHENYLMETHANE.

TABLE 1

ADIPRENE RUBBER L-100

23-18-10-2-1(200-8-3-349-46)--



EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 13:16:19U 06/14

172 FRAMES PLOTTED



SECTION D

-----

MIXTURES

10-9--29---1

## CHLORINETRIFLUORIDE-ALUMINUM MIXTURE

CL-F3 72.3 WT. PERCENT  
 AL 27.7 - -

T0 = 0.0 +OR-0.7 DEG. C.

V0 = 0.4850 +OR-5 CC/G.

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR.

TABLE

| RHOD  | SAMPLE |      | P    | V/V0  | - STANDARD - |       |
|-------|--------|------|------|-------|--------------|-------|
|       | US     | UP   |      |       | UP(ST)       | P(ST) |
| 2.081 | 3.55   | 1.12 | 82.  | 0.685 | 0.80         | 144.  |
| -     | 4.32   | 1.53 | 136. | 0.647 | 1.14         | 220.  |
| -     | 5.20   | 2.07 | 222. | 0.603 | 1.61         | 336.  |
| -     | 6.44   | 2.95 | 392. | 0.59  | 2.37         | 565.  |

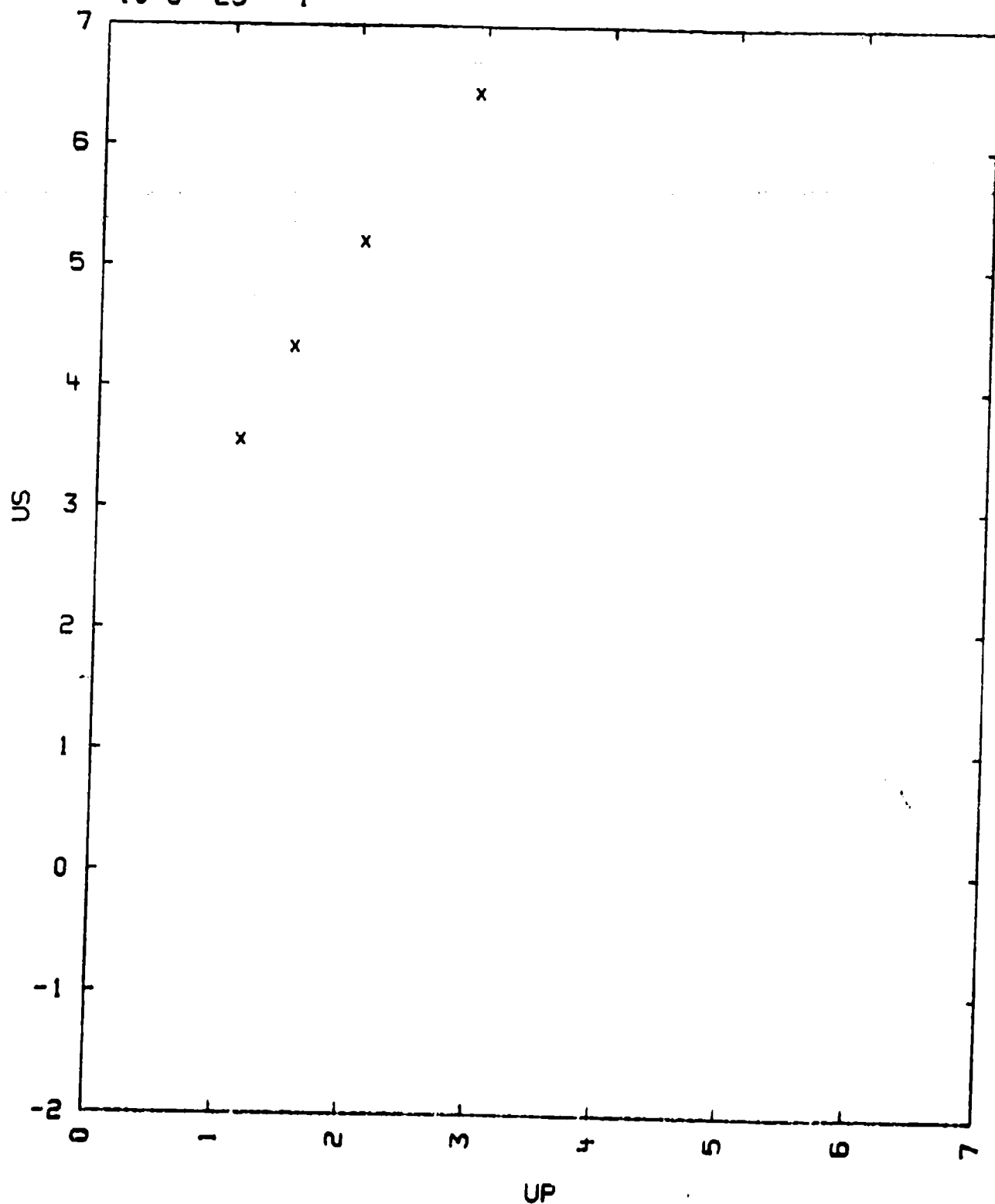
$$US = 1.17 + 2.33 \cdot UP - 0.186 \cdot UP^2 \text{ KM/SEC}$$

$$SIG.US = 0.014 \text{ KM/SEC.}$$

## COMMENTS:

- 1) SOURCE: JEFFRIES, R. A. AND WACKERLE J.  
 LOS ALAMOS REPORT: LA-3453 (1966)  
 LOS ALAMOS SCIENTIFIC LAB., BOX 1663, LOS ALAMOS, N. M. 87544
- 2) EXPERIMENTAL TECHNIQUE: B  
 DATA REDUCTION TECHNIQUE: B (STANDARD MATERIAL: 2024 AL. ALLOY)
- 3) ERROR ESTIMATES FOR US ARE: .02 .02 .02 .13 KM/SEC.  
 ERROR ESTIMATES FOR UP ARE: .02 .01 .02 .06 KM/SEC.  
 IN THE ORDER OF THE TABLE LISTING.

TABLE 1  
CHLORINETRIFLUORIDE-ALUMINUM MIXTURE  
10-9--29---1



18-10-2-1--29--23-18-2-1(3-3-5-9)--23-18-2-1(6-2-8-9)---1  
 NITROSOL PROPELLANT, CAST

## NITROCELLULOSE

(O-C5(CH2-O-H)(H)5(NO3)2-O) = (C6-N2-H8-O9)3000 10.1 WT PERCENT

## PLASTICIZER

## NITROGLYCERENE

((H2-C(N-O3))2-C(H)-NO3) 20.1 - - -

## GLYCEROLTRIACETATE

((H2-C(O-C-H3))-C(H)-O-C(O)-C-H3) 6.4 - - -

## 2-NITRODEPHENYLAMINE

(C6(H5)-N(H)-C6(H4)-N-O3) 0.3 - - -

## ALUMINUM

27.6 - - -

AMMONIUM PERCHLORATE (NH4)(CL-O4) = N-CL-H4-O4

35.5 - - -

$V_0 = 0.533 \text{ CC/G}$

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND  
 PRESSURE IN KILOBARS.

TABLE

| RH00  | US   | UP   | P     | V/V0  |
|-------|------|------|-------|-------|
| 1.877 | 2.92 | 0.43 | 23.6  | 0.853 |
| -     | 3.04 | 0.42 | 23.7  | 0.862 |
| -     | 3.22 | 0.54 | 32.6  | 0.832 |
| -     | 3.35 | 0.53 | 33.3  | 0.842 |
| -     | 3.75 | 0.73 | 51.4  | 0.805 |
| -     | 3.73 | 0.73 | 51.1  | 0.804 |
| -     | 3.92 | 0.88 | 64.7  | 0.776 |
| -     | 3.87 | 0.88 | 63.9  | 0.773 |
| -     | 4.62 | 1.03 | 89.3  | 0.777 |
| -     | 4.22 | 1.08 | 85.5  | 0.744 |
| -     | 4.41 | 1.32 | 109.3 | 0.701 |
| -     | 4.53 | 1.14 | 96.9  | 0.748 |
| -     | 4.49 | 1.15 | 96.9  | 0.744 |
| -     | 4.99 | 1.11 | 103.9 | 0.778 |
| -     | 3.94 | 0.82 | 60.6  | 0.792 |
| -     | 4.12 | 0.81 | 62.6  | 0.803 |
| -     | 3.79 | 0.83 | 59.0  | 0.781 |
| -     | 4.43 | 0.79 | 65.7  | 0.822 |

$US = 1.97 + 2.29 \cdot UP \text{ KM/SEC}$

$SIGMA US = 0.24 \text{ KM/SEC}$

## COMMENTS:

1) SOURCE: BOYLE, V. M.

PRIVATE COMMUNICATION

BALLISTIC RESEARCH LABORATORIES, AMXBR-TD

ABERDEEN PROVING GROUND, MARYLAND 21005.

2) EXPERIMENTAL TECHNIQUE: THE SHOCK VELOCITY IN THE SAMPLE WAS MEASURED  
 BY A SHEAR CAMERA THAT SWEEPED THE SHADOWGRAPH OF A TRANSPARENT

CHANNEL IN THE SAMPLE ACROSS THE FILM PLANE. THE CHANNEL WAS MADE BY SPLITTING THE SAMPLE IN TWO ALONG THE SHOCK DIRECTION AND SEPARATING THE TWO HALVES BY A THIN (0.127 MM) TRANSPARENT PLASTIC SHEET (EXTRUDED ACETATE).

DATA REDUCTION TECHNIQUE: B

STANDARD MATERIALS USED:

ALUMINUM, 2024-T4,  $U_S = 5.360 + 1.351 \cdot U_P$  KM/SEC

$RHO = 2.783$  G/CC

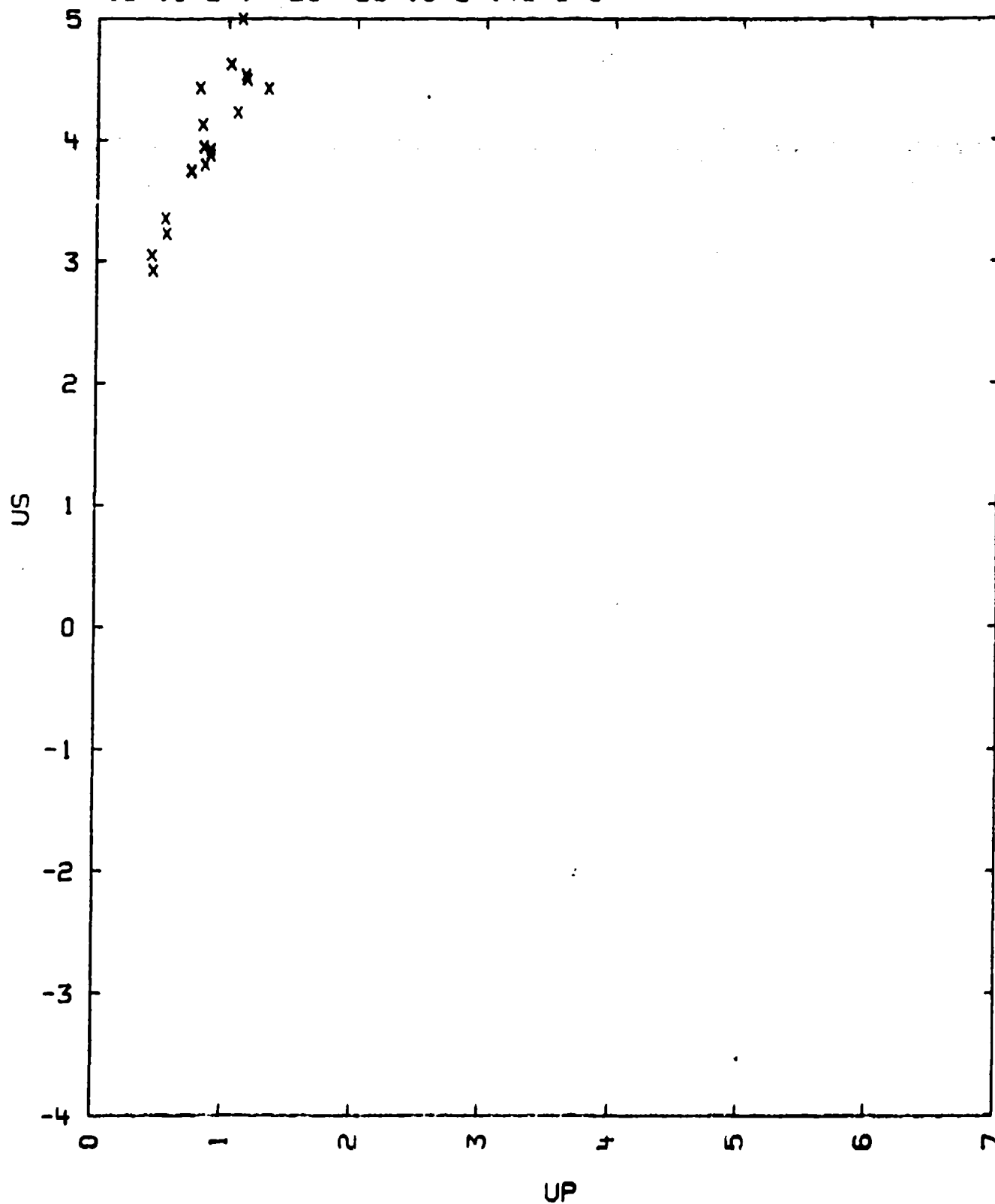
PLEXIGLASS,  $U_S = 2.702 + 1.544 \cdot U_P$  KM/SEC,  $RHO = 1.184$  G/CC

$U_P = 1/2 U_S$  WAS ASSUMED FOR THE STANDARD MATERIALS SO THAT THE PRESSURE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS.  $U_P$  HOGONIOT IN THE LINE  $U_P = 1/2 U_S$ .

- 3) THE DEGREE TO WHICH THE RESULTS MAY BE AFFECTED BY CHEMICAL REACTION OF THE SHOCKED EXPLOSIVE SAMPLE HAS NOT BEEN DETERMINED AT THIS TIME.

TABLE I

NITROSOL PROPELLANT, CAST  
18-10-2-1--29--23-18-2-1(3-3-5



23-2-1(7-6-2)--23-2-1(8-10-5)---

NICARTA

PHENOLIC (C7-H6-02-)N  
 CELLULOSE (C6-H10-05)N  
 IMPURITIES NOTE 3

VO = 0.717 CC/G CL = 2.67 KM/SEC CO = 2.03 KM/SEC  
 CS = 1.50 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
 AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |       |
|------------------|------|------|------|--------|--------------------|-------|
| RH00             | US   | UP   | P    | V/VO   | MATERIAL US(ST)    |       |
| 1.394            | 4.73 | 1.22 | 80.  | 0.7421 | 2024 AL            | 6.47  |
| 1.394            | 4.72 | 1.23 | 81.  | 0.7394 | 2024 AL            | 6.47  |
| 1.394            | 4.90 | 1.28 | 87.  | 0.7388 | 2024 AL            | 6.53  |
| 1.394            | 5.20 | 1.55 | 112. | 0.7019 | 2024 AL            | 6.80  |
| 1.394            | 6.15 | 2.08 | 178. | 0.6618 | 2024 AL            | 7.37  |
| 1.394            | 6.18 | 2.18 | 188. | 0.6472 | 2024 AL            | 7.46  |
| 1.394            | 7.15 | 2.92 | 291. | 0.5916 | 2024 AL            | 8.24  |
| 1.394            | 8.51 | 3.75 | 445. | 0.5593 | 2024 AL            | 9.16  |
| 1.394            | 9.84 | 4.85 | 665. | 0.5071 | 2024 AL            | 10.35 |

US = 3.048 + 1.422\*UP KM/SEC  
 SIGMA US = 0.096 KM/SEC

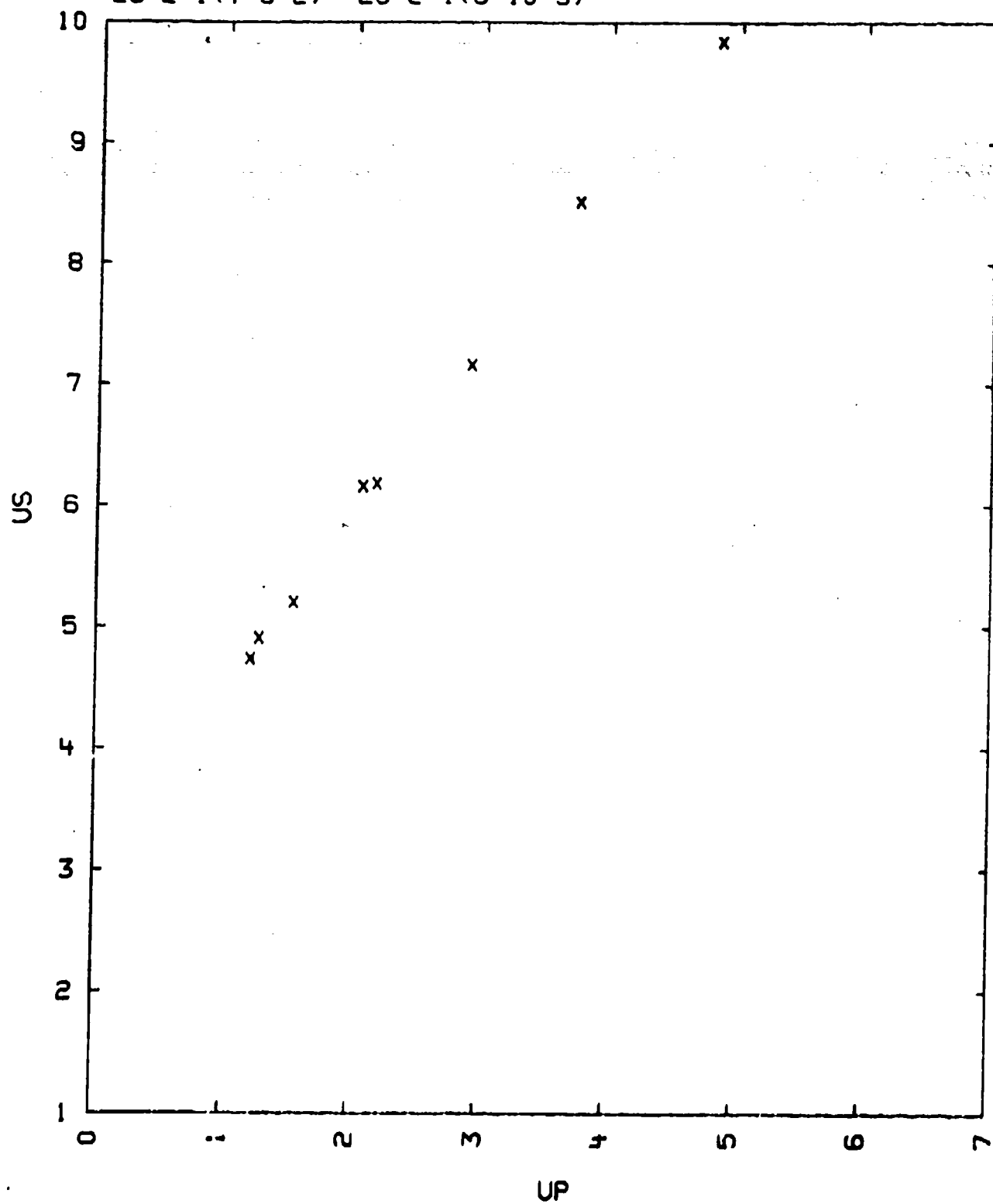
## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
 AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES.  
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
 DATA REDUCTION TECHNIQUE: B
- 3) THE SAMPLE IS A PULP FILLED FORMALDEHYDE PHENOLIC. THE PULP IS  
 NORMALLY ABOUT 90 PERCENT CELLULOSE. THE EXACT QUANTITY OF PULP  
 ADDED IS NOT KNOWN.

TABLE I

MICARTA

23-2-1(7-6-2)--23-2-1(6-10-5)-





23-18-2-1(1-1-3-3)--23-2-1(3-6-1)---1  
 NITROMETHANE-ACETONE MIXTURE

NITROMETHANE C-H3-N-O3 75 WT PERCENT  
 ACETONE C3-H6-O 25 WT PERCENT

$V_0 = 0.952 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC. AND PRESSURE IN KILOBARS. (ST) DENOTES STANDARD MATERIAL.

TABLE

| -----SAMPLE----- |      |      |      |       | -ST- |
|------------------|------|------|------|-------|------|
| RH00             | US   | UP   | P    | V/V0  | UP   |
| 1.050            | 4.78 | 1.62 | 81.3 | 0.661 | 1.07 |
| 1.050            | 4.09 | 1.23 | 52.8 | 0.699 | 0.79 |
| 1.050            | 3.10 | 0.67 | 21.8 | 0.784 | 0.41 |

$US = 1.91 + 1.77 \cdot UP \text{ KM/SEC}$      $SIGMA \text{ US} = 2.5 \text{ PERCENT}$

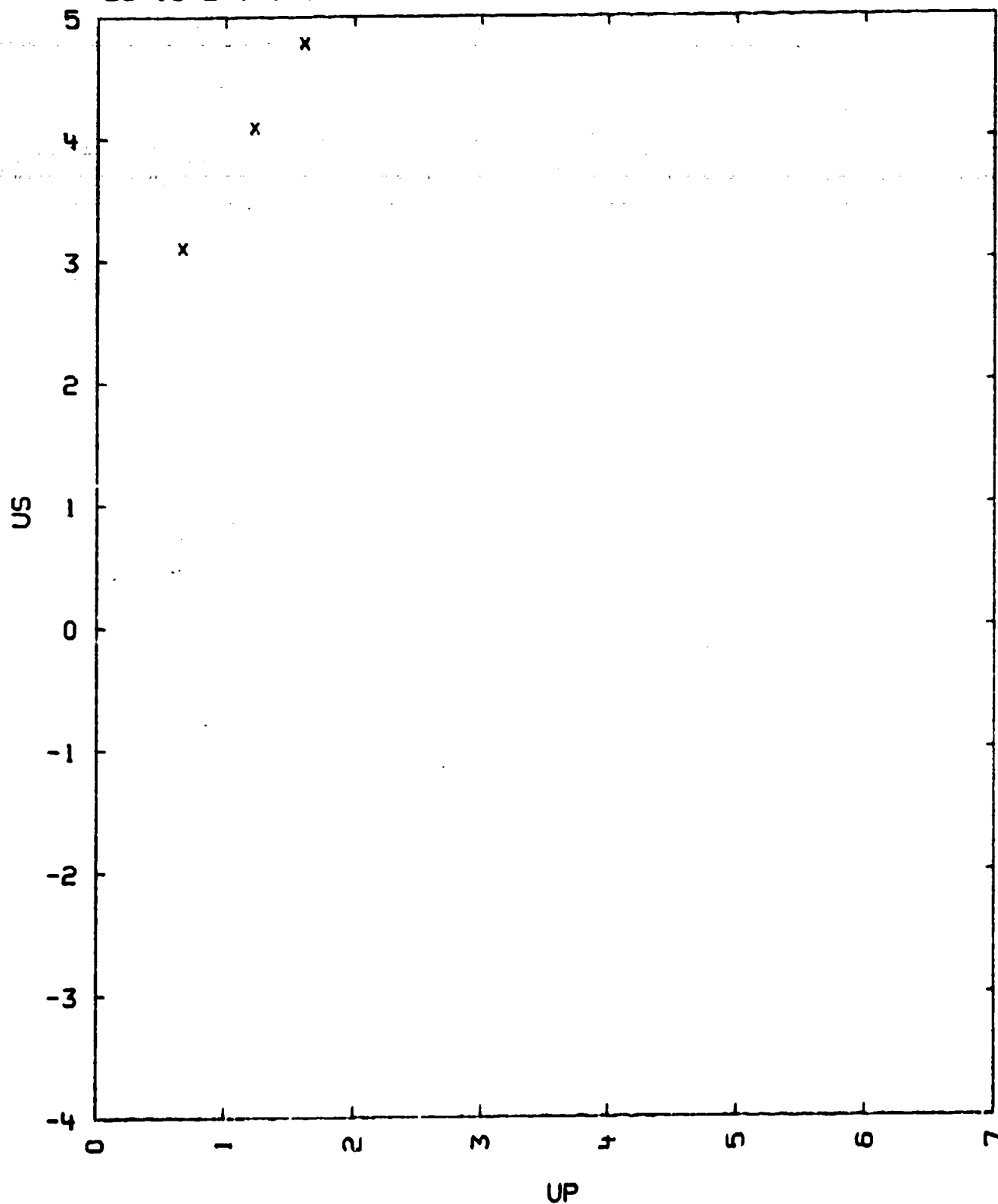
## COMMENTS:

- 1) SOURCE: DREMIN, A. N. AND ROZANOV, O. K.  
 IZVESTIYA AKADEMII NAUK SSSR, SERIYA KHIMICHESKAYA, NO. 8,  
 P. 1513 (1964) (RUSS)  
 ACADEMY OF SCIENCES, U.S.S.R. BULL., CHEM. SCI.  
 P. 1417 (1964) (ENGLISH).
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION TECHNIQUE B  
 STANDARD MATERIAL ALUMINUM:  $P = RH00 \cdot (5.25 + 1.39 \cdot UP) \cdot UP$
- 3) THE AVERAGE ERROR OF THE SHOCK VELOCITY MEASUREMENTS IS  
 +OR- 2.5 PERCENT.
- 4) THE MEASURED DETONATION VELOCITY ON 5.75 KM/SEC AND YIELDS A VON  
 NEUMAN SPIKE PRESSURE OF 131 KBARS.
- 5) THE CHAPMAN-JOUQUET PRESSURE OF 89 KILOBARS HAS CALCULATED USING A  
 PARTICLE VELOCITY OF 1.47 KM/SEC. THIS PARTICLE VELOCITY WAS  
 MEASURED USING THE ELECTROMAGNETIC METHOD OF:  
 ZAITSEV, V. M., POKHIL, P. F. AND SHVEDOV, K. K.  
 DOKL. A.N. SSSR, VOL. 132, P. 1339 (1960) (RUSS)  
 ACADEMY OF SCIENCES, U.S.S.R. BULL. CHEM. SEC., VOL. 132,  
 P. 529 (1960) (ENGLISH).

TABLE 1

NITROMETHANE-ACETONE MIXTURE

23-18-2-1(1-1-3-3)--23-2-1(3-6)



23-18-2-1(1-1-3-31)-23-2-1(3-5-1)---2  
 NITROMETHANE-ACETONE MIXTURE

NITROMETHANE C-H3-N-O3 84 WT PERCENT  
 ACETONE C3-H6-O 16 WT PERCENT

$V_0 = 0.925 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND PRESSURE IN KILOBARS. (ST) DENOTES STANDARD MATERIAL.

TABLE

| -----SAMPLE----- |      |      |      |       | -ST- |
|------------------|------|------|------|-------|------|
| RHOD             | US   | UP   | P    | V/V0  | UP   |
| 1.081            | 4.64 | 1.63 | 81.8 | 0.649 | 1.07 |
| 1.081            | 4.03 | 1.24 | 54.0 | 0.692 | 0.79 |
| 1.081            | 3.30 | 0.84 | 30.  | 0.746 | 0.45 |

$US = 1.89 + 1.70 \cdot UP \text{ KM/SEC}$      $SIGMA \text{ US} = 2.5 \text{ PERCENT}$

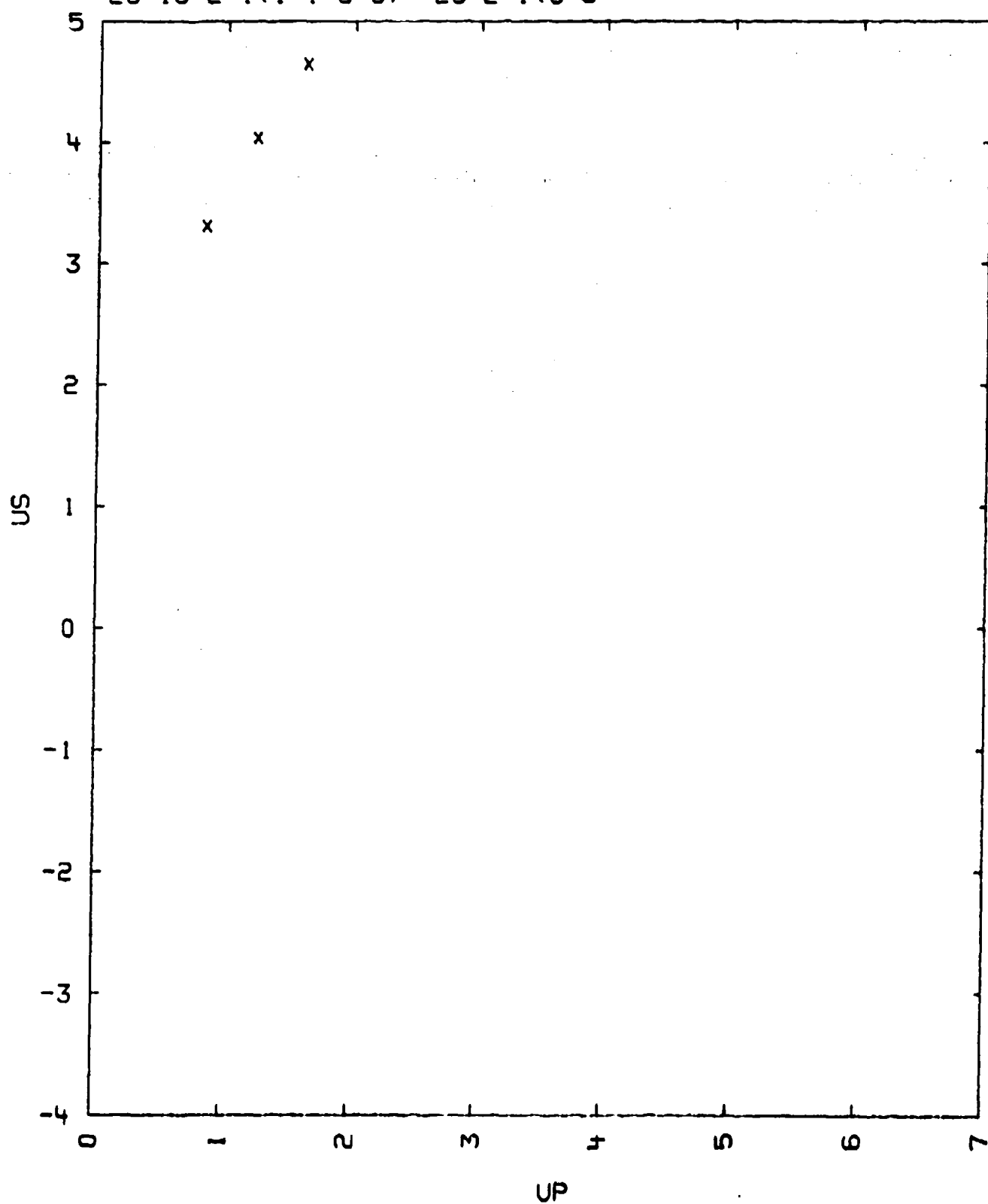
## COMMENTS:

- 1) SOURCE: DREMIN, A. N. AND ROZANOV, O. K.  
 (ZVESTIYA AKADEMII NAUK SSSR, SERIYA KHIMICHESKAYA, NO. 8,  
 ACADEMY OF SCIENCES, U.S.S.R. BULL., CHEM. SCI.  
 P. 1417 (1964) (ENGLISH)  
 P. 1513 (1964) (RUSS)
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION TECHNIQUE B  
 STANDARD MATERIAL ALUMINUM:  $P = RHOD \cdot (5.25 + 1.39 \cdot UP) \cdot UP$ .
- 3) THE AVERAGE ERROR OF THE SHOCK VELOCITY MEASUREMENTS IS  
 +OR- 2.5 PERCENT.
- 4) THE MEASURED DETONATION VELOCITY ON 6.00 KM/SEC YIELDS A VON  
 NEUMAN SPIKE PRESSURE OF 158 KBARS.
- 5) THE CHAPMAN-JOUQUET PRESSURE OF 109 KILOBARS WAS CALCULATED USING A  
 PARTICLE VELOCITY OF 1.68 KM/SEC. THIS PARTICLE VELOCITY WAS  
 MEASURED USING THE ELECTROMAGNETIC METHOD OF:  
 ZAITSEV, V. M., POKHIL, P. F. AND SHVEDOV, V. K.  
 DOKL. A.N. SSSR, VOL. 132, P. 1339 (1960) (RUSS)  
 ACADEMY OF SCIENCES, U.S.S.R. BULL. CHEM. SEC., VOL. 132,  
 P. 529 (1960) (ENGLISH)

TABLE I

NITROMETHANE-ACETONE MIXTURE

23-18-2-1(1-1-3-3)--23-2-1(3-6)



23-18-2-1(3-6-6-6)--23-18-2-1(7-3-5-6)---1  
COMP. B-3 (EXPLOSIVE)

## CYCLOTRIMETHYLENETRINITRAMINE

 $(\text{H}_2)\text{C}-\text{N}(\text{N}-\text{O}_2)-\text{N}_3 = \text{C}_3-\text{N}_6-\text{H}_6-\text{O}_6$ 

60 WT PERCENT

## TRINITROTOLUENE

 $(\text{N}-\text{O}_2)_3-\text{C}_6(\text{H}_2)-\text{C}-\text{H}_3 = \text{C}_7-\text{N}_3-\text{H}_5-\text{O}_6$ 

40 WT PERCENT

 $V_0 = 0.5952 \text{ CC/G}$ 
 $C_0 = 2.736 \text{ KM/SEC}$ 
 $V_{01} = 0.5576 \text{ CC/G}$ 

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND  
PRESSURE IN KILOBARS. BR DENOTES THE BRASS SAMPLE HOLDER.

TABLE

| - - - - - SAMPLE - - - - - |       |       |      |        |       | HOLDER |       |
|----------------------------|-------|-------|------|--------|-------|--------|-------|
| RH00                       | US    | UP    | P    | V/V0   | SHAPE | MATRL  | UP    |
| 1.680                      | 3.387 | 0.380 | 21.6 | 0.8878 | DISK  | BR     | 0.226 |
| -                          | 3.437 | 0.421 | 24.3 | 0.8775 | DISK  | BR     | 0.251 |
| -                          | 3.510 | 0.466 | 27.4 | 0.8672 | DISK  | BR     | 0.278 |
| -                          | 3.628 | 0.462 | 28.1 | 0.8726 | DISK  | BR     | 0.278 |
| -                          | 3.713 | 0.460 | 28.6 | 0.8761 | DISK  | BR     | 0.278 |
| -                          | 3.439 | 0.469 | 27.0 | 0.8636 | WEDGE | BR     | 0.279 |
| -                          | 3.971 | 0.741 | 49.4 | 0.8133 | DISK  | BR     | 0.449 |
| -                          | 4.243 | 0.819 | 55.3 | 0.8069 | DISK  | BR     | 0.501 |
| -                          | 4.377 | 0.884 | 65.0 | 0.7980 | DISK  | BR     | 0.543 |
| -                          | 4.314 | 0.886 | 64.2 | 0.7946 | DISK  | BR     | 0.543 |
| -                          | 4.469 | 0.881 | 66.1 | 0.8028 | DISK  | BR     | 0.543 |
| -                          | 4.346 | 0.869 | 63.4 | 0.8000 | DISK  | BR     | 0.534 |
| -                          | 4.441 | 0.936 | 69.8 | 0.7892 | WEDGE | BR     | 0.576 |

 $US = 2.71 + 1.86 \cdot UP \text{ KM/SEC}$ 
 $SIG US = 0.087 \text{ KM/SEC}$ 

## COMMENTS

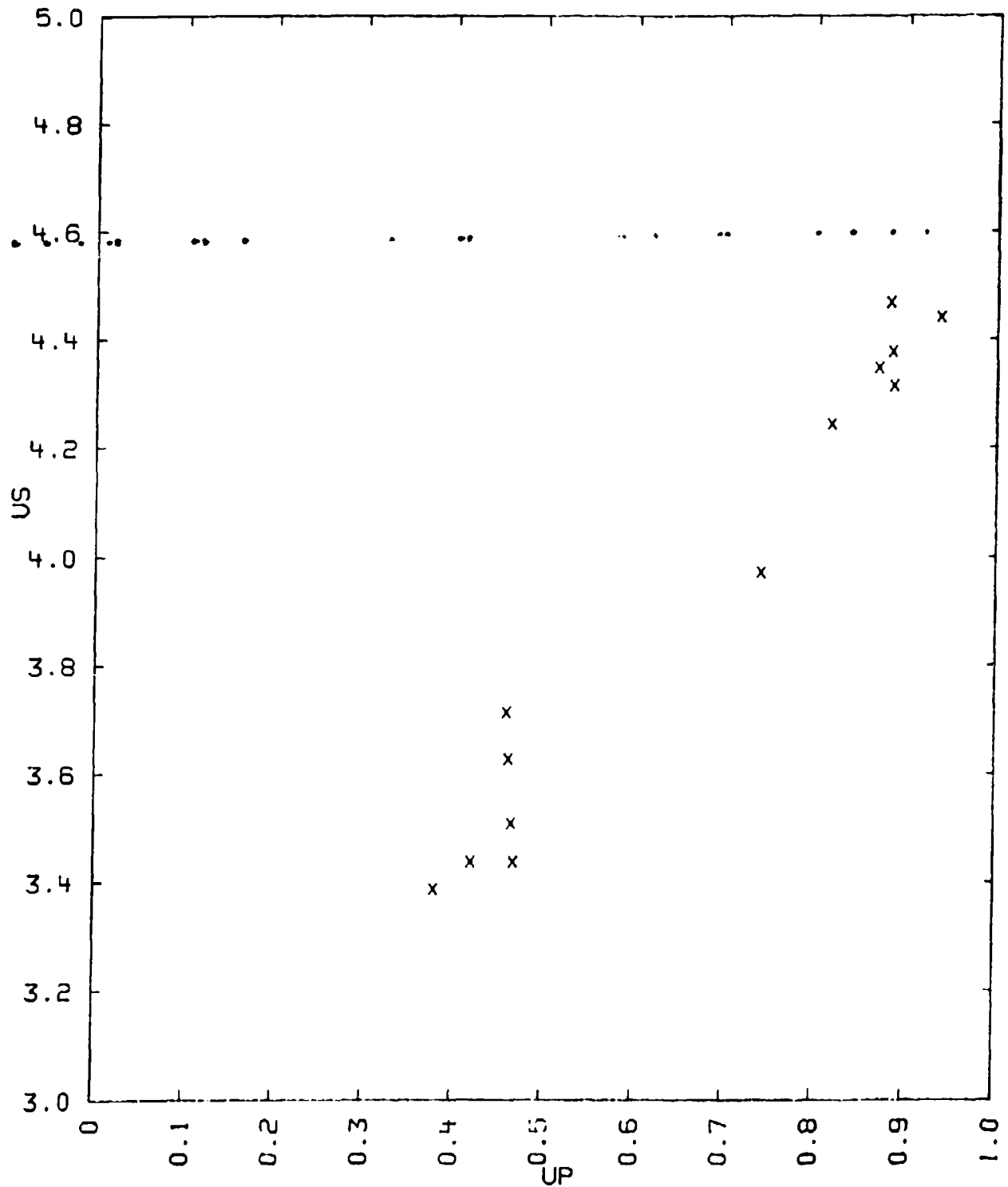
- 1) SOURCE: COLEBURN N. L. AND LIDDIARD JR. T. P.  
J. CHEM. PHYS., VOL.44, P.1929 (1965)  
ALSO: PRIVATE COMMUNICATION.
- 2) EXPERIMENTAL TECHNIQUE C1  
DATA REDUCTION METHOD B  
THE HUGONIOT AND RELEASE ISENTROPES OF THE SAMPLE HOLDER WERE  
TAKEN TO BE MIRROR IMAGES IN THE P VS UP PLANE.  
FOR BRASS  $US = 3.560 + 1.833 \cdot UP \text{ KM/SEC}$  WAS USED WITH  
 $RH00 = 8.37 \text{ G/CC}$ .
- 3) AN ALUMINIZED MYLAR FILM WAS PLACED ON THE SAMPLE WITH A THIN LAYER  
OF SILICONE GREASE TO INCREASE THE REFLECTIVITY.
- 4) THE GRUNEISEN COEFFICIENT  $\gamma = V(DP/DE) = 0.947$ .
- 5) THE VALUE OF  $V_{01}$  WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE  
VOLUMES OF THE COMPONENTS:  $RDX:V_{01} = 0.5494 \text{ CC/G}$   
 $TNT:V_{01} = 0.6046 \text{ CC/G}$

6)  $C_0$  IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN  
UNCERTAINTY OF ABOUT 10 PERCENT.

TABLE I

COMP. B-3 (EXPLOSIVE)

23-18-2-1(3-6-6-6)--23-18-2-1(



23-18-2-113-6-6)---23-18-2-117-3-5-6)---2  
COMPOSITION B, CAST (EXPLOSIVE)

## CYCLOTRIMETHYLENETRINITRAMINE

(-H<sub>2</sub>)C-N(N-O<sub>2</sub>)-)3 = C3-N6-H6-O6

60 WT PERCENT

## TRINITROTOLUENE

-(C-H<sub>3</sub>)C-C(N-O<sub>2</sub>)-(C(H)-C(N-O<sub>2</sub>)-)2 = C7-N3-H5-O6

40 WT PERCENT

## WAX

(C<sub>46</sub>-H<sub>92</sub>-O<sub>2</sub>) UNCERTAIN

1 WT PERCENT

V<sub>0</sub> = 0.588 CC/G

V<sub>01</sub> = 0.5576 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| RH00  | US   | UP   | P     | V/V <sub>0</sub> |
|-------|------|------|-------|------------------|
| 1.700 | 4.22 | 0.81 | 58.1  | 0.808            |
| -     | 3.60 | 0.54 | 33.0  | 0.850            |
| -     | 3.43 | 0.55 | 32.1  | 0.839            |
| -     | 4.98 | 1.31 | 110.9 | 0.737            |
| -     | 4.99 | 1.31 | 111.1 | 0.737            |
| -     | 3.71 | 0.53 | 33.4  | 0.857            |
| -     | 4.14 | 0.82 | 57.7  | 0.802            |
| -     | 4.35 | 1.04 | 76.9  | 0.761            |
| -     | 3.49 | 0.50 | 29.7  | 0.857            |
| -     | 4.09 | 0.82 | 57.0  | 0.799            |
| -     | 5.25 | 1.27 | 113.3 | 0.758            |
| -     | 3.89 | 0.84 | 55.5  | 0.784            |
| -     | 5.22 | 1.25 | 110.9 | 0.761            |
| -     | 4.67 | 1.17 | 92.9  | 0.749            |
| -     | 4.78 | 1.16 | 94.3  | 0.757            |
| -     | 4.77 | 1.16 | 94.1  | 0.757            |
| -     | 4.88 | 1.15 | 95.4  | 0.764            |
| -     | 4.26 | 0.82 | 59.4  | 0.808            |
| -     | 4.07 | 0.83 | 57.4  | 0.796            |
| -     | 4.23 | 0.82 | 58.9  | 0.806            |
| -     | 4.07 | 0.83 | 57.4  | 0.796            |

US = 2.49 + 1.99•UP KM/SEC

SIGMA US = 0.14 KM/SEC

## COMMENTS:

1) SOURCE: BOYLE, V. M. AND ERVIN, L. H.

BRL MEMO. REPORT NO. 1814, JANUARY 1967

BALLISTIC RESEARCH LABORATORIES, AMXBR-TD

ABERDEEN PROVING GROUND, MARYLAND 21005.

2) EXPERIMENTAL TECHNIQUE: THE SHOCK VELOCITY IN THE SAMPLE WAS MEASURED

U06/15/77



BY A SMEAR CAMERA THAT SWEEPED THE SHADOWGRAPH OF A TRANSPARENT CHANNEL IN THE SAMPLE ACROSS THE FILM PLANE. THE CHANNEL WAS MADE BY SPLITTING THE SAMPLE IN TWO ALONG THE SHOCK DIRECTION AND SEPARATING THE TWO HALVES BY A THIN (0.127 MM) TRANSPARENT PLASTIC SHEET (EXTRUDED ACETATE).

DATA REDUCTION TECHNIQUE: B

STANDARD MATERIALS USED:

ALUMINUM, 2024-T4,  $US = 5.360 + 1.351 \cdot UP$  KM/SEC

$RHO = 2.785$  G/CC

PLEXIGLASS,  $US = 2.702 + 1.544 \cdot UP$ , KM/SEC,  $RHO = 1.184$  G/CC

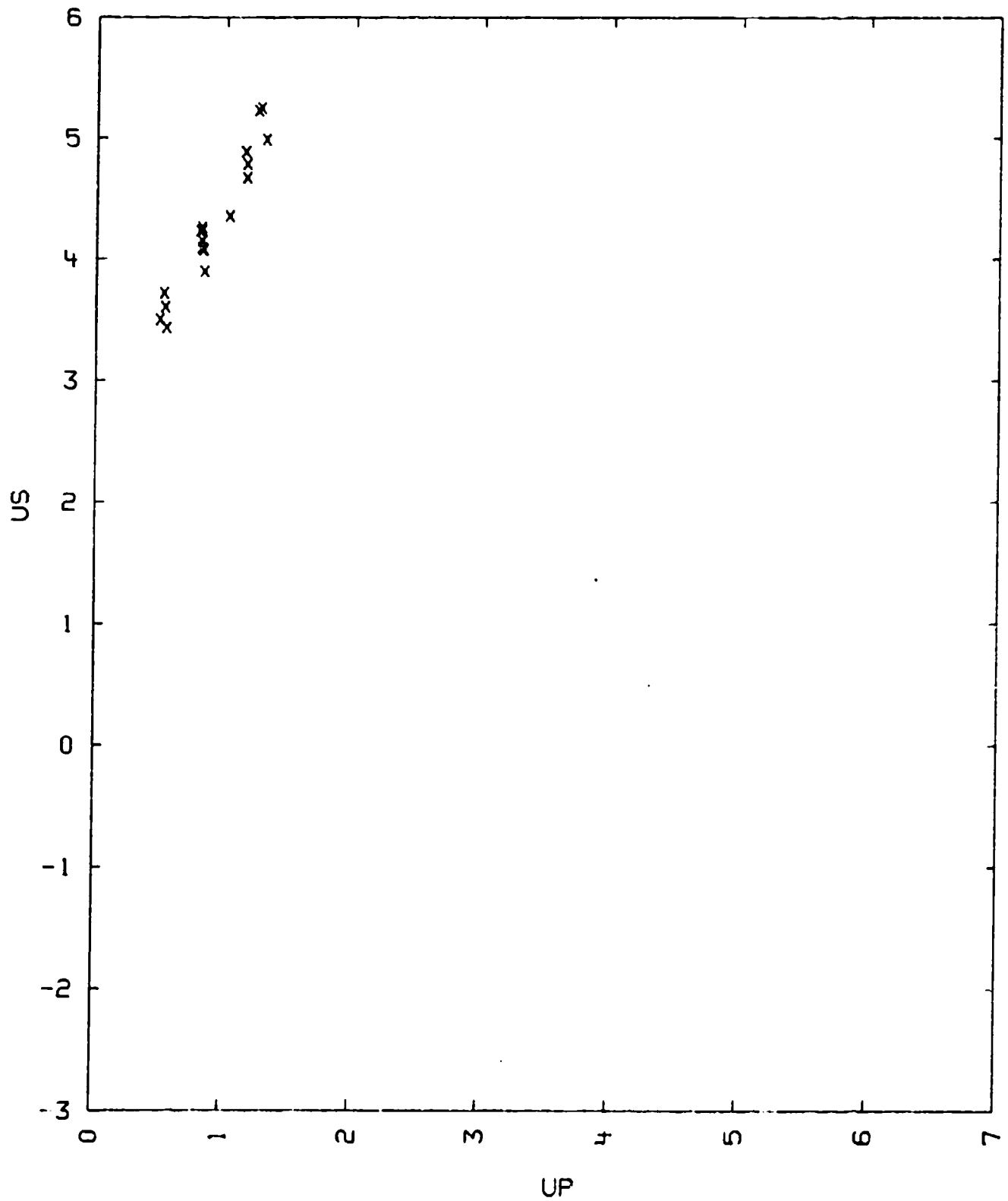
$UP = 1/2$  UFS WAS ASSUMED FOR THE STANDARD MATERIALS SO THAT THE PRESSURE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS. UP HUGONIOT IN THE LINE  $UP = 1/2$  UFS.

- 3) THE DEGREE TO WHICH THE RESULTS MAY BE AFFECTED BY CHEMICAL REACTION OF THE SHOCKED EXPLOSIVE SAMPLE HAS NOT BEEN DETERMINED AT THIS TIME.
- 4) THE VALUE OF VOI WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE VOLUMES OF THE COMPONENTS: RDX VOI = 0.5494 CC/G AND FOR TNT VOI = 0.6046 CC/G.
- 5) THESE DATA ARE FELT TO BE MORE ACCURATE THAN PREVIOUSLY REPORTED DATA REPRESENTED BY  $US = 2.88 + 1.60 \cdot UP$  KM/SEC BY BOYLE, V.M., JAMESON, R.L., AND ALLISON, F.E. BRL REPORT NO. 1250, (1964). THE PRESENT DATA REPLACE THE OLDER DATA..

TABLE 1

COMPOSITION B, CAST (EXPLOSIVE)

23-18-2-1(3-6-6-6)--23-18-2-1(



23-18-2-1(3-6-6-6)---23-18-2-1(7-3-5-6)---3  
 COMP. B-3 (EXPLOSIVE)

RDX (CYCLOTRIMETHYLENETRINITRAMINE)  
 (-(H2)C-N(N-O2)-)3 = C3-N6-H6-O6 59.5 WT PERCENT  
 TNT (TRINITROTOLUENE)  
 (N-O2)3-C6(H2)-C-H3 = C7-N3-H5-O6 40.5 WT PERCENT

V0 = 0.580 CC/G  
 V01 = 0.558 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND PRESSURE IN KILOBARS. X DENOTES BRASS PLATE THICKNESS IN CM.

TABLE

| RH00  | X     | US   | UP    | P     |        |
|-------|-------|------|-------|-------|--------|
| 1.723 | 1.283 | 5.07 | 1.366 | 119.3 | 0.7306 |
| -     | 2.520 | 4.75 | 1.251 | 102.3 | 0.7367 |
| -     | 3.753 | 4.42 | 1.135 | 86.4  | 0.7433 |

$$US = 1.23 + 2.81 \cdot UP + 0R - 0.05 \text{ KM/SEC}$$

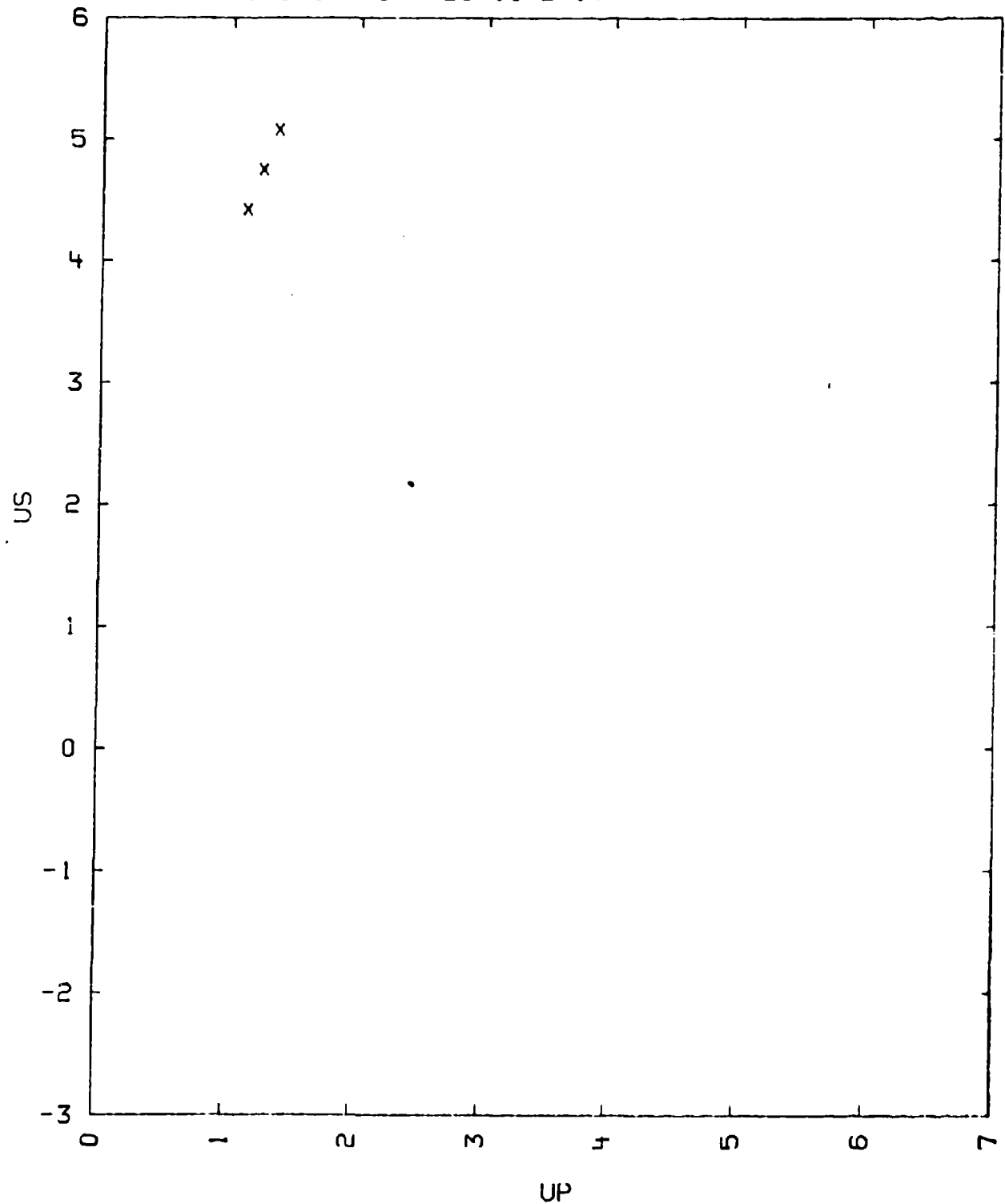
## COMMENTS:

- 1) SOURCE: MAJOWICZ, M. J. AND JACOBS, S. J.  
 NAVORD REPORT NO. 5710, 1958  
 U.S. NAVAL ORDNANCE LAB., WHITE OAK, MARYLAND, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE C  
 DATA REDUCTION TECHNIQUE B. WHERE  $UP = 1/2(UFS)$ . IT WAS ASSUMED THE RELEASE ISENTROPE WAS A STRAIGHT LINE WITH SLOPE  $RH00(US)$ .  
 STANDARD MATERIAL BRASS.
- 3) US IS THE VELOCITY AT ZERO THICKNESS OF THE EXPLOSIVE OBTAINED BY  
 EXTRAPOLATING THE VELOCITY VERSUS THICKNESS CURVE OBTAINED FROM A  
 WEDGE OF EXPLOSIVE.
- 4) THE DETONATION VELOCITY IS 7.99 KM/SEC,  $SIGMA = 0.005 \text{ KM/SEC}$ .  
 THIS VELOCITY WAS REACHED AT THICKNESS BETWEEN 1.7-2.7 MM DEPENDING  
 ON INPUT PRESSURE.
- 5) THE VALUE OF V01 WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE  
 VOLUME OF THE COMPONENTS:  $RDX:V01 = 0.5494$ ,  $TNT:V01 = 0.6046 \text{ CC/G}$ .
- 6) THE UNCERTAINTY OF THE FIT IS ESTIMATED FROM ALL DATA GIVEN BY THE  
 ABOVE REFERENCE.

TABLE I

COMP. B-3 (EXPLOSIVE)

23-18-2-1(3-6-6-6)--23-18-2-1(



23-18-2-1(3-6-6)---23-18-2-1(7-3-5-6)---4  
CYCLOTOL (EXPLOSIVE)

RDX (EXPLOSIVE) 75 WT PERCENT  
(-C(H2)-N(N-O2)-)3 = C3-N6-H6-O6  
TNT (TRINITROTOLUENE)  
(N-O2)3-C6(H2)-C-H3 = C7-N3-H5-O6 25 WT PERCENT

V0 = 0.5783 CC/G  
V01 = 0.5650 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND PRESSURE IN KILOBARS. X DENOTES BRASS STANDARD THICKNESS IN CM.

TABLE

| RH00  | X     | US   | UP    | P     | V/V0  |
|-------|-------|------|-------|-------|-------|
| 1.729 | 1.285 | 5.22 | 1.357 | 122.5 | 0.744 |
| -     | 2.499 | 4.95 | 1.242 | 106.3 | 0.740 |
| -     | 3.762 | 4.67 | 1.124 | 90.8  | 0.759 |

US = 2.02 + 2.36\*UP +OR- 0.05 KM/SEC

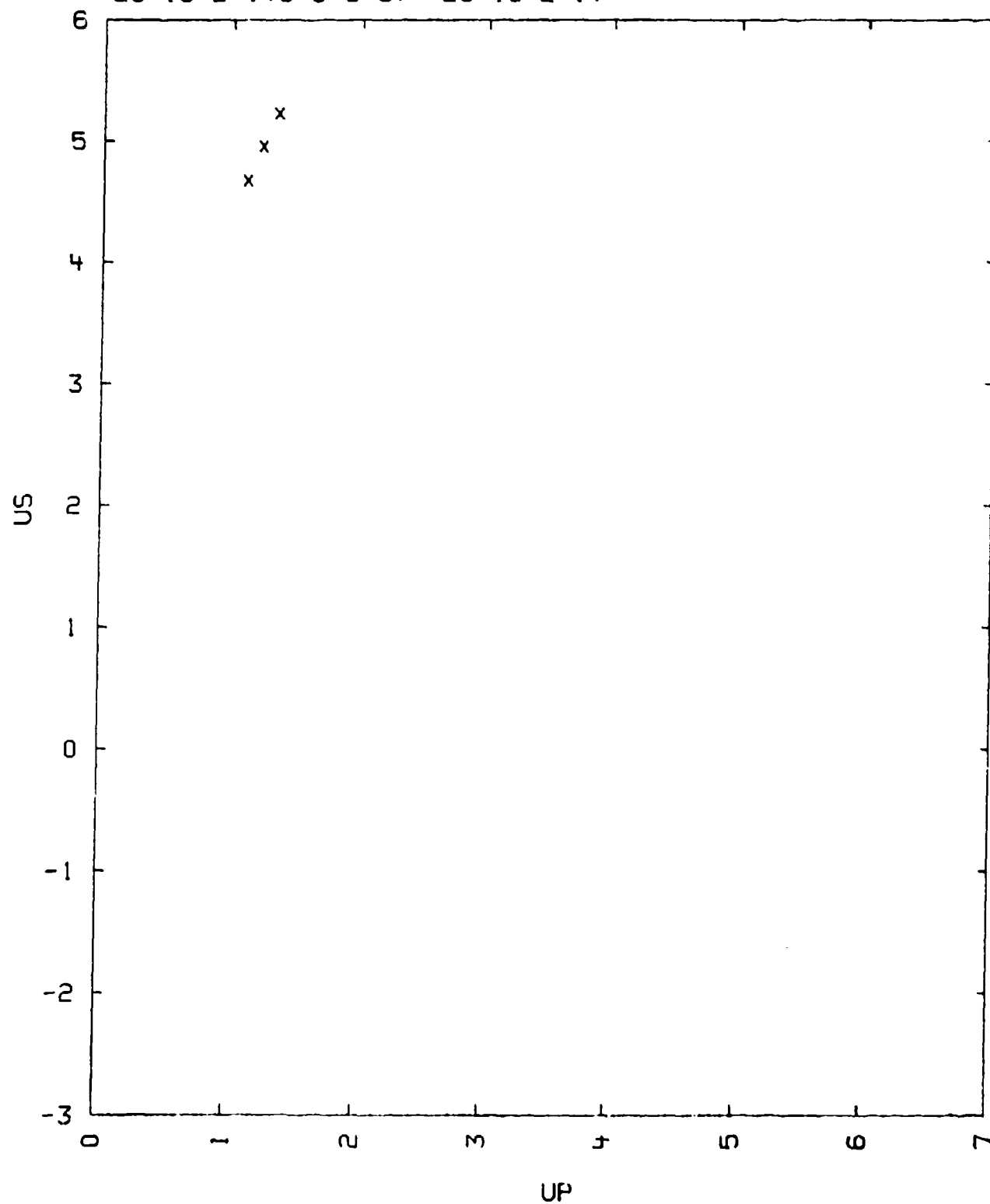
## COMMENTS:

- 1) SOURCE: MAJOWICZ, M. J. AND JACOBS, S. J.  
NAVORD REPORT NO. 5710, 1958  
U.S. NAVAL ORDNANCE LAB., WHITE OAK, MARYLAND, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE C  
DATA REDUCTION TECHNIQUE B. WHERE  $UP = 1/2(UFS)$ , IT WAS ASSUMED THE RELEASE ISENTROPE WAS A STRAIGHT LINE WITH SLOPE  $RH00(US)$ .  
STANDARD MATERIAL BRASS.
- 3) US IS THE VELOCITY AT ZERO THICKNESS OF THE EXPLOSIVE OBTAINED BY EXTRAPOLATING THE VELOCITY VERSUS THICKNESS CURVE OBTAINED FROM A WEDGE OF EXPLOSIVE.
- 4) THE DETONATION VELOCITY IS 8.22 KM/SEC,  $SIGMA = 0.001$  KM/SEC.  
THIS VELOCITY WAS REACHED AT THICKNESS BETWEEN 3.6-6.1 MM DEPENDING ON INPUT PRESSURE.
- 5) THE VALUE OF V01 WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE VOLUMES OF THE COMPONENTS:  $RDX:V01 = 0.5494$ ,  $TNT:V01 = 0.6046$  CC/G.
- 6) THE UNCERTAINTY OF THE FIT IS ESTIMATED FROM ALL DATA GIVEN BY THE ABOVE REFERENCE.

TABLE I

CYCLOTOL (EXPLOSIVE)

23-18-2-1(3-6-6-6)--23-18-2-1(



23-18-2-1(3-6-6)---23-18-2-1(7-3-5-6)---5  
 COMP. B (EXPLOSIVE)

RDX (CYCLOTRIMETHYLENETRINITRAMENE)  
 (-C(H2)-N(N-O2)-)3 = C3-N6-H6-O6 63.0 WT PERCENT  
 TNT (TRINITROTOLUENE)  
 (N-O2)3-C6(H2)-C-H3 = C7-N3H5.O6 36.0 WT PERCENT  
 WAX (C-H2)N 1.0 WT PERCENT

V0 = 0.5847 CC/G  
 V0 = 0.4578 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND  
 PRESSURE IN KILOBARS. X DENOTES BRASS STANDARD THICKNESS IN CM.

TABLE

| RH00  | X     | US   | UP    | P     | V/V0   |
|-------|-------|------|-------|-------|--------|
| 1.710 | 1.282 | 5.06 | 1.368 | 118.4 | 0.7296 |
| -     | 2.434 | 4.71 | 1.257 | 101.3 | 0.7331 |
| -     | 3.753 | 4.41 | 1.137 | 85.6  | 0.7422 |

US = 1.20 + 2.81\*UP +OR- 0.04 KM/SEC

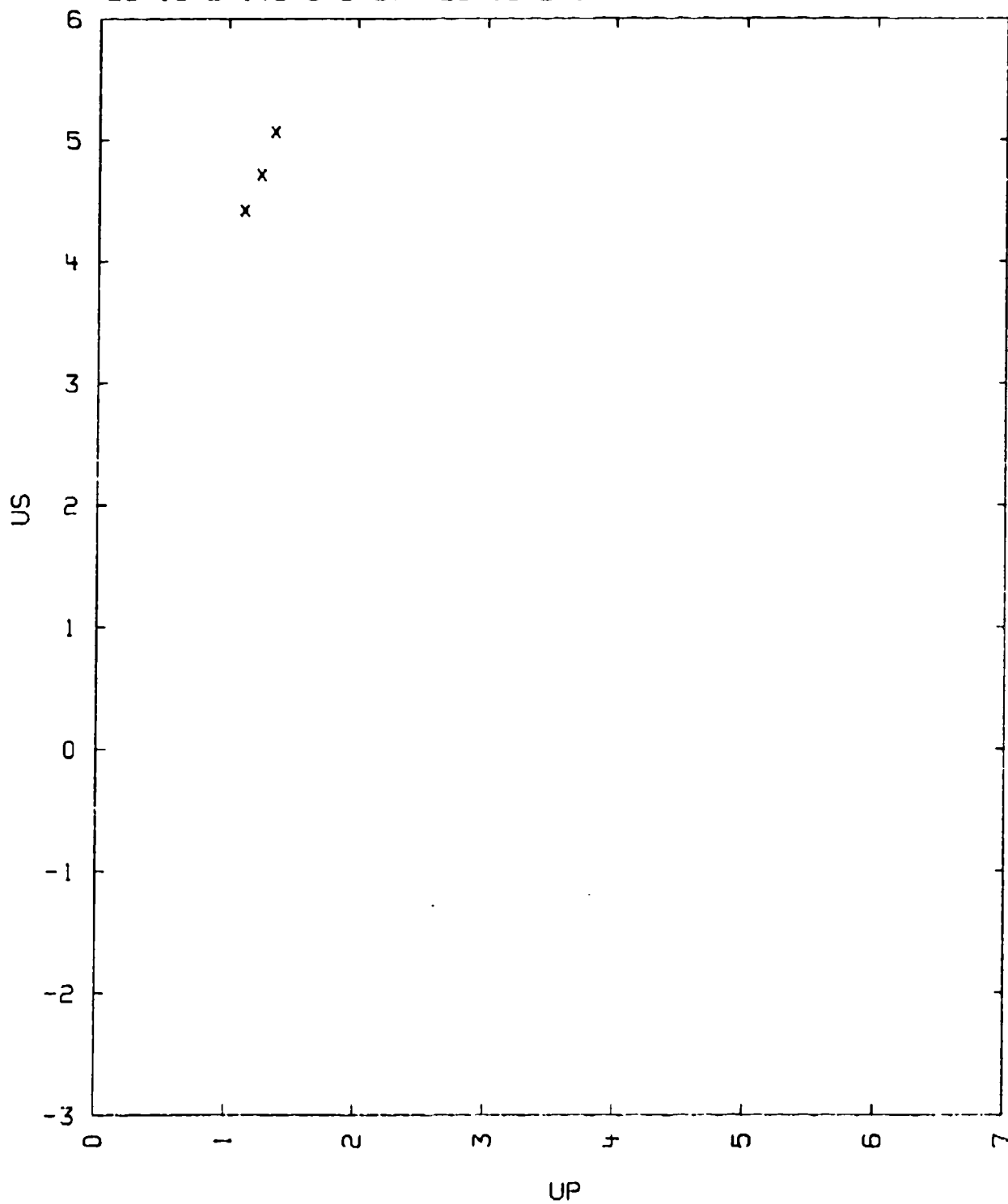
## COMMENTS:

- 1) SOURCE: MAJOWICZ, M. J. AND JACOBS, S. J.  
 NAVORD REPORT NO. 5700, 1958  
 U.S. NAVAL ORDNANCE LAB., WHITE OAK, MARYLAND, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE C  
 DATA REDUCTION TECHNIQUE B. WHERE UP = 1/2(UPS). IT WAS ASSUMED THE  
 RELEASE ISENTROPE WAS A STRAIGHT LINE WITH SLOPE RH00(US).  
 STANDARD MATERIAL BRASS.
- 3) US IS THE VELOCITY AT ZERO THICKNESS OF THE EXPLOSIVE OBTAINED BY  
 EXTRAPOLATING THE VELOCITY VERSUS THICKNESS CURVE OBTAINED FROM A  
 WEDGE OF EXPLOSIVE.
- 4) THE DETONATION VELOCITY IS 7.93 KM/SEC, SIGMA = 0.015 KM/SEC.  
 THIS VELOCITY WAS REACHED AT THICKNESS BETWEEN 2.8-6 MM DEPENDING  
 ON INPUT PRESSURE.
- 5) THE VALUE OF V01 WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE  
 VOLUME OF THE COMPONENTS: RDX:V01 = 0.5494, TNT:V01 = 0.6046 CC/G.

TABLE 1

COMP. B (EXPLOSIVE)

23-18-2-1(3-6-6-6)--23-18-2-1(





23-18-2-1(3-6-6-6)--23-18-2-1(7-3-5-6)--29---1  
 RDX/TNT/ALUMINUM/WAX (HBX-1) (EXPLOSIVE)

|          |                                  |               |               |
|----------|----------------------------------|---------------|---------------|
| RDX      | (-C(H2)-N(N-02)-)3               | = C3-N6-H6-06 | 40 WT PERCENT |
| TNT      | -C(C-H3)-C(N-02)(C(H)-C(N-02)-)2 | = C7-N3-H5-06 | 38 - -        |
| ALUMINUM | AL                               |               | 17 - -        |
| WAX      | (C-H2)N UNCERTAIN                |               | 5 - -         |

V0 = 0.5714 CC/G

C0 = 2.860 KM/SEC

VOI = 0.563 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS

TABLE

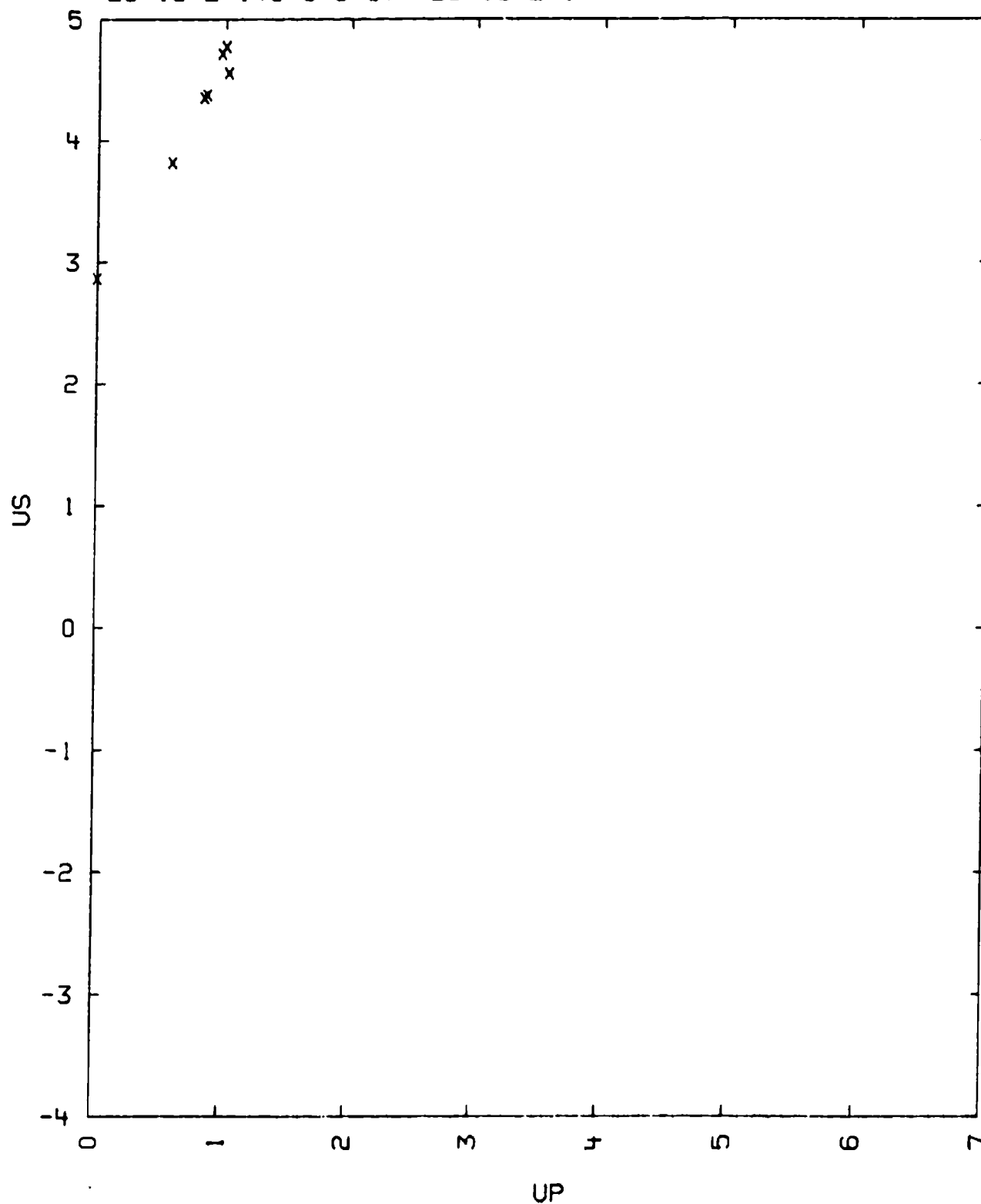
| RH00  | US    | UP    | P    | V/V0  |
|-------|-------|-------|------|-------|
| 1.750 | 2.860 | 0.000 | 0.0  | 1.00  |
| -     | 3.810 | 0.580 | 38.6 | 0.847 |
| -     | 4.347 | 0.835 | 63.5 | 0.807 |
| -     | 4.707 | 0.977 | 80.4 | 0.792 |
| -     | 4.767 | 1.000 | 83.4 | 0.790 |
| -     | 4.550 | 1.020 | 81.2 | 0.775 |
| -     | 4.368 | 0.855 | 65.3 | 0.804 |

US = A + B\*UP    A = 2.936 KM/SEC,    SIGA = 0.078 KM/SEC  
 SIG US = 0.10 KM/SEC    B = 1.651    SIGB = 0.095

COMMENTS:

- 1) SOURCE: COLEBURN N. L. AND LIDDIARD JR. T. P.  
 J. CHEM. PHYS., VOL. 44, P. 1929 (1965)  
 ALSO: PRIVATE COMMUNICATION
- 2) EXPERIMENTAL TECHNIQUE C1  
 DATA REDUCTION METHOD B:  $UP = 1/2 * UP$  WAS ASSUMED FOR THE STANDARD MATERIALS BRASS AND PLEXIGLAS, SO THAT THE PRESSURE RELEASE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS UP HUGONIOT IN THE LINE  $UP = 1/2 * UFS$
- 3) FOR BRASS  $US = 3.560 + 1.833 * UP$  KM/SEC.  
 FOR PLEXIGLAS  $US = 2.710 + 1.568 * UP - 0.037 * UP^2$
- 4) THE GRUNEISEN COEFFICIENT  $\gamma = V(DP/DE) = 2.43$
- 5) THE VALUE OF VOI WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE VOLUMES OF THE COMPONENTS: RDX:VOI = 0.5494 CC/G  
 TNT:VOI = 0.6046 CC/G  
 AL :VOI = 0.3704 CC/G  
 WAX:VOI = 1.01 CC/G
- 6) C0 IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN UNCERTAINTY OF ABOUT 10 PERCENT

TABLE I  
RDX/TNT/ALUMINUM/WAX (HBX-1) (EXPLOSIVE)  
23-18-2-1(3-6-6-6)--23-18-2-1(



23-18-2-1(3-6-6-6)--23-18-2-1(7-3-5-6)--29---2  
 RDX/TNT/ALUMINUM/WAX (HBX-3) (EXPLOSIVE)

|          |                                   |    |            |
|----------|-----------------------------------|----|------------|
| RDX      | (-C(H2)-N(N-O2)-)3                | 31 | WT PERCENT |
| TNT      | -C(C-H3)-C(N-O2)-(C(H)-C(N-O2)-)2 | 29 | -          |
| ALUMINUM | AL                                | 35 | -          |
| WAX      | (C-H2)N UNCERTAIN                 | 5  | -          |

V0 = 0.5405 CC/G  
 V01 = 0.526 CC/G

C0 = 3.095 KM/SEC

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS

TABLE

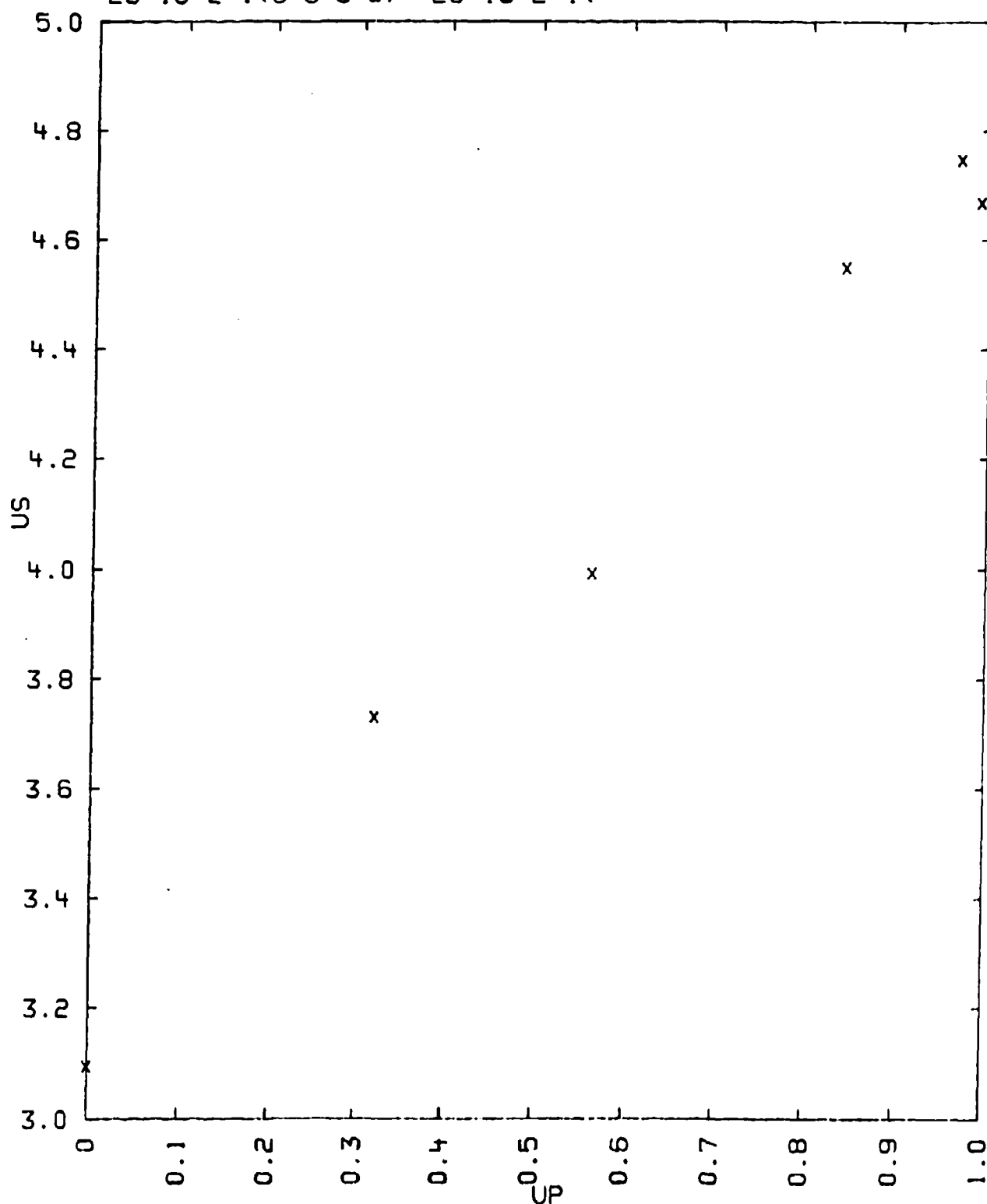
| RH00  | US    | UP    | P    | V/V0  |
|-------|-------|-------|------|-------|
| 1.850 | 3.990 | 0.560 | 41.3 | 0.859 |
| -     | 4.668 | 0.990 | 85.4 | 0.787 |
| -     | 4.745 | 0.967 | 84.8 | 0.796 |
| -     | 3.728 | 0.320 | 22.0 | 0.914 |
| -     | 4.550 | 0.840 | 70.7 | 0.815 |
| -     | 3.095 | 0.000 | 0.0  | 1.000 |

US = A + B\*UP    A = 3.134 KM/SEC.    SIGA = 0.017 KM/SEC.  
 SIG US = 0.070 KM/SEC    B = 1.605    SIGB = 0.024

COMMENTS:

- 1) SOURCE: COLEBURN N. L. AND LIDDARD JR. T. P.  
 J. CHEM. PHYS., VOL. 44, P. 1929 (1965)  
 ALSO: PRIVATE COMMUNICATION
- 2) EXPERIMENTAL TECHNIQUE C1  
 DATA REDUCTION METHOD B:  $UP = 1/2 * UP$  WAS ASSUMED FOR THE STANDARD MATERIALS BRASS AND PLEXIGLAS, SO THAT THE PRESSURE RELEASE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS UP HUGONOT IN THE LINE  $UP = 1/2 * UFS$
- 3) FOR BRASS  $US = 3.560 + 1.833 * UP$  KM/SEC.  
 FOR PLEXIGLAS  $US = 2.710 + 1.568 * UP - 0.037 * UP^{1.2}$
- 4) THE GRUNEISEN COEFFICIENT  $\gamma = V(DP/DE) = 2.77$
- 5) THE VALUE OF V01 WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE VOLUMES OF THE COMPONENTS: RDX:V01 = 0.5494 CC/G  
 TNT:V01 = 0.6046 CC/G  
 AL :V01 = 0.3704 CC/G  
 WAX:V01 = 1.01 CC/G
- 6) C0 IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN UNCERTAINTY OF ABOUT 10 PERCENT

TABLE I  
RDX/TNT/ALUMINUM/WAX (HBX-3) (EXPLOSIVE)  
23-18-2-1(3-6-6-6)--23-18-2-1(



23-18-2-1(3-6-6-6)--23-18-2-1(7-3-5-6)--29---3  
 RDX/TNT/ALUMINUM/WAX (H-6) (EXPLOSIVE)

|          |                                   |       |
|----------|-----------------------------------|-------|
| RDX      | (-C(H2)-N(N-02)-)3                | 44.76 |
| TNT      | -C(CH3)-C(N-02)-(C(H2)-C(N-02)-)2 | 29.53 |
| ALUMINUM | AL                                | 20.95 |
| WAX      | (C-H2)N UNCERTAIN                 | 4.76  |

V0 = 0.5692 CC/G  
 V01 = 0.5501 CC/G

C0 = 2.759 KM/SEC

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS

TABLE

| RH00  | US    | UP    | P    | V/V0  |
|-------|-------|-------|------|-------|
| 1.760 | 3.970 | 0.560 | 39.1 | 0.859 |
| -     | 4.482 | 1.005 | 79.3 | 0.776 |
| -     | 4.450 | 0.985 | 77.1 | 0.779 |
| -     | 2.76  | 0.000 | 0.0  | 1.000 |
| -     | 2.82  | 0.000 | 0.0  | 1.000 |

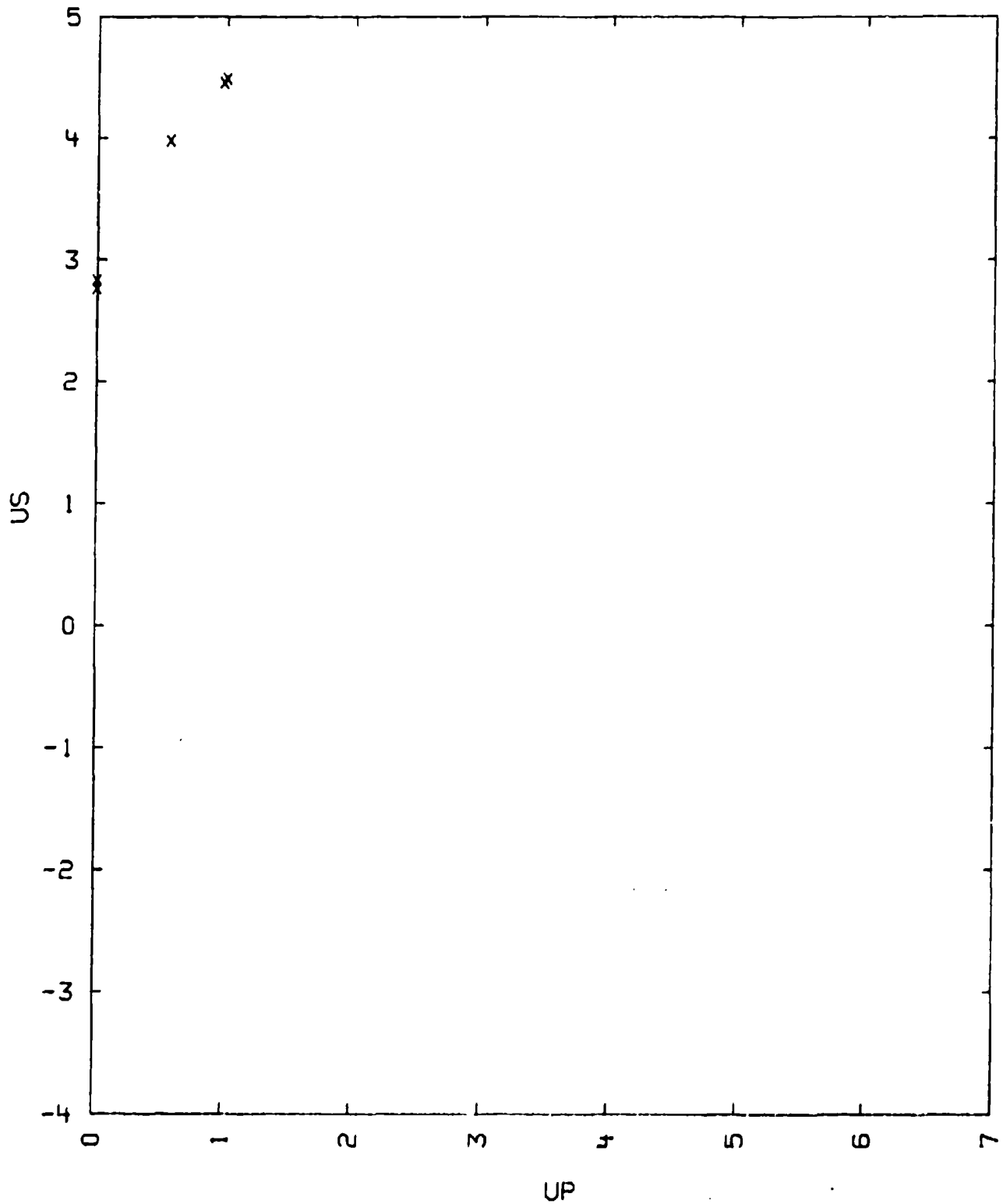
US = A + B\*UP      A = 2.832 KM/SEC,      SIGA = 0.068 KM/SEC.  
 SIG US = 0.12 KM/SEC      B = 1.695      SIGB = 0.083

COMMENTS:

- 1) SOURCE: COLEBURN N. L. AND LIDDIARD JR. T. P.  
 J. CHEM. PHYS., VOL. 44, P. 1929 (1965)  
 ALSO: PRIVATE COMMUNICATION
- 2) EXPERIMENTAL TECHNIQUE C1  
 DATA REDUCTION METHOD B:  $UP = 1/2 * UP$  WAS ASSUMED FOR THE STANDARD MATERIALS BRASS AND PLEXIGLAS, SO THAT THE PRESSURE RELEASE ISENTROPE COULD BE OBTAINED BY REFLECTING THE P VS UP HUGONIOT IN THE LINE  $UP = 1/2 * UFS$
- 3) FOR BRASS  $US = 3.560 + 1.833 * UP$  KM/SEC.  
 FOR PLEXIGLAS  $US = 2.710 + 1.568 * UP - 0.037 * UP^2$
- 4) THE VALUE OF V01 WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE VOLUMES OF THE COMPONENTS: RDX:V01 = 0.5494 CC/G  
 TNT:V01 = 0.6046 CC/G  
 AL :V01 = 0.3704 CC/G  
 WAX:V01 = 1.01 CC/G
- 5) C0 IS THE VELOCITY MEASURED ON VERY WEAK SHOCKS WITH AN UNCERTAINTY OF ABOUT 10 PERCENT

TABLE 1

RDX/TNT/ALUMINUM/WAX (H-6) (EXPLOSIVE)  
 23-18-2-1(3-6-6-6)--23-18-2-1(



23-18-2-1(4-8-8-8)--23-9-2(10-13-7)---1  
 LX-04-1 (EXPLOSIVE) (PHBV 85/15)

HMX (C(H2)-N(N-O2)-)4 = C4-N8-H8-O8 85 WT PERCENT  
 VITON (C10-F13-H7)N 15 WT PERCENT

V0 = 0.5373 CC/G  
 V01 = 0.5309 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. L IS SAMPLE THICKNESS IN MM. AND PQ IS AN INDEPENDENT PRESSURE OBTAINED FROM A QUARTZ PRESSURE GAUGE. SEE COMMENTS. DELUS IS THE DIFFERENCE IN AVERAGE VELOCITY BETWEEN THE FOOT OF THE WAVE AND THE LISTED PRESSURE (COMMENTS)

TABLE

| RH00  | US    | UP     | P     | V/V0   | L    | PQ    | DELUS |
|-------|-------|--------|-------|--------|------|-------|-------|
| 1.860 | 2.608 | 0.1038 | 5.04  | 0.9602 | 12.7 | 4.15  | 0.24  |
| 1.863 | 2.833 | 0.1738 | 9.17  | 0.9387 | 6.3  | 9.49  | 0.22  |
| 1.860 | 2.929 | 0.2346 | 12.78 | 0.9199 | -    | 13.69 | 0.10  |
| 1.860 | 1.962 | 0.2502 | 9.13  | 0.8725 | -    | 10.08 | 0.16  |
| 1.860 | 2.975 | 0.2880 | 15.93 | 0.9032 | -    | 16.05 | 0.14  |
| 1.864 | 1.858 | 0.3124 | 10.82 | 0.8319 | -    | 12.76 | 0.19  |
| 1.862 | 3.293 | 0.3616 | 22.16 | 0.8902 | -    | 21.65 | 0.05  |

US = 2.36 + 2.43\*UP KM/SEC  
 SIG.US = 0.06 KM/SEC.

## COMMENTS:

- 1) SOURCE: WASLEY R. J. AND OBRIEN J. F.  
 PRIVATE COMMUNICATION  
 LAWRENCE RAD. LAB., LIVERMORE, CALIFORNIA, U. S. A.
- 2) EXPERIMENTAL METHOD: A AND 12  
 DATA REDUCTION METHOD: A  
 THE PRESSURE WAS PRODUCED BY IMPACTING TWO  
 SAMPLES OF LX-04-1, SO THAT  
 UP = 1/2 PROJECTILE VELOCITY
- 3) FURTHER WORK IS IN PROGRESS ON THIS MATERIAL
- 4) THE WIDTH OF MOST SHOCK FRONTS MAKES CHOICE OF THE APPROPRIATE SHOCK VELOCITY TO BE USED IN THIS SIMPLE ANALYSIS UNCERTAIN. THE VALUE OF US USED CORRESPONDS TO THE TIME AT WHICH THE QUARTZ GAUGE READS 1/2 OF PEAK VOLTAGE. IN THE OPINION OF THE COMPILER THIS DOES NOT MAKE THE VALUE OF US UNCERTAIN BY MORE THAN 5 PERCENT FOR THE WIDEST SHOCK IN THE TABLE. THE ACCURACY OF PQ IS ALSO 5 PERCENT.
- 5) THE VALUE OF V01 WAS COMPUTED ASSUMING ADDITIVITY OF THE VOLUMES OF VITON (V01 = 1/1.81 CC/G) AND HMX WITH MONOCLINIC UNIT CELL.  
 A = 6.54 B = 11.05 C = 7.37 ANGSTROM BETHA = 102.8 DEGREES  
 AND 2 MOLECULES PER UNIT CELL  
 SEE P. F. EILAND AND R. PEPINSKY Z. KRISTALLOGRAPHY, VOL. 106  
 P. 274 (1955)

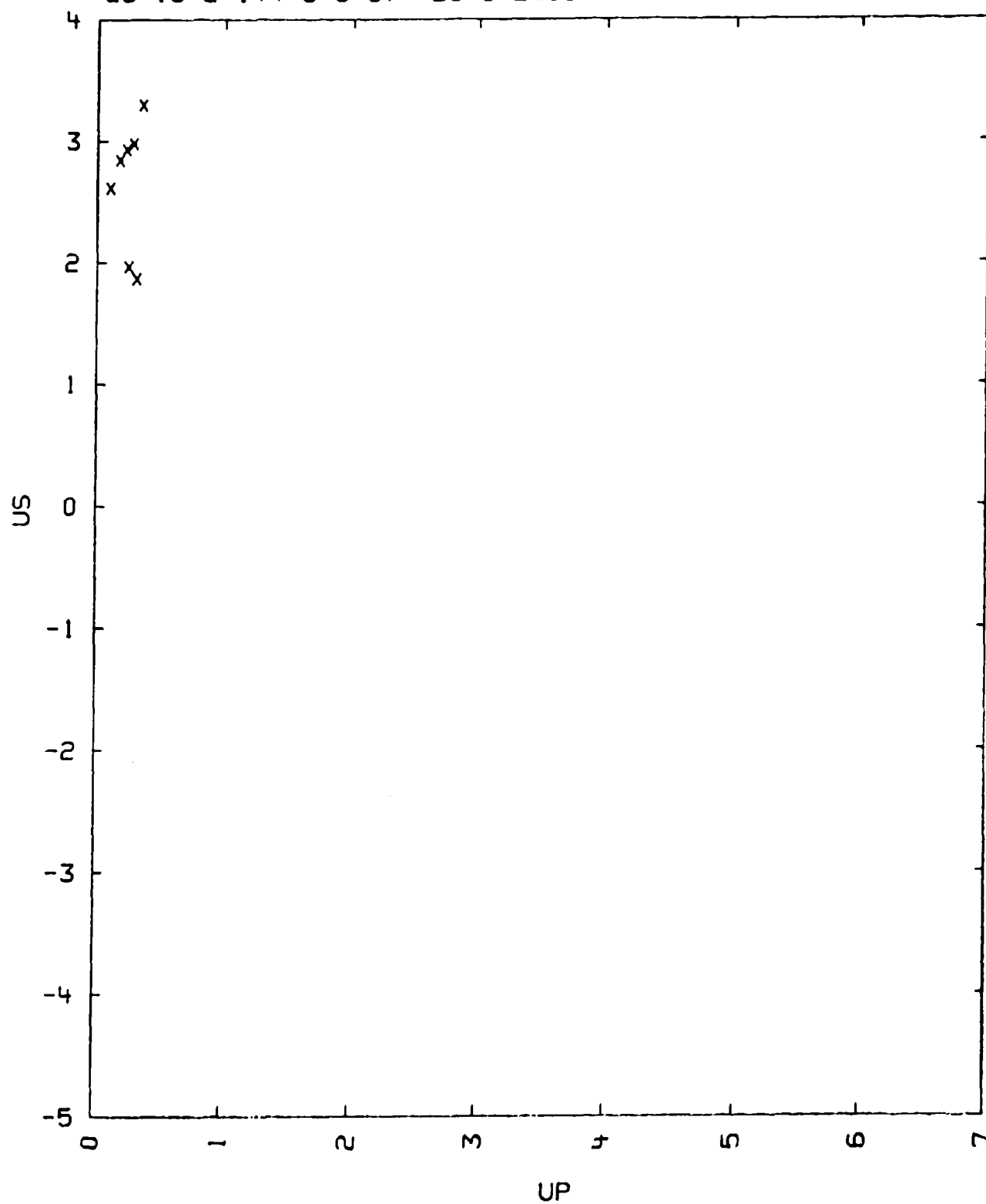
- 6) THE RELATIVELY LOW PRESSURE OBSERVED IN THE 4TH AND 6TH ENTRY ABOVE ARE NOT EXPLAINED. BUT THESE SHOTS WERE NOT USED IN THE LEAST SQUARE FITS



TABLE I

LX-04-1 (EXPLOSIVE) (PHBV 85/15)

23-18-2-1(4-8-8-8)--23-9-2(10-



23-18-2-1(4-8-8-8)--23-18-2-1(7-3-5-6)---1  
OCTOL (EXPLOSIVE)

HMX (EXPLOSIVE)

(-C(H2)-N(N-O2)-14 = C4-N8-H8-O8 65 WT PERCENT

TNT (TRINITROTOLUENE)

(N-O2)3-C6(H2)-C-H3 = C7-N3-H5-O6 35 WT PERCENT

V0 = 0.560 CC/G

V01 = 0.553 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND PRESSURE IN KILOBARS. X DENOTES BRASS STANDARD THICKNESS IN CM.

TABLE

| RH00  | X     | US   | UP    | P     | V/V0  |
|-------|-------|------|-------|-------|-------|
| 1.787 | 1.267 | 5.30 | 1.375 | 130.0 | 0.741 |
| -     | 2.494 | 4.91 | 1.239 | 108.6 | 0.748 |
| -     | 3.759 | 4.69 | 1.118 | 93.6  | 0.762 |

US = 2.00 + 2.38\*UP +OR- 0.13 KM/SEC

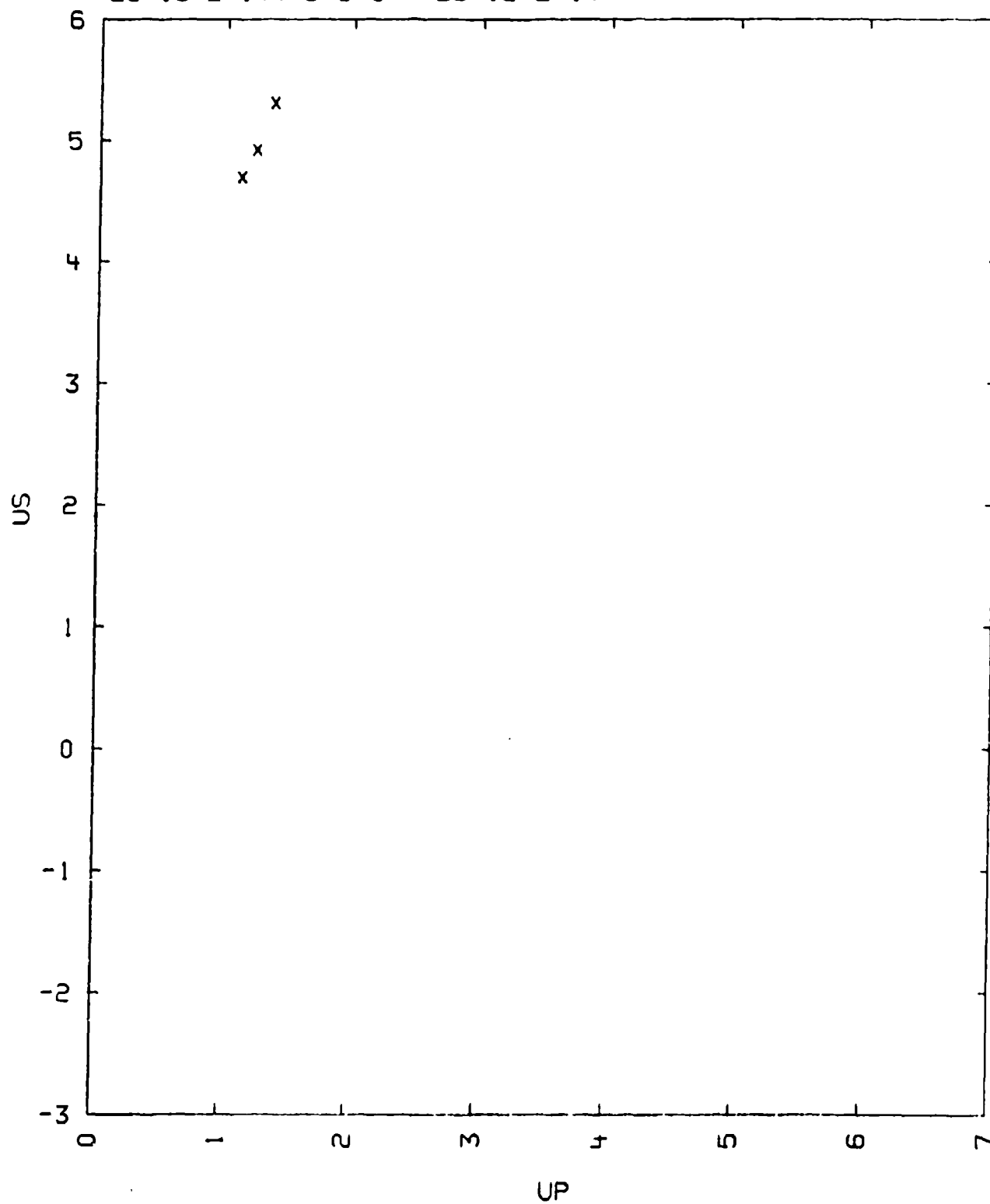
COMMENTS:

- 1) SOURCE: MAJOWICZ, M. J. AND JACOBS, S. J.  
NAVORD REPORT NO. 5710, 1958  
U.S. NAVAL ORDNANCE LAB., WHITE OAK, MARYLAND, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE C  
DATA REDUCTION TECHNIQUE B. WHERE UP = 1/2(UFS). IT WAS ASSUMED THE RELEASE ISENTROPE WAS A STRAIGHT LINE WITH SLOPE RH00(US).  
STANDARD MATERIAL BRASS.
- 3) US IS THE VELOCITY AT ZERO THICKNESS OF THE EXPLOSIVE OBTAINED BY EXTRAPOLATING THE VELOCITY VERSUS THICKNESS CURVE OBTAINED FROM A WEDGE OF EXPLOSIVE.
- 4) THE DETONATION VELOCITY IS 8.17 KM/SEC. SIGMA = 0.01 KM/SEC.  
THIS VELOCITY WAS REACHED AT THICKNESS BETWEEN 1.8-3.5 MM DEPENDING ON INPUT PRESSURE.
- 5) THE VALUE OF V01 WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE VOLUME OF THE COMPONENTS: HMX:V01 = 0.5263, TNT:V01 = 0.6046 CC/G.

TABLE I

OCTOL (EXPLOSIVE)

23-18-2-1(4-8-8-8)--23-18-2-1(



23-18-2-1(4-8-8-8)--23-18-2-1(7-3-5-6)---2  
 OCTOL, CAST (EXPLOSIVE)

HMX (-C(H2)-N(N-O2)-)4 = C4-N8-H8-O8 75 WT PERCENT  
 TNT -C(C-H3)-C(N-O2)(-C(H)-C(N-O2)-)2 = C7-N3-H5-O6 25 - - - -

V0 = 0.555 CC/G

V01 = 0.547 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND  
 PRESSURE IN KILOBARS.

TABLE

| RHO0  | US   | UP   | P    | V/V0  |
|-------|------|------|------|-------|
| 1.803 | 4.68 | 1.05 | 88.6 | 0.776 |
| -     | 4.49 | 0.84 | 68.0 | 0.813 |
| -     | 4.34 | 0.86 | 67.3 | 0.802 |
| -     | 4.06 | 0.71 | 52.0 | 0.825 |
| -     | 3.94 | 0.72 | 51.1 | 0.817 |
| -     | 3.45 | 0.53 | 32.9 | 0.846 |
| -     | 3.50 | 0.53 | 33.4 | 0.849 |
| -     | 3.25 | 0.41 | 24.0 | 0.874 |
| -     | 3.09 | 0.43 | 23.9 | 0.861 |
| -     | 4.89 | 1.09 | 96.1 | 0.777 |
| -     | 4.77 | 1.10 | 94.6 | 0.769 |
| -     | 4.99 | 1.09 | 98.1 | 0.782 |
| -     | 4.95 | 1.09 | 97.3 | 0.780 |
| -     | 4.15 | 0.79 | 59.1 | 0.809 |
| -     | 4.44 | 0.78 | 62.4 | 0.824 |
| -     | 4.42 | 0.78 | 62.2 | 0.824 |

US =  $2.21 + 2.51 \cdot UP$  KM/SEC

SIGMA US = 0.14 KM/SEC

## COMMENTS:

- 1) SOURCE: BOYLE, V. M.  
 PRIVATE COMMUNICATION  
 BALLISTIC RESEARCH LABORATORIES. AMXBR-TD  
 ABERDEEN PROVING GROUND, MARYLAND 21005.
  - 2) EXPERIMENTAL TECHNIQUE: THE SHOCK VELOCITY IN THE SAMPLE WAS MEASURED  
 BY A SMEAR CAMERA THAT SWEEPED THE SHADOWGRAPH OF A TRANSPARENT  
 CHANNEL IN THE SAMPLE ACROSS THE FILM PLANE. THE CHANNEL WAS  
 MADE BY SPLITTING THE SAMPLE IN TWO ALONG THE SHOCK DIRECTION  
 AND SEPARATING THE TWO HALVES BY A THIN (0.127 MM)  
 TRANSPARENT PLASTIC SHEET (EXTRUDED ACETATE).
- DATA REDUCTION TECHNIQUE: B  
 STANDARD MATERIALS USED:  
 ALUMINUM, 2024-T4, US =  $5.360 + 1.351 \cdot UP$  KM/SEC  
 RHO = 2.785 G/CC  
 PLEXIGLASS, US =  $2.702 + 1.544 \cdot UP$ , KM/SEC, RHO = 1.184 G/CC  
 UP = 1/2 UFS WAS ASSUMED FOR THE STANDARD MATERIALS SO THAT

THE PRESSURE ISENTROPE COULD BE OBTAINED BY REFLECTING THE  
P VS. UP HUGONIOT IN THE LINE  $UP = 1/2 UFS$ .

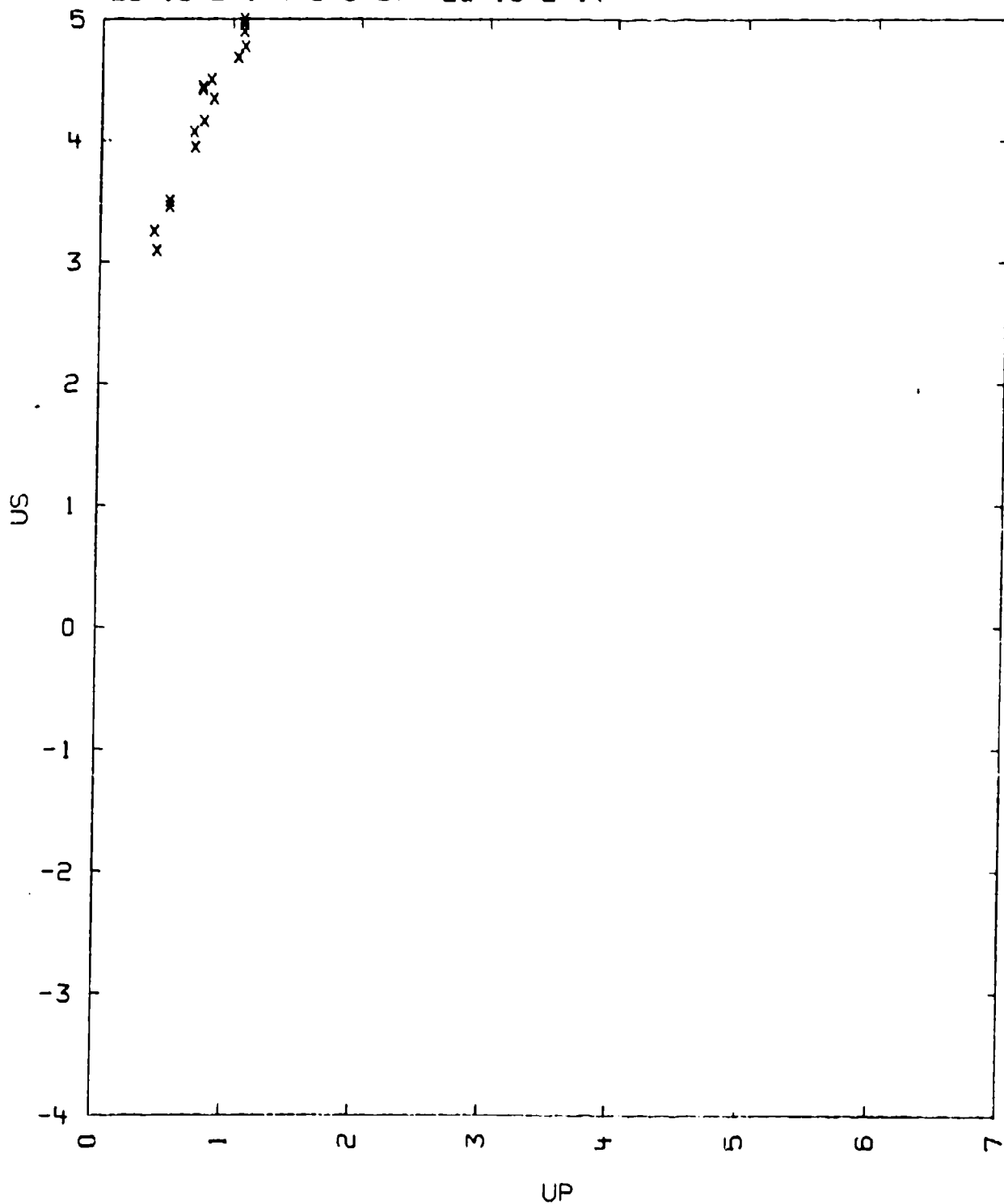
- 3) THE DEGREE TO WHICH THE RESULTS MAY BE AFFECTED BY CHEMICAL REACTION  
OF THE SHOCKED EXPLOSIVE SAMPLE HAS NOT BEEN DETERMINED AT THIS TIME.
- 4) VOI WAS CALCULATED ASSUMING VOLUME ADDITIVITY OF THE COMPONENTS:  
VOI(TNT) = 0.6046 CC/G, HANDBOOK OF CHEM. AND PHYS. (CHEM. RUBBER  
PUBL. CO. 1964) 45TH ED.  
VOI(HMX) = 0.5280 CC/G,

P. F. FILAND AND R. PEPINSKY  
Z. KRISTALLOGRAPHY, V. 106, P. 274 (1955).

TABLE I

OCTOL, CAST (EXPLOSIVE)

23-18-2-1(4-8-8-8)--23-18-2-1(



23-18-2-1(5-4-8-12)--23-18-2-1(7-3-5-6)---1  
PENTOLITE (EXPLOSIVE)

PETN (PENTAERYTHRITOL TETRANITRATE)

C(C(H)2-N-O3)4 = C5-N4-H8-O12 50 WT PERCENT

TNT (TRINITROTOLUENE)

(N-O2)3-C6(H2)-C-H3 = C7-N3-H5-O6 50 WT PERCENT

V0 = 0.5967 CC/G

V01 = 0.6024 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND PRESSURE IN KILOBARS. X DENOTES BRASS STANDARD THICKNESS IN CM.

TABLE

| RH00  | X     | US   | UP    | P     | V/V0   |
|-------|-------|------|-------|-------|--------|
| 1.676 | 1.285 | 5.25 | 1.364 | 120.3 | 0.7402 |
| -     | 2.502 | 4.90 | 1.252 | 102.8 | 0.7445 |
| -     | 3.762 | 4.52 | 1.136 | 86.1  | 0.7487 |

US = 0.885 + 3.20\*UP +OR- 0.04 KM/SEC

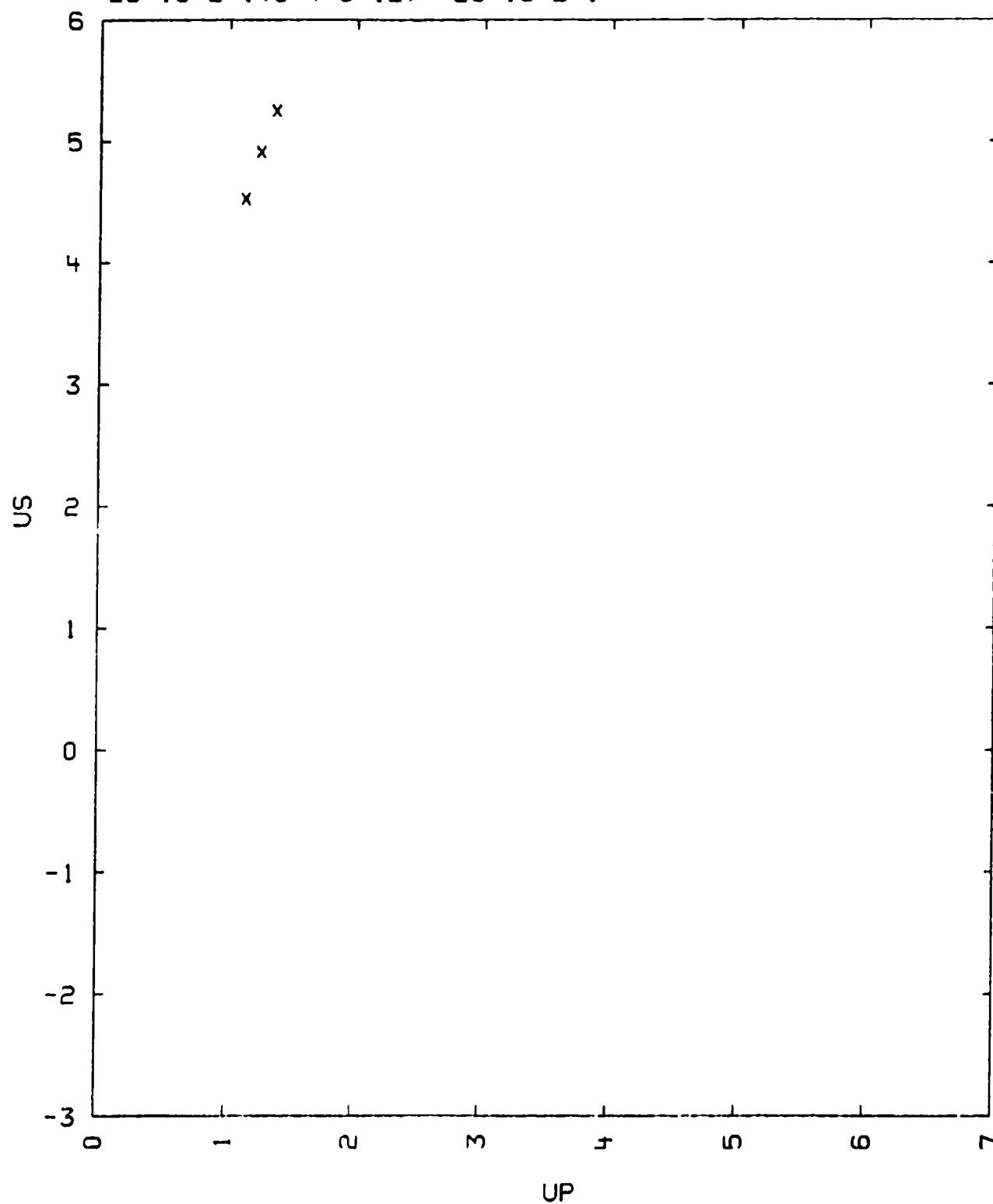
COMMENTS:

- 1) SOURCE: MAJOWICZ, M. J. AND JACOBS, S. J.  
NAVORD REPORT NO. 5710, 1958  
U.S. NAVAL ORDNANCE LAB., WHITE OAK, MARYLAND, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE C  
DATA REDUCTION TECHNIQUE B. WHERE  $UP = 1/2(US)$ . IT WAS ASSUMED THE RELEASE ISENTROPE WAS A STRAIGHT LINE WITH SLOPE  $RH00(US)$ .  
STANDARD MATERIAL BRASS
- 3) US IS THE VELOCITY AT ZERO THICKNESS OF THE EXPLOSIVE OBTAINED BY EXTRAPOLATING THE VELOCITY VERSUS THICKNESS CURVE OBTAINED FROM A WEDGE OF EXPLOSIVE.
- 4) THE DETONATION VELOCITY IS 7.53 KM/SEC, SIGMA = 0.02 KM/SEC.  
THIS VELOCITY WAS REACHED AT THICKNESS BETWEEN 3-4.5 MM DEPENDING ON INPUT PRESSURE.
- 5) THE VALUE OF V01 WAS OBTAINED BY ASSUMING VOLUME ADDITIVITY OF THE VOLUME OF THE COMPONENTS: PETN:V01 = 0.6068, TNT:V01 = 0.6064 CC/G.

TABLE I

PENTOLITE (EXPLOSIVE)

23-18-2-1(5-4-8-12)--23-18-2-1





24-1--2-1---1

SAND-WATER MIXTURE (20 PERCENT SATURATED)

SI-O2 96 PERCENT BY WT.

H2-O 4 PERCENT BY WT.

POROSITY 30 PERCENT BY VOLUME

PARTICLE SIZE 74-149 MICRONS

V0 = 0.581 CC/G.

IN THE TABLE BELOW, TEMPERATURE (T0) IS GIVEN IN DEGREES CENTIGRADE.  
 DENSITY IS IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

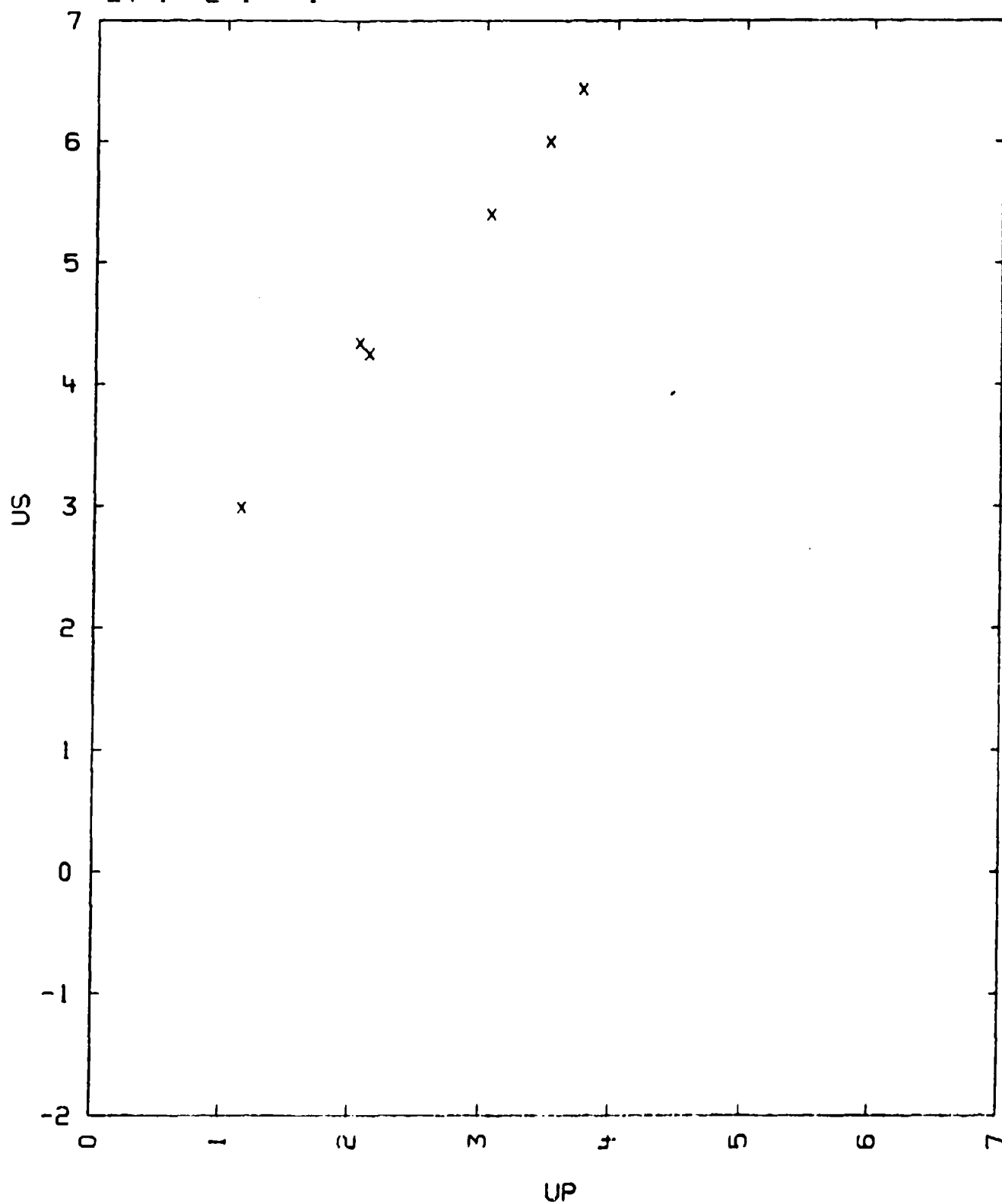
| T0  | RH00 | US   | UP   | P   | V/V0  |
|-----|------|------|------|-----|-------|
| -10 | 1.72 | 2.98 | 1.14 | 58  | 0.618 |
| -10 | 1.72 | 4.34 | 2.05 | 153 | 0.528 |
| -10 | 1.72 | 4.24 | 2.12 | 156 | 0.500 |
| -10 | 1.72 | 5.39 | 3.04 | 282 | 0.436 |
| -10 | 1.72 | 5.99 | 3.49 | 360 | 0.417 |
| -10 | 1.72 | 6.43 | 3.74 | 413 | 0.418 |

$$US = 1.56 + 1.28 \cdot UP \text{ KM/SEC} \quad \text{SIGMA US} = 0.10 \text{ KM/SEC}$$

## COMMENTS:

- 1) SOURCE: ANDERSON, G. D.  
 INTERIM DATA REPORT FGU-6392 (1967)  
 STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA, USA.
- 2) EXPERIMENTAL TECHNIQUE D.  
 DATA REDUCTION TECHNIQUE B  
 STANDARD MATERIAL 2024 ALUMINUM
- 3) THE SAMPLE WAS OTTAWA BANDING SAND, OBTAINED FROM THE OTTAWA SILICA CO., OTTAWA, ILLINOIS, U.S.A.
- 4) THE WT. PERCENT VALUES WERE CALCULATED FROM THE AUTHORS DENSITY OF DRY SAND (1.65 G/CC) AND THE DENSITY OF THIS WET SAND (RH00 = 1.72 G/CC AT 25 DEG. CENTIGRADE).  
 THE POROSITY WAS CALCULATED ASSUMING AS ABOVE, THAT THE SAND DOES NOT EXPAND WHEN WATER IS ADDED AND FROZEN AND THAT 100 PERCENT SATURATED SAND WITH RH00 = 2.02 G/CC AT 25 DEG. CENTIGRADE IS VOID FREE.

TABLE I  
SAND-WATER MIXTURE (20 PERCENT SATURATED)  
24-1--2-1---1



24-1--2-1---2

SAND-WATER MIXTURE (50 PERCENT SATURATED)

S1-02 90 PERCENT BY WT.

H2-O 10 PERCENT BY WT.

POROSITY 16 PERCENT BY VOLUME

PARTICLE SIZE 74-149 MICRONS

V0 = 0.534 CC/G.

IN THE TABLE BELOW. TEMPERATURE (T0) IS GIVEN IN DEGREES CENTIGRADE.  
 DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

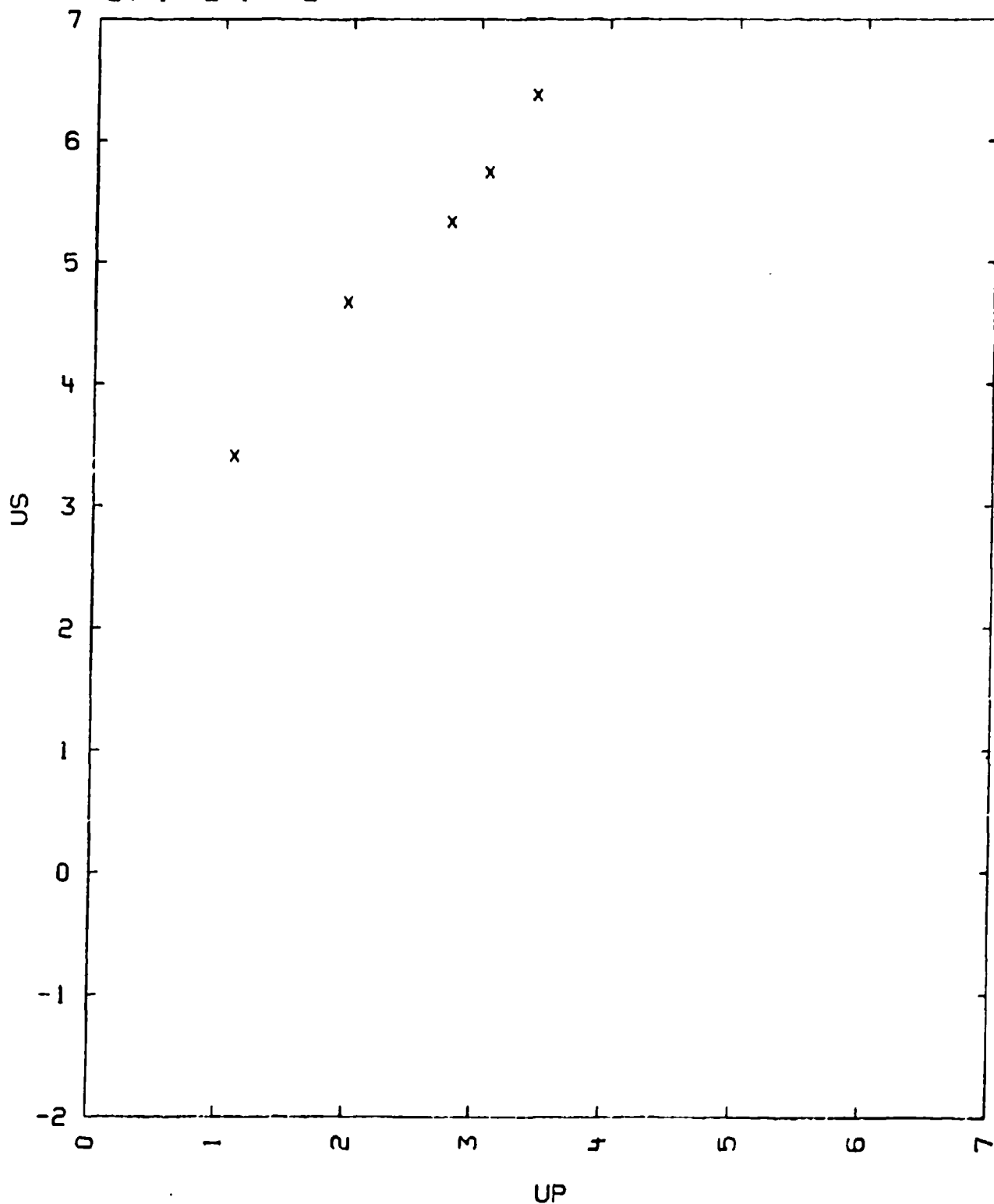
| T0  | RH00 | US   | UP   | P    | V/V0  |
|-----|------|------|------|------|-------|
| -10 | 1.84 | 3.40 | 1.11 | 69.5 | 0.674 |
| -10 | 1.84 | 4.66 | 1.98 | 170  | 0.575 |
| -10 | 1.84 | 5.32 | 2.79 | 273  | 0.475 |
| -10 | 1.84 | 5.73 | 3.08 | 325  | 0.462 |
| -10 | 1.84 | 6.37 | 3.44 | 403  | 0.460 |

$$US = 2.11 + 1.20 \cdot UP \text{ KM/SEC} \quad \text{SIGMA US} = 0.16 \text{ KM/SEC}$$

## COMMENTS:

- 1) SOURCE: ANDERSON, G. D.  
 INTERIM DATA REPORT FGU-6392 (1967)  
 STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA, USA.
- 2) EXPERIMENTAL TECHNIQUE D.  
 DATA REDUCTION TECHNIQUE B.  
 STANDARD MATERIAL 2024 ALUMINUM
- 3) THE SAMPLE WAS OTTAWA BANDING SAND, OBTAINED FROM THE OTTAWA SILICA CO., OTTAWA, ILLINOIS, U.S.A.
- 4) THE WT. PERCENT VALUES WERE CALCULATED FROM THE AUTHORS DENSITY OF DRY SAND (1.65 G/CC) AND THE DENSITY OF THIS WET SAND (RH00 = 1.84 G/CC AT 25 DEG. CENTIGRADE).  
 THE POROSITY WAS CALCULATED ASSUMING AS ABOVE, THAT THE SAND DOES NOT EXPAND WHEN WATER IS ADDED AND FROZEN AND THAT 100 PERCENT SATURATED SAND WITH RH00 = 2.02 G/CC AT 25 DEG. CENTIGRADE IS VOID FREE.

TABLE 1  
SAND-WATER MIXTURE (50 PERCENT SATURATED)  
24-1--2-1---2



24-1--2-1---3

SAND-WATER MIXTURE (100 PERCENT SATURATED)

S1-O2 81 PERCENT BY WT.

H2-O 19 PERCENT BY WT.

PARTICLE SIZE 74-149 MICRONS

T0 = -10 DEGREES CENTIGRADE

V0 = 0.510 CC/G

IN THE TABLE BELOW, TEMPERATURE (T0) IS GIVEN IN DEGREES CENTIGRADE,  
DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

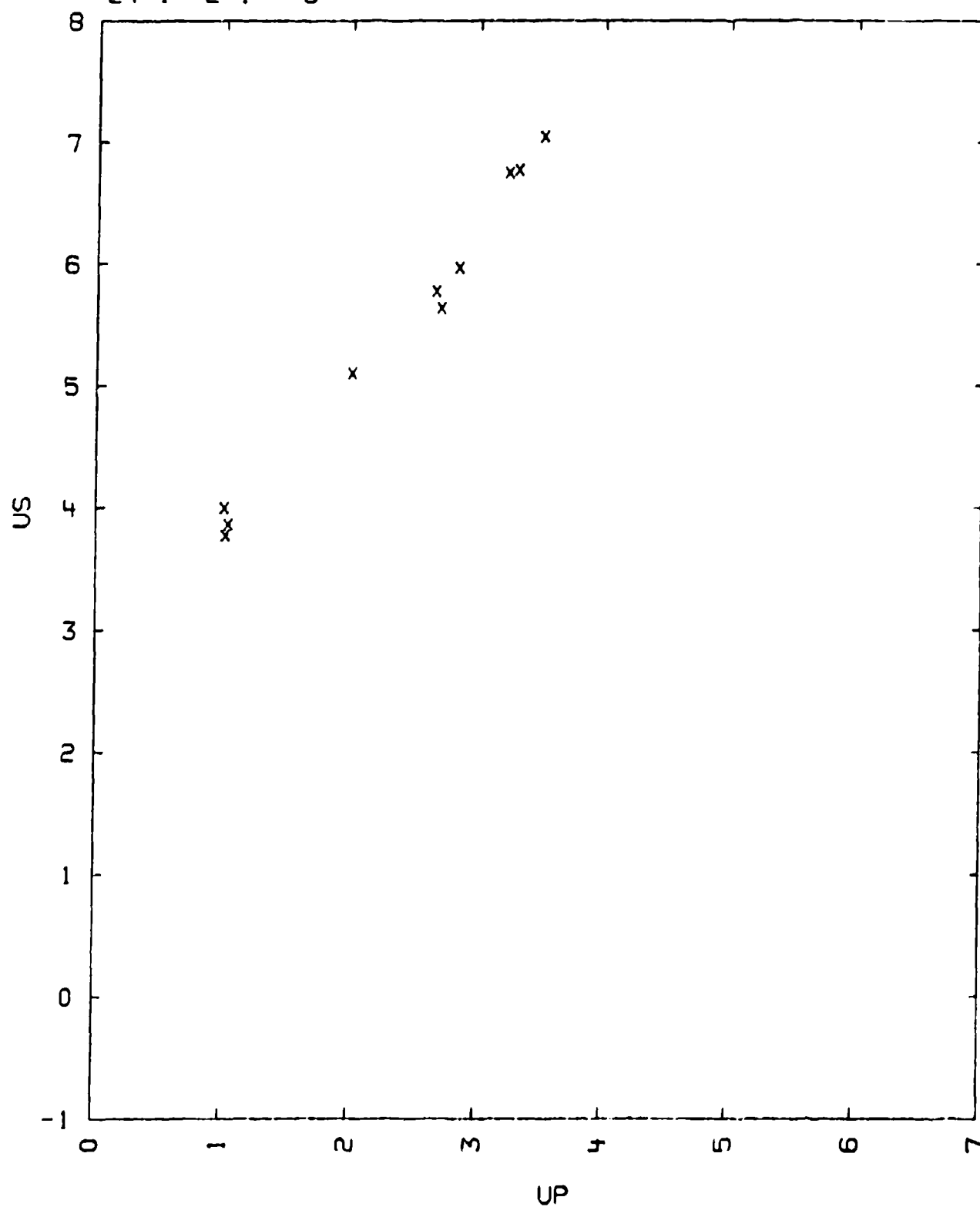
| T0  | RH00 | US   | UP   | P   | V/V0  |
|-----|------|------|------|-----|-------|
| -10 | 1.96 | 3.77 | 1.03 | 76  | 0.727 |
| -10 | 1.96 | 4.00 | 1.01 | 80  | 0.747 |
| -10 | 1.96 | 3.86 | 1.05 | 80  | 0.728 |
| -10 | 1.96 | 5.10 | 2.01 | 201 | 0.606 |
| -10 | 1.96 | 5.77 | 2.67 | 303 | 0.537 |
| -10 | 1.96 | 5.63 | 2.71 | 300 | 0.519 |
| -10 | 1.96 | 5.96 | 2.85 | 333 | 0.522 |
| -10 | 1.96 | 6.74 | 3.24 | 429 | 0.51  |
| -10 | 1.96 | 6.77 | 3.31 | 440 | 0.5   |
| -10 | 1.96 | 7.04 | 3.52 | 487 | 0.5   |

$$US = 2.56 + 1.24 \cdot UP \text{ KM/SEC} \quad \text{SIGMA US} = 0.1$$

## COMMENTS:

- 1) SOURCE: ANDERSON, G. D.  
INTERIM DATA REPORT FGU-6392 (1967)  
STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA, USA.
- 2) EXPERIMENTAL TECHNIQUE D.  
DATA REDUCTION TECHNIQUE B.  
STANDARD MATERIAL 2024 ALUMINUM
- 3) THE SAMPLE WAS OTTAWA BANDING SAND, OBTAINED FROM THE OTTAWA SILICA CO., OTTAWA, ILLINOIS, U.S.A.
- 4) THE SPECIMEN CHARACTERISTICS BEFORE COOLING:  
S1-O2 82 PERCENT BY WT.  
H2-O 18 PERCENT BY WT.  
THE SAMPLE EXPANDS WHEN THE WATER IN IT FREEZES. THE INCREASE IN THE VOLUME IS ASSUMED TO BE DUE TO THE INCREASE IN VOLUME OF THE WATER WHEN IT FREEZES. THE DENSITY OF ICE AT -10 DEG. CENTIGRADE WAS TAKEN AS 0.917 G/CC.

TABLE I  
SAND-WATER MIXTURE (100 PERCENT SATURATED)  
24-1--2-1---3



24-1--23-2-1(7-6-2)---1  
PHENOLIC REFRA SIL

PAGE 635

PHENOLIC (C7-H6-O2)N 0.60 - 0.54 WT PERCENT  
QUARTZ FIBER SI-O2 0.40 - 0.46 WT PERCENT

$V_0 = 0.589 - 0.614 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |      |
|------------------|------|------|------|--------|--------------------|------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |      |
| 1.667            | 3.74 | 0.66 | 41.  | 0.8235 | 2024 AL            | 5.95 |
| 1.641            | 3.72 | 0.68 | 42.  | 0.8172 | 2024 AL            | 5.96 |
| 1.647            | 3.90 | 0.93 | 60.  | 0.7615 | 2024 AL            | 6.20 |
| 1.699            | 4.24 | 1.20 | 86.  | 0.7170 | 2024 AL            | 6.48 |
| 1.642            | 4.24 | 1.27 | 88.  | 0.7005 | 2024 AL            | 6.53 |
| 1.645            | 4.60 | 1.60 | 121. | 0.6522 | 2024 AL            | 6.87 |
| 1.637            | 5.34 | 2.28 | 199. | 0.5730 | 2024 AL            | 7.56 |
| 1.646            | 5.36 | 2.37 | 209. | 0.5578 | 2024 AL            | 7.65 |
| 1.646            | 5.32 | 2.63 | 230. | 0.5056 | 2024 AL            | 7.88 |
| 1.645            | 5.77 | 2.91 | 276. | 0.4957 | 2024 AL            | 8.19 |
| 1.643            | 6.42 | 3.34 | 352. | 0.4798 | 2024 AL            | 8.67 |
| 1.650            | 7.13 | 3.66 | 431. | 0.4867 | 2024 AL            | 9.08 |
| 1.651            | 7.18 | 3.81 | 452. | 0.4694 | 2024 AL            | 9.22 |
| 1.643            | 7.53 | 4.04 | 500. | 0.4635 | 2024 AL            | 9.48 |
| 1.630            | 8.17 | 4.38 | 583. | 0.4639 | 2024 AL            | 9.88 |

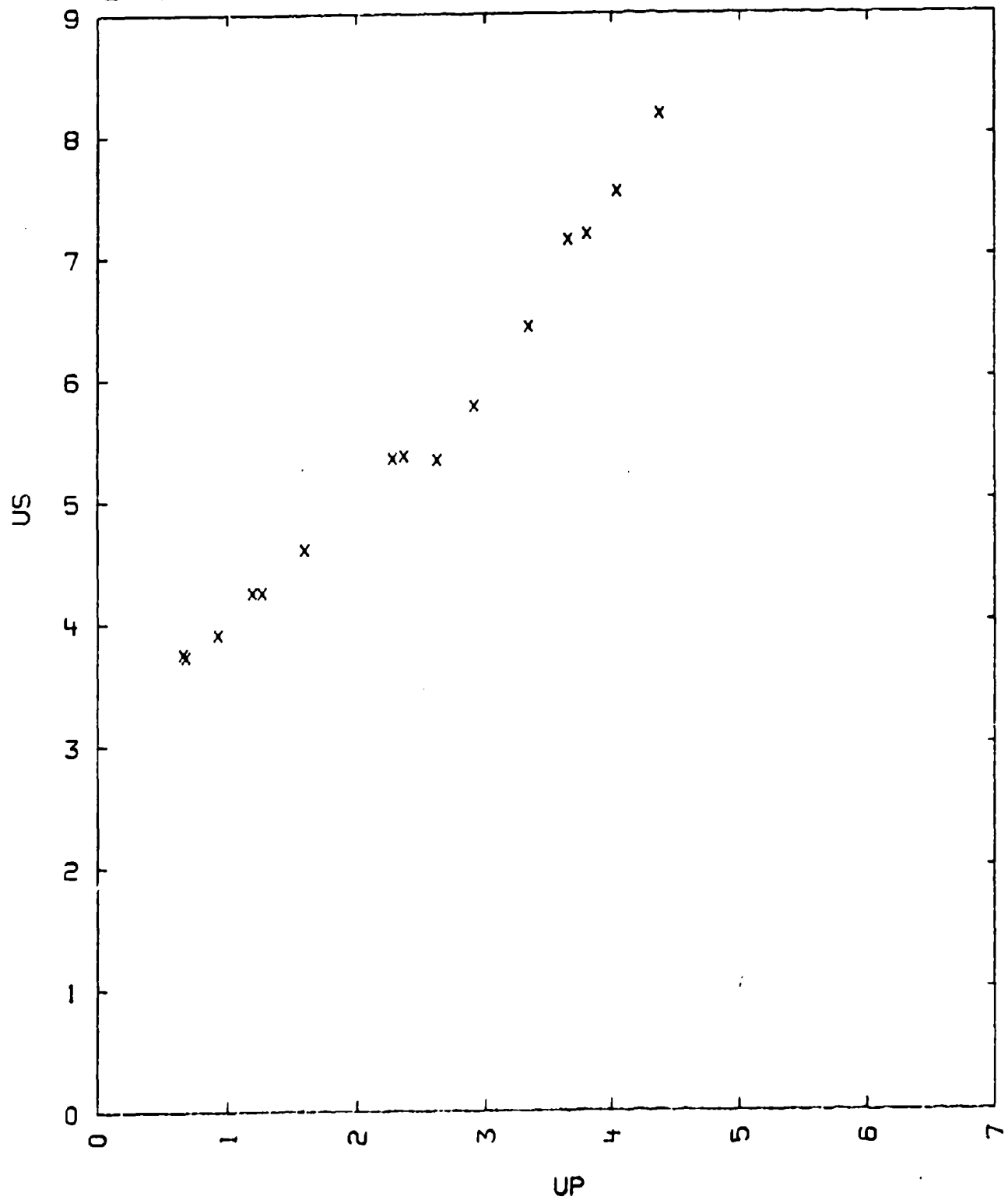
$US = 3.016 + 1.005 \cdot UP \text{ KM/SEC FOR UP BELOW 2.5 KM/SEC}$   
 $SIG US = 0.044 \text{ KM/SEC}$   
 $US = 1.070 + 1.616 \cdot UP \text{ KM/SEC FOR UP ABOVE 2.5 KM/SEC}$   
 $SIG US = 0.078 \text{ KM/SEC}$

COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) THE COMPOSITION WAS CALCULATED ASSUMING VOLUME ADDITIVITY OF THE  
COMPONENTS AND PHENOLIC AND QUARTZ FIBER FIBER DENSITIES OF 1.3 AND  
2.66 G/CC RESPECTIVELY. THE COMPOSITION RANGE IS THEREFORE DUE TO  
THE OBSERVED DENSITY RANGE ONLY. THE SAMPLE CONSISTS OF OBLIQUE  
WOUND QUARTZ FIBER TAPE AND PHENOLIC

TABLE I

PHENOLIC REFRASIL  
24-1--23-2-1(7-6-2)---1





24-1--28-1---

PYREX

|        |             |            |
|--------|-------------|------------|
| SI-02  | 80.4 - 81.4 | WT PERCENT |
| B2-03  | 13.0 - 10.5 | -          |
| AL2-03 | 3.5 - 1.5   | -          |
| CA-0   | 0.13 - 0.7  | -          |
| MGO    | 0.06 - 0.6  | -          |
| NA2-0  | 3.2 - 5.1   | -          |
| K2-0   | 0.2 - 1.8   | -          |
| AS2-03 | 0.5 - 0.75  | -          |

VO = 0.448 CC/G      CL = 5.55 KM/SEC      CO = 3.88 KM/SEC  
CS = 3.45 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

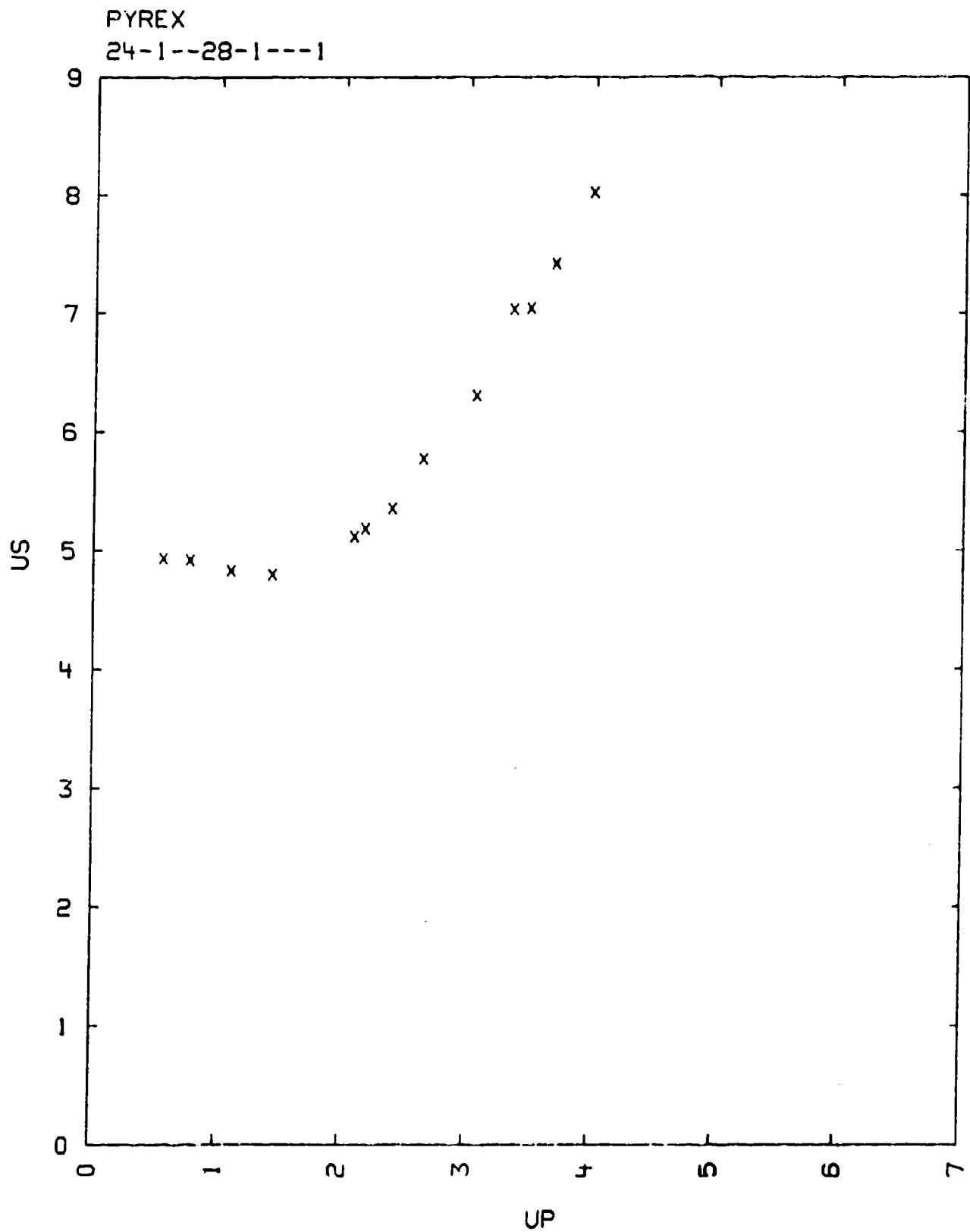
| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |      |
|------------------|------|------|------|--------|--------------------|------|
| RH00             | US   | UP   | P    | V/VO   | MATERIAL US(ST)    |      |
| 2.230            | 4.93 | 0.56 | 62.  | 0.8864 | 2024 AL            | 5.96 |
| 2.230            | 4.91 | 0.78 | 85.  | 0.8411 | 2024 AL            | 6.20 |
| 2.230            | 4.82 | 1.11 | 119. | 0.7697 | 2024 AL            | 6.53 |
| 2.230            | 4.79 | 1.44 | 154. | 0.6994 | 2024 AL            | 6.87 |
| 2.230            | 5.11 | 2.10 | 239. | 0.5890 | 2024 AL            | 7.56 |
| 2.230            | 5.18 | 2.19 | 253. | 0.5772 | 2024 AL            | 7.65 |
| 2.230            | 5.35 | 2.40 | 286. | 0.5514 | 2024 AL            | 7.88 |
| 2.230            | 5.77 | 2.65 | 341. | 0.5407 | 2024 AL            | 8.19 |
| 2.230            | 6.30 | 3.06 | 430. | 0.5143 | 2024 AL            | 8.67 |
| 2.230            | 7.03 | 3.35 | 525. | 0.5235 | 2024 AL            | 9.08 |
| 2.230            | 7.04 | 3.49 | 548. | 0.5043 | 2024 AL            | 9.22 |
| 2.230            | 7.41 | 3.69 | 610. | 0.5020 | 2024 AL            | 9.48 |
| 2.230            | 8.02 | 3.99 | 714. | 0.5025 | 2024 AL            | 9.88 |

US = 1.353 + 1.654\*UP KM/SEC FOR UP ABOVE 2.3 KM/SEC  
SIG US = 0.10 KM/SEC

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) COMPOSITION FROM M.B. VOLF, D. SC. - TECHNICAL GLASSES (SIR ISAAC  
FITMAN AND SONS, LTD., LONDON, 1961) P. 130

TABLE I



24-1--99-94-29-24-1--100-93-41-29-24-2-1--100-29-24-2-1---1  
GNEIS

|             |                                     |                    |
|-------------|-------------------------------------|--------------------|
| QUARTZ      | SI-02                               | 35 VOL. PERCENT    |
| PLAGIOCLASE |                                     | 21-22 - -          |
| ALBITE      | NA-AL-SI3-O8                        | 90-50 MOL. PERCENT |
| ANORTHITE   | CA-AL2-SI2-O8                       | 10-50 - -          |
| BIOTITE     | K(MG,FE)3(AL-SI3-O10)(O-H)2         | 15-20 - -          |
| MUSCOVITE   | K-AL2(AL-SI3-O10)(O-H)2             | 15-10 - -          |
| CHLORITE    | MG3(SI4-O10)(O-H)2-MG3(O-H)6        | 7 - -              |
| GARNET      | (MG,FE,MN,CA)3-(AL,FE,CR)2-(SI-O4)3 | 5 - -              |
| PYRITE      | FE-S2                               | 1-.5 - -           |
| MAGNETITE   | FE3-O4                              | 1-.5 - -           |
| GRAIN SIZE  |                                     | 0.1 - 2. MM        |

V0 = 0.358 CC/G

V01 =

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURES IN KBAR.

TABLE

| RH00 | US    | UP   | P     | V/V0  |
|------|-------|------|-------|-------|
| 2.79 | 6.57  | 2.56 | 469.  | 0.611 |
| -    | 7.63  | 3.17 | 667.  | 0.576 |
| -    | 8.47  | 3.74 | 885.  | 0.558 |
| -    | 8.74  | 3.98 | 970.  | 0.545 |
| -    | 8.99  | 3.99 | 1000. | 0.557 |
| -    | 9.08  | 4.27 | 1082. | 0.530 |
| -    | 9.22  | 4.34 | 1117. | 0.529 |
| -    | 9.47  | 4.42 | 1169. | 0.533 |
| -    | 11.35 | 5.25 | 1673. | 0.537 |
| -    | 11.99 | 6.08 | 2034. | 0.493 |

US = 2.49 + 1.593\*UP KM/SEC.

SIG.US = 0.22 KM/SEC.

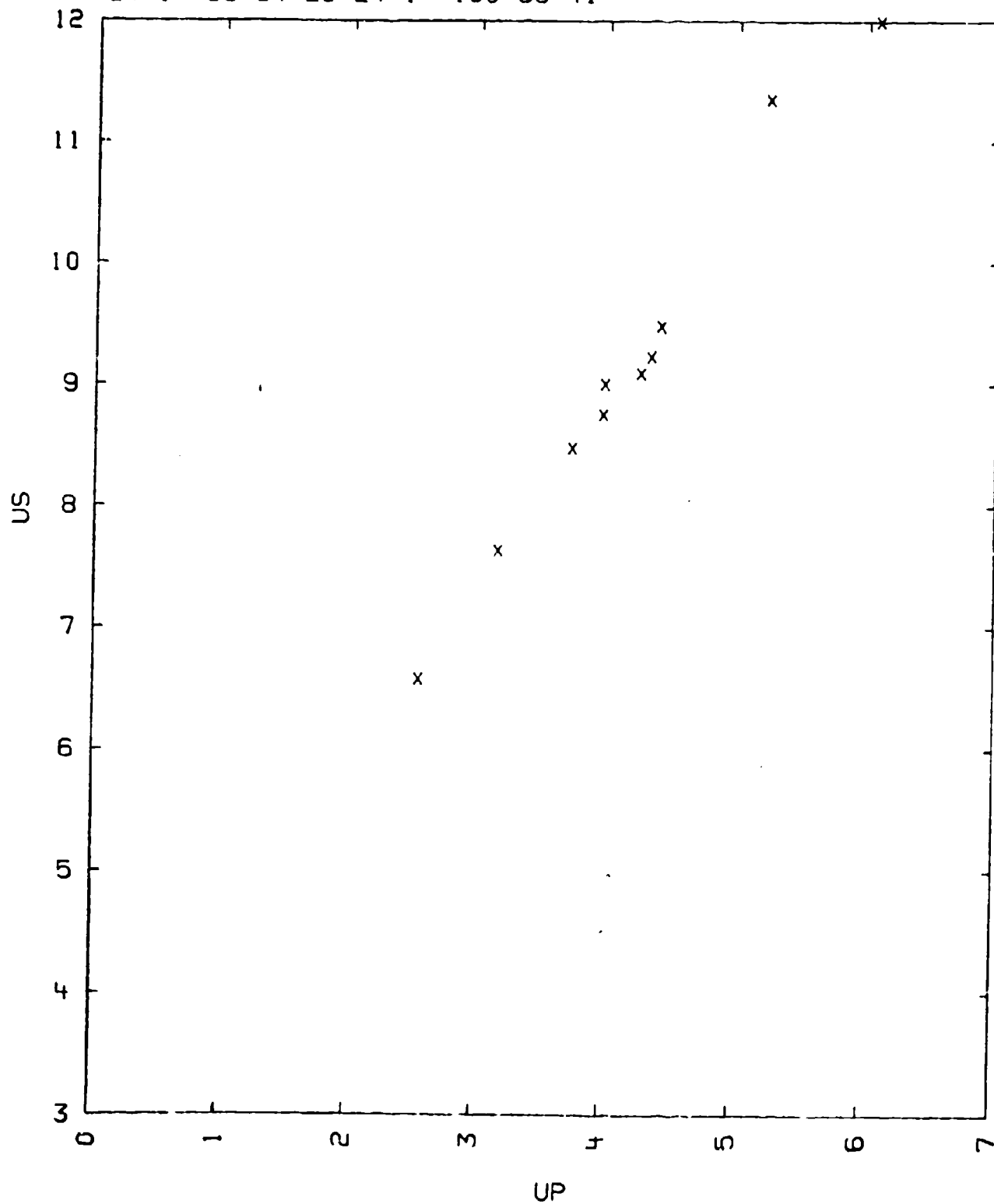
COMMENTS:

- 1) SOURCE: ISBELL W. M., SHIPMAN F. H. AND JONES A. H.  
PROGRESS REPORT NO. 5, CONTRACT DA-49-146-X2-429  
MATERIALS AND STRUCTURES LAB.  
GENL. MOTORS TECHNICAL CENTER  
WARREN, MICHIGAN 48090, U. S. A.
  - 2) EXPERIMENTAL TECHNIQUE: A. THE PROTECTILE VELOCITIES WERE DETERMINED  
FROM TWO TIMED FLASH X-RAY SHADOWGRAPHS.  
STANDARDS: CU AND FANSTEEL
- DATA REDUCTION TECHNIQUE: A.

TABLE I

GNEIS

24-1--99-94-29-24-1--100-93-41



24-23-2-1(100-321-608-200)--24-1---1  
 SILICONE RUBBER-SILICA MIXTURE

|                   |                        |      |      |         |
|-------------------|------------------------|------|------|---------|
| RUBBER STOCK      | SI100-C321-H608-0200 : | 68.4 | WT.  | PERCENT |
| SILICONE DIMETHYL | (-SI(C-H3)2-O-)X       | 96.8 | MOL. | -       |
| DIPHENYL          | (-SI(C6-H5)2-O-)Y      | 2.0  | -    | -       |
| VINYL-METHYL      | (-C(H3)SI(C2-H3)-O-)Z  | 1.2  | -    | -       |
| CABOSYL           | SI-02                  | 31.  | WT.  | -       |
| DICUMYL PEROXIDE  | ((C6-H5)-C(C-H3)2-O-)2 | 0.6  | -    | -       |

$V_0 = 0.8203 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC AND PRESSURE IN KBAR. MET INDICATES DATA RECORDING METHOD.

TABLE

| RH00  | US   | UP   | P    | V/V0 | MET |
|-------|------|------|------|------|-----|
| 1.219 | 5.71 | 2.51 | 175. | 0.56 | A   |
| -     | 5.76 | 2.44 | 172. | 0.58 | F   |
| -     | 5.39 | 2.13 | 139. | 0.60 | F   |
| -     | 4.58 | 1.72 | 96.  | 0.62 | F   |
| -     | 3.22 | 0.87 | 34.  | 0.73 | F   |
| -     | 3.20 | 0.92 | 35.  | 0.71 | A   |

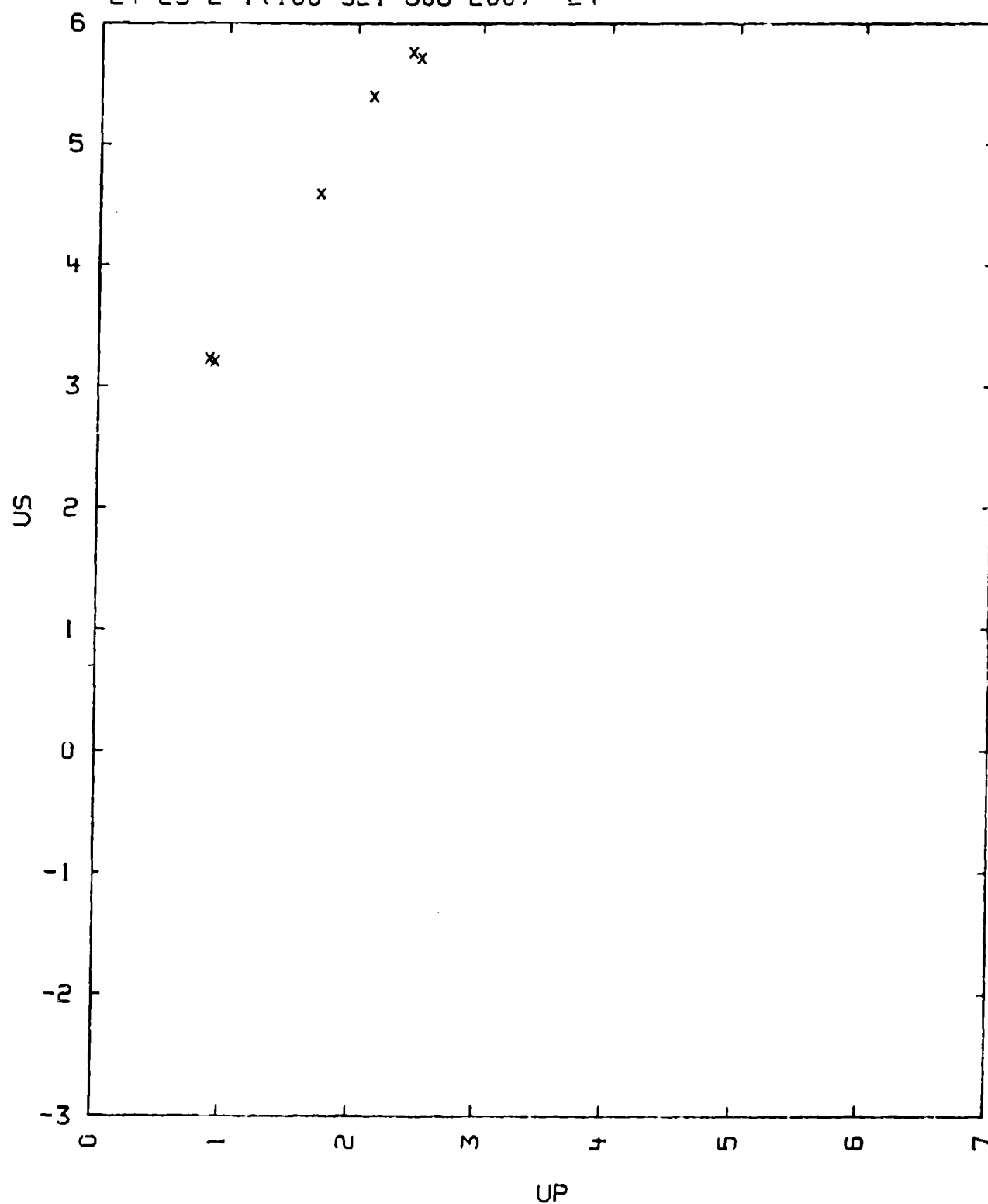
$US = 1.7A + 1.62 \cdot UP \text{ KM/SEC}$   
 $SIG.US = 0.11 \text{ KM/SEC.}$

COMMENTS:

- 1) SOURCE: MAY, R.P., BIESECKER, R.G. AND KING, T.N.  
 SANDIA LABORATORY REPORT SC-TM-68-187, MAY 1968  
 SANDIA CORP., ALBUQUERQUE, NEW MEXICO
- 2) EXPERIMENTAL TECHNIQUE: A AND F  
 DATA REDUCTION TECHNIQUE. B AND B\* FOR EXP.METS. A AND F RESP.
- 3) THE RUBBER STOCK WAS SE5603 SILICONE RUBBER FROM GENERAL ELECTRIC CO.  
 CURING AGENT WAS DICUMYL PEROXIDE FROM HERCULES POWDER CO. 0.6 PARTS  
 OF CURING AGENT WERE MIXED WITH 100 PARTS BY WT. OF RUBBER STOCK TO  
 TO MAKE THE ABOVE CURED MIXTURE. DUROMETER HARDNESS = 55 D.

TABLE I

SILICONE RUBBER-SILICA MIXTURE  
24-23-2-1(100-321-608-200)--24



24-23-2-1--58-24-1--24-1--33-1---1  
 SILASTIC RUBBER, RTV- 521

|                                              |                 |
|----------------------------------------------|-----------------|
| DIMETHYLPOLYSILOXANE ((C-H3)-SI-O)N          | 56.1 WT PERCENT |
| DIATOMACEOUS EARTH SI-O2                     | 12.9 WT PERCENT |
| ZINC OXIDE ZN-O                              | 8.2 WT PERCENT  |
| ZIRCONIUMSILICATE ZR-SI-O4                   | 21.6 WT PERCENT |
| OXIDES M-O                                   | 1.1 WT PERCENT  |
| DIBUTYLINDILAUATE H9-C4-SN-O2-C(C-H2)10-C-H3 | 0.1 WT PERCENT  |

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
 AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RHO0             | US   | UP   | P    | V/V0   | MATERIAL           | US(ST) |
| 1.370            | 3.69 | 1.40 | 71.  | 0.6206 | 2024 AL            | 6.55   |
| 1.380            | 4.17 | 1.77 | 102. | 0.5755 | 2024 AL            | 6.91   |
| 1.380            | 5.48 | 2.37 | 179. | 0.5675 | 2024 AL            | 7.56   |
| 1.370            | 7.03 | 3.50 | 337. | 0.5021 | 2024 AL            | 8.74   |
| 1.370            | 7.46 | 3.73 | 381. | 0.5000 | 2024 AL            | 9.00   |
| 1.360            | 7.42 | 3.78 | 381. | 0.4906 | 2024 AL            | 9.03   |
| 1.380            | 7.54 | 3.88 | 404. | 0.4854 | 2024 AL            | 9.16   |
| 1.370            | 8.31 | 4.56 | 519. | 0.4513 | 2024 AL            | 9.86   |
| 1.370            | 8.10 | 4.66 | 517. | 0.4247 | 2024 AL            | 9.93   |

US = 0.218 + 2.694\*UP - 0.208\*UP\*\*2 KM/SEC  
 SIG US = 0.12 KM/SEC

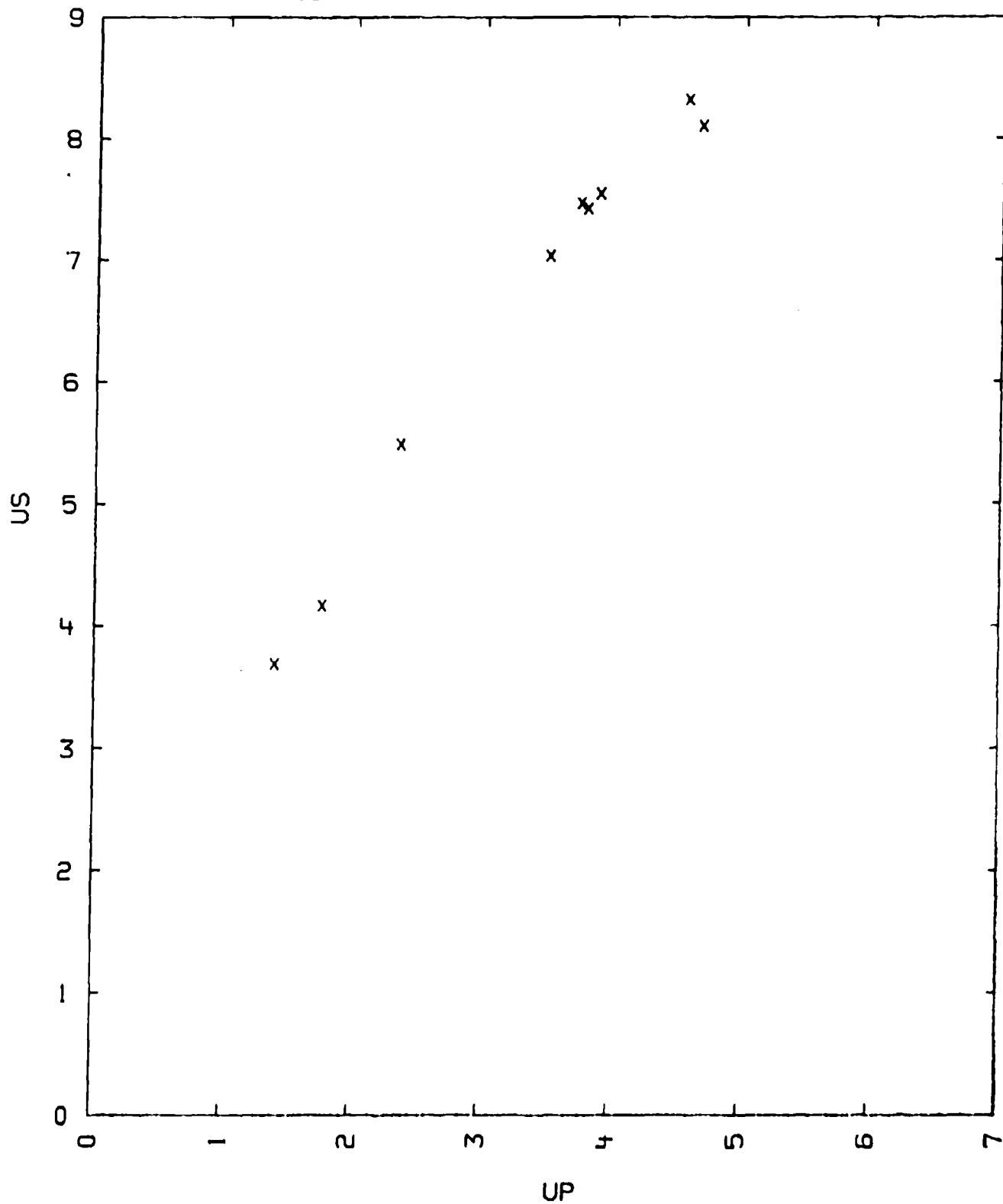
## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
 AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES.  
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
 DATA REDUCTION TECHNIQUE: B (STANDARD BASE PLATE AS SHOWN)
- 3) CHEMICAL ANALYSIS OF A RTV-521 SAMPLE IS CONSISTENT WITH THE ABOVE  
 NOMINAL COMPOSITION  
 PRIVATE COMMUNICATION, PHILLIP G. FLEMING  
 LAWRENCE LIVERMORE LABORATORY, LIVERMORE, CALIFORNIA 94553

TABLE I

SILASTIC RUBBER, RTV- 521

24-23-2-1--58-24-1--24-1--33-1





27--23-18-2-1(100-1-110-20)---1  
LEAD EPON (EPON-LEAD)

EPON C100-H113-020-N 15.0 PERCENT BY WEIGHT  
PB 85.0 PERCENT BY WEIGHT

$V_0 = 0.206 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,  
AND PRESSURE IN KILOBARS.

TABLE

| ----- SAMPLE ----- |      |      |      |     |                  | BASE PLATE |
|--------------------|------|------|------|-----|------------------|------------|
| RH00               | US   | UFS  | UP   | P   | V/V <sub>0</sub> | P          |
| 4.846              | 4.20 | 3.35 | 1.64 | 334 | 0.610            | 339        |
| 4.863              | 3.27 | 1.81 | 0.93 | 148 | 0.716            | 159        |
| 4.868              | 3.66 | 2.44 | 1.22 | 217 | 0.667            | 228        |
| 4.866              | 3.87 | 2.80 | 1.38 | 260 | 0.643            | 268        |
| 4.869              | 3.28 | 1.94 | 0.99 | 158 | 0.698            | 171        |

US =  $1.98 \pm 1.36$  UP KM/SEC      FOR UP BETWEEN 0.9 AND 1.6 KM/SEC  
SIGMA US = 0.034 KM/SEC

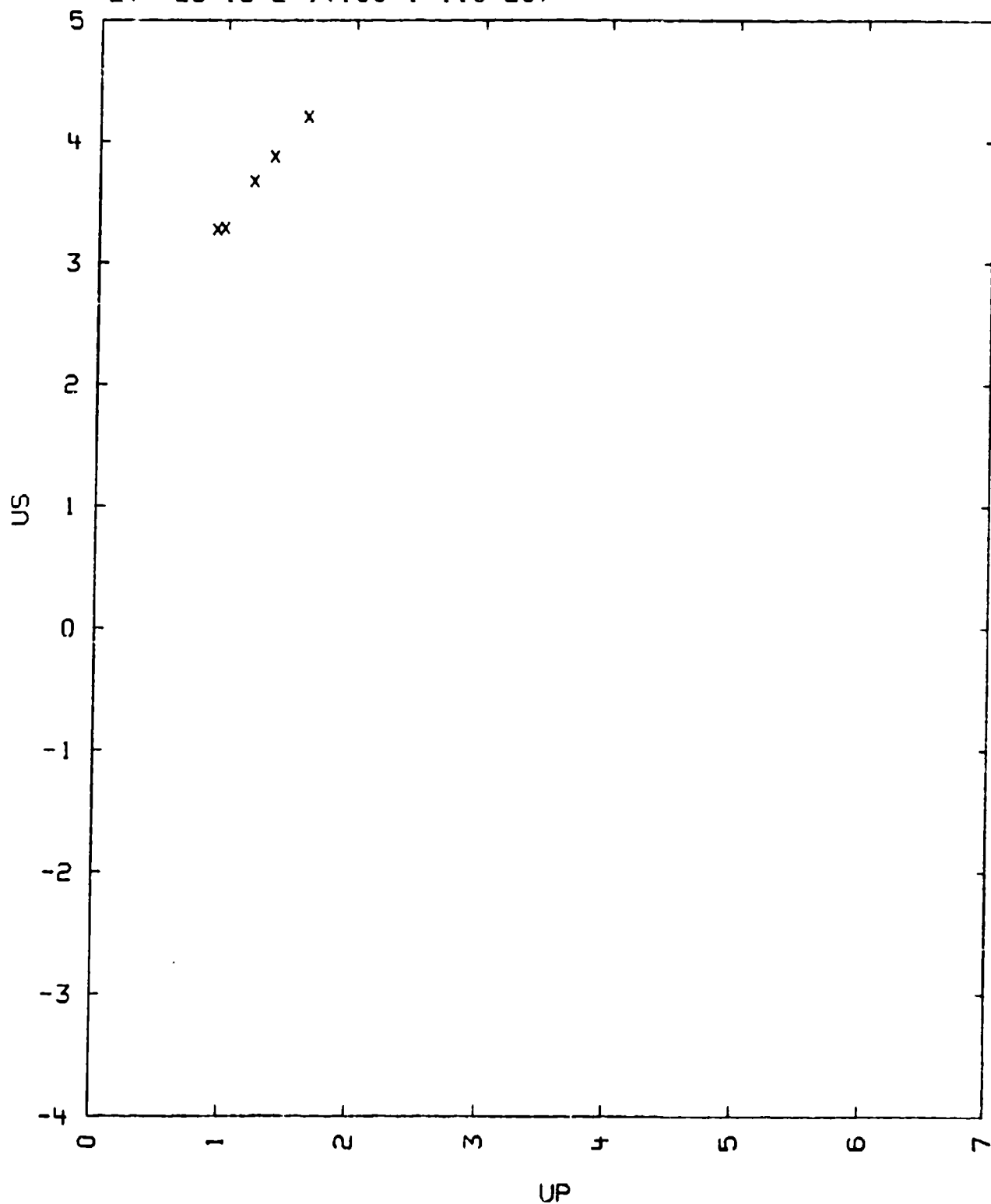
## COMMENTS:

- 1) SOURCE: COMPILER  
L.R.L. EQUATION OF STATE FILE  
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE B. (ALUMINUM STANDARD BASE PLATE)  
DATA REDUCTION TECHNIQUE B.
- 3) THE EPON USED IN THIS MIXTURE WAS A LIQUID CONDENSATION PRODUCT OF  
BISPHENOL-A AND EPICHLOROHYDRIN ACTIVATED TO SOLIDIFY WITH PIPERIDINE  
TO GIVE THE ABOVE NOMINAL ATOMIC COMPOSITION.
- 4) A TYPICAL EPON-PIPERIDINE MIXTURE ANALYSIS:  
C 74.14 PERCENT BY WEIGHT  
H 7.39 -  
O 17.69 -  
N 0.78 -

TABLE 1

LEAD EPON (EPON-LEAD)

27--23-18-2-1(100-1-110-20)---



27--34--93---1  
LEAD ALLOY

PB-CD-MG-ZN

PB 35 PERCENT BY WEIGHT  
CD 33 PERCENT -  
MG 30 PERCENT -  
ZN 2 PERCENT -

$V_0 = 0.231 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN CC/G, VELOCITIES IN KM/SEC,  
AND PRESSURE IN KILOBARS.

TABLE

| ----- SAMPLE ----- |      |      |      |     |                  | BASE PLATE |
|--------------------|------|------|------|-----|------------------|------------|
| RH00               | US   | UFS  | UP   | P   | V/V <sub>0</sub> | P          |
| 4.301              | 4.23 | 1.81 | 0.94 | 171 | 0.778            | 172        |
| 4.318              | 4.57 | 2.41 | 1.22 | 241 | 0.732            | 240        |
| 4.343              | 5.23 | 2.94 | 1.47 | 333 | 0.719            | 317        |

$US = 2.41 + 1.87 UP \text{ KM/SEC}$

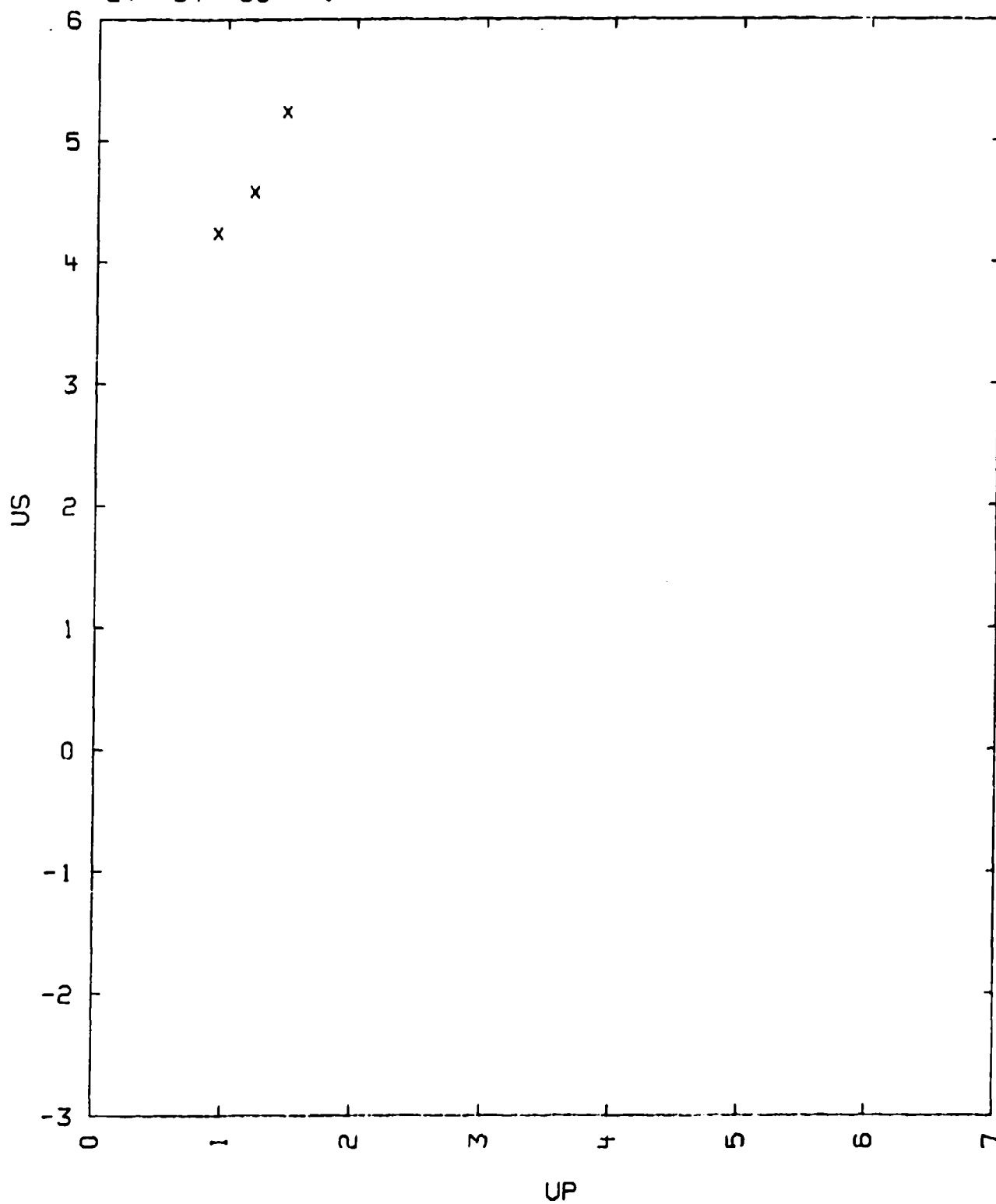
$SIGMA US = 0.154 \text{ KM/SEC}$

COMMENTS:

- 1) SOURCE: COMPILER  
L.R.L. EQUATION OF STATE FILE  
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE B. (ALUMINUM STANDARD BASE PLATE)  
DATA REDUCTION TECHNIQUE B.
- 3) SOME OF THE VARIATION IN RH00 MAY BE DUE TO A LACK OF UNIFORMITY  
IN THE ORIGINAL BATCH FROM WHICH THE SAMPLES WERE DERIVED.  
THE ABOVE COMPOSITION OF THE ALLOY IS THE AVERAGE BATCH COMPOSITION.
- 4) THIS ALLOY IS PROBABLY A TWO PHASE SYSTEM:
  - A) A SOLUTION OF CD AND ZN IN MG
  - B) A MG2-PB PHASE (F. FULTON, METALLURGY L.R.L.)

TABLE 1

LEAD ALLOY  
27--34--93---1



33-10--2-1---1  
ZINC CHLORIDE AQUEOUS

ZN-CL2 66.5 WT PERCENT  
H2-O REST

$V_0 = 0.532 \text{ CC/G}$

$C_0 = 1.538 \pm 0.004 \text{ KM/SEC}$

IN THE TABLE BELOW, TEMPERATURE (T0) IS GIVEN IN DEGREES CENTIGRADE.  
DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| T0 | RH00 | US   | UP   | P   | V/V0  |
|----|------|------|------|-----|-------|
| 25 | 1.88 | 3.68 | 1.12 | 75  | 0.696 |
| 25 | 1.88 | 4.13 | 1.49 | 115 | 0.639 |
| 25 | 1.88 | 4.91 | 1.91 | 176 | 0.611 |
| 25 | 1.88 | 5.24 | 2.13 | 212 | 0.594 |

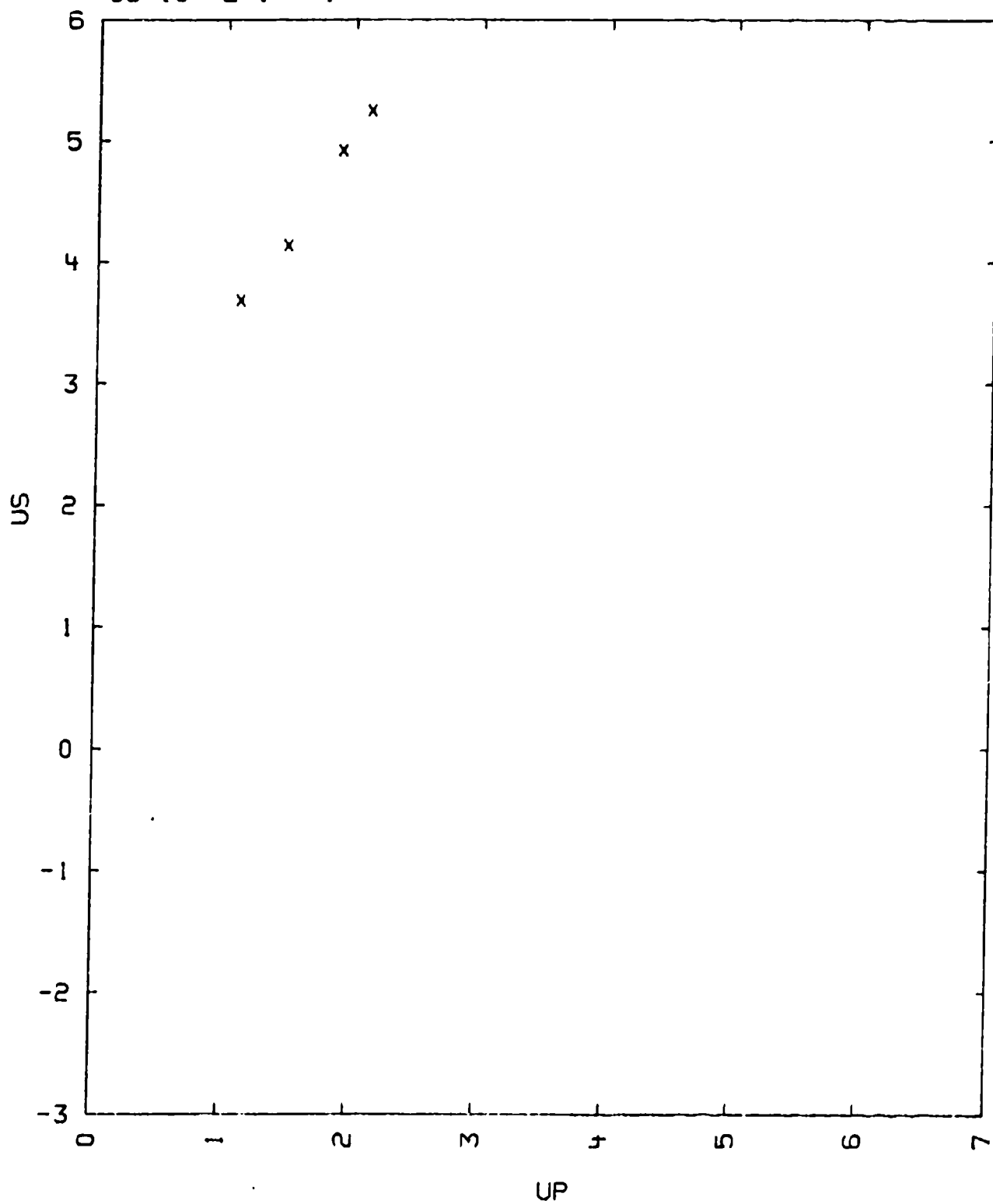
$US = 1.858 + 1.593 \cdot UP \text{ KM/SEC}$ ,  $SIGMA US = 0.007 \text{ KM/SEC}$

COMMENTS:

- 1) SOURCE: RAMSAY, J. B.  
PRIVATE COMMUNICATION (1966)  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL ALUMINUM 2024
- 3) THE ABOVE COMPOSITION WAS CALCULATED FROM THE MEASURED DENSITY AND  
THE DATA IN INTERNATIONAL CRITICAL TABLES, VOL. 3, (MCGRAW-HILL BOOK  
CO., NEW YORK, N. Y., 1929) P. 64.
- 4)  $C_0$  IS A MEASURED VALUE GIVEN BY THE SOURCE.

TABLE I

ZINC CHLORIDE AQUEOUS  
33-10--2-1---1



36--33---1  
BRASS

CU 60.56 PER CENT  
ZN 39.31 PER CENT  
MISC. 0.13 PER CENT

$V_0 = 0.1189 \text{ G/CC.}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC.  
PRESSURE IN KILOBARS, AND DENSITY IN G/CC.

TABLE

| RH00  | US    | UFS   | UP    | P     | V/V0   |
|-------|-------|-------|-------|-------|--------|
| 8.413 | 4.446 | 1.181 | 0.590 | 220.7 | 0.8673 |
| -     | 4.440 | 1.143 | 0.571 | 213.3 | 0.8714 |
| -     | 4.731 | 1.553 | 0.791 | 314.8 | 0.8328 |
| -     | 4.726 | 1.569 | 0.770 | 306.2 | 0.8371 |
| -     | 5.236 | 2.200 | 1.085 | 478.0 | 0.7928 |
| -     | 5.220 |       | 1.077 | 473.0 | 0.7937 |

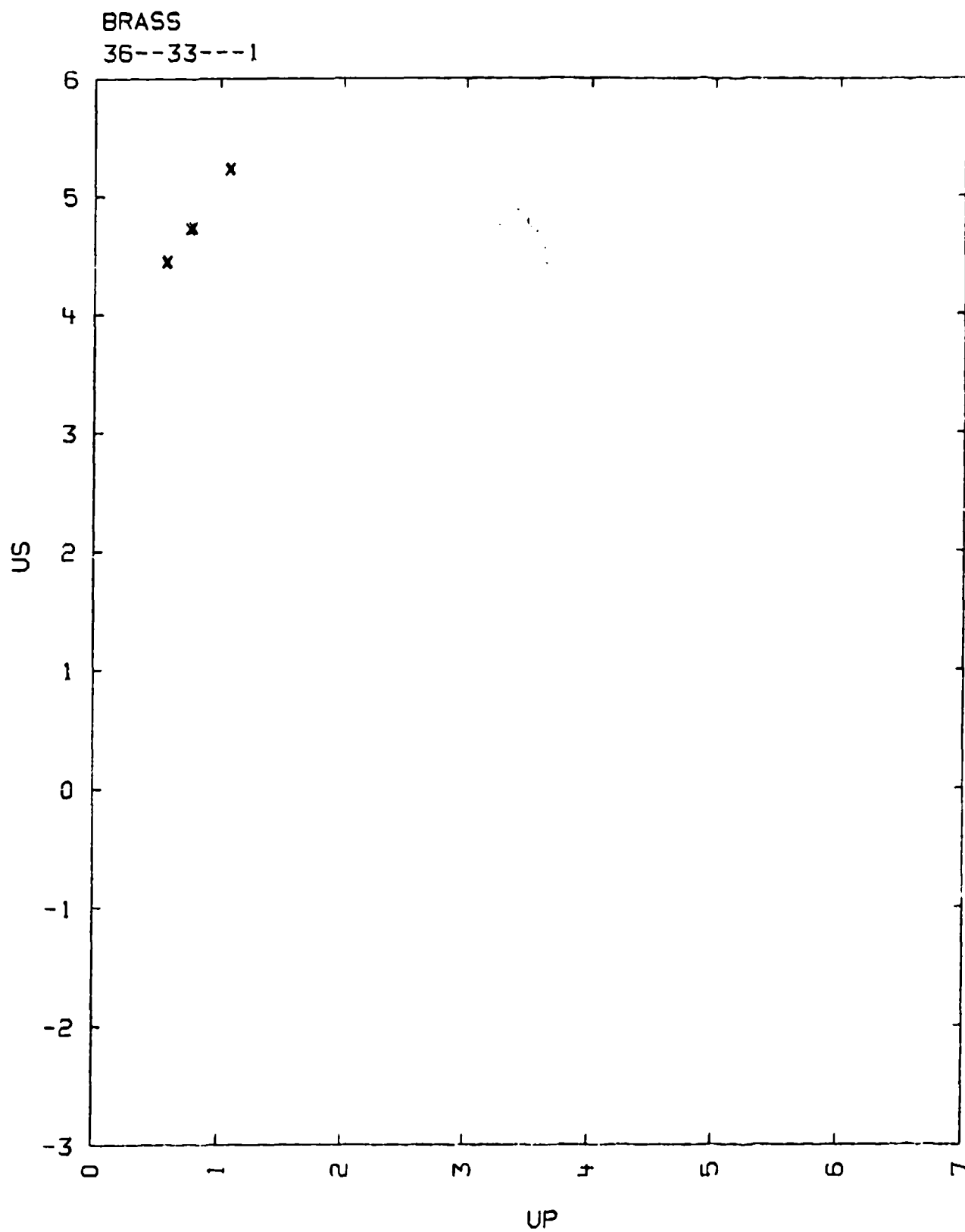
$US = 3.519 + 1.574 UP$

SIGMA 0.4 PERCENT

## COMMENTS:

- 1) SOURCE: WALSH, J. M., RICE, M. H., MCQUEEN, R. G. AND YARGER, F. L.  
PHYS. REV., VOL. 108, P. 169 FF. (1957)  
LOS ALAMOS SCIENTIFIC LABORATORY, GMX-6, LOS ALAMOS, N. MEX.
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE PROBABLE ERROR PER DATA POINT IS 0.7 PER CENT IN SHOCK VELOCITY  
FOR A GIVEN FREE SURFACE VELOCITY AND APPROXIMATELY 1 PERCENT IN  
COMPRESSION AT A GIVEN PRESSURE.
- 4) THE COMPOSITION WAS DETERMINED BY SPECTROCHEMICAL ANALYSIS

TABLE 1





36--33---2

BRASS

CU 61.5 PERCENT  
 ZN 36.0 PERCENT  
 PB 2.5 PERCENT  
 FE 0.05 PERCENT OR GREATER

 $V_0 = 0.1183 \text{ CC/G.}$ 

IN THE TABLE BELOW, VELOCITIES ARE GIVEN MM/MICROSEC.,  
 PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| RH00 | UFS  | US   | UP   | P    | V/V0  |
|------|------|------|------|------|-------|
| 8.45 | 0.90 | 4.38 | 0.45 | 167  | 0.897 |
| -    | 0.90 | 4.41 | 0.45 | 168  | 0.898 |
| -    | 1.01 | 4.50 | 0.50 | 192  | 0.888 |
| -    | 1.00 | 4.51 | 0.50 | 191  | 0.889 |
| -    | 1.12 | 4.54 | 0.56 | 214  | 0.877 |
| -    | 1.19 | 4.56 | 0.59 | 229  | 0.869 |
| -    | 1.40 | 4.77 | 0.70 | 282  | 0.853 |
| -    | 1.41 | 4.79 | 0.70 | 284  | 0.853 |
| -    | 1.82 | 5.10 | 0.91 | 391  | 0.822 |
| -    | 1.80 | 5.14 | 0.90 | 389  | 0.826 |
| -    | 1.92 | 5.15 | 0.96 | 415  | 0.814 |
| -    | 1.82 | 5.15 | 0.91 | 394  | 0.824 |
| -    | 1.89 | 5.17 | 0.94 | 411  | 0.818 |
| -    | 1.89 | 5.19 | 0.94 | 412  | 0.819 |
| -    | 3.50 | 6.22 | 1.72 | 906  | 0.723 |
| -    | 3.63 | 6.29 | 1.78 | 947  | 0.717 |
| -    | 3.72 | 6.39 | 1.82 | 985  | 0.715 |
| -    | 4.07 | 6.59 | 1.99 | 1108 | 0.698 |
| -    | 4.61 | 6.92 | 2.24 | 1308 | 0.677 |
| -    | 4.71 | 6.97 | 2.28 | 1342 | 0.673 |
| -    | 4.68 | 7.04 | 2.26 | 1348 | 0.679 |
| -    | 4.74 | 7.05 | 2.29 | 1365 | 0.675 |
| -    | 4.85 | 7.17 | 2.34 | 1420 | 0.674 |
| -    | 5.57 | 7.54 | 2.66 | 1694 | 0.648 |
| -    | 5.57 | 7.57 | 2.66 | 1702 | 0.649 |
| -    | 5.64 | 7.77 | 2.69 | 1764 | 0.654 |

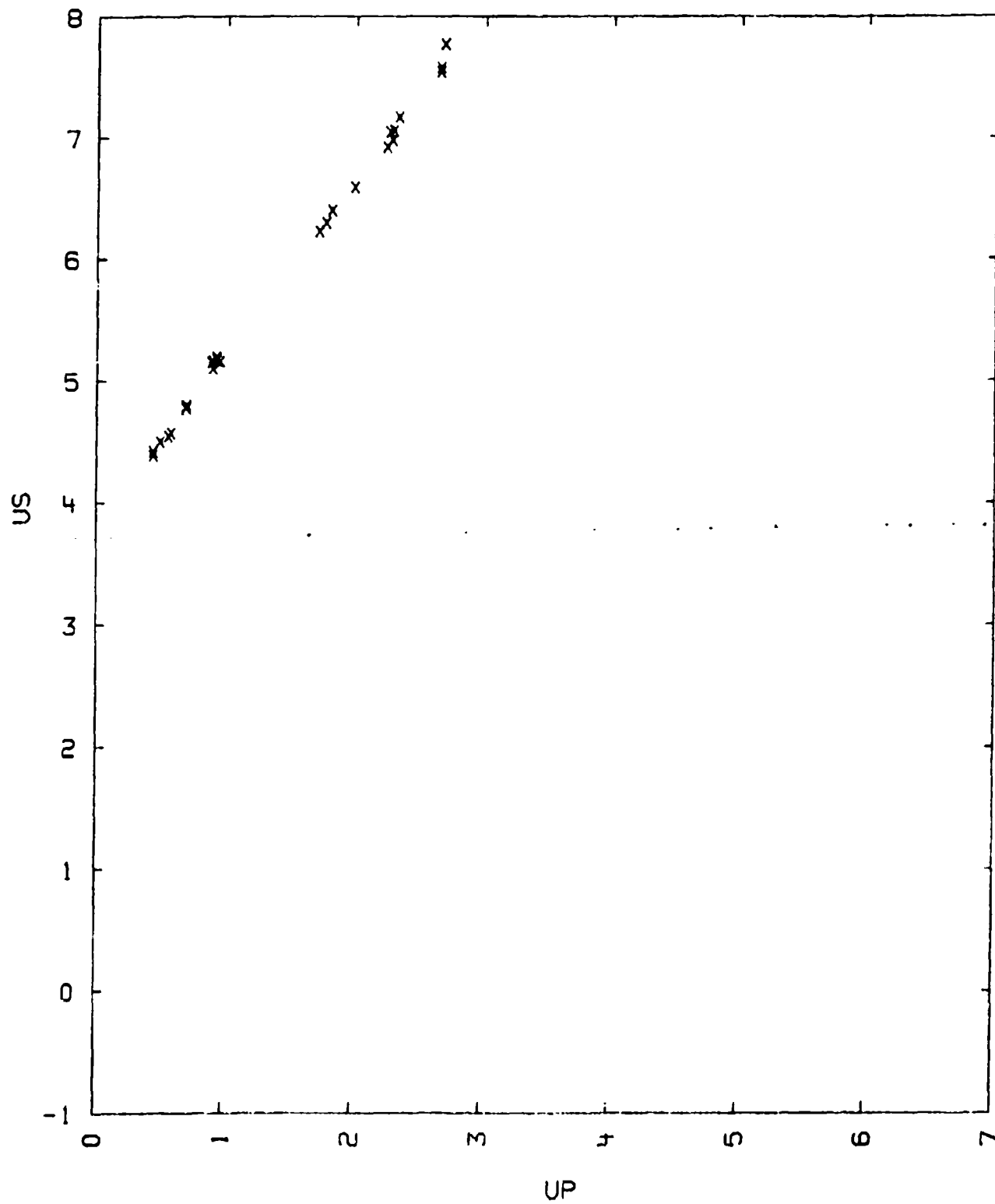
 $US = 3.791 + 1.431 \cdot UP \text{ KM/SEC} \quad \text{SIGMA US} = 0.051 \text{ KM/SEC}$ 

## COMMENTS:

- 1) SOURCE: MCQUEEN, R. G., AND MARSH, S. P.  
 J. APPL. PHYS., VOL. 31, P. 1253 (1960)  
 LOS ALAMOS SCIENTIFIC LABORATORY, GMX-6, LOS ALAMOS, N. MEX.

2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION TECHNIQUE D

TABLE I

BRASS  
36---33---2

36--33---3

BRASS

SVENSKA METALLVERKEN ALLOY 1163

CU 63.0 PERCENT

ZN 36.6 PERCENT

PB 0.4 PERCENT

VO = 0.118 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,  
AND PRESSURE IN KILOBARS.

TABLE

| RH00 | SAMPLE |      |      |      | V/VO  | PROJECTILE |
|------|--------|------|------|------|-------|------------|
|      | US     | UFS  | UP   | P    |       | VELOCITY   |
| 8.48 | 5.95   | 3.21 | 1.52 | 767  | 0.744 | 3.05       |
| -    | 6.12   | 3.34 | 1.58 | 806  | 0.742 | 3.16       |
| -    | 6.32   |      | 1.73 | 927  | 0.727 | 3.45       |
| -    | 6.65   |      | 2.07 | 1168 | 0.689 | 4.14       |

US = 4.19 + 1.20 UP KM/SEC

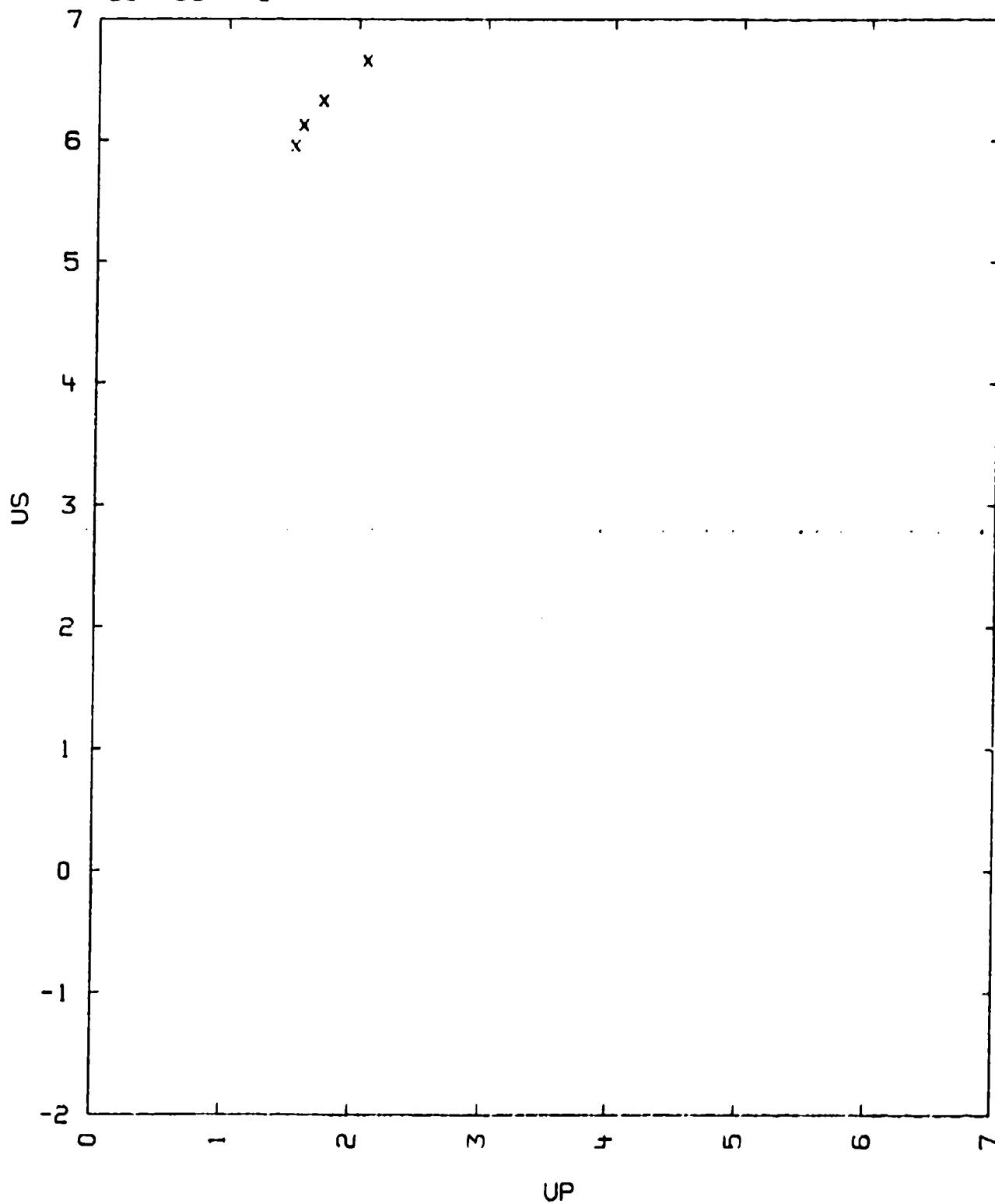
SIGMA US = 0.066 KM/SEC

## COMMENTS:

- 1) SOURCE: PERSSON, P. A., PERSSON, I.  
FOA 2 REPORT A 2299-222, SEPT. 1964.  
FORSVARTES FORSKNINGSANSTALT AVDELNING, SWEDEN.  
UCRL TRANSLATION 1173(L).
- 2) EXPERIMENTAL TECHNIQUE B.  
DATA REDUCTION TECHNIQUE B.
- 3) THE PARTICLE VELOCITY UP OF THE SAMPLE WAS TAKEN AS HALF THE PROJECTILE VELOCITY. (BRASS PROJECTILE WAS MOST LIKELY USED).
- 4) THE REPORTED RESULTS AGREE TO 1 PERCENT WITH DATA BY MCQUEEN, R. G., AND MARSH, S. P., J. APPL. PHYS., VOL. 31, P. 1253 (1960).

TABLE I

BRASS  
36--33---3



36--33---4

BRASS

CU 61.5 PERCENT  
 ZN 36.0 -  
 PB 2.5 -  
 FE .05 - OR GREATER

V0 = 0.1183 CC/G

THE TABLE BELOW LISTS PRESSURE (P IN KILOBARS), PARTICLE- SHOCK- AND FREE SURFACE VELOCITY (UP, US AND UFS IN KM/SEC.) OF THE HUGONIOT. THIS HUGONIOT MAY BE CALCULATED FROM THE LINEAR FIT BELOW THE TABLE. THE OTHER COLUMNS ARE THE COEFFICIENTS OF THE FIT TO THE ISENTROPIC CURVES

$$P = A1 \cdot (UFS - U) + A2 \cdot (UFS - U)^2 + \dots + A4 \cdot (UFS - U)^4,$$

WHICH IN THE P VS U PLANE PASS THROUGH THE HUGONIOT AT THE LISTED POINTS THE DENSITY AT THE FOOT OF THE HUGONIOT IS 8.450 G/CC.

TABLE

| RHO0  | US     | UP    | UFS   | P      | A1     | A2     | A3    | A4    |
|-------|--------|-------|-------|--------|--------|--------|-------|-------|
| 8.453 | 3.9369 | 0.100 | 0.200 | 33.3   | 321.29 | 117.70 | -0.24 | 1.17  |
| -     | 5.0764 | 0.900 | 1.809 | 386.1  | 320.22 | 113.14 | 1.37  | 0.89  |
| -     | 6.0736 | 1.600 | 3.246 | 821.1  | 318.61 | 99.24  | 5.80  | 0.18  |
| -     | 6.7858 | 2.100 | 4.300 | 1204.1 | 316.34 | 86.85  | 8.80  | -0.24 |
| -     | 7.4981 | 2.600 | 5.435 | 1647.3 | 256.32 | 115.31 | -4.25 | 1.40  |
| -     | 8.0678 | 3.000 | 6.346 | 2045.2 | 235.36 | 113.08 | -4.62 | 1.31  |

$$US = 3.79446 + 1.42446 UP \quad \text{KM/SEC.}$$

## COMMENTS:

- 1) SOURCE: MARSH, S. P.  
 PRIVATE COMMUNICATION (1965)  
 GMX-6, LOS ALAMOS SCIENTIFIC LABORATORY  
 LOS ALAMOS, NEW MEXICO.

- 2) EXPERIMENTAL TECHNIQUE : NONE

DATA REDUCTION METHOD: D

THE ISENTROPES WERE CALCULATED WITH A CONSTANT VALUE OF 0.0518 CC/G FOR THE PARTIAL DERIVATIVE AT CONSTANT VOLUME (DE/DP). FURTHERMORE THE ABOVE HUGONIOT RELATION BETWEEN US AND UP WAS USED, CONSISTENT WITH BRASS DATA FROM THE SAME SOURCE

- 3) MAXIMUM ERRORS FOR THE ISENTROPE FITS TO THE ABOVE COMPUTER OUTPUT ARE AS FOLLOWS:

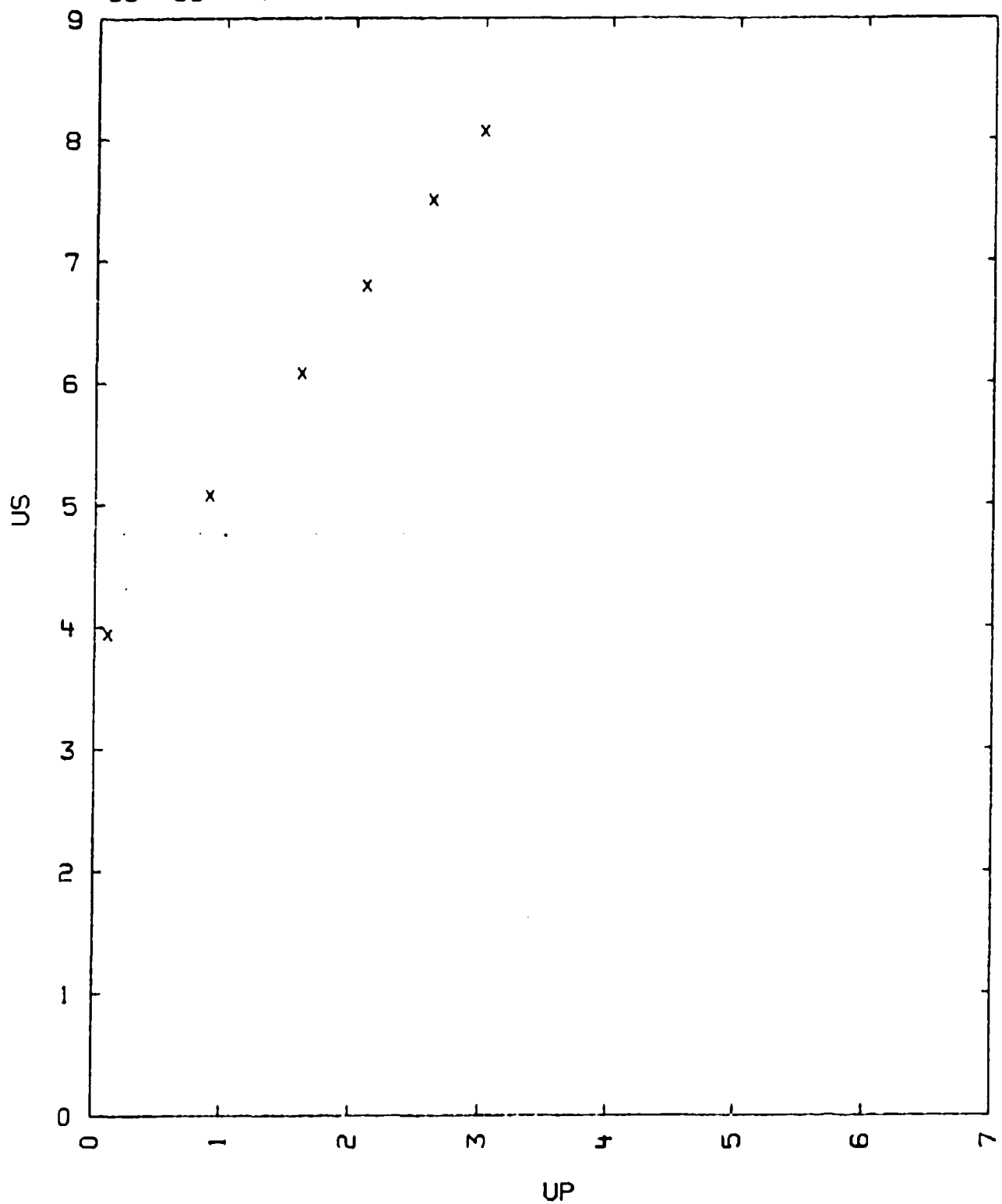
ENTRY 1: LESS THAN 0.1 KBAR OVER THE TOTAL PRESSURE RANGE

- 2: 0.6 KBAR BELOW- AND 0.04 KBAR ABOVE 80 KBAR
- 3: 2.1 KBAR BELOW- AND 0.3 KBAR ABOVE 120 KBAR
- 4: 2.9 KBAR BELOW- AND 0.6 KBAR ABOVE 160 KBAR
- 5: -9.2 KBAR BELOW- AND 0.3 KBAR ABOVE 170 KBAR
- 6: -9.2 KBAR BELOW- AND 0.2 KBAR ABOVE 220 KBAR

- 4) THE ERROR AT LOW PRESSURE OCCURS AT THE VOLUME OF THE 300 DEGREE KELVIN SAMPLE. IT TAKES THE FORM OF A DISCONTINUITY IN THE SLOPE OF THE CALCULATED ADIABAT. WHILE THE VALUE OF THE FREE SURFACE IS NOT AFFECTED BY THIS PECULIARITY OF THE CODE OUTPUT, THE FRACTIONAL UNCERTAINTY IS LARGER BELOW THE PRESSURE LISTED IN COMMENT 3
- 5) THE MAXIMUM PRESSURE TO WHICH THE ABOVE FITS ARE VALID RANGE FROM 1800 KBARS FOR THE FIRST LINE TO 2300 KBARS FOR THE LAST TABLE ENTRY

TABLE I

BRASS  
36--33---4





39--57---1  
TITANIUM-NICKEL ALLOY

NI 50.3 WT. PERCENT  
TI 49.7 - -

V0 = 0.1548 CC/G  
V01 = 0.1542 CC/G

CO = 3.80 KM/SEC.

THE TABLE LISTS VELOCITY IN KM/SEC., PRESSURE IN KBAR., DENSITY IN G/CC.  
AND INITIAL TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| TO  | RH00 | US   | UP    | P    | V/V0  |
|-----|------|------|-------|------|-------|
| 15  | 6.46 | 4.54 | 0.268 | 78.5 | 0.941 |
| -   | -    | 4.92 | 0.413 | 131. | 0.916 |
| -   | -    | 5.19 | 0.490 | 164. | 0.906 |
| -   | -    | 5.48 | 0.580 | 205. | 0.894 |
| -   | -    | 5.55 | 0.665 | 238. | 0.880 |
| -   | -    | 5.68 | 0.637 | 233. | 0.888 |
| -   | -    | 5.83 | 0.725 | 273. | 0.876 |
| -   | -    | 5.88 | 0.730 | 277. | 0.876 |
| -   | -    | 6.05 | 0.720 | 281. | 0.881 |
| -   | -    | 6.15 | 1.07  | 425. | 0.826 |
| -   | -    | 6.45 | 1.14  | 475. | 0.823 |
| -   | -    | 6.52 | 1.21  | 510. | 0.814 |
| -   | -    | 7.01 | 1.38  | 625. | 0.803 |
| -   | -    | 7.65 | 1.42  | 702. | 0.814 |
| -   | -    | 7.72 | 1.54  | 768. | 0.801 |
| 115 | 6.46 | 4.81 | 0.328 | 102. | 0.932 |
| -   | -    | 5.33 | 0.610 | 210. | 0.880 |
| -   | -    | 5.53 | 0.718 | 256. | 0.870 |
| -   | -    | 5.95 | 1.04  | 400. | 0.825 |
| -   | -    | 6.15 | 1.14  | 453. | 0.815 |
| -   | -    | 6.19 | 1.23  | 492. | 0.801 |
| -   | -    | 6.61 | 1.32  | 564. | 0.800 |

AT 15 DEG.

US = A + B\*UP ; A=4.04 B=2.38 FOR UP LESS THAN 0.8 KM/SEC.

SIG.A = 0.09 KM/SEC. SIG.B = 0.16

A=2.27 B=3.62 FOR UP GREATER THAN 0.8 KM/SEC.

SIG.A = 0.38 KM/SEC SIG.B = 0.30

COMMENTS:

- 1) SOURCE: COLEBURN, N. L.  
REPORT NOLTR 67-78 (1967)  
EXPLOSION DYN. DIV., EXPL. RES. DEP.  
US NAVAL ORDNANCE LAB., WHITE OAK, MD, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: C1.  
DATA REDUCTION TECHNIQUE: D1.

3) THE ALLOY WAS PREPARED BY ARC CASTING THE MIXTURE AND SWAGING AT 925 DEG. CENTIGRADE. 30 MINUTES ANNEALING AT 950 DEG., PRECEDED FINAL COOLING.

4) KNOOP HARDNESS OF SHOCK COMPRESSED AND RECOVERED SMAPLES:

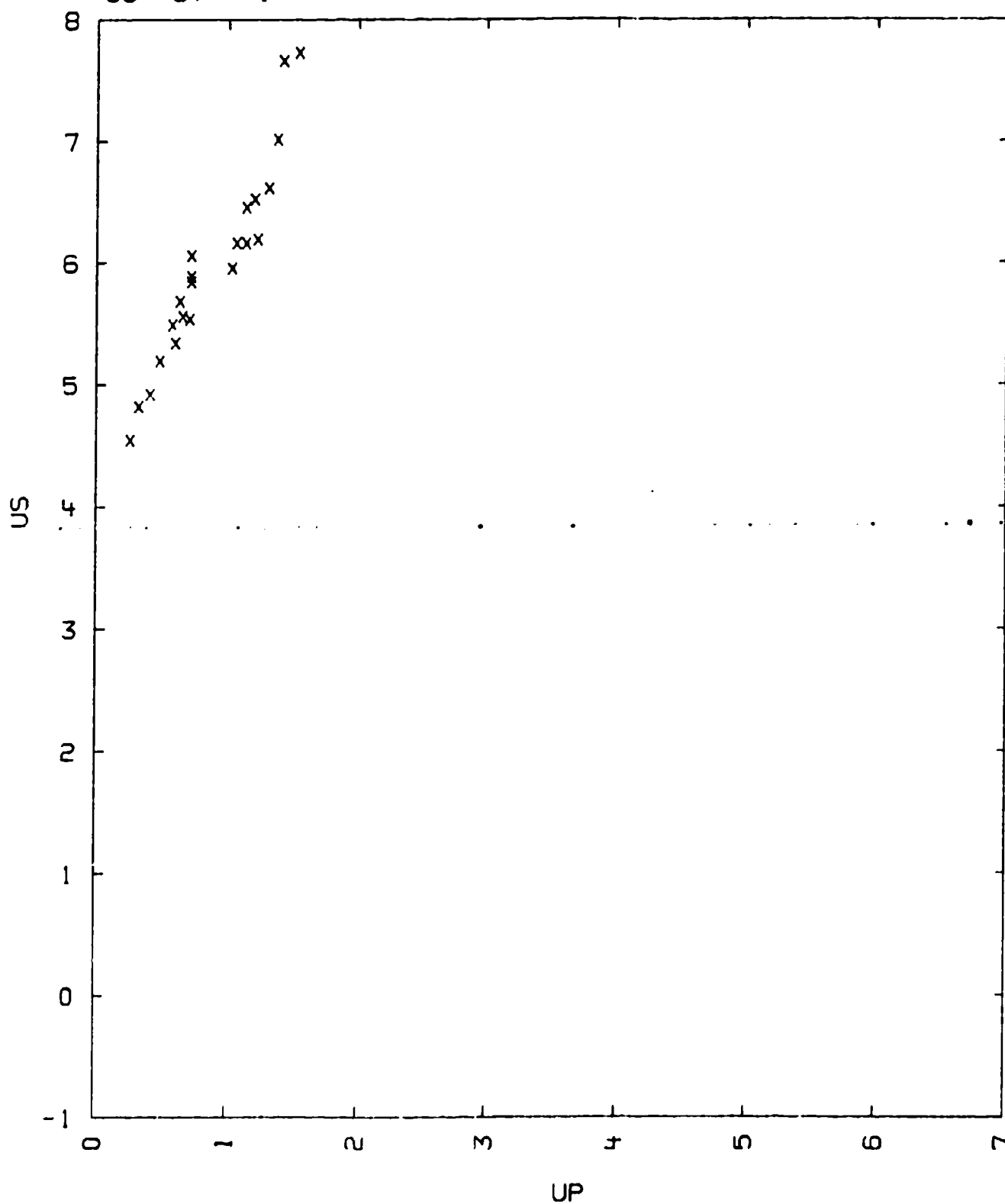
| PMAX | K   |
|------|-----|
| 0    | 93  |
| 35   | 101 |
| 45   | 115 |
| 65   | 116 |
| 90   | 123 |
| 340  | 175 |

5) V01 WAS CALCULATED FROM A SMOOTH FIT OF THE CUBE ROOT OF THE ATOMIC VOLUME VERSUS ATOM PERCENT TI. POOLE AND HUME-ROTHERY LATTICE PARAMETERS AS LISTED BY PEARSON, METAL PHYSICS AND PHYSICAL METALLURGY (PERGAMON PRESS, NEW-YORK, 1958), WERE USED.

6) THE TWO SEGMENTS OF THE US,UP LINE OF THIS MATERIAL WERE SUGGESTED BY THE AUTHORS TO BELONG TO THE TWO PHASES OF A MARTENSITIC TRANSFORMATION.

TABLE I

TITANIUM-NICKEL ALLOY  
39--57---1



39--57---2  
TITANIUM-NICKEL ALLOY

NI 51.4 WT. PERCENT  
TI 48.6 - -

V0 = 0.1536

V01 = 0.1528

THE TABLE LISTS VELOCITY IN KM/SEC., PRESSURE IN KBAR., DENSITY IN G/CC.  
AND INITIAL TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| TO  | RH00 | US   | UP    | P    | V/V0  |
|-----|------|------|-------|------|-------|
| 15  | 6.51 | 4.73 | 0.279 | 85.9 | 0.941 |
| -   | -    | 5.01 | 0.400 | 130. | 0.920 |
| -   | -    | 5.08 | 0.495 | 164. | 0.903 |
| -   | -    | 5.56 | 0.673 | 244. | 0.879 |
| -   | -    | 5.64 | 0.664 | 244. | 0.882 |
| -   | -    | 5.70 | 0.735 | 273. | 0.871 |
| -   | -    | 5.88 | 0.720 | 275. | 0.878 |
| -   | -    | 5.89 | 0.725 | 278. | 0.877 |
| -   | -    | 6.08 | 0.980 | 388. | 0.839 |
| -   | -    | 6.46 | 1.20  | 505. | 0.815 |
| -   | -    | 6.48 | 1.20  | 506. | 0.815 |
| -   | -    | 7.46 | 1.48  | 714. | 0.808 |
| -   | -    | 7.52 | 1.56  | 764. | 0.792 |
| 115 | 6.51 | 4.97 | 0.328 | 106. | 0.934 |
| -   | -    | 5.63 | 0.695 | 255. | 0.877 |
| -   | -    | 6.01 | 1.05  | 411. | 0.825 |
| -   | -    | 6.21 | 1.13  | 457. | 0.818 |
| -   | -    | 6.65 | 1.29  | 558. | 0.806 |

US = A + B\*UP AT 15 DEG:

A = 4.00 B = 2.45 FOR UP LESS THAN 0.8 KM/SEC

SIG.A = 0.10 KM/SEC. SIG.B = 0.15 KM/SEC

A = 3.32 B = 2.75 FOR UP GREATER THAN 0.8 KM/SEC.

SIG.A = 0.22 KM/SEC. SIG.B = 0.17 KM/SEC

COMMENTS:

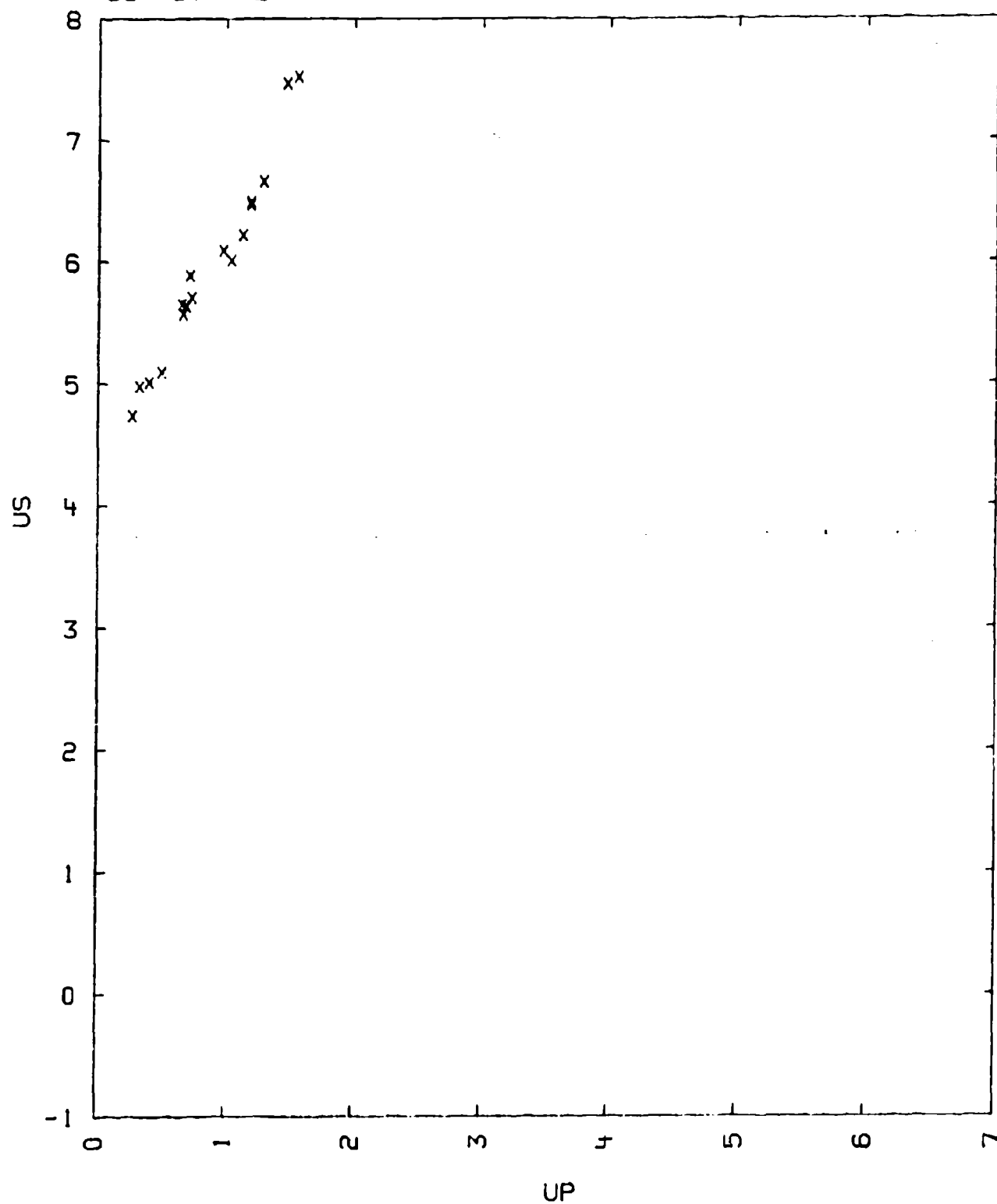
- 1) SOURCE: COLEBURN, N. L.  
REPORT NOLTR 67-78 (1967)  
EXPLOSION DYN. DIV., EXPL. RES. DEP.  
US NAVAL ORDNANCE LAB., WHITE OAK, MD, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: C1.  
DATA REDUCTION TECHNIQUE: D1.
- 3) THE ALLOY WAS PREPARED BY ARC CASTING THE MIXTURE AND SWAGING AT 925 DEG. CENTIGRADE. 30 MINUTES ANNEALING AT 950 DEG., PRECEDED FINAL COOLING.
- 4) KNOOP HARDNES OF SHOCK COMPRESSED AND RECOVERED SAMPLES

| PMAX | K   |
|------|-----|
| 0    | 157 |
| 35   | 178 |
| 45   | 185 |
| 65   | 193 |
| 90   | 205 |

- 5) V01 WAS CALCULATED FROM A SMOOTH FIT OF THE CUBE ROOT OF THE ATOMIC VOLUME VERSUS ATOM PERCENT TI. POOLE AND HUME-ROTHERY LATTICE PARAMETERS AS LISTED BY PEARSON, METAL PHYSICS AND PHYSICAL METALLURGY (PERGAMON PRESS, NEW-YORK, 1958), WERE USED.
- 6) THE TWO SEGMENTS OF THE US,UP LINE ARE PROBABLY RELATED TO THE TRANSFORMATION OBSERVED IN THE 50-50 COMPOSITION.

TABLE I

TITANIUM-NICKEL ALLOY  
39--57---2



39--57---3  
TITANIUM-NICKEL ALLOY

NI 55.0 WT. PERCENT  
TI 45.0 WT. PERCENT

V0 = 0.1490 CC/G  
V01 = 0.1488 CC/G

THE TABLE LISTS VELOCITY IN KM/SEC., PRESSURE IN KBAR., DENSITY IN G/CC.  
AND INITIAL TEMPERATURE IN DEG. CENTIGRADE.

TABLE

| T0 | RH00 | US   | UP    | P    | V/V0  |
|----|------|------|-------|------|-------|
| 15 | 6.71 | 4.76 | 0.280 | 89.4 | 0.941 |
| -  | -    | 5.56 | 0.660 | 246. | 0.881 |
| -  | -    | 5.67 | 0.669 | 256. | 0.882 |
| -  | -    | 5.69 | 0.618 | 236. | 0.891 |
| -  | -    | 5.78 | 0.705 | 273. | 0.878 |
| -  | -    | 5.90 | 0.725 | 287. | 0.877 |
| -  | -    | 6.48 | 1.17  | 509. | 0.819 |
| -  | -    | 6.49 | 1.20  | 523. | 0.815 |
| -  | -    | 6.74 | 1.41  | 638. | 0.791 |
| -  | -    | 7.17 | 1.58  | 760. | 0.780 |
| -  | -    | 4.61 | 0.320 | 99.0 | 0.931 |
| -  | -    | 5.37 | 0.625 | 225. | 0.884 |
| -  | -    | 5.39 | 0.710 | 257. | 0.868 |
| -  | -    | 6.00 | 1.03  | 415. | 0.828 |
| -  | -    | 6.21 | 1.06  | 442. | 0.829 |
| -  | -    | 6.53 | 1.15  | 504. | 0.824 |

US = A + B\*UP AT 15 DEG:

A = 4.08 KM/SEC B = 2.42 FOR UP LESS THAN 0.8  
SIG.A = 0.11 KM/SEC. SIG.B = 0.16

A = 4.51 KM/SEC B = 1.65 FOR UP GREATER THAN 0.8  
SIG.A = 0.24 KM/SEC. SIG.B = 0.18

## COMMENTS:

- 1) SOURCE: COLEBURN, N. L.  
REPORT NOLTR 67-78 (1967)  
EXPLOSION DYN. DIV., EXPL. RES. DEP.  
US NAVAL ORDNANCE LAB., WHITE OAK, MD, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: C1.  
DATA REDUCTION TECHNIQUE: D1.
- 3) THE ALLOY WAS PREPARED BY ARC CASTING THE MIXTURE AND SWAGING AT 925 DEG. CENTIGRADE. 30 MINUTES ANNEALING AT 950 DEG., PRECEDED FINAL COOLING.
- 4) KNOOP HARDNES OF SHOCK COMPRESSED AND RECOVERED SAMPLES  
P MAX K  
0 168.

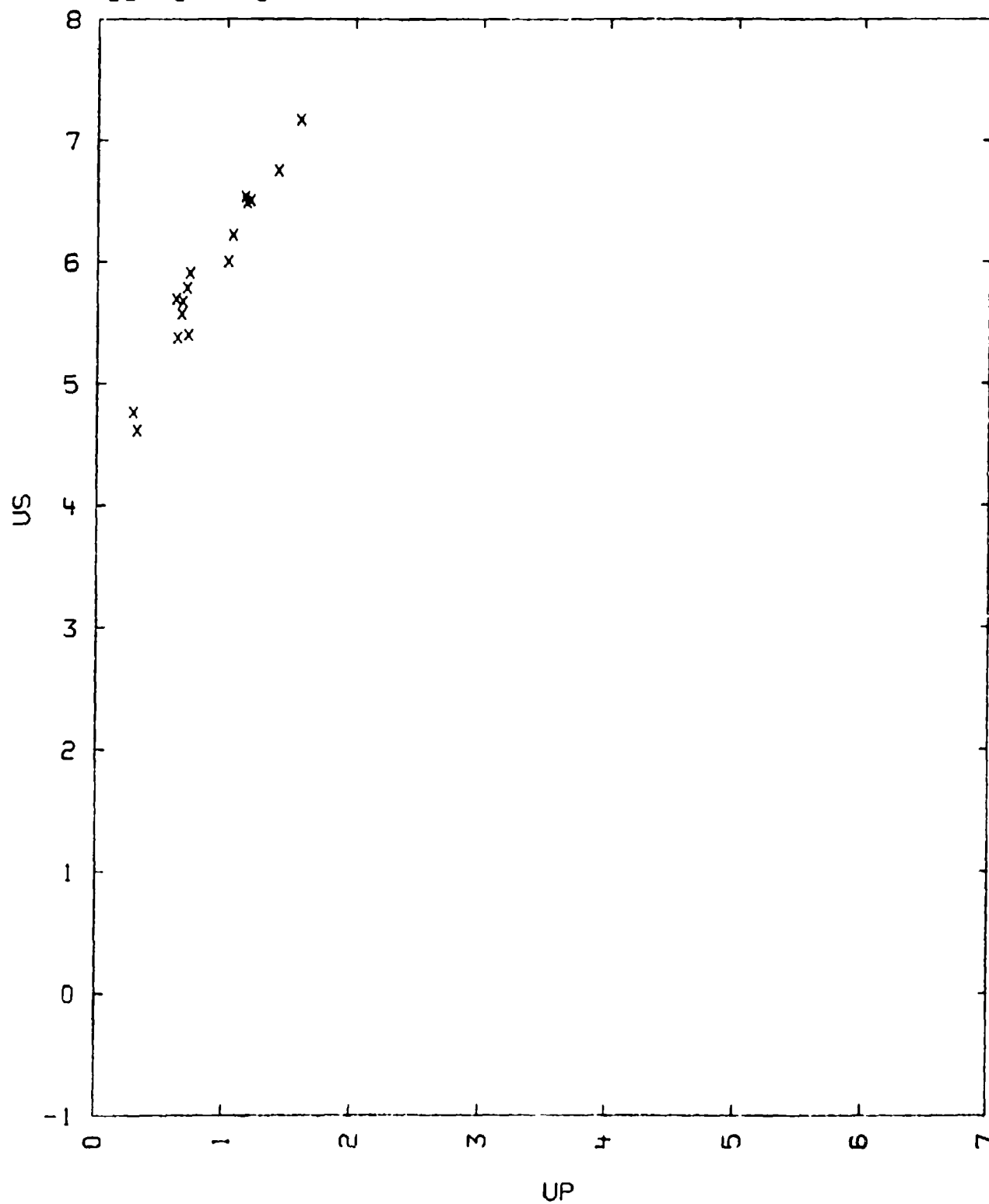
35 183.  
90 225

- 5) VOI WAS CALCULATED FROM A SMOOTH FIT OF THE CUBE ROOT OF THE ATOMIC VOLUME VERSUS ATOM PERCENT TI. POOLE AND HUME-ROTHERY LATTICE PARAMETERS AS LISTED BY PEARSON. METAL PHYSICS AND PHYSICAL METALLURGY (PERGAMON PRESS, NEW-YORK, 1958), WERE USED.
- 6) THE TWO SEGMENTS OF THE US,UP LINE ARE PROBABLY RELATED TO THE TRANSFORMATION OBSERVED IN THE 50-50 COMPOSITION.



TABLE I

TITANIUM-NICKEL ALLOY  
39--57---3



36-1--23-18-2-1(200-10-286-33)---1  
COPPER OXIDE- EPOXY

|                     |                         |               |
|---------------------|-------------------------|---------------|
| COPPEROXIDE         | CU-O                    | 44 WT PERCENT |
| EPOXY               | C200-N10-H286-033)      | 56 WT PERCENT |
| EPON 815            | C200-H261-036.          | 90 WT PERCENT |
| DIETHYLENETRIAMINE, | H-N(-C(H2)-C(H2)-N-H2)2 | 10 WT PERCENT |

$V_0 = 0.566 - 0.606 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |       |
|------------------|------|------|------|--------|--------------------|-------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |       |
| 1.761            | 4.25 | 1.28 | 96.  | 0.6988 | 2024 AL            | 6.56  |
| 1.684            | 4.85 | 1.65 | 135. | 0.6598 | 2024 AL            | 6.94  |
| 1.717            | 5.73 | 2.18 | 214. | 0.6195 | 2024 AL            | 7.54  |
| 1.682            | 7.74 | 3.73 | 486. | 0.5181 | 2024 AL            | 9.24  |
| 1.651            | 8.20 | 3.99 | 540. | 0.5134 | 2024 AL            | 9.53  |
| 1.766            | 8.76 | 4.44 | 687. | 0.4932 | 2024 AL            | 10.10 |

$US = 2.110 + 1.767 \cdot UP - 0.062 \cdot UP^2 \text{ KM/SEC}$   
SIG US = 0.071 KM/SEC

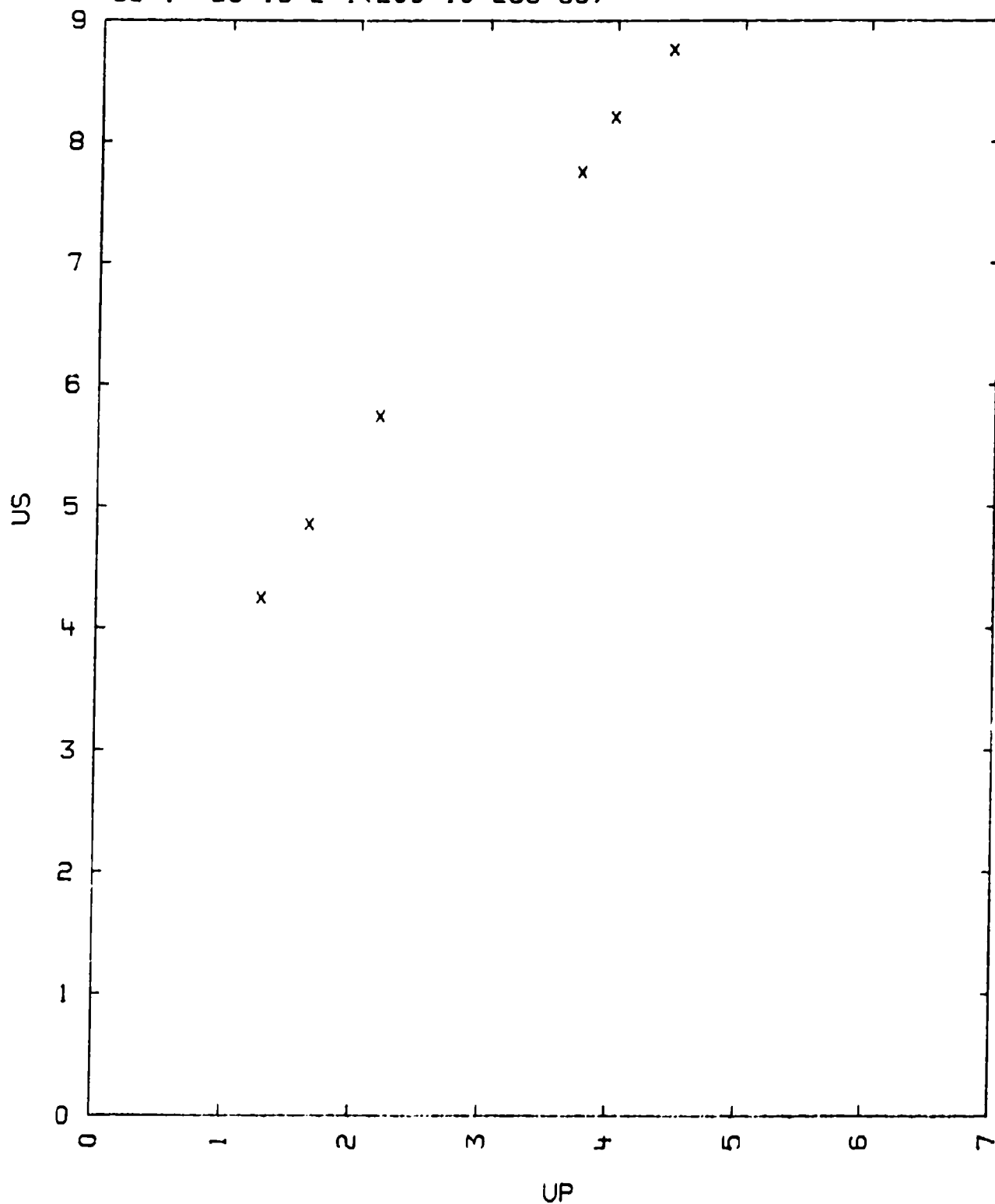
## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) THE EPON 815 COMPOSITION WAS OBTAINED FROM P. FLEMING, PRIVATE COM-  
MUNICATION. (L.L. LAP, LIVERMORE, CA 1975) ALSO SEE MODERN PLASTICS  
ENCYCLOPEDIA (MC GRAW HILL, N.Y., 1975) VOL. 51

TABLE I

COPPER OXIDE- EPOXY

36-1--23-18-2-1(200-10-286-33)



38--25---1  
GOLD- GERMANIUM

AU 94.2 WT PERCENT NOTE 3  
GE 5.8 WT PERCENT

VO = 0.0591 - 0.0596 CC/G CL = 3.326 KM/SEC CO = 2.95 KM/SEC  
CS = 1.329 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RHO0             | US   | UP   | P     | V/VO   | MATERIAL           | US(ST) |
| 16.880           | 3.23 | 0.29 | 158.  | 0.9102 | CU                 | 4.45   |
| 16.820           | 3.29 | 0.42 | 232.  | 0.8723 | CU                 | 4.67   |
| 16.850           | 3.61 | 0.60 | 365.  | 0.8338 | CU                 | 4.98   |
| 16.880           | 4.19 | 0.88 | 622.  | 0.7900 | CU                 | 5.51   |
| 16.830           | 4.86 | 1.29 | 1055. | 0.7346 | CU                 | 6.23   |
| 16.910           | 5.71 | 1.80 | 1738. | 0.6848 | CU                 | 7.16   |
| 16.760           | 6.14 | 2.09 | 2151. | 0.6596 | CU                 | 7.65   |

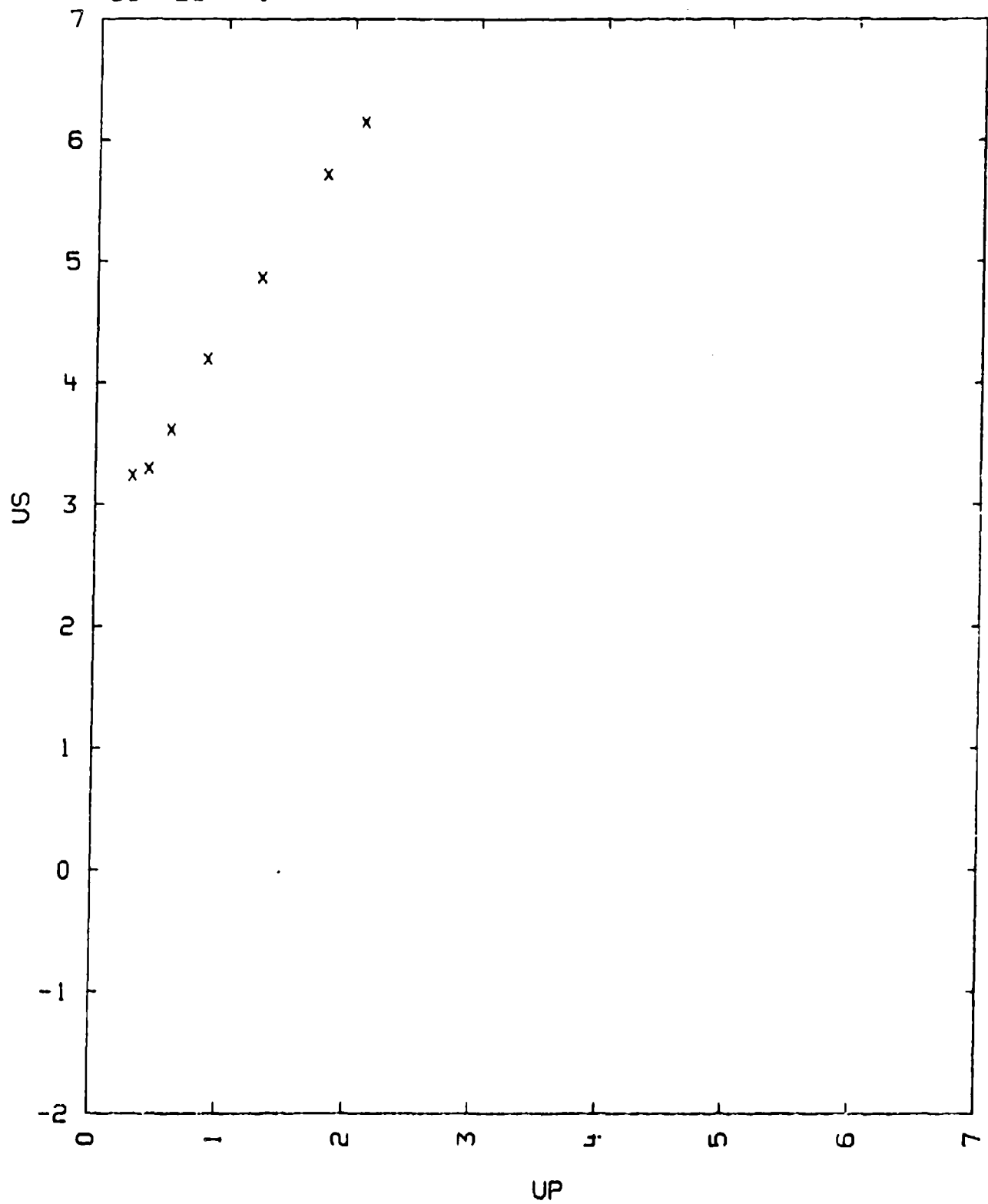
US =  $2.430 + 2.099 \cdot UP - 0.155 \cdot UP^2$  KM/SEC FOR UP ABOVE 0.4 KM/SEC  
SIG US = 0.026 KM/SEC

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) THE COMPOSITION WAS CALCULATED FROM THE DENSITY, ASSUMING VOLUME  
ADDITIVITY.

TABLE I

GOLD- GERMANIUM  
38--25---1



38--25---2  
GOLD- GERMANIUM

AU 90.7 WT PERCENT NOTE 3  
GE 9.3 WT PERCENT

VO = 0.0643 - 0.0646 CC/G CL = 3.388 KM/SEC CO = 2.94 KM/SEC  
CS = 1.465 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RH00             | US   | UP   | P     | V/VO   | MATERIAL           | US(ST) |
| 15.460           | 3.23 | 0.30 | 150.  | 0.9071 | CU                 | 4.45   |
| 15.480           | 3.45 | 0.64 | 342.  | 0.8145 | CU                 | 4.98   |
| 15.510           | 4.05 | 0.94 | 590.  | 0.7679 | CU                 | 5.51   |
| 15.550           | 4.81 | 1.34 | 1002. | 0.7214 | CU                 | 6.23   |
| 15.490           | 5.34 | 1.67 | 1381. | 0.6873 | CU                 | 6.79   |
| 15.480           | 5.34 | 1.67 | 1380. | 0.6873 | CU                 | 6.79   |
| 15.840           | 5.73 | 1.86 | 1688. | 0.6754 | CU                 | 7.16   |
| 15.520           | 6.15 | 2.16 | 2062. | 0.6488 | CJ                 | 7.65   |

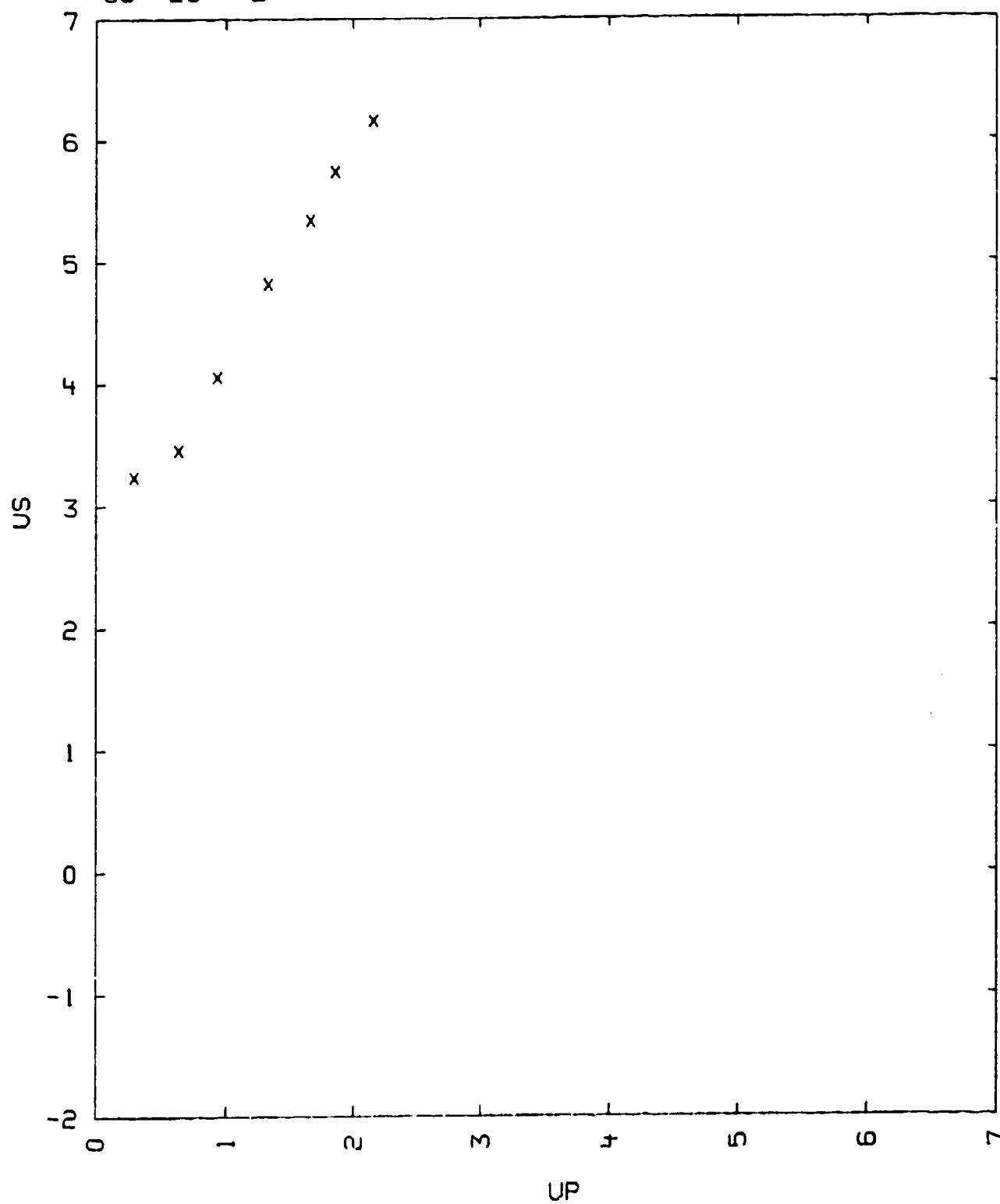
US = 2.090 + 2.235\*UP - 0.163\*UP\*\*2 KM/SEC FOR UP ABOVE .5 KM/SEC  
SIG.US = 0.032 KM/SEC

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE : B  
DATA REDUCTION TECHNIQUE : B
- 3) THE COMPOSITION WAS CALCULATED FROM THE DENSITY ASSUMING VOLUME  
ADDITIVITY OF THE COMPONENTS.

TABLE 1

GOLD- GERMANIUM  
38--25---2



41--24---1  
IRON-SILICON MIXTURE

FE 79.8 WT. PERCENT  
SI 19.8 WT. PERCENT  
W 0.3-0.4 WT. PERCENT

$V_0 = 0.1425 \text{ CC/G}$   
 $V_{01} = 0.1430 \text{ CC/G.}$

IN THE TABLE BELOW, THE DENSITY IS GIVEN IN G/CC, VELOCITIES ARE IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| RH00  | US    | UF    | P     | V/V0  |
|-------|-------|-------|-------|-------|
| 7.016 | 6.323 | 0.780 | 346.  | 0.877 |
| -     | 6.588 | 1.047 | 484.  | 0.841 |
| -     | 7.199 | 1.353 | 683.  | 0.812 |
| -     | 7.354 | 1.448 | 747.  | 0.803 |
| -     | 7.596 | 1.638 | 872.  | 0.784 |
| -     | 7.651 | 1.856 | 996.  | 0.757 |
| -     | 7.656 | 1.805 | 969.  | 0.764 |
| -     | 7.732 | 1.832 | 994.  | 0.763 |
| -     | 7.732 | 1.897 | 1029. | 0.755 |
| -     | 7.887 | 2.016 | 1116. | 0.744 |
| -     | 8.125 | 2.193 | 1250. | 0.730 |
| -     | 8.436 | 2.569 | 1521. | 0.695 |
| -     | 8.635 | 2.516 | 1524. | 0.709 |
| -     | 8.979 | 2.960 | 1865. | 0.670 |
| -     | 9.287 | 3.126 | 2037. | 0.663 |
| -     | 9.317 | 3.134 | 2048. | 0.664 |
| -     | 9.615 | 3.185 | 2148. | 0.669 |
| -     | 9.939 | 3.627 | 2529. | 0.635 |

$$US = 5.444 + 1.235 \cdot UP \text{ KM/SEC.} \quad \text{SIGMA US} = 0.103 \text{ KM/SEC}$$

## COMMENTS:

- 1) SOURCE: BALCHAN, A. S. AND COWAN, G. R.  
JOURNAL OF GEOPHYSICAL RESEARCH, VOL. 71, P. 3577, (1966)
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION TECHNIQUE B  
STANDARD MATERIAL IS NICKEL
- 3) THE STANDARD HUGONOT WAS OBTAINED FROM THE FOLLOWING EQUATION:  
 $US = 4.612 + 1.523 \cdot UP - 0.0148 \cdot UP^2 \text{ KM/SEC.}$   
THIS EQUATION IS A COMPOSITE FIT OF DATA OBTAINED FROM WALSH, J. H.,  
ET AL., MATERIAL 39---1, MCQUEEN, R. G. AND MARSH, S. P., MATERIAL  
39---2 AND AL TSHULER, L. V., ET AL., MATERIAL 39---3.
- 4) THE INITIAL DENSITY (RH00) IS A AVERAGE DENSITY.
- 5) A SHOCK TILT CORRECTION WAS APPLIED TO THE MEASURED SHOCK VELOCITIES  
FOR BOTH THE DRIVER PLATE AND SAMPLE.
- 6) SEE MATERIAL 41---15 FOR A DIFFERENT COMPOSITION

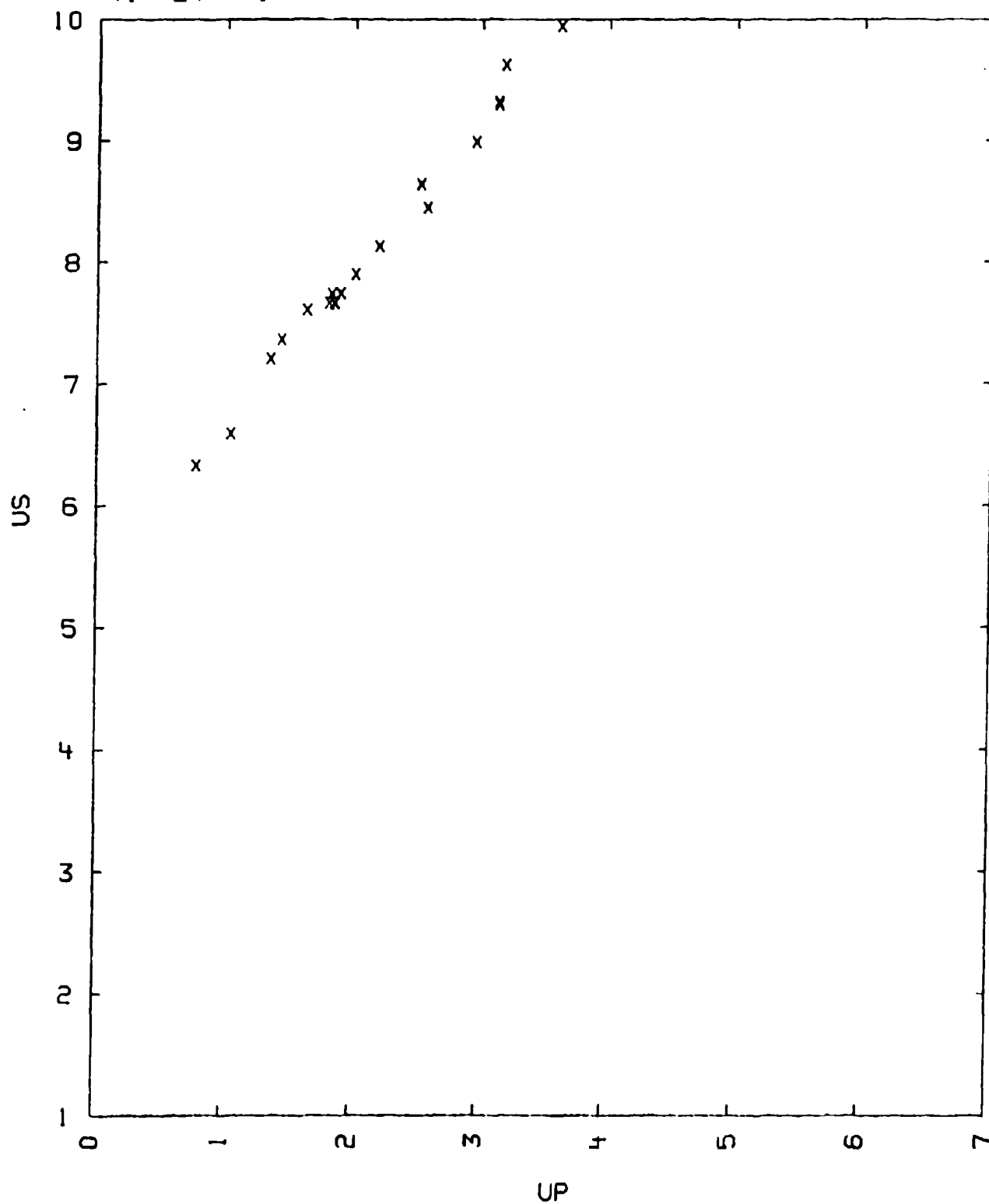


- 7) VOI WAS CALCULATED WITH A BODY CENTERED LATTICE PARAMETER OF 2.8101  
+OR- 5 ANGSTROM; W. B. PEARSON, HANDBOOK OF LATTICE SPACINGS AND  
STRUCTURES OF METALS, VOL. 4 ( PERGAMON PRESS, NEW-YORK, 1958).  
0.001 ANGSTROM WAS ADDED TO THE LATTICE PARAMETER OF FE-SI AS A  
CORRECTION FOR THE W CONTENT.

TABLE I

IRON-SILICON MIXTURE

41--24---1



41--39---1  
IRON-NICKEL ALLOY

FE 90 WT PERCENT  
NI 10 WT PERCENT

V0 = 0.1269 CC/G  
V01 = 0.1267 CC/G

C0 = 4.46 KM/SEC

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RH00             | US   | UP   | P     | V/V0   | MATERIAL           | US(ST) |
| 7.883            | 5.39 | 1.04 | 442.  | 0.8071 | CU                 | 5.40   |
| 7.885            | 5.41 | 1.09 | 465.  | 0.7985 | CU                 | 5.47   |
| 7.883            | 6.38 | 1.60 | 805.  | 0.7492 | CU                 | 6.22   |
| 7.895            | 6.47 | 1.63 | 833.  | 0.7481 | CU                 | 6.27   |
| 7.883            | 6.79 | 1.80 | 963.  | 0.7349 | CU                 | 6.53   |
| 7.896            | 7.71 | 2.38 | 1449. | 0.6913 | CU                 | 7.37   |
| 7.885            | 8.00 | 2.54 | 1602. | 0.6825 | CU                 | 7.61   |
| 7.896            | 8.02 | 2.55 | 1615. | 0.6820 | CU                 | 7.63   |
| 7.870            | 7.98 | 2.58 | 1620. | 0.6767 | CU                 | 7.65   |
| 7.883            | 8.27 | 2.75 | 1793. | 0.6675 | CU                 | 7.92   |

US = 3.626 + 1.711\*UP KM/SEC  
SIG US = 0.058 KM/SEC

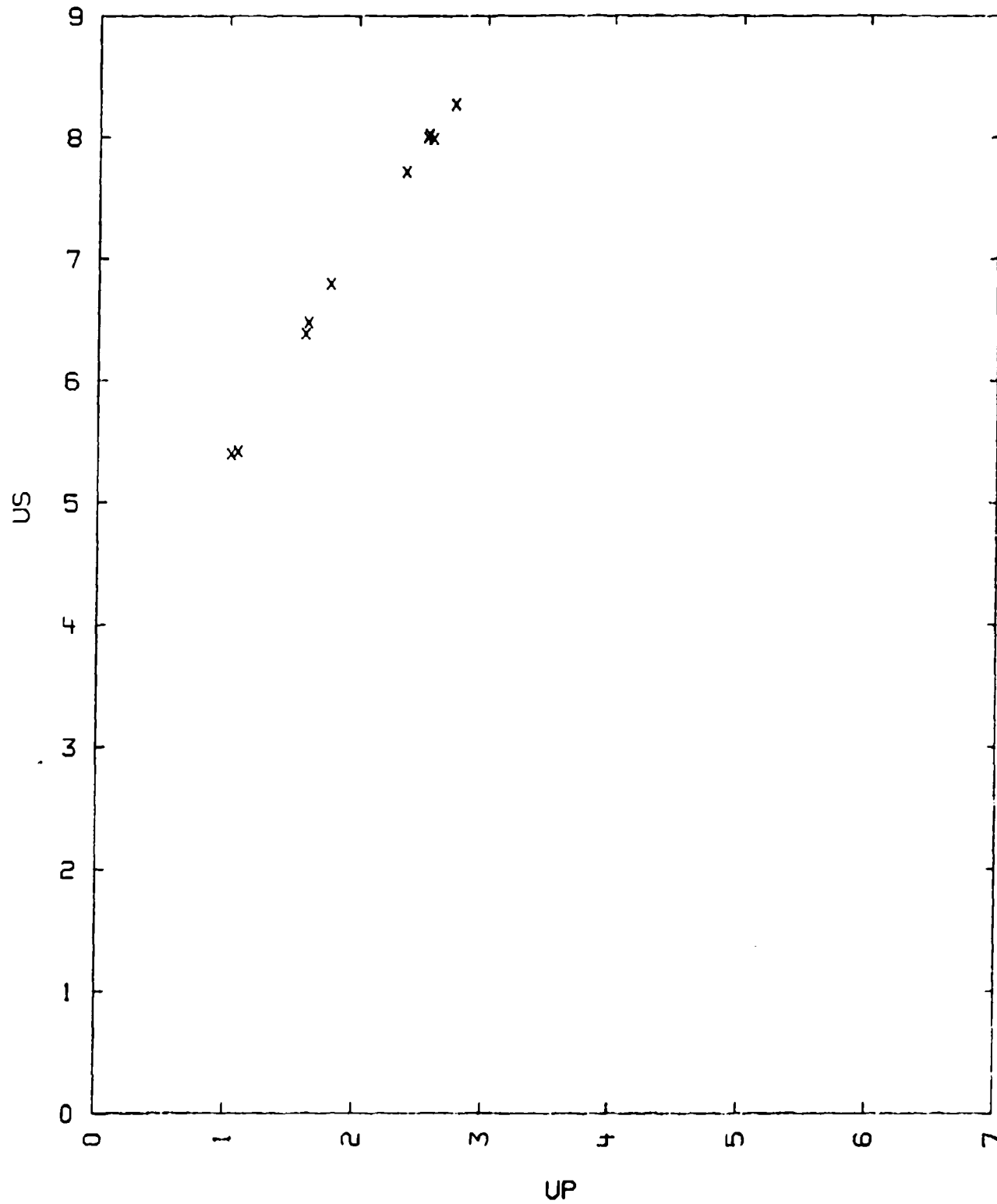
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES, HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B STANDARD MATERIAL COPPER
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY OWEN YATES AND SULLY, PROC. PHYS. SOC. (LONDON) VOL 49, P. 315 (1937)

TABLE I

IRON-NICKEL ALLOY

41--39---1



41--39---2  
IRON-NICKEL ALLOY

FE 82 WT PERCENT  
NI 18 - -

V0 = 0.1256 CC/G  
V01 = 0.1262 CC/G

C0 = 4.40 KM/SEC

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RHO0             | US   | UP   | P     | V/V0   | MATERIAL           | US(ST) |
| 7.962            | 5.56 | 1.02 | 452.  | 0.8165 | CU                 | 5.40   |
| 7.962            | 5.61 | 1.06 | 473.  | 0.8111 | CU                 | 5.45   |
| 7.962            | 6.52 | 1.58 | 820.  | 0.7577 | CU                 | 6.22   |
| 7.962            | 6.58 | 1.61 | 843.  | 0.7553 | CU                 | 6.27   |
| 7.962            | 6.90 | 1.78 | 978.  | 0.7420 | CU                 | 6.53   |
| 7.962            | 7.13 | 1.95 | 1107. | 0.7265 | CU                 | 6.77   |
| 7.962            | 7.62 | 2.26 | 1371. | 0.7034 | CU                 | 7.22   |
| 7.962            | 7.74 | 2.37 | 1461. | 0.6938 | CU                 | 7.37   |
| 7.962            | 8.00 | 2.53 | 1612. | 0.6837 | CU                 | 7.61   |
| 7.962            | 8.03 | 2.54 | 1624. | 0.6837 | CU                 | 7.63   |
| 7.962            | 7.98 | 2.56 | 1627. | 0.6792 | CU                 | 7.65   |
| 7.962            | 8.42 | 2.72 | 1823. | 0.6770 | CU                 | 7.91   |
| 7.962            | 8.38 | 2.73 | 1821. | 0.6742 | CU                 | 7.92   |
| 7.962            | 8.35 | 2.73 | 1815. | 0.6731 | CU                 | 7.91   |
| 7.962            | 8.32 | 2.76 | 1828. | 0.6683 | CU                 | 7.94   |

US =  $3.957 + 1.608 \cdot UP$  KM/SEC  
SIG US = 0.055 KM/SEC

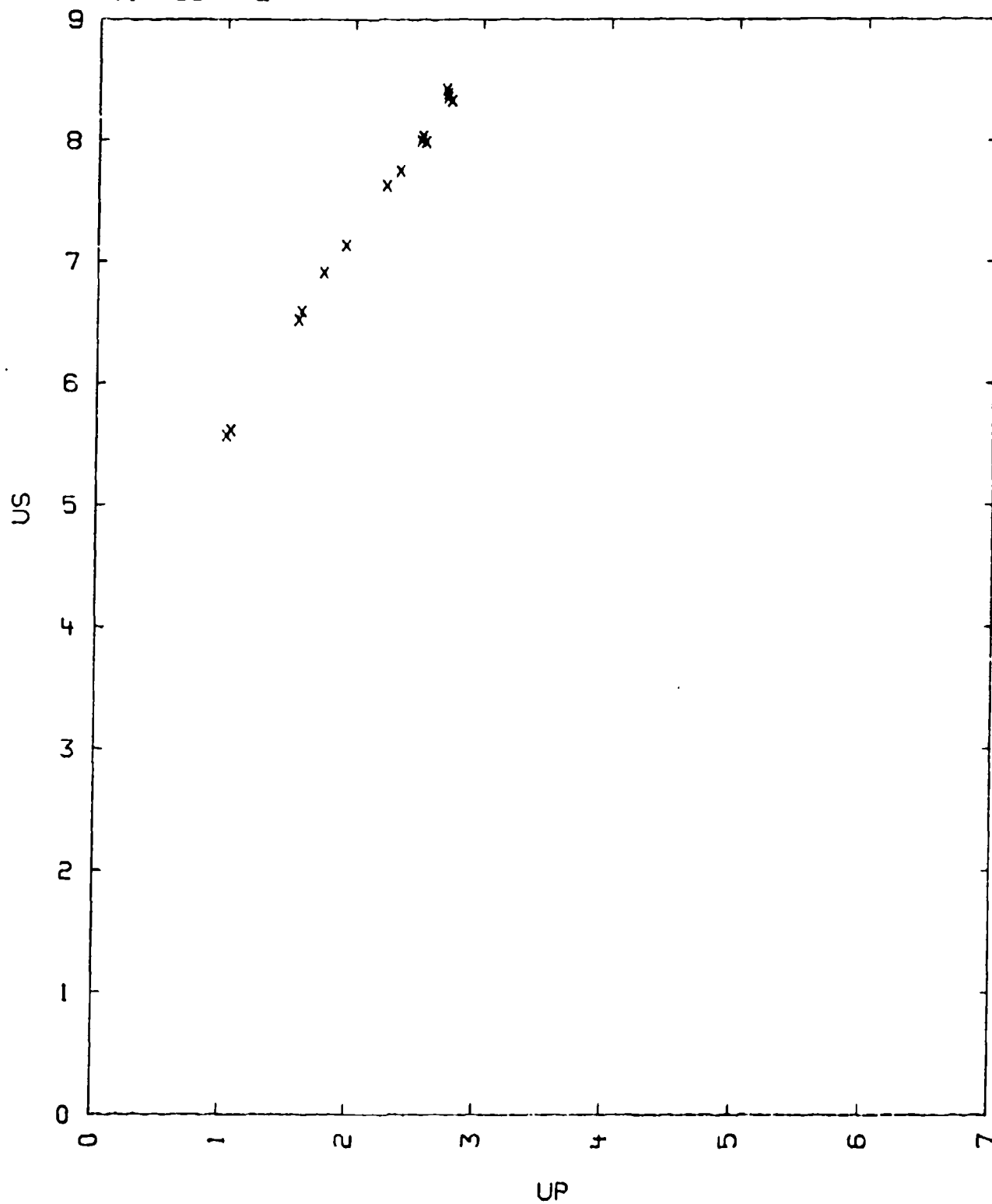
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES, HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B STANDARD MATERIAL COPPER
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY OWEN YATES AND SULLY, PROC. PHYS. SOC. (LONDON) VOL 49, P. 315 (1937)

TABLE I

IRON-NICKEL ALLOY

41--39---2



41--39--3  
IRON-NICKEL ALLOY

FE 74 WT PERCENT  
NI 26 - -

VO = 0.1255  
VOI = 0.1256 CC/G

CO = 4.37 KM/SEC

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TAB

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RH00             | US   | UP   | P     | V/VO   | MATERIAL           | US(ST) |
| 7.974            | 5.48 | 1.03 | 450.  | 0.8120 | CU                 | 5.40   |
| 7.974            | 5.49 | 1.06 | 464.  | 0.8069 | CU                 | 5.45   |
| 7.974            | 5.49 | 1.08 | 473.  | 0.8033 | CU                 | 5.47   |
| 7.974            | 6.44 | 1.58 | 811.  | 0.7547 | CU                 | 6.22   |
| 7.974            | 6.53 | 1.61 | 838.  | 0.7534 | CU                 | 6.27   |
| 7.974            | 6.84 | 1.79 | 976.  | 0.7383 | CU                 | 6.53   |
| 7.974            | 7.07 | 1.96 | 1105. | 0.7228 | CU                 | 6.77   |
| 7.974            | 7.48 | 2.27 | 1354. | 0.6965 | CU                 | 7.22   |
| 7.974            | 7.69 | 2.37 | 1453. | 0.6918 | CU                 | 7.37   |
| 7.974            | 7.94 | 2.54 | 1608. | 0.6801 | CU                 | 7.61   |
| 7.974            | 7.96 | 2.55 | 1619. | 0.6796 | CU                 | 7.63   |
| 7.974            | 8.03 | 2.56 | 1639. | 0.6812 | CU                 | 7.65   |
| 7.974            | 8.13 | 2.76 | 1789. | 0.6605 | CU                 | 7.92   |
| 7.974            | 8.18 | 2.78 | 1813. | 0.6601 | CU                 | 7.94   |

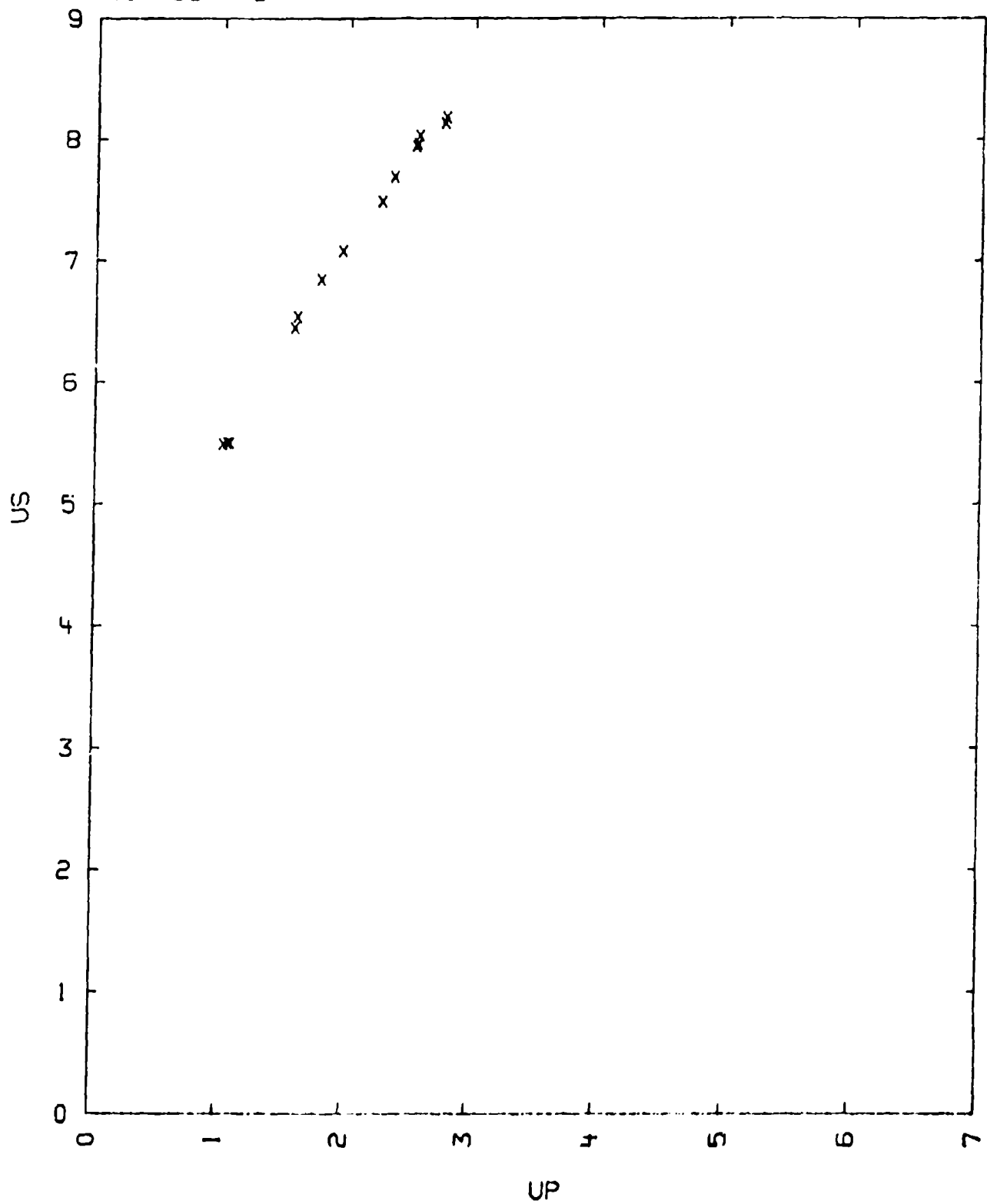
US = 3.877 + 1.591\*UP KM/SEC  
SIC US = 0.087 KM/SEC

COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES.  
HIGH VELOCITY IMPACT PHENOMENA. KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B STANDARD MATERIAL COPPER
- 3) VOI WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY OWEN YATES AND SULLY, PROC. PHYS. SOC. (LONDON) VOL. 49, P. 315, (1937)

TABLE I

IRON-NICKEL ALLOY  
41--39---3





41--51---1  
 IRON-CHROMIUM MIXTURE  
 FE-CR

NI 0.3-0.03 WT PERCENT  
 CU 0.00'-0.0001 WT PERCENT  
 SI 0.0 -0.0001 WT PERCENT  
 MN 0.003-0.0003 WT PERCENT  
 CR SEE TABLE  
 FE REMAINDER

V0 = 0.1297-0.1313 CC/G  
 V01 = 0.1284-0.1306 CC/G

IN THE TABLE BELOW, THE PERCENTAGE OF CHROMIUM IS LISTED IN THE FIRST COLUMN. THE DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND PRESSURES IN KILOBARS.

TABLE

| W(CR) | RHO0  | US1  | UP1   | P1  | V1/V0 | US2  | UP2   | P2  | V2/V0 |
|-------|-------|------|-------|-----|-------|------|-------|-----|-------|
| 9.77  | 7.757 | 5.14 | 0.337 | 134 | 0.934 | 3.97 | 0.349 | 138 | 0.931 |
| 9.77  | 7.757 | 5.14 | 0.329 | 131 | 0.936 | 3.89 | 0.338 | 134 | 0.934 |
| 17.3  | 7.726 | 5.17 | 0.393 | 157 | 0.924 | 4.39 | 0.572 | 217 | 0.883 |
| 17.3  | 7.773 | 5.17 | 0.384 | 155 | 0.926 | 4.31 | 0.560 | 213 | 0.885 |
| 25.7  | 7.645 | 5.43 | 0.499 | 207 | 0.908 | 5.21 | 0.744 | 304 | 0.861 |
| 25.7  | 7.642 | 5.43 | 0.499 | 207 | 0.908 | 5.12 | 0.750 | 305 | 0.859 |
| 30.1  | 7.615 | 5.46 | 0.536 | 223 | 0.902 | 5.12 | 0.784 | 311 | 0.857 |
| 30.1  | 7.620 | 5.46 | 0.572 | 238 | 0.895 | 5.03 | 0.742 | 302 | 0.861 |

US1 =

# COMMENTS:

- 1) SOURCE: GUST W.H. AND ROYCE E.B.  
 J. APPL. PHYS., VOL.41, P.2443, (1970)  
 LAWRENCE LIVERMORE LABORATORY,  
 LIVERMORE, CALIFORNIA 94550
- 2) EXPERIMENTAL TECHNIQUE C1: FOR EACH WAVE THE SHOCK AND FREE SURFACE VELOCITIES WERE MEASURED.  
 DATA REDUCTION TECHNIQUE A: WHERE UFS = 2UP  
 STANDARD MATERIAL ALUMINUM 2024.
- 3) THE FREE SURFACE VELOCITIES WERE MEASURED BY A MIRROR INCLINED AT A SMALL ANGLE WITH RESPECT TO THE SAMPLE SURFACE. THE ANGLES USED WERE 0.5 DEGREES AND 1.5 DEGREES.
- 4) THE AVERAGE UNCERTAINTIES OF THE MEASURED SHOCK AND FREE SURFACE VELOCITIES ARE 2 PERCENT.
- 5) P1 IS THE PRESSURE OF THE LOW TEMPERATURE ALPHA TO EPSILON TRANSITION -PHASE DIAGRAM: SEE MATERIAL 41---17.
- 6) V01 HAS BEEN CALCULATED FROM THE FOLLOWING CUBIC LATTICE CONSTANTS:  
 A = 2.8703 ANGSTROM FOR CR/FE = 9.77/90.23, AND A = 2.8725 ANGSTROM FOR CR/FE = 30.1/69.9. SEE PEARSON, METAL PHYSICS AND PHYSICAL METALLURGY, VOL. 4 (PERGAMON PRESS, N.Y. 1958).

TABLE I

IRON-CHROMIUM MIXTURE

41--51----

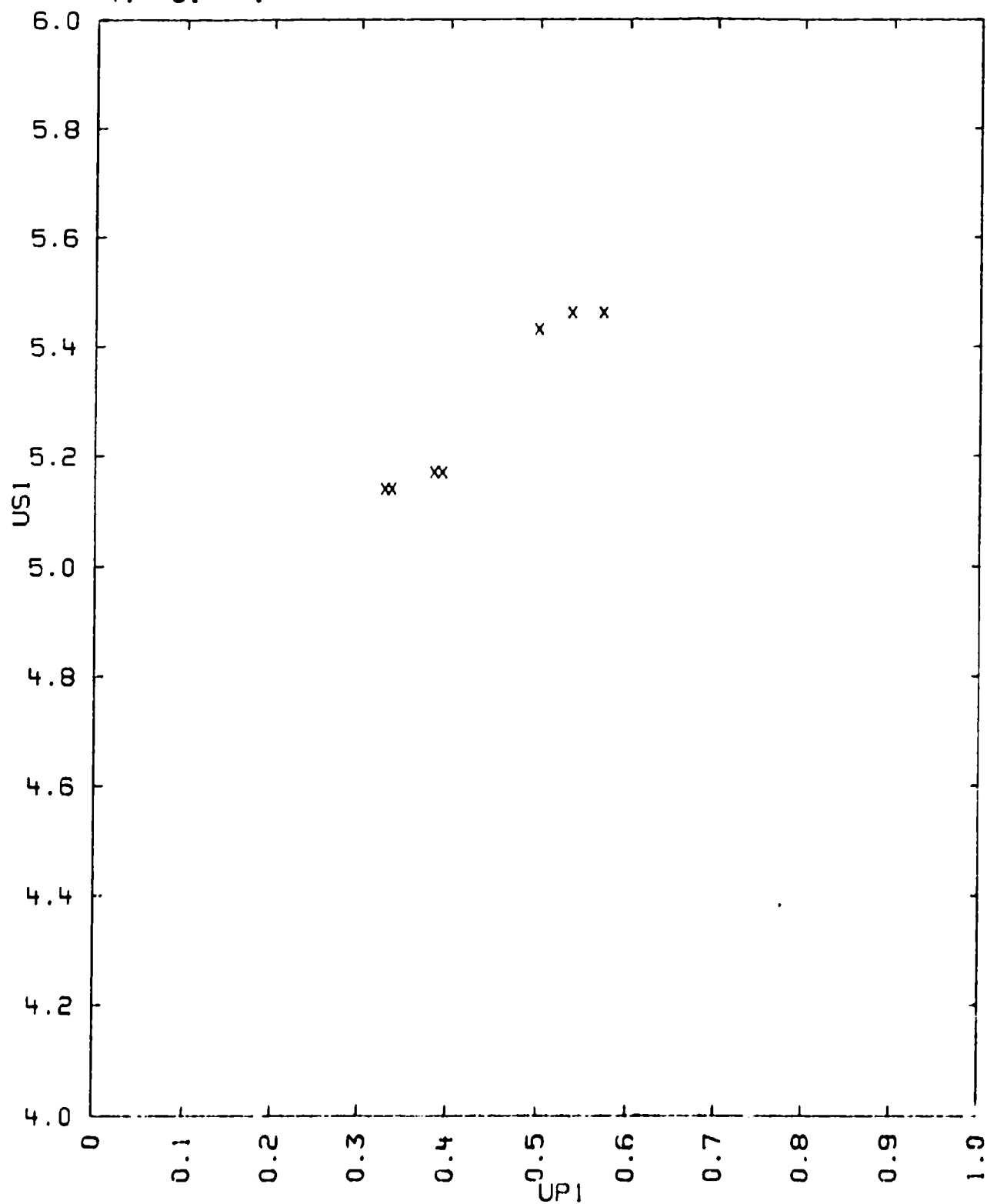
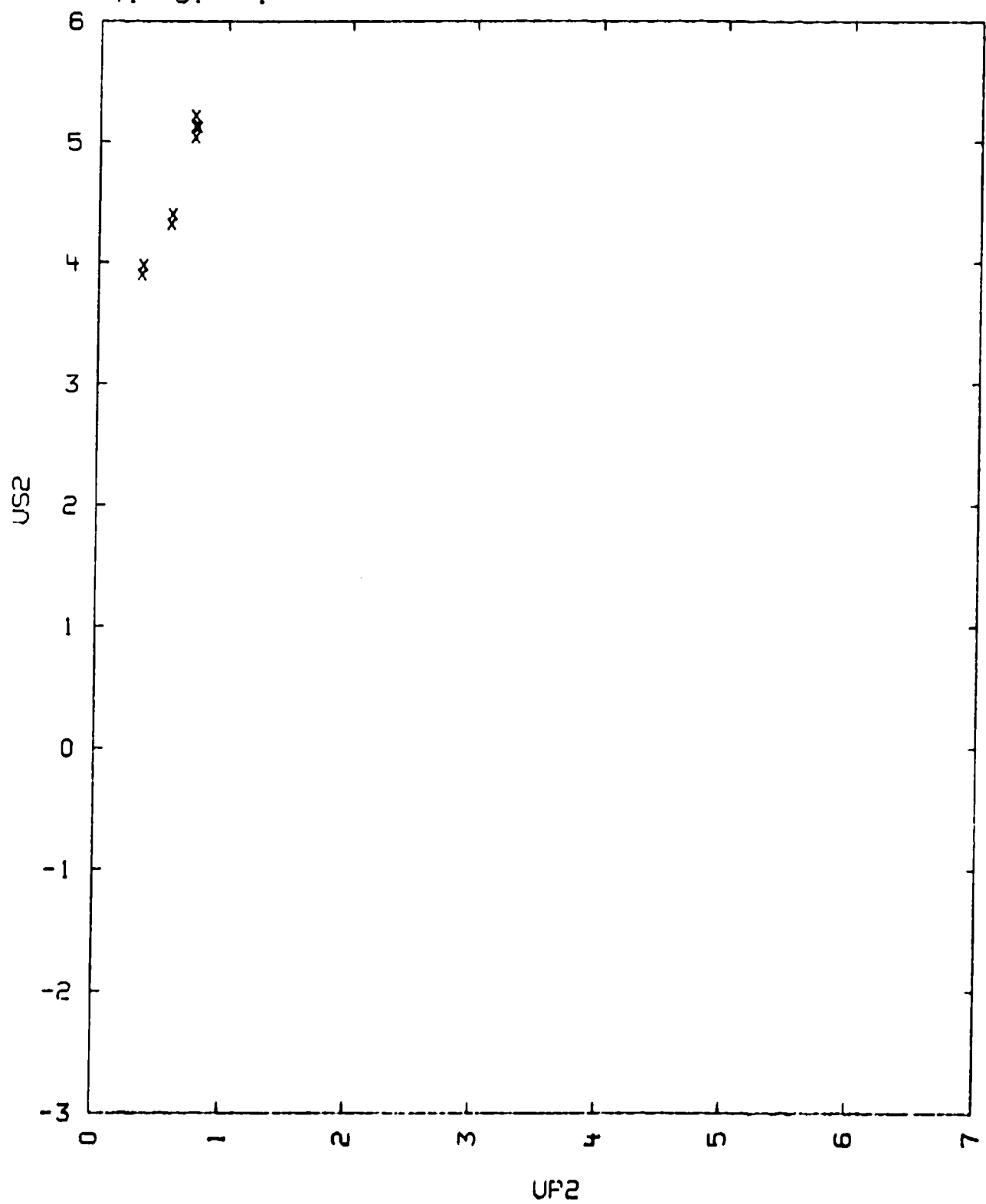


TABLE I

IRON-CHROMIUM MIXTURE  
41--51---1



41--51--39---1

## IRON-CHROMIUM-NICKEL MIXTURE (STEEL-STAINLESS)

FE-CR-NI

CU 0.003 - 0.0001 WT PERCENT

SI 0.10 - 0.001 WT PERCENT

MN 0.003 - 0.0003 WT PERCENT

CR SEE TABLE

NI SEE TABLE

FE REMAINDER

V0 = 0.1257-0.1289 CC/G

IN TABLE I BELOW, THE PERCENTAGES OF CR AND NI ARE LISTED IN THE FIRST TWO COLUMNS. SUBSCRIPTS 1, 2 AND 3 ARE THE ELASTIC WAVE AND THE FIRST AND SECOND SHOCK WAVES RESPECTIVELY. THE DENSITY IS GIVEN IN G/CC AND VELOCITIES IN KM/SEC. (ID) IS THE IDENTIFICATION BETWEEN TABLES. IN TABLE II, PRESSURES ARE GIVEN IN KILOBARS.

TABLE I

| W(CR) | W(NI) | PH00  | US1  | UP1   | US2  | UP2   | US3  | UP3   | ID |
|-------|-------|-------|------|-------|------|-------|------|-------|----|
| 5.93  | 8.79  | 7.821 |      |       | 5.18 | 0.271 | 3.74 | 0.329 | 1  |
| 5.93  | 8.79  | 7.823 |      |       | 5.18 | 0.265 | 3.72 | 0.359 | 2  |
| 12.1  | 7.73  | 7.778 | 5.72 | 0.045 | 4.98 | 0.217 | 3.42 | 0.263 | 3  |
| 15.9  | 7.8   | 7.761 |      |       | 4.99 | 0.205 | 3.64 | 0.263 | 4  |
| 15.9  | 7.8   | 7.759 |      |       | 4.99 | 0.209 | 3.68 | 0.263 | 5  |
| 18.1  | 8.22  | 7.830 |      |       | 5.45 | 0.193 | 4.43 | 0.276 | 6  |
| 18.1  | 8.22  | 7.833 |      |       | 5.45 | 0.164 |      |       | 7  |
| 21.7  | 8.15  | 7.881 |      |       | 5.31 | 0.291 |      |       | 8  |
| 21.7  | 8.15  | 7.880 |      |       | 5.38 | 0.297 |      |       | 9  |
| 6.32  | 12.2  | 7.852 |      |       | 4.77 | 0.262 | 3.24 | 0.281 | 10 |
| 11.7  | 12.1  | 7.888 |      |       | 4.98 | 0.210 | 3.56 | 0.270 | 11 |
| 5.91  | 16.0  | 7.894 |      |       | 4.90 | 0.203 | 3.82 | 0.304 | 12 |

US =

TABLE II

| W(CR) | W(NI) | P1 | V1/V0 | P2  | V2/V0 | P3  | V3/V0 | ID |
|-------|-------|----|-------|-----|-------|-----|-------|----|
| 5.93  | 8.79  |    |       | 110 | 0.947 | 127 | 0.931 | 1  |
| 5.93  | 8.79  |    |       | 107 | 0.949 | 134 | 0.923 | 2  |
| 12.1  | 7.73  | 20 | 0.992 | 87  | 0.957 | 99  | 0.943 | 3  |
| 15.9  | 7.8   |    |       | 79  | 0.959 | 92  | 0.943 | 4  |
| 15.9  | 7.8   |    |       | 81  | 0.958 | 94  | 0.943 | 5  |
| 18.1  | 8.22  |    |       | 78  | 0.966 | 110 | 0.943 | 6  |
| 18.1  | 8.22  |    |       | 70  | 0.970 |     |       | 7  |
| 21.7  | 8.15  |    |       | 122 | 0.945 |     |       | 8  |
| 21.7  | 8.15  |    |       | 126 | 0.945 |     |       | 9  |
| 6.32  | 12.2  |    |       | 98  | 0.945 | 103 | 0.939 | 10 |

11.7 12.1

83 0.958 99 0.941 11

5.91 16.0

78 0.959 108 0.932 12

## COMMENTS:

- 1) SOURCE: GUST, W. H. AND ROYCE, E. B.  
J. APPL. PHYS. VOL.41, P.2443, (1970)  
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA, USA.
- 2) EXPERIMENTAL TECHNIQUE C1: FOR EACH WAVE THE SHOCK VELOCITY (US) AND THE FREE SURFACE VELOCITY (UFS) WERE MEASURED.  
DATA REDUCTION TECHNIQUE A: WHERE UFS = 2UP  
THE ELASTIC WAVE IS IGNORED EXCEPT IN ENTRY 3.
- 3) THE FREE SURFACE VELOCITIES WERE MEASURED BY A MIRROR INCLINED AT A SMALL ANGLE WITH RESPECT TO THE SAMPLE SURFACE. THE ANGLES USED WERE 0.5 DEGREES AND 1.5 DEGREES.
- 4) THE AVERAGE UNCERTAINTIES OF THE MEASURED SHOCK AND FREE SURFACE VELOCITIES ARE 2 PERCENT.
- 5) P2 IS THE PRESSURE OF THE LOW TEMPERATURE ALPHA TO EPSILON TRANSITION -PHASE DIAGRAM: SEE MATERIAL 41---17.

TABLE I  
IRON-CHROMIUM-NICKEL MIXTURE (STEEL-STAINLESS)  
41--51--39---1

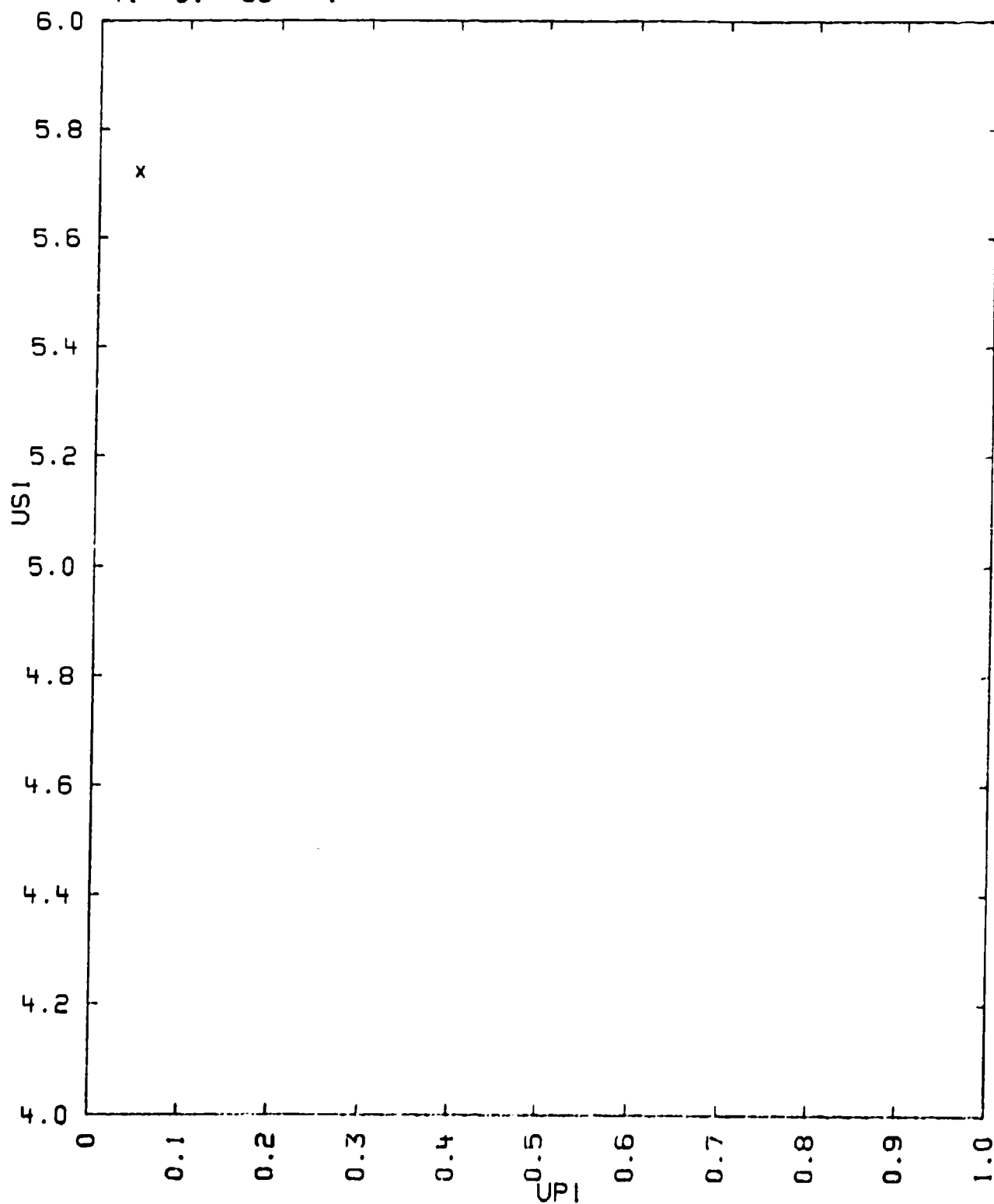


TABLE I  
IRON-CHROMIUM-NICKEL MIXTURE (STEEL-STAINLESS)  
41--51--39---

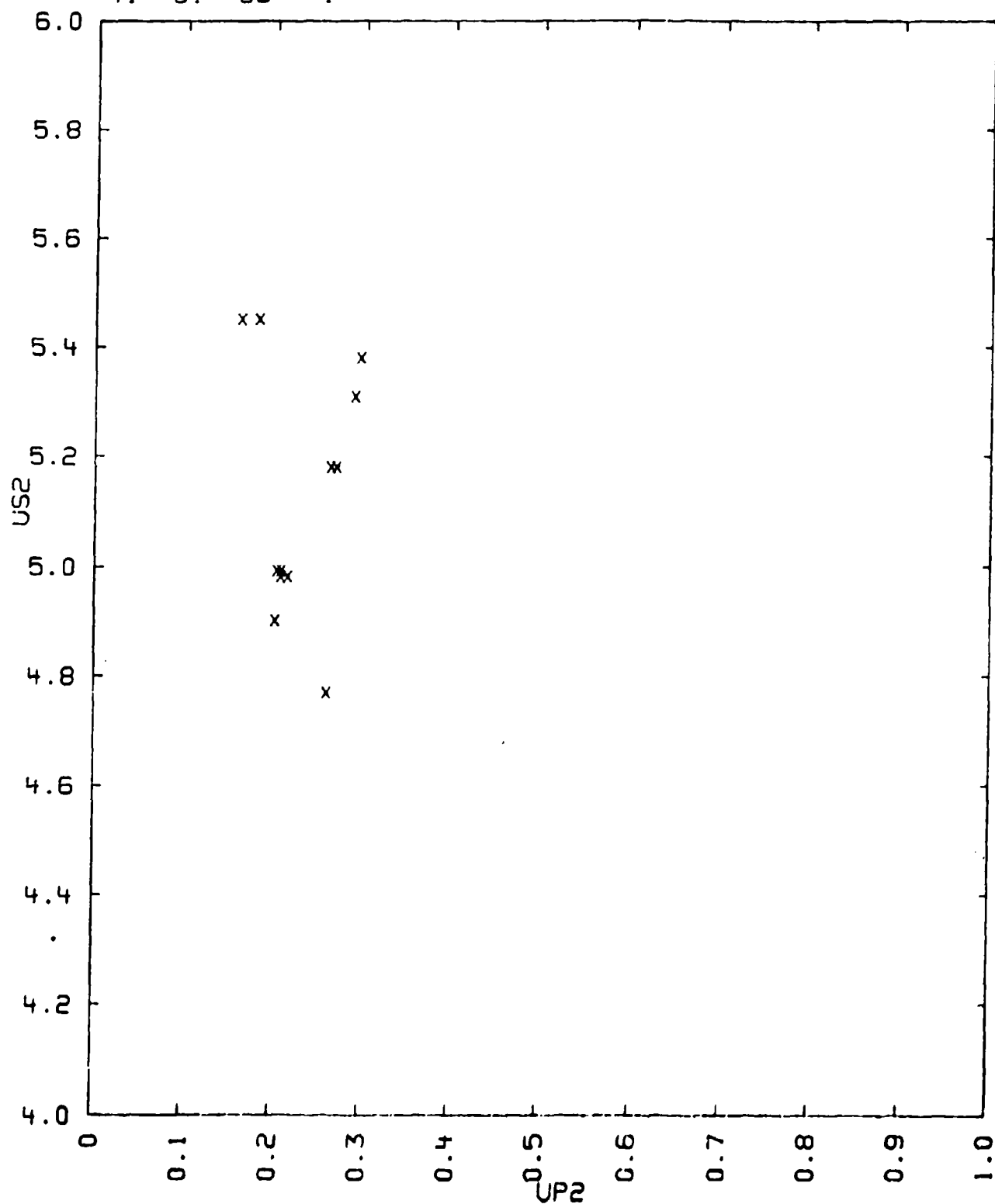
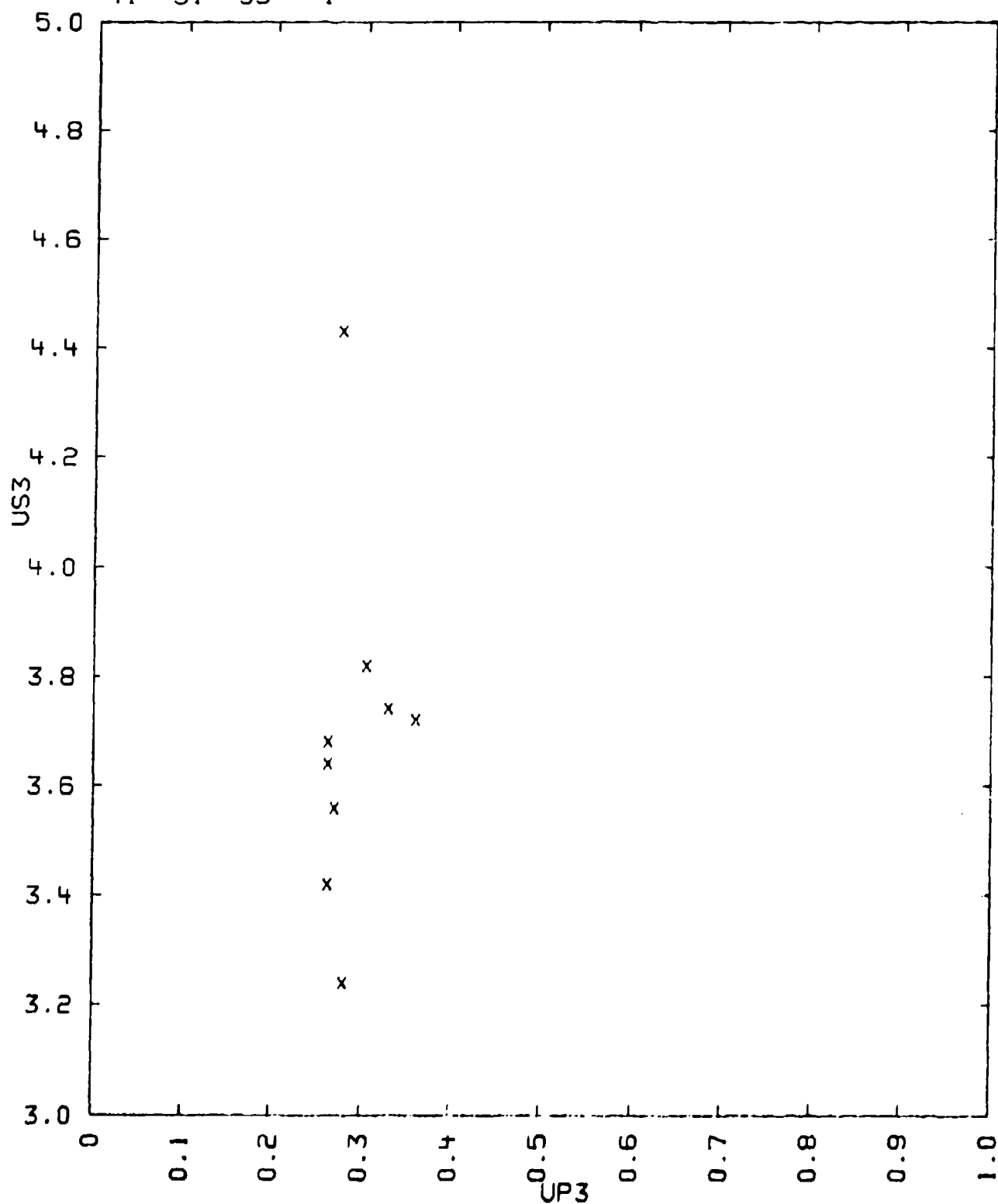


TABLE I  
IRON-CHROMIUM-NICKEL MIXTURE (STEEL-STAINLESS)  
41--51--39---1





|    |           |            |
|----|-----------|------------|
| FE | REMAINDER |            |
| CR | 18-20     | WT PERCENT |
| NI | 8-12      | WT PERCENT |
| MN | 2.        | WT PERCENT |
| SI | 1.        | WT PERCENT |
| C  | 0.08      | WT PERCENT |

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RH00             | US   | UP   | P     | V/VO   | MATERIAL           | US(ST) |
| 7.890            | 4.92 | 0.23 | 89.   | 0.9533 | CU                 | 4.29   |
| 7.890            | 5.06 | 0.34 | 136.  | 0.9328 | CU                 | 4.45   |
| 7.890            | 5.35 | 0.53 | 224.  | 0.9009 | CU                 | 4.73   |
| 7.890            | 5.58 | 0.66 | 291.  | 0.8817 | CU                 | 4.92   |
| 7.890            | 5.65 | 0.74 | 330.  | 0.8690 | CU                 | 5.04   |
| 7.890            | 5.89 | 0.89 | 414.  | 0.8489 | CU                 | 5.26   |
| 7.890            | 6.01 | 0.97 | 460.  | 0.8386 | CU                 | 5.37   |
| 7.890            | 6.08 | 1.01 | 485.  | 0.8339 | CU                 | 5.44   |
| 7.890            | 6.15 | 1.06 | 514.  | 0.8276 | CU                 | 5.51   |
| 7.890            | 6.64 | 1.38 | 723.  | 0.7922 | CU                 | 5.96   |
| 7.890            | 6.73 | 1.41 | 749.  | 0.7905 | CU                 | 6.03   |
| 7.890            | 6.73 | 1.41 | 749.  | 0.7905 | CU                 | 6.03   |
| 7.890            | 7.01 | 1.85 | 913.  | 0.7646 | CU                 | 6.37   |
| 7.890            | 7.46 | 1.91 | 1124. | 0.7440 | CU                 | 6.76   |
| 7.890            | 8.05 | 2.33 | 1480. | 0.7106 | CU                 | 7.37   |
| 7.903            | 8.56 | 2.63 | 1779. | 0.6928 | CU                 | 7.81   |
| 7.890            | 8.60 | 2.71 | 1839. | 0.6849 | CU                 | 7.91   |
| 7.890            | 8.67 | 2.77 | 1895. | 0.6805 | CU                 | 8.00   |
| 7.903            | 8.62 | 2.79 | 1901. | 0.6763 | CU                 | 8.13   |

$$US = 4.569 + 1.490 \cdot UP \text{ KM/SEC}$$

$$SIGMA US = 0.041 \text{ KM/SEC}$$

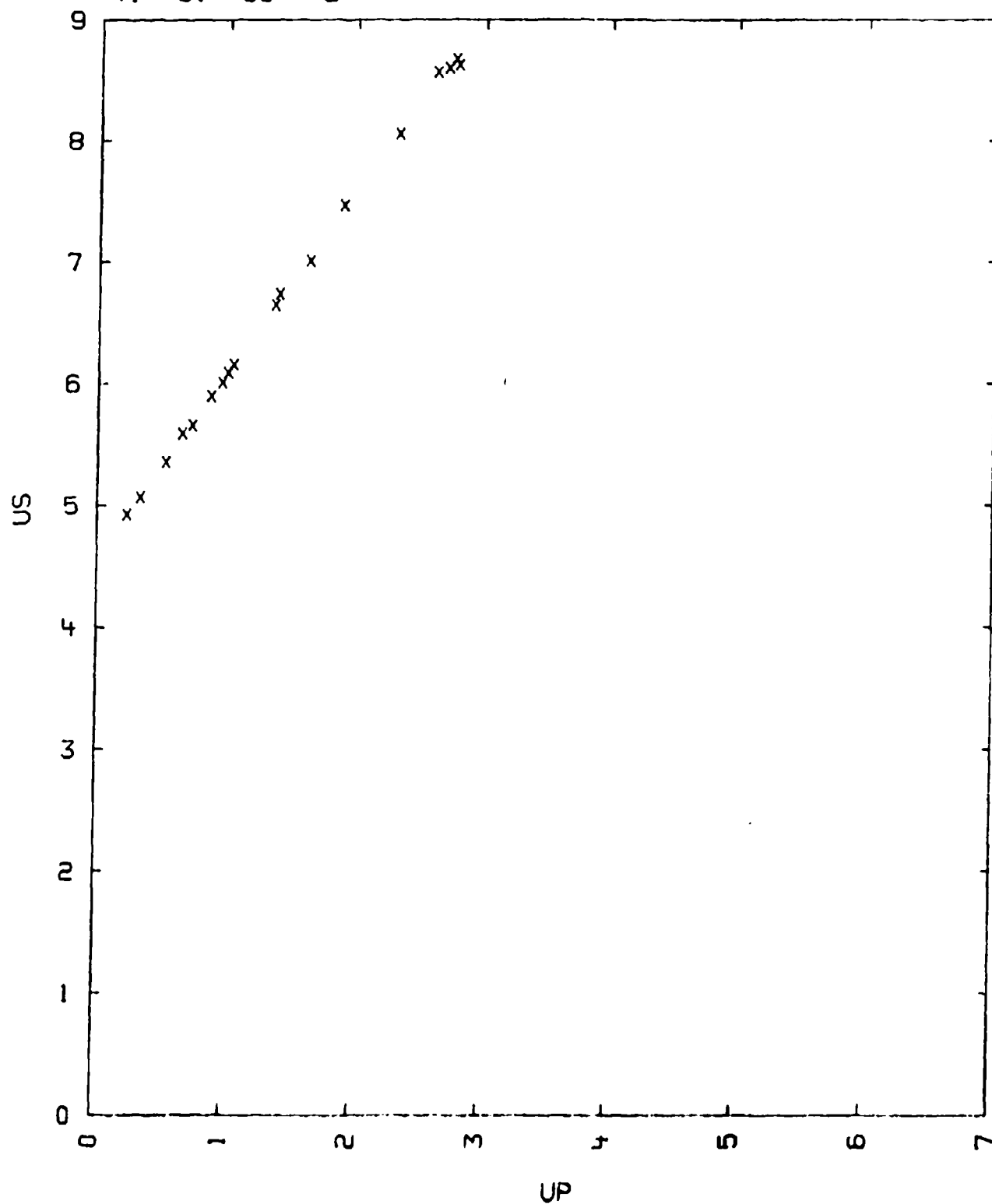
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES, HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B
- DATA REDUCTION TECHNIQUE: B (STANDARD BASE PLATE AS SHOWN)
- 3)  $V(UP/DE) = 2.17$ ,  $HEL = 2.3$  KBAR
- 4) COMPOSITION FROM AMERICAN SOC. FOR METALS HANDBOOK (A.S.M., OHIO (1961)) VOL. 1
- 5) HUGONOT ELASTIC LIMIT 2.3 KBAR

TABLE 1

STAINLESS STEEL (TYPE 304)

41--51--39---2



41--51--39---3  
STAINLESS STEEL (TYPE 304L)

|    |           |            |
|----|-----------|------------|
| FE | REMAINDER |            |
| CR | 18-20     | WT PERCENT |
| NI | 8-12      | WT PERCENT |
| MN | 2.        | WT PERCENT |
| SI | 1.        | WT PERCENT |
| C  | 0.03      | WT PERCENT |

$V_0 = 0.1265 \text{ CC/G}$

$CL = 5.79 \text{ KM/SEC}$   
 $CS = 3.16 \text{ KM/SEC}$

$C_0 = 4.49 \text{ KM/SEC}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |       |                  | -----STANDARD----- |        |
|------------------|------|------|-------|------------------|--------------------|--------|
| R400             | US   | UP   | P     | V/V <sub>0</sub> | MATERIAL           | US(ST) |
| 7.903            | 4.90 | 0.23 | 89.   | 0.9531           | CU                 | 4.29   |
| 7.903            | 5.10 | 0.34 | 137.  | 0.9333           | CU                 | 4.45   |
| 7.903            | 5.35 | 0.53 | 224.  | 0.9009           | CU                 | 4.73   |
| 7.903            | 5.55 | 0.66 | 289.  | 0.8811           | CU                 | 4.92   |
| 7.903            | 5.65 | 0.74 | 330.  | 0.8690           | CU                 | 5.04   |
| 7.903            | 5.86 | 0.89 | 412.  | 0.8481           | CU                 | 5.26   |
| 7.903            | 6.02 | 0.97 | 461.  | 0.8389           | CU                 | 5.37   |
| 7.903            | 6.06 | 1.01 | 484.  | 0.8333           | CU                 | 5.44   |
| 7.903            | 6.26 | 1.14 | 564.  | 0.8179           | CU                 | 5.62   |
| 7.903            | 6.60 | 1.38 | 720.  | 0.7909           | CU                 | 5.98   |
| 7.903            | 6.68 | 1.41 | 744.  | 0.7889           | CU                 | 6.03   |
| 7.903            | 6.98 | 1.65 | 910.  | 0.7636           | CU                 | 6.37   |
| 7.903            | 7.46 | 1.91 | 1126. | 0.7440           | CU                 | 6.76   |
| 7.903            | 8.05 | 2.33 | 1482. | 0.7106           | CU                 | 7.37   |
| 7.903            | 8.57 | 2.71 | 1835. | 0.6838           | CU                 | 7.91   |

$US = 4.569 + 1.490 \cdot UP \text{ KM/SEC}$   
 $SIGMA US = 0.030 \text{ KM/SEC}$

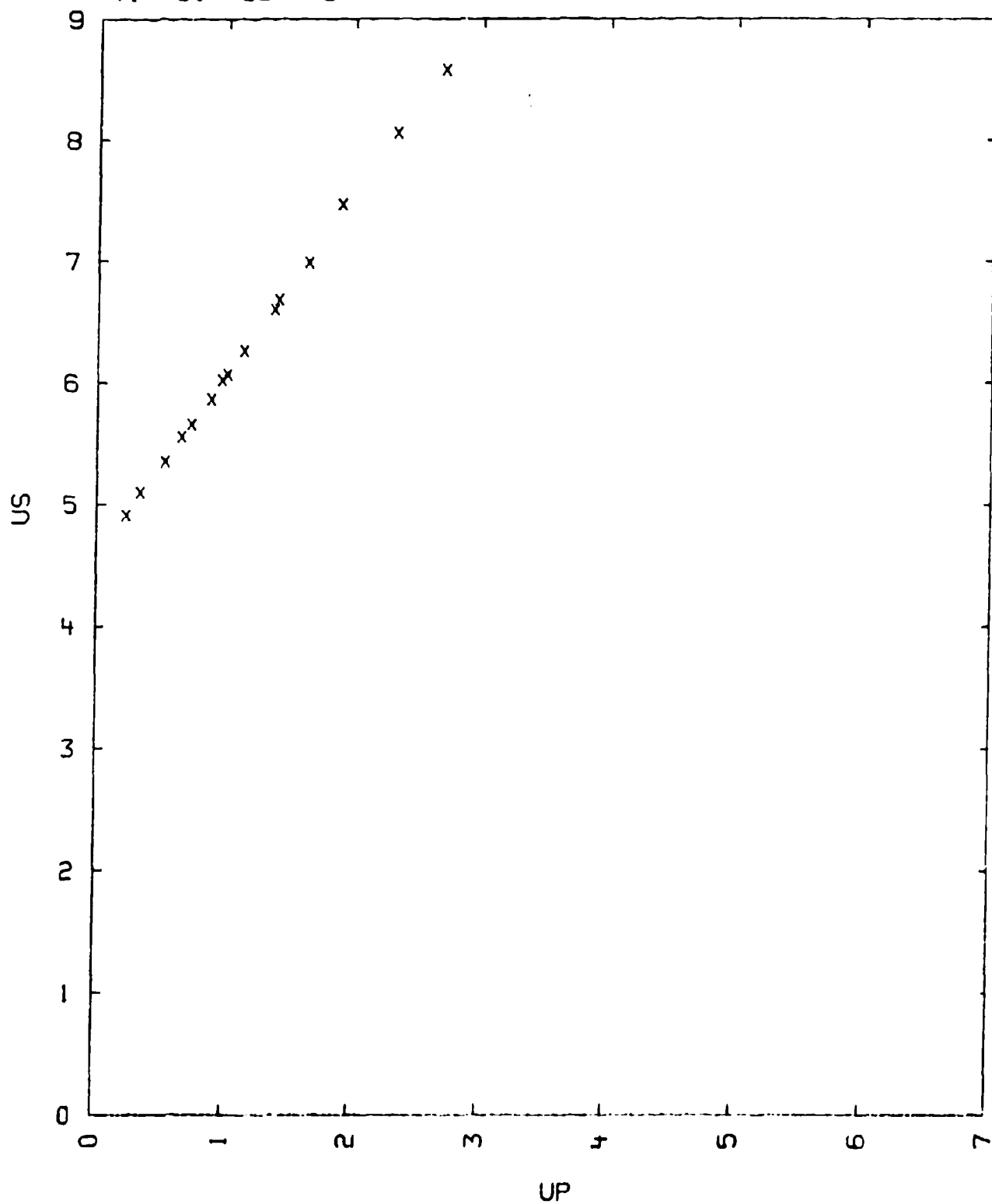
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES, HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) COMPOSITION FROM AMERICAN SOC. FOR METALS HANDBOOK (A.S.M., OHIO, 1961) VOL. 1

TABLE I

STAINLESS STEEL (TYPE 304L)

41--51--39---3



41--51--39---4  
STAINLESS STEEL (TYPE 347)

|    |           |            |
|----|-----------|------------|
| FE | REMAINDER |            |
| CR | 17.-19.   | WT PERCENT |
| NI | 9.-13.    | WT PERCENT |
| MN | 2.        | WT PERCENT |
| SI | 2.        | WT PERCENT |
| C  | 0.08      | WT PERCENT |

$V_0 = 0.1263 \text{ CC/G}$

$C_0 = 4.55 \text{ KM/SEC}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL           | US(ST) |
| 7.920            | 4.55 | 0.   | 0.   | 1.0000 | C0                 | 0.     |
| 7.920            | 5.60 | 0.72 | 319. | 0.8714 | 2024 AL            | 6.84   |
| 7.920            | 6.03 | 0.96 | 458. | 0.8408 | 2024 AL            | 7.34   |

$US = 4.541 + 1.522 \cdot UP \text{ KM/SEC}$

$SIGMA US = 0.047 \text{ KM/SEC}$

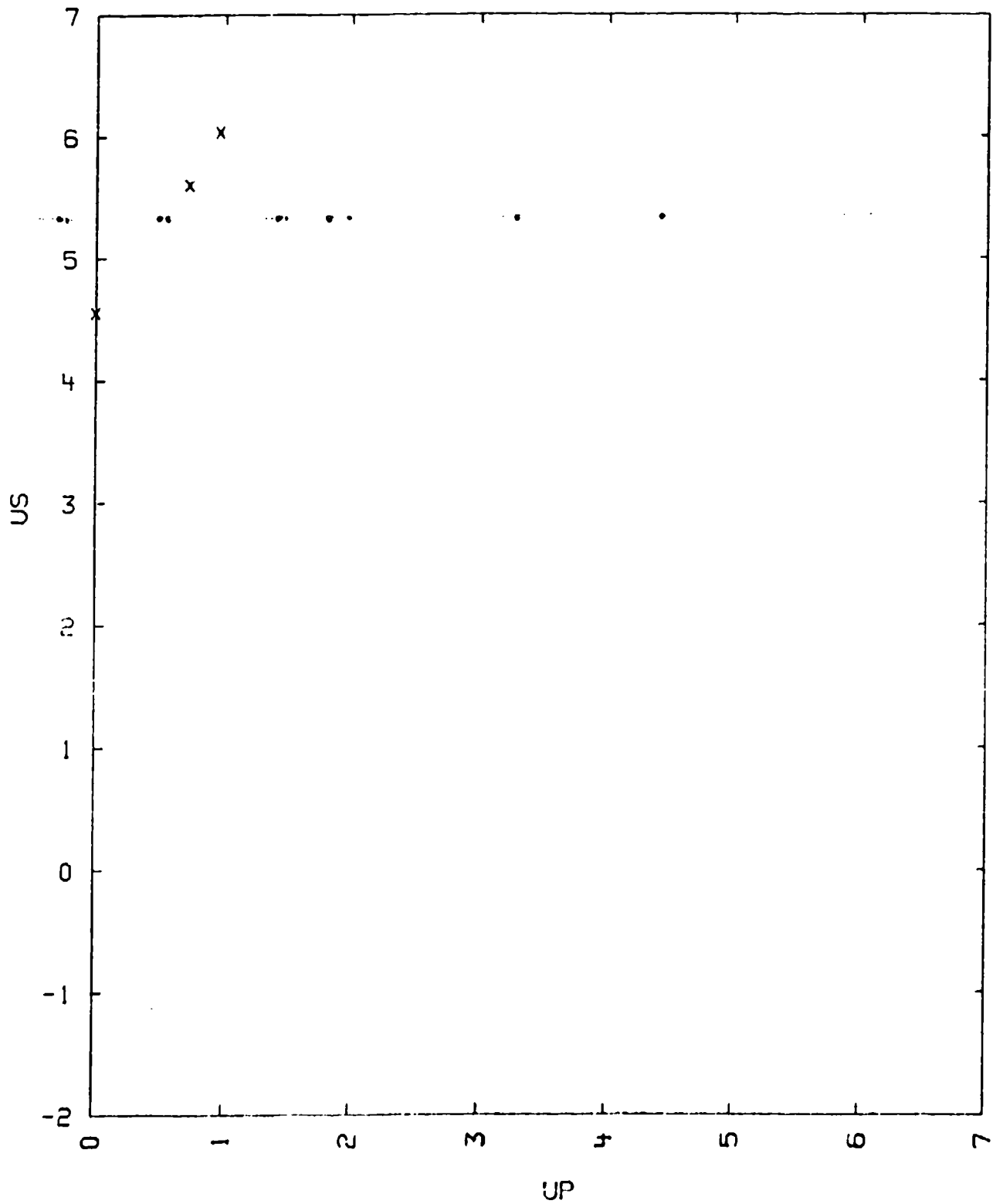
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES.  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B (STANDARD BASE PLATE AS SHOWN)
- 3) COMPOSITION FROM AMERICAN SOC. FOR METALS HANDBOOK (A.S.M., OHIO, 1961) VOL. 1

TABLE I

STAINLESS STEEL (TYPE 347)

41--51--39---4



41--51--39---5  
STEEL, 304 STAINLESS

|    |       |             |      |      |             |
|----|-------|-------------|------|------|-------------|
| FE | 69.86 | WT. PERCENT | C    | .065 | WT. PERCENT |
| CR | 18.73 | -           | P    | .029 | -           |
| NI | 8.80  | -           | S    | .028 | -           |
| MN | 1.62  | -           | REST | .070 | -           |
| SI | .49   | -           |      |      |             |
| MO | .14   | -           |      |      |             |
| CU | .17   | -           |      |      |             |

V0 = 0.1265 CC/G      CL = 5.74 KM/SEC      C0 = 4.47 KM/SEC  
CS = 3.12 KM/SEC

THE TABLE LISTS RH00 IN G/CC, VELOCITIES IN KM/SEC AND P IN KBARS. FS =  
FANSTEEL, ST.ST. = STAINLESS STEEL AND WF = WEIGHTING FACTOR.

TABLE

| - - - - - SAMPLE - - - - - |        |       |       |       | - - IMPACTOR - - - |       |    |
|----------------------------|--------|-------|-------|-------|--------------------|-------|----|
| RH00                       | US     | UP    | P     | V/V0  | MAT                | U     | WF |
| 7.905                      | 6.877  | 1.497 | 814.  | .7823 | ST.ST.             | 2.993 | 3  |
| 7.905                      | 8.760  | 2.824 | 1956. | .6776 | ST.ST.             | 5.648 | 3  |
| 7.905                      | 9.980  | 3.607 | 2846. | .6386 | ST.ST.             | 7.214 | 3  |
| 7.905                      | 11.459 | 4.730 | 4285. | .587  | FS                 | 7.883 | 1  |

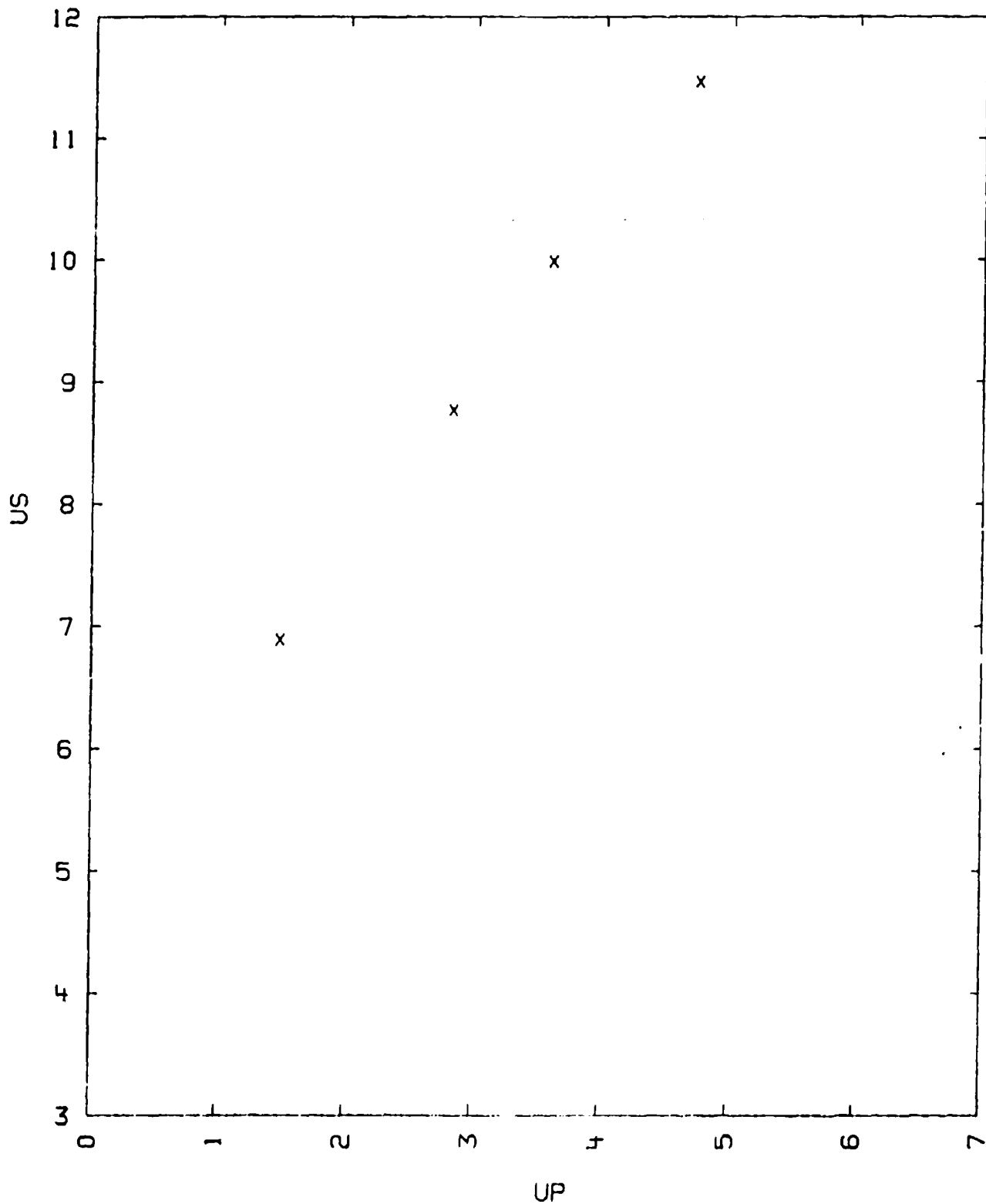
US = 4.722 + 1.441\*UP KM/SEC  
SIG.US = 0.023 KM/SEC

## COMMENTS:

- 1) SOURCE: ISBELL W.M., SHIPMAN F.H. AND JONES A.H.  
HUGONIOT EQUATION OF STATE OF ELEVEN MATERIALS TO FIVE MBARS  
MATERIALS SCIENCE LABORATORY REPORT: MSL-68-13
- 2) EXPERIMENTAL TECHNIQUE: A  
DATA REDUCTION METHOD: A
- 3) NOMINAL UNCERTAINTIES ARE: (SIG.US)/US = .005 AND (SIG.U)/U = .0005
- 4) ALSO LISTED ARE: POISSONS RATIO = 0.29, YIELD STRENGTH = 3.8 KBAR  
TENSILE - = 6.24 -

TABLE I

STEEL, 304 STAINLESS  
41--51--39---5





41-24-1--93-24-1---1  
DUNIT MOOIHOEK MINE, TRANSVAAL (SILICATE ROCK)

OLIVINE: 90 VOLUME PERCENT  
FAYALITE FE2-SI-04 50 - -  
FORSTERITE MG2-SI-04 40 - -  
BOWLINGITE (MG,FE)9-AL2-SI10-O30-(O-H)6-MG2 9 - -  
ORE FE3-O4 (PROBABLE) 1

V0 = 0.260 TO 0.272 CC/G CL = 7.31 KM/SEC  
V01 = 0.268 CC/G (NOTE 3)

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 3.83 | 6.55 | 0.49 | 123. | 0.925 | 6.16   |
| 3.83 | 6.71 | 0.74 | 190. | 0.890 | 6.54   |
| 3.78 | 6.96 | 1.03 | 272. | 0.852 | 6.97   |
| 3.77 | 6.71 | 1.06 | 268. | 0.842 | 6.97   |
| 3.   | 6.71 | 1.10 | 267. | 0.836 | 6.99   |
| 3.77 | 7.05 | 1.22 | 326. | 0.827 | 7.23   |
| 3.78 | 7.05 | 1.26 | 336. | 0.821 | 7.28   |
| 3.78 | 7.09 | 1.37 | 368. | 0.807 | 7.44   |
| 3.83 | 7.29 | 1.46 | 408. | 0.800 | 7.59   |
| 3.82 | 7.41 | 1.52 | 429. | 0.795 | 7.68   |
| 3.80 | 7.45 | 1.53 | 434. | 0.795 | 7.70   |
| 3.85 | 7.40 | 1.62 | 461. | 0.781 | 7.82   |
| 3.76 | 7.32 | 1.63 | 448. | 0.777 | 7.80   |
| 3.82 | 7.40 | 2.09 | 589. | 0.718 | 8.41   |
| 3.83 | 7.50 | 2.23 | 640. | 0.703 | 8.61   |
| 3.80 | 7.43 | 2.31 | 653  | 0.690 | 8.68   |
| 3.82 | 7.55 | 2.39 | 687  | 0.685 | 8.80   |
| 3.80 | 7.52 | 2.39 | 683  | 0.682 | 8.79   |
| 3.81 | 7.62 | 2.49 | 721  | 0.674 | 8.93   |
| 3.85 | 7.93 | 2.61 | 796  | 0.671 | 9.16   |
| 3.78 | 8.13 | 2.84 | 872  | 0.651 | 9.44   |
| 3.84 | 8.22 | 2.89 | 911  | 0.649 | 9.54   |
| 3.82 | 8.47 | 2.96 | 960  | 0.650 | 9.67   |
| 3.77 | 8.54 | 2.97 | 957  | 0.652 | 9.67   |
| 3.73 | 8.45 | 3.05 | 962  | 0.639 | 9.73   |
| 3.68 | 8.48 | 3.06 | 955  | 0.639 | 9.73   |
| 3.82 | 8.69 | 3.11 | 1031 | 0.643 | 9.88   |
| 3.75 | 8.79 | 3.32 | 1094 | 0.623 | 10.12  |
| 3.82 | 9.08 | 3.37 | 1168 | 0.629 | 10.27  |
| 3.80 | 9.00 | 3.37 | 1154 | 0.625 | 10.25  |
| 3.77 | 9.09 | 3.47 | 1190 | 0.618 | 10.37  |

US = 6.033 + 0.828\*UP KM/SEC. FOR UP FROM 0.5 TO 1.6 KM/SEC.  
SIGMA US = 0.12 KM/SEC

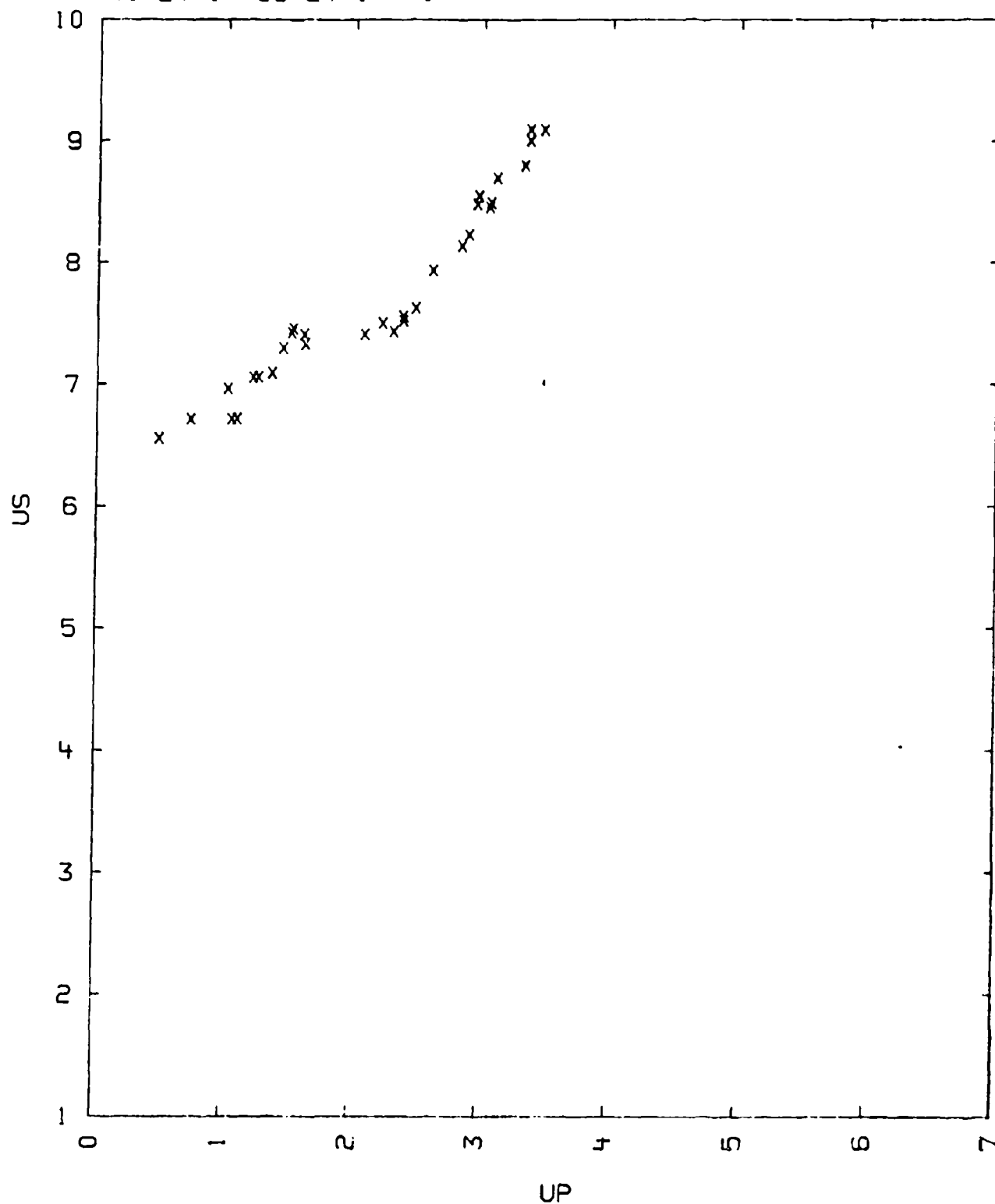
US = 4.008 + 1.477\*UP KM/SEC. FOR UP FROM 2.3 TO 3.5 KM/SEC.

SIGMA US = 0.079 KM/SEC.

## COMMENTS :

- 1) SOURCE: MCQUEEN R. G. AND MARSH S. P.  
PRIVATE COMMUNICATION (1966)  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VOI WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED FOR OLIVINES IN  
CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYSTALLOGRAPHIC ASSOC.,  
POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.  
THE EXACT COMPOSITION OF BOWLINGITE AND ORE WERE NOT GIVEN BUT THEIR  
DENSITIES WERE ASSUMED TO BE 2.27 AND 5.18 G/CC RESPECTIVELY, WHERE  
THE ORE WAS TAKEN AS PURE MAGNETITE. SEE W. E. FORD, DANAS TEXTBOOK  
OF MINERALOGY (JOHN WILEY 1932) 4TH. ED., FOR DESCRIPTION OF  
BOWLINGITE. THE BOWLINGITE FORMULA GIVEN IS A SIMPLIFICATION OF THE  
COMPOSITION GIVEN BY S. CAILLERE AND S. HENIN, CLAY MINERAL BULLETIN,  
VOL. 1, P 138 (1951). THEIR BOWLINGITES BESIDES HAVING 20 WT PERCENT  
WATER OF HYDRATION ALSO SHOWED VARYING AMOUNTS OF CA AND TI
- 4) THE MODAL ANALYSIS OF THESE SAMPLES OBTAINED THROUGH BIRCH WAS TAKEN  
FROM: F. BIRCH, J. GEOPHYS. RES., VOL. 65, P. 1083 (1960)
- 5) FURTHER WORK IS IN PROGRESS.

TABLE I  
DUNITE MOOIHOEK MINE, TRANSVAAL (SILICATE ROCK)  
41-24-1--93-24-1---1



53--36---1

ELKONITE 2125C (TUNGSTEN COPPER MIXTURE)

CU 74.5 WT PERCENT  
W 25.5 WT PERCENT

VO = 0.102 - 0.105 CC/G CL = 4.18 KM/SEC CO = 3.36 KM/SEC  
VOI = 0.09663 CC/G CS = 2.15 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RHO0             | US   | UP   | P     | V/VO   | MATERIAL           | US(ST) |
| 9.734            | 2.87 | 0.29 | 81.   | 0.8990 | CU                 | 4.31   |
| 9.724            | 3.28 | 0.40 | 128.  | 0.8780 | CU                 | 4.48   |
| 9.722            | 3.44 | 0.51 | 171.  | 0.8517 | CU                 | 4.63   |
| 9.642            | 3.76 | 0.59 | 214.  | 0.8431 | CU                 | 4.76   |
| 9.611            | 3.98 | 0.67 | 256.  | 0.8317 | CU                 | 4.88   |
| 9.547            | 4.14 | 0.79 | 312.  | 0.8092 | CU                 | 5.05   |
| 9.551            | 4.57 | 1.01 | 441.  | 0.7790 | CU                 | 5.38   |
| 9.767            | 5.00 | 1.17 | 571.  | 0.7660 | CU                 | 5.66   |
| 9.638            | 5.15 | 1.27 | 630.  | 0.7534 | CU                 | 5.80   |
| 9.762            | 5.56 | 1.45 | 787.  | 0.7392 | CU                 | 6.10   |
| 9.672            | 5.47 | 1.45 | 767.  | 0.7349 | CU                 | 6.08   |
| 9.796            | 5.79 | 1.62 | 919.  | 0.7202 | CU                 | 6.35   |
| 9.669            | 5.85 | 1.69 | 956.  | 0.7111 | CU                 | 6.45   |
| 9.776            | 5.92 | 1.76 | 1019. | 0.7027 | CU                 | 6.55   |
| 9.654            | 6.66 | 2.19 | 1408. | 0.6712 | CU                 | 7.20   |
| 9.775            | 7.10 | 2.44 | 1693. | 0.6563 | CU                 | 7.61   |
| 9.758            | 7.50 | 2.67 | 1954. | 0.6440 | CU                 | 7.96   |
| 9.578            | 7.61 | 2.77 | 2019. | 0.6360 | CU                 | 8.08   |

US = 3.289 + 1.581\*UP - 0.19/(1+U) 13 KM/SEC  
SIG US = 0.057 KM/SEC

## COMMENTS:

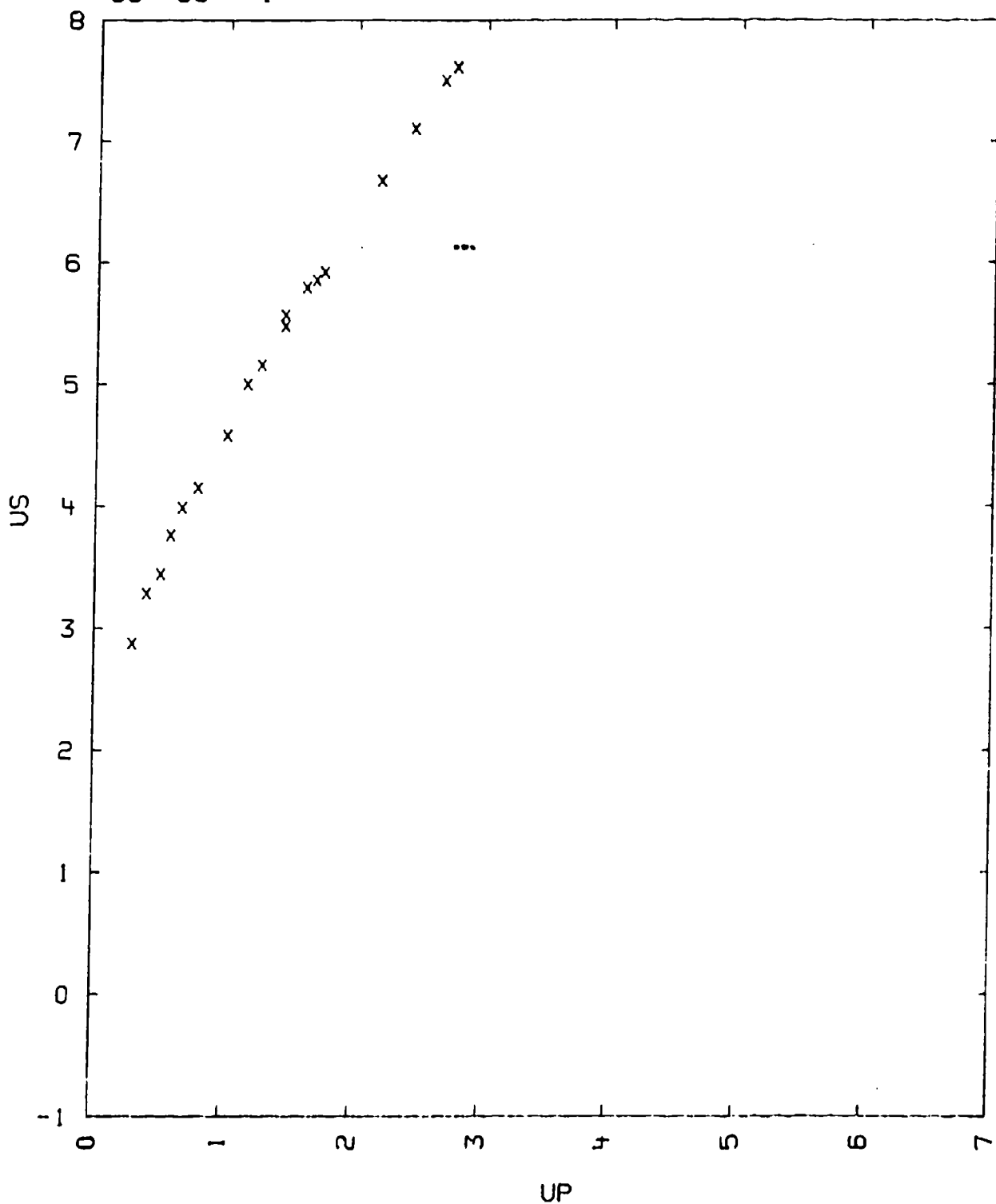
- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE : B  
DATA REDUCTION TECHNIQUE : B
- 3) VOI IS CALCULATED FROM IDEAL MIXTURE THEORY WITH :  
VOI(W) = 0.05192 CC/G, FROM WYCKOFF CRYSTAL STRUCTURES (JOHN WILEY  
AND SONS, N.Y., 1963) VOL. 1.  
VO(CU) = 0.1120 CC/G.
- 4) THE SAMPLES CONSIST OF SINTERED W, INFILTRATED WITH CU.

5)  $V(DP/DE) = 1.92$

PAGE 673

U06/15/77

TABLE 1  
ELKONITE 2125C (TUNGSTEN COPPER MIXTURE  
53--36---1



ELKONITE 1W3 (TUNGSTEN-COPPER MIXTURE)

W 55 WT PERCENT  
CU 45 WT PERCENT

VO = 0.0800 - 0.0845 CC/G CL = 4.55 KM/SEC CO = 3.36 KM/SEC  
VOI = 0.07893 CC/G CS = 2.66 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RHOO             | US   | UP   | P     | V/VO   | MATERIAL           | US(ST) |
| 12.440           | 3.67 | 0.34 | 155.  | 0.9074 | CU                 | 4.48   |
| 12.410           | 3.83 | 0.44 | 209.  | 0.8851 | CU                 | 4.63   |
| 12.170           | 4.09 | 0.51 | 254.  | 0.8753 | CU                 | 4.76   |
| 12.430           | 4.21 | 0.58 | 304.  | 0.8622 | CU                 | 4.88   |
| 12.450           | 4.42 | 0.68 | 374.  | 0.8462 | CU                 | 5.05   |
| 11.950           | 4.44 | 0.80 | 424.  | 0.8198 | CU                 | 5.21   |
| 12.460           | 4.73 | 0.88 | 519.  | 0.8140 | CU                 | 5.38   |
| 12.500           | 5.03 | 1.05 | 660.  | 0.7913 | CU                 | 5.66   |
| 12.460           | 5.18 | 1.16 | 749.  | 0.7761 | CU                 | 5.84   |
| 12.450           | 5.43 | 1.30 | 879.  | 0.7606 | CU                 | 6.08   |
| 12.240           | 5.31 | 1.34 | 871.  | 0.7476 | CU                 | 6.10   |
| 12.360           | 5.65 | 1.48 | 1034. | 0.7381 | CU                 | 6.35   |
| 12.320           | 5.78 | 1.53 | 1090. | 0.7353 | CU                 | 6.45   |
| 12.360           | 5.90 | 1.59 | 1159. | 0.7305 | CU                 | 6.55   |
| 11.790           | 6.50 | 2.03 | 1556. | 0.6877 | CU                 | 7.20   |
| 12.300           | 6.79 | 2.26 | 1887. | 0.6672 | CU                 | 7.61   |
| 12.020           | 7.22 | 2.48 | 2152. | 0.6565 | CU                 | 7.96   |
| 12.460           | 7.31 | 2.56 | 2332. | 0.6498 | CU                 | 8.13   |

US =  $3.43 + 1.516 \cdot UP - 1.25 / (1 + UP) \cdot 5$  KM/SEC  
SIG US = 0.065 KM/SEC

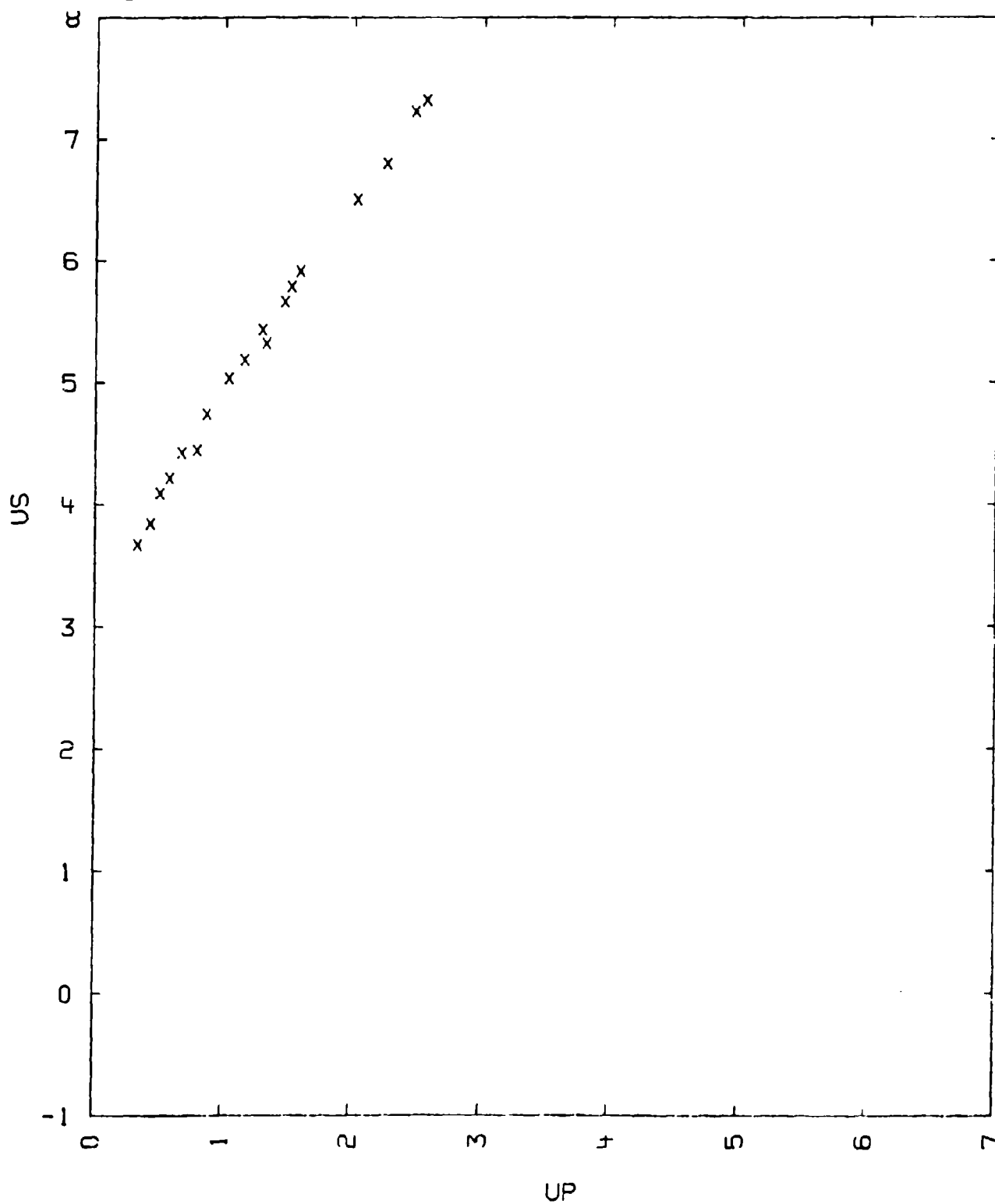
## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE : B  
DATA REDUCTION TECHNIQUE : B
- 3) VOI CALCULATED BY ASSUMING VOLUME ADDITIVITY AND THE CRYSTAL  
DENSITIES FROM WYCKOFF, CRYSTAL STRUCTURES (JOHN WILEY AND SONS,  
N.Y., 1963).

- 4) THE SAMPLES CONSIST OF SINTERED W INFILTRATED WITH CU.
- 5)  $VDP/DEL = 1.8$



TABLE I  
ELKONITE 1W3 (TUNGSTEN-COPPER MIXTURE)  
53--36---2



53--36---3

ELKONITE 3W3 (TUNGSTEN-COPPER MIXTURE)

W 68 WT PERCENT  
 CU 32 WT PERCENT

V0 = 0.0729 - 0.0721 CC/G CL = 4.75 KM/SEC CO = 3.77 KM/SEC  
 V01 = 0.07112 CC/G CS = 2.50 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
 AND DENSITY IN G/CC.

TABLE

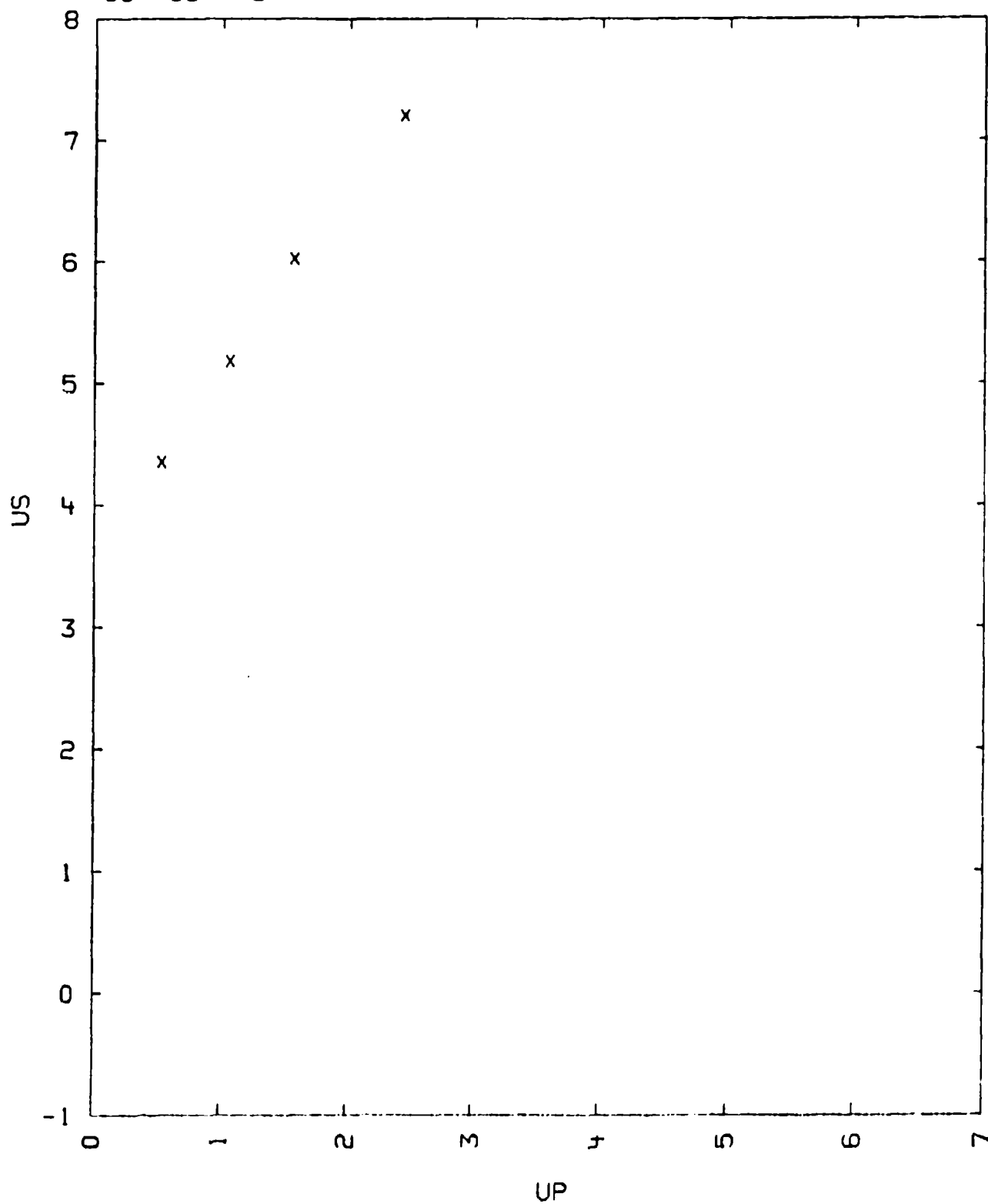
| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RH00             | US   | UP   | P     | V/V0   | MATERIAL           | US(ST) |
| 13.860           | 4.35 | 0.53 | 320.  | 0.8782 | CU                 | 4.87   |
| 13.870           | 5.18 | 1.07 | 769.  | 0.7934 | CU                 | 5.80   |
| 13.820           | 6.02 | 1.57 | 1306. | 0.7392 | CU                 | 6.65   |
| 13.710           | 7.20 | 2.44 | 2409. | 0.6611 | CU                 | 8.08   |

US = 3.807 + 1.404\*UP - 0.75/(1+UP)\*\*3 KM/SEC  
 SIG US = 0.071 KM/SEC

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MAPSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
 AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE : B  
 DATA REDUCTION TECHNIQUE : B
- 3) V01 IS CALCULATED BY ASSUMING VOLUME ADDITIVITY AND THE DENSITIES  
 GIVEN BY WYCKOFF CRYSTAL STRUCTURES. (JOHN WILEY AND SONS, N.Y.,  
 1963) VOL. 1.
- 4) THE SAMPLE IS MADE OF SINTERED W INFILTRATED WITH CU.
- 5) V(OP/DE) = 1.74

TABLE I  
ELKONITE 3W3 (TUNGSTEN-COPPER MIXTURE)  
53--36---3



53--36---4

ELKONITE 10W3 (TUNGSTEN-COPPER MIXTURE)

W 76 WT PERCENT  
 CU 24 WT PERCENT

VO = 0.0671 - 0.0675 CC/G    CL = 4.77 KM/SEC    CO = 3.77 KM/SEC  
 VOI = 0.06632 CC/G    CS = 2.53 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
 AND DENSITY IN G/CC.

TABLE

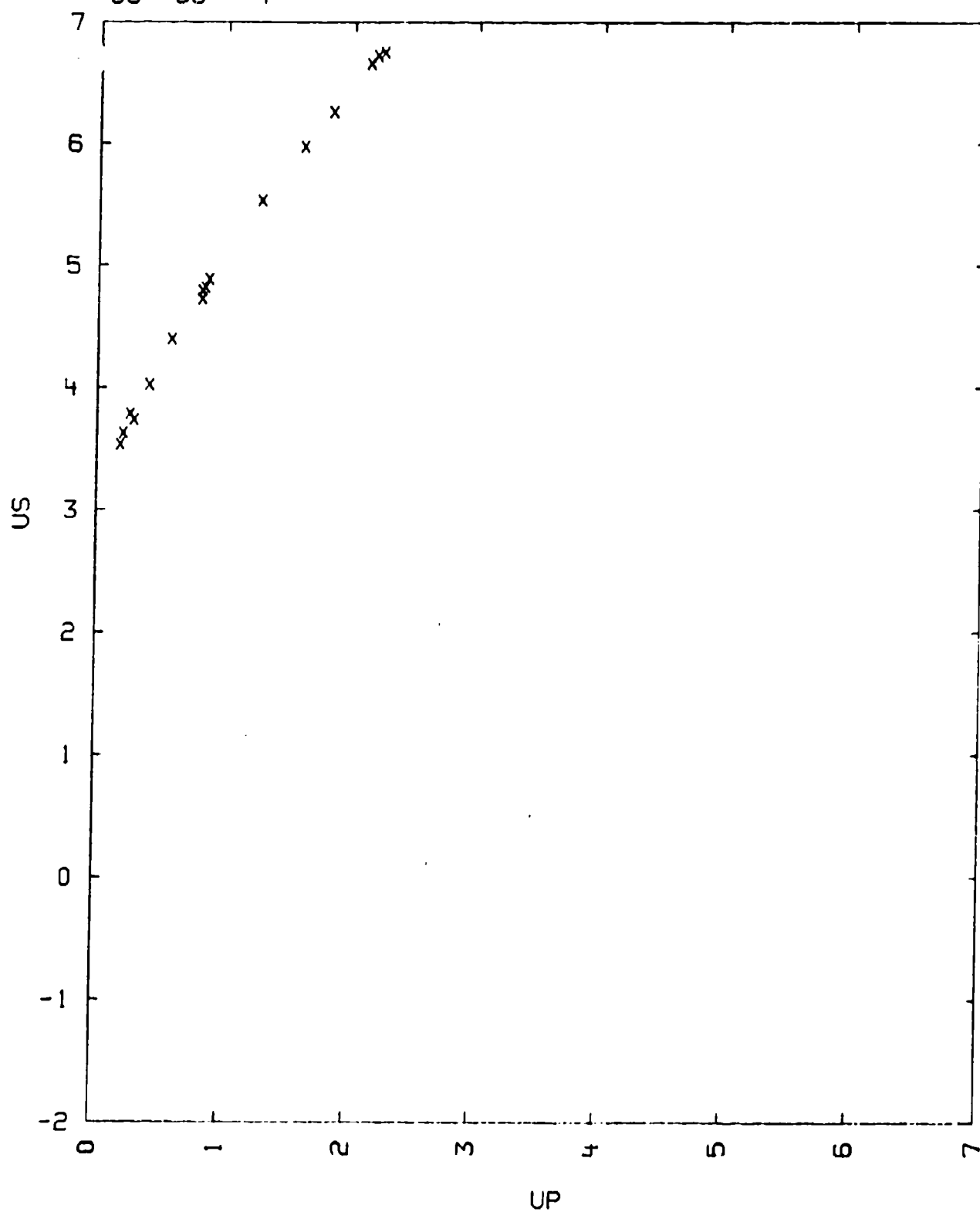
| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |        |
|------------------|------|------|-------|--------|--------------------|--------|
| RH00             | US   | UP   | P     | V/VO   | MATERIAL           | US(ST) |
| 14.890           | 3.53 | 0.19 | 100.  | 0.9462 | CU                 | 4.27   |
| 14.830           | 3.62 | 0.21 | 113.  | 0.9420 | CU                 | 4.31   |
| 14.840           | 3.78 | 0.26 | 146.  | 0.9312 | CU                 | 4.41   |
| 14.830           | 3.73 | 0.29 | 160.  | 0.9223 | CU                 | 4.45   |
| 14.830           | 4.02 | 0.41 | 244.  | 0.8980 | CU                 | 4.67   |
| 14.810           | 4.39 | 0.58 | 377.  | 0.8679 | CU                 | 4.98   |
| 14.900           | 4.79 | 0.82 | 585.  | 0.8288 | CU                 | 5.41   |
| 14.860           | 4.72 | 0.82 | 575.  | 0.8263 | CU                 | 5.41   |
| 14.880           | 4.81 | 0.84 | 601.  | 0.8254 | CU                 | 5.44   |
| 14.840           | 4.88 | 0.87 | 630.  | 0.8217 | CU                 | 5.51   |
| 14.830           | 5.53 | 1.28 | 1050. | 0.7685 | CU                 | 6.23   |
| 14.820           | 5.97 | 1.62 | 1433. | 0.7286 | CU                 | 6.79   |
| 14.860           | 6.26 | 1.84 | 1712. | 0.7061 | CU                 | 7.16   |
| 14.820           | 6.65 | 2.13 | 2099. | 0.6797 | CU                 | 7.65   |
| 14.880           | 6.72 | 2.19 | 2190. | 0.6741 | CU                 | 7.75   |
| 14.890           | 6.74 | 2.24 | 2248. | 0.6677 | CU                 | 7.82   |

US = 3.865 + 1.318\*UP - 0.97/(1+UP)\*.3 KM/SEC  
 SIG US = 0.04 KM/SEC

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE : B  
 DATA REDUCTION TECHNIQUE : B
- 3) VOI IS CALCULATED BY ASSUMING VOLUME ADDITIVITY AND THE COMPONENT  
 DENSITIES OBTAINED FROM WYCKOFF, CRYSTAL STRUCTURES (JOHN WILEY AND  
 SONS, N.Y., 1963).
- 4) THE SAMPLES ARE SINTERED W INFILTRATED WITH CU.
- 5) V(OP/DE) = 1.70

TABLE I  
ELKONITE 10W3 (TUNGSTEN-COPPER MIXTURE)  
53--36---4



53--39--36---1  
TUNGSTEN-NICKEL-COPPER ALLOY

W 90 PERCENT  
NI 7.5 PERCENT  
CU 2.5 PERCENT

$V_0 = 0.05952 \text{ CC/G.}$   
 $V_{01} = 0.05774 \text{ CC/G.}$

IN THE TABLE BELOW, DENSITY IS GIVEN G/CC., VELOCITIES IN KM/SEC.,  
AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US   | UP   | P    | V/V0  |
|------|------|------|------|-------|
| 16.8 | 3.94 | 0.41 | 271  | 0.896 |
| -    | 3.87 | 0.42 | 273  | 0.891 |
| -    | 3.94 | 0.42 | 278  | 0.893 |
| -    | 4.85 | 0.82 | 668  | 0.831 |
| -    | 4.67 | 0.85 | 667  | 0.818 |
| -    | 4.81 | 0.85 | 687  | 0.823 |
| -    | 4.88 | 0.89 | 730  | 0.818 |
| -    | 5.08 | 1.04 | 887  | 0.795 |
| -    | 5.20 | 1.04 | 908  | 0.800 |
| -    | 5.85 | 1.51 | 1484 | 0.742 |
| -    | 5.92 | 1.49 | 1482 | 0.748 |
| -    | 6.35 | 1.82 | 1941 | 0.713 |
| -    | 6.31 | 1.85 | 1961 | 0.707 |
| -    | 6.34 | 1.86 | 1981 | 0.707 |

$US = 2.95 + 2.47 \cdot UP - 0.342 \cdot UP^2 \text{ KM/SEC.}$   $SIGMA US = 0.07 \text{ KM/SEC.}$

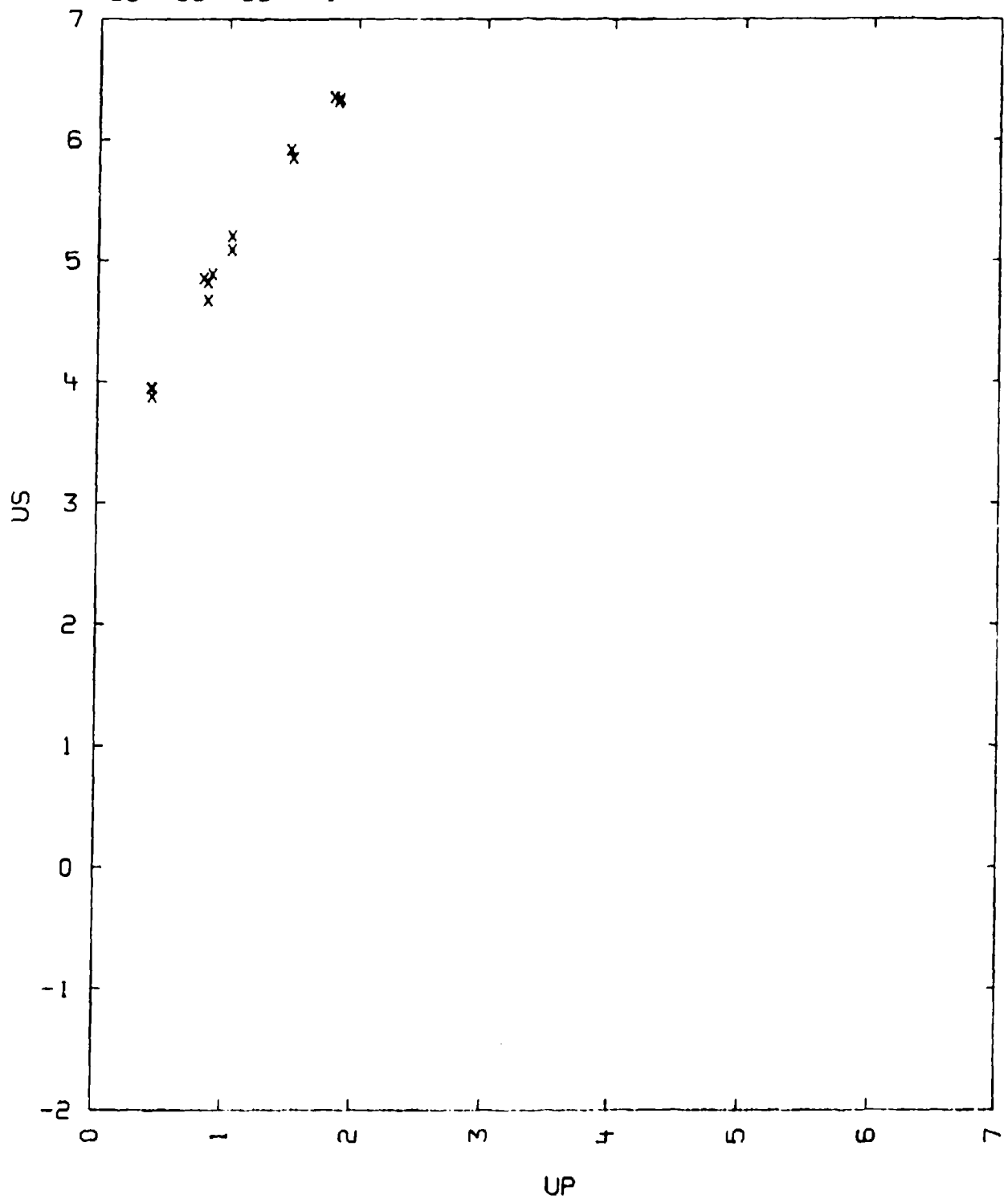
## COMMENTS:

- 1) SOURCE: HART AND SKIDMORE I. C.  
PRIVATE COMMUNICATION (1965)  
SKIDMORE, I. C.  
APPLIED MATERIALS RESEARCH, VOL. 4, P. 131. (1965)
- 2) EXPERIMENTAL TECHNIQUE A.  
DATA REDUCTION TECHNIQUE B  
FE AND BRASS STANDARDS WERE USED.
- 3) THE TUNGSTEN ALLOY SAMPLE WAS A POROUS SINTER. ASSUMING A GRUNEISEN EQUATION OF STATE WITH A CONSTANT GRUNEISEN CONSTANT OF 1.88, IT IS FOUND THAT THE DATA IS CONSISTENT WITH THE RELATIONS FOR THE VOIDLESS MATERIAL WHICH MAY BE REPRESENTED BY  $US = 3.94 + 1.44 UP \text{ KM/SEC.}$

TABLE I

TUNGSTEN-NICKEL-COPPER ALLOY

53--39--36---1



53--39--36---2  
FANSTEEL 77 (TUNGSTEN ALLOY)

TUNGSTEN W 90.0 +OR- 0.5 WT PERCENT  
NICKEL NI 6.0 +OR- 0.3 WT PERCENT  
COPPER CU 4.0 +OR- 0.2 WT PERCENT

$V_0 = 0.05893 \pm 0.0013 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC, AND PRESSURE IN KILOBARS.

TABLE

| RHOD  | US   | UP    | P    | V/V <sub>0</sub> |
|-------|------|-------|------|------------------|
| 16.89 | 5.34 | 1.076 | 970  | 0.7985           |
| -     | 5.79 | 1.387 | 1360 | 0.7604           |
| -     | 6.38 | 1.809 | 1850 | 0.7165           |
| -     | 8.42 | 3.468 | 4930 | 0.5881           |
| -     | 9.08 | 3.818 | 5860 | 0.5795           |

$US = 3.94 + 1.32 \cdot UP \pm 0.09 \text{ KM/SEC}$

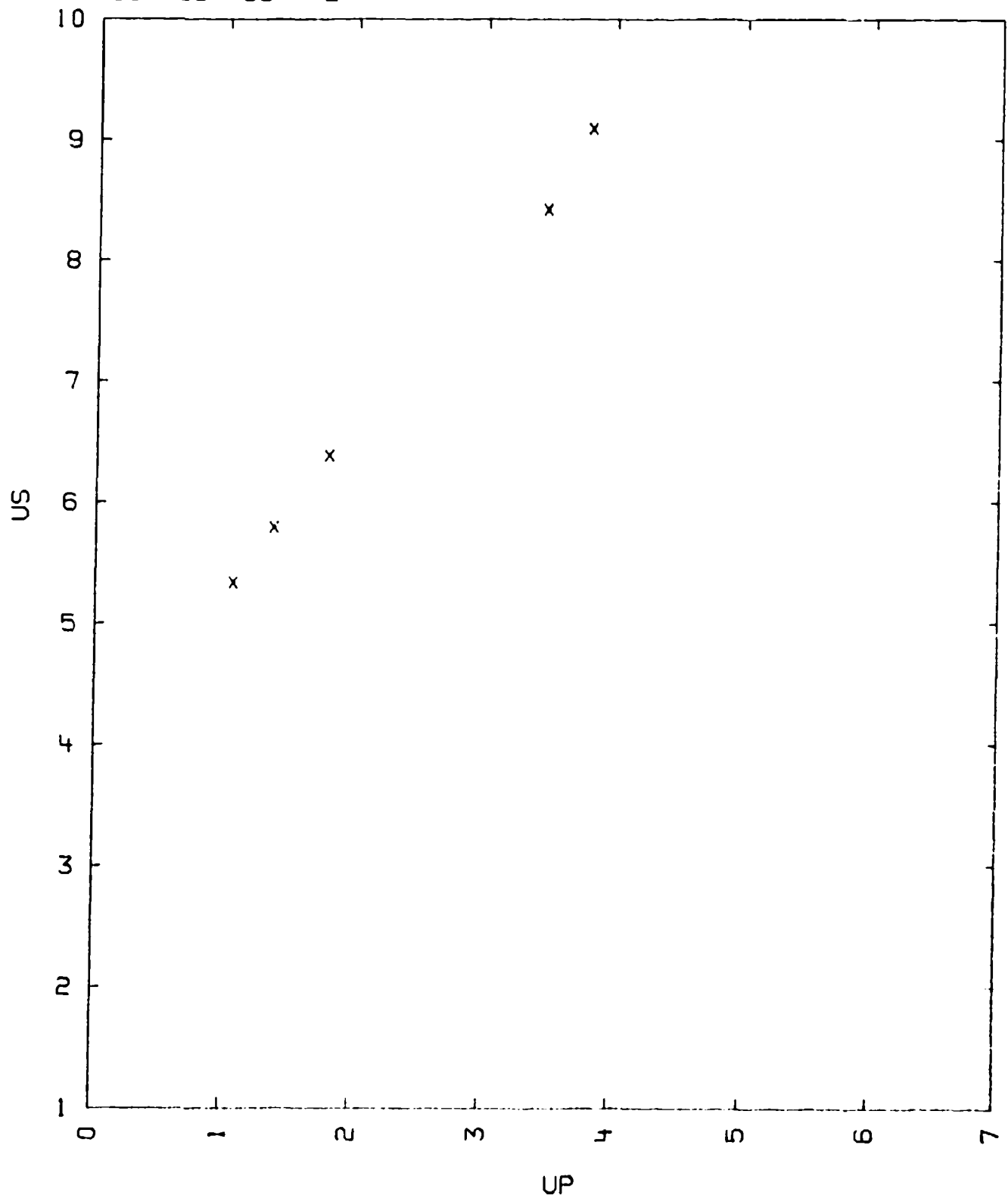
## COMMENTS:

- 1) SOURCE: JONES, A. H., ISBELL, W. M. AND MAIDEN C. J.  
JOURNAL OF APPLIED PHYSICS, VOL.37, P.3493 (1966)
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION METHOD A  
STANDARD MATERIAL FANSTEEL 77.
- 3) THE DRIVER PLATES WERE ACCELERATED BY MEANS OF A LIGHT GAS GUN.
- 4) THE DRIVER PLATE VELOCITY AND SPATIAL ORIENTATION WAS MEASURED USING TWO-PULSE X-RAY STATIONS PRIOR TO IMPACT. THE X-RAY EXPOSURES TIMES WERE 30 NSEC, AND THE INTERVAL TIME BETWEEN X-RAY PULSES WAS MEASURED ON A 100-MC/SEC. COUNTER.
- 5) FOR BOTH THE IMPACT VELOCITY AND SHOCK VELOCITY THE MEASURED EXPERIMENTAL ERROR IS WITHIN 1 PERCENT.



TABLE 1

FANSTEEL 77 (TUNGSTEN ALLOY)  
53--39--36---2



53--39--36---3  
FANSTEEL

|    |             |            |
|----|-------------|------------|
| W  | 89.9 - 90.1 | WT PERCENT |
| CU | 3.2 - 4.4   | - -        |
| NI | 5.9 - 6.3   | - -        |

V0 = 0.0588 CC/G      C1 = 5.049 KM/SEC      C0 = 3.912 KM/SEC  
CS = 2.765 KM/SEC

IN THE TABLE BELOW, RH00 IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,  
PRESSURE IN KBARS, WF IS WEIGHTING FACTOR USED IN FIT AND IMPACTOR  
MATERIAL IS FANSTEEL.

TABLE

| -----SAMPLE----- |       |       |       |       | IMPACTOR |       |
|------------------|-------|-------|-------|-------|----------|-------|
| RH00             | US    | UP    | P     | V/V0  | WF       | U     |
| 17.01            | 4.599 | 0.453 | 0.354 | .9015 | 3        | 0.906 |
| 17.01            | 4.978 | 0.740 | 0.627 | .8514 | 1        | 1.478 |
| 17.01            | 5.194 | 0.976 | 0.862 | .8121 | 3        | 1.952 |
| 17.01            | 5.336 | 1.076 | 0.977 | .7984 | 1        | 2.152 |
| 17.01            | 5.661 | 1.344 | 1.294 | .7626 | 3        | 2.689 |
| 17.01            | 5.756 | 1.344 | 1.316 | .7665 | 3        | 2.689 |
| 17.01            | 5.786 | 1.387 | 1.365 | .7603 | 2        | 2.774 |
| 17.01            | 5.855 | 1.425 | 1.419 | .7566 | 3        | 2.849 |
| 17.01            | 6.163 | 1.706 | 1.788 | .7232 | 3        | 3.413 |
| 17.01            | 6.221 | 1.774 | 1.877 | .7148 | 1        | 3.548 |
| 17.01            | 6.365 | 1.809 | 1.959 | .7158 | 3        | 3.618 |
| 17.01            | 6.412 | 1.824 | 1.989 | .7155 | 1        | 3.648 |
| 17.01            | 6.490 | 1.997 | 2.205 | .6923 | 2        | 3.994 |
| 17.01            | 6.939 | 2.329 | 2.749 | .6644 | 1        | 4.657 |
| 17.01            | 7.082 | 2.405 | 2.897 | .6604 | 3        | 4.809 |
| 17.01            | 9.239 | 3.323 | 4.529 | .6077 | 1        | 6.646 |
| 17.01            | 8.390 | 3.468 | 4.949 | .5867 | 1        | 6.936 |

US = 4.008 + 1.262\*UP KM/SEC  
SIG US = 0.021 KM/SEC

## COMMENTS:

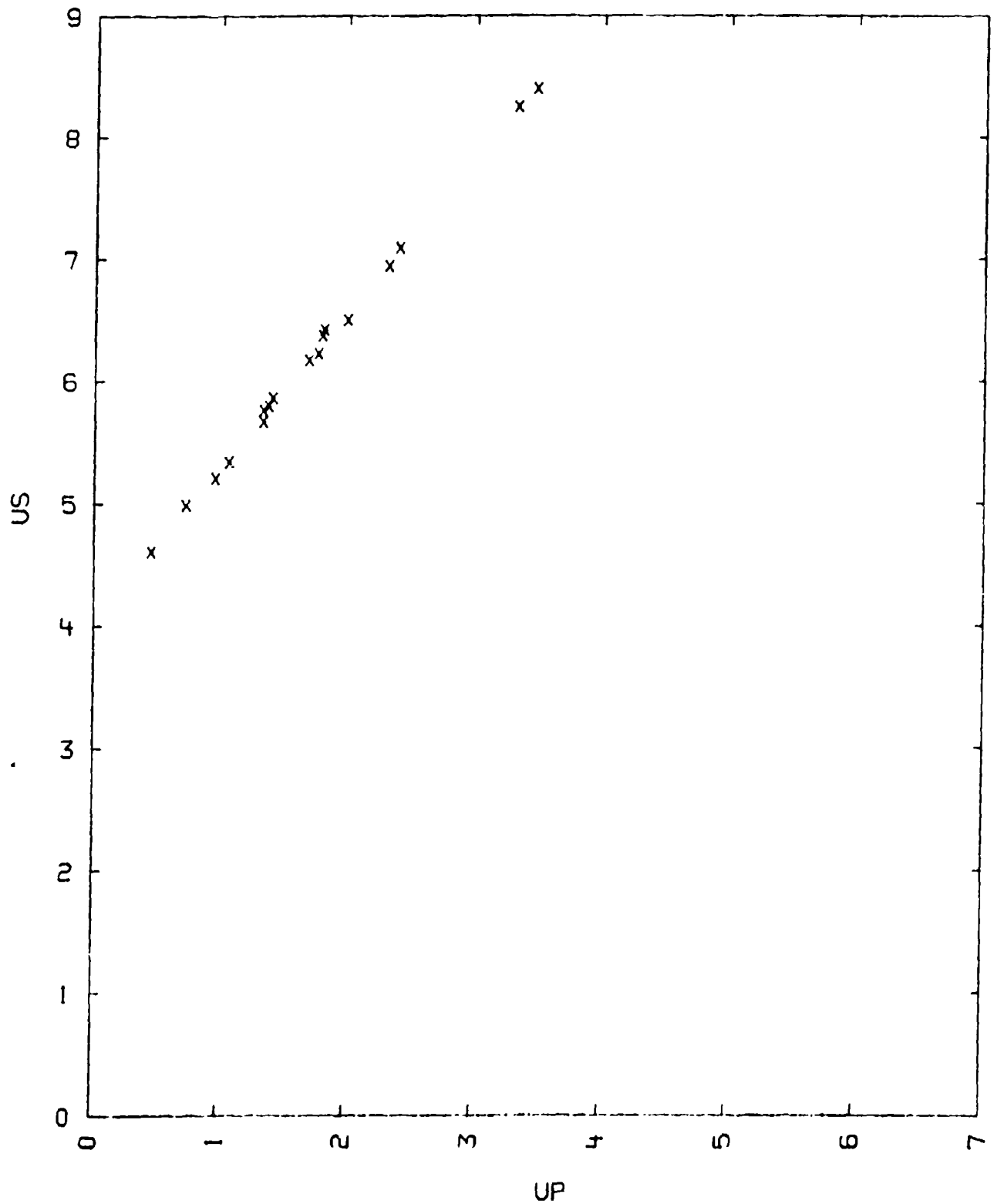
- 1) SOURCE: ISBELL, W.M., SHIPMAN, F.H. AND JONES A.H.  
HUGONIOT EQUATION OF STATE MEASUREMENTS TO FIVE MEGABARS  
REPORT MSL-68-13 (DECEMBER 1968)  
MATERIALS AND STRUCTURES LABORATORY  
GENERAL MOTORS TECHNOLOGY CENTER, WARREN, MICHIGAN 48090
- 2) EXPERIMENTAL TECHNIQUE: A  
DATA REDUCTION TECHNIQUE: A
- 3) IMPACTOR VELOCITY IS ESTIMATED IN ENTRY 2. THE UNCERTAINTY IN UP  
IS THEREFORE .019 KM/SEC UNCERTAINTIES IN US AND U ARE NORMALLY  
0.5 AND 0.05 PERCENT
- 4) ALSO MEASURED WERE YIELD STRENGTH 5.86 KBARS  
ULTIMATE TENSILE STRENGTH 6.76 KBARS  
POISSON RATIO 0.286

006/15/77

TABLE I

FANSTEEL

53--39--36---3



53-23--36---1

ELKONITE TC-10 (TUNGSTEN CARBIDE - COPPER MIXTURE)

|                  |     |                 |
|------------------|-----|-----------------|
| TUNGSTEN CARBIDE | W-C | 58.0 WT PERCENT |
| COPPER           | CU  | 42 WT PERCENT   |

|                    |                  |                  |
|--------------------|------------------|------------------|
| VO = 0.0857 CC/G   | CL = 5.43 KM/SEC | CO = 4.23 KM/SEC |
| VOI = 0.08403 CC/G | CS = 2.95 KM/SEC |                  |

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |       |        | -----STANDARD----- |       |
|------------------|------|------|-------|--------|--------------------|-------|
| RH00             | US   | UP   | P     | V/VO   | MATERIAL           | US(1) |
| 11.670           | 4.13 | 0.20 | 96.   | 0.9516 | CU                 | 4.27  |
| 11.660           | 4.30 | 0.22 | 110.  | 0.9488 | CU                 | 4.31  |
| 11.670           | 4.36 | 0.28 | 142.  | 0.9358 | CU                 | 4.41  |
| 11.460           | 4.33 | 0.30 | 149.  | 0.9307 | CU                 | 4.45  |
| 11.690           | 4.65 | 0.43 | 234.  | 0.9075 | CU                 | 4.67  |
| 11.670           | 4.93 | 0.62 | 357.  | 0.8742 | CU                 | 4.98  |
| 11.680           | 5.42 | 0.94 | 595.  | 0.8266 | CU                 | 5.51  |
| 11.670           | 6.09 | 1.38 | 981.  | 0.7734 | CU                 | 6.23  |
| 11.680           | 6.61 | 1.72 | 1328. | 0.7398 | CU                 | 6.79  |
| 11.660           | 6.96 | 1.95 | 1582. | 0.7198 | CU                 | 7.16  |
| 11.660           | 7.38 | 2.26 | 1945. | 0.6938 | CU                 | 7.65  |

US = 4.057 + 1.479\*UP - 0.428/(1+UP)\*\*5 KM/SEC  
 SIG US = 0.041 KM/SEC

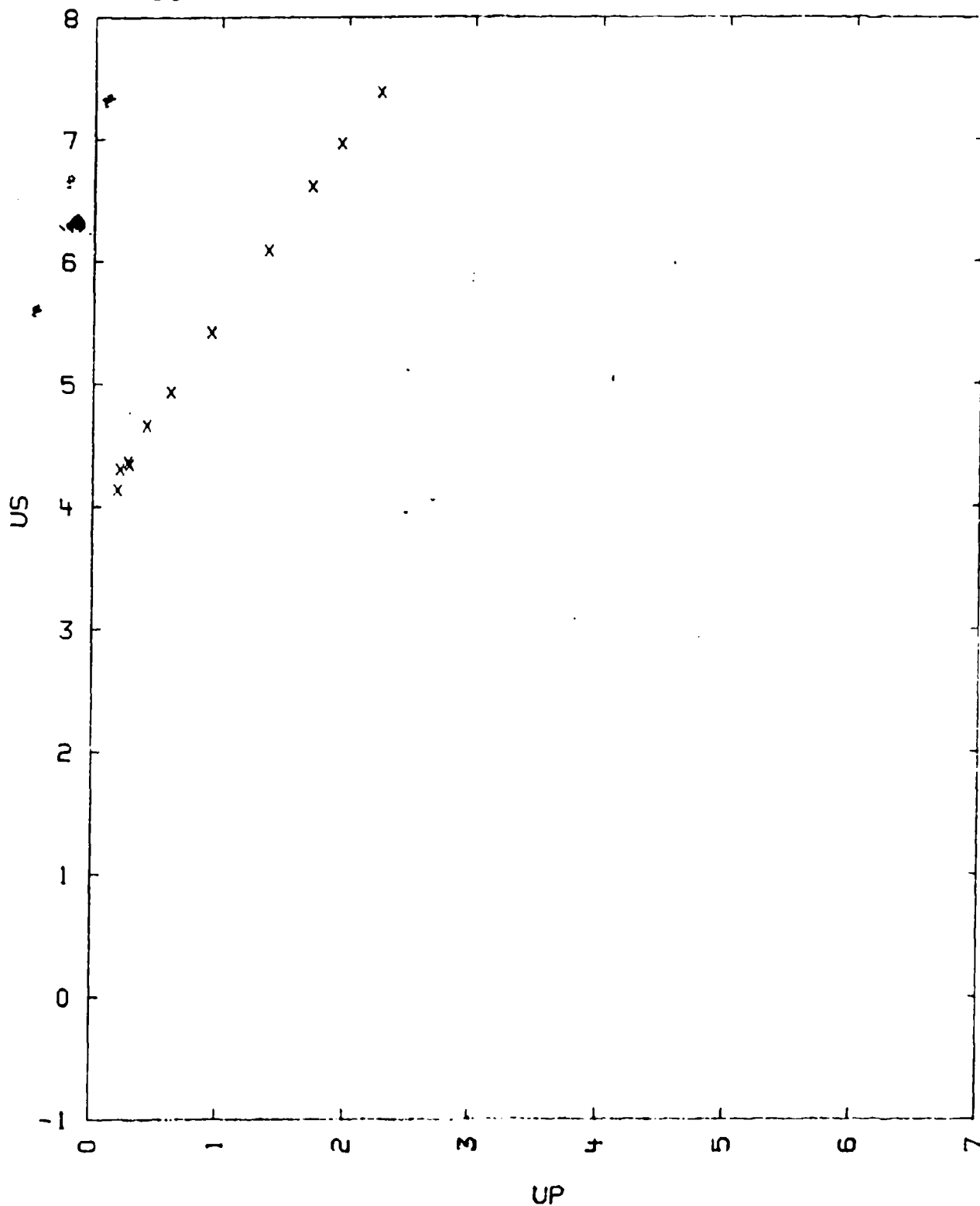
## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES, HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
 DATA REDUCTION TECHNIQUE: B
- 3) VOI FROM IDEAL MIXTURE THEORY.  
 VOI(W-C) = 0.063812 CC/G FROM WYCKOFF, CRYSTAL STRUCTURES (JOHN WILEY AND SONS, N.Y., 1963), VOL. 1 RH00(CU) = 8.93 G/CC.
- 4) THE SAMPLES CONSIST OF SINTERED W-C INFILTRATED WITH CU.
- 5) V(DP/DE) = 1.74

TABLE I

ELKONITE TC-10 (TUNGSTEN CARBIDE - COPPER MIXTURE)

53-23--36---1



88-55-58---1  
NULBERRY

|    |                |            |
|----|----------------|------------|
| U  | 90.0           | WT PERCENT |
| NB | 7.5 + OR - 0.5 | -          |
| ZR | 2.5 + OR - 0.5 | -          |

VO = .0603 - 0.0614 CC/G CL = 2.92 KM/S CO = 2.57 KM/S  
VOI = .0602 - 0.0606 CC/G CS = 1.19 KM/S

IN THE TABLE BELOW VELOCITIES ARE IN KM/S, PRESSURE IN KILOBARS AND D MM. EXP. INDICATES THE EXPERIMENTAL TECHNIQUE AND MAT IS THE STANDARD BASEPLATE OR IMPACTOR MATERIAL.

TABLE

| -----SAMPLE-----STANDARD |      |      |       |      |        |      |     |     |      |
|--------------------------|------|------|-------|------|--------|------|-----|-----|------|
| RH00                     | US   | UP   | UFS   | P    | V/V0   | D    | EXP | MAT | P    |
| 16.53                    | 3.00 | .03  |       | 14.  | 0.9906 | 6.4  | 12  | STU | 14.  |
| 16.59                    | 2.94 | .09  |       | 46.  | 0.9679 | 6.4  | 12  | STU | 46.  |
| 16.59                    | 2.95 | .16  |       | 77.  | 0.9467 | 6.4  | 12  | STU | 77.  |
| 16.59                    | 3.04 | .16  |       | 81.  | 0.9472 | 6.4  | 12  | STU | 81.  |
| 16.59                    | 3.04 | .25  |       | 126. | 0.9178 |      | A   | STU | 126. |
| 16.59                    | 3.16 | .30  |       | 157. | 0.9052 |      | A   | STU | 157. |
| 16.59                    | 3.51 | .35  |       | 204. | 0.9003 |      | A   | STU | 204. |
| 16.35                    | 3.0  | .115 | .226  | 54.  | 0.9633 | 6.4  | C3  | PB  | 40.  |
| 16.49                    | 2.97 | .115 | .248  | 54.  | 0.9629 | 6.4  | C3  | PB  | 40.  |
| 16.29                    | 3.06 | .113 | .272  | 54.  | 0.9646 | 6.4  | C3  | PB  | 39.  |
| 16.41                    | 3.02 | .113 | .280  | 54.  | 0.9639 | 6.4  | C3  | PB  | 39.  |
| 16.36                    | 3.06 | .113 | .290  | 54.  | 0.9647 | 6.4  | C3  | PB  | 40.  |
| 16.44                    | 3.07 | .113 | .304  | 54.  | 0.9651 | 6.4  | C3  | PB  | 40.  |
| 16.44                    | 3.04 | .113 | .276  | 54.  | 0.9645 | 6.4  | C3  | PB  | 40.  |
| 16.38                    | 3.00 | .150 | .290  | 73.  | 0.9505 | 6.4  | C3  | PB  | 54.  |
| 16.39                    | 3.01 | .150 | .276  | 73.  | 0.9508 | 6.4  | C3  | PB  | 54.  |
| 16.24                    | 3.04 | .195 | .368  | 98.  | 0.9347 | 6.4  | C3  | PB  | 73.  |
| 16.28                    | 3.03 | .195 | .394  | 98.  | 0.9344 | 6.4  | C3  | PB  | 73.  |
| 16.40                    | 3.02 | .20  | .460  | 102. | 0.9318 | 6.4  | C3  | PB  | 75.  |
| 16.45                    | 3.01 | .20  | .487  | 102. | 0.9316 | 6.4  | C3  | PB  | 75.  |
| 16.44                    | 3.05 | .2   | .458  | 102. | 0.9333 | 6.4  | C3  | PB  | 75.  |
| 16.32                    | 3.04 | .213 | .444  | 105. | 0.9304 | 12.7 | C3  | PB  | 79.  |
| 16.40                    | 2.98 | .195 | .490  | 97.  | 0.9334 | 25.4 | C3  | PB  | 72.  |
| 16.42                    | 3.05 | .233 | .432  | 117. | 0.9234 | 6.4  | C3  | PB  | 86.  |
| 16.43                    | 3.08 | .233 | .424  | 117. | 0.9249 | 6.4  | C3  | PB  | 86.  |
| 16.48                    | 3.12 | .275 | .568  | 141. | 0.9121 | 6.4  | C3  | PB  | 106. |
| 16.43                    | 3.14 | .275 | .540  | 141. | 0.9130 | 6.4  | C3  | PB  | 106. |
| 16.43                    | 3.15 | .273 | .526  | 142. | 0.9129 | 6.4  | C3  | PB  | 107. |
| 16.29                    | 3.15 | .273 | .528  | 142. | 0.9121 | 6.4  | C3  | PB  | 107. |
| 16.39                    | 3.02 | .285 | .568  | 145. | 0.9030 | 12.7 | C3  | PB  | 114. |
| 16.44                    | 3.15 | .275 | .544  | 142. | 0.9130 | 6.4  | C3  | PB  | 107. |
| 16.44                    | 3.13 | .275 | .548  | 142. | 0.9118 | 6.4  | C3  | PB  | 107. |
| 16.34                    | 3.10 | .230 | .470  | 117. | 0.9255 | 25.4 | C3  | PB  | 93.  |
| 16.44                    | 3.28 | .44  | .842  | 236. | 0.8666 | 6.4  | C3  | BR  | 200. |
| 16.49                    | 3.09 | .44  | .844  | 237. | 0.8495 | 6.4  | C3  | BR  | 200. |
| 16.45                    | 3.53 | .563 | 1.146 | 327. | 0.8405 | 6.4  | C3  | BR  | 252. |

## MULBERRY

| RH00  | US   | UP   | UFS   | P     | V/V0   | D   | EXP | MAT | P     |
|-------|------|------|-------|-------|--------|-----|-----|-----|-------|
| 16.48 | 3.54 | .563 | 1.154 | 327.  | 0.8417 | 6.4 | C3  | BR  | 252.  |
| 16.59 | 3.30 | .292 | .610  | 160.  | 0.9114 | 6.4 | B   | BR  | 131.  |
| 16.58 | 3.53 | .614 |       | 360.  | 0.8258 | 6.4 | B   | BR  | 300.  |
| 16.58 | 3.51 | .653 |       | 380.  | 0.8140 | 6.4 | B   | BR  | 300.  |
| 16.59 | 3.99 | .995 | 1.92  | 658.  | 0.7509 | 6.4 | B   | BR  | 542.  |
| 16.58 | 4.26 | 1.11 | 2.18  | 783.  | 0.7378 | 6.4 | B   | BR  | 642.  |
| 16.56 | 4.82 | 1.51 | 3.10  | 1200. | 0.6881 | 6.4 | B   | BR  | 965.  |
| 16.56 | 5.59 | 2.03 | 4.22  | 1880. | 0.6367 | 6.4 | B   | BR  | 1500. |

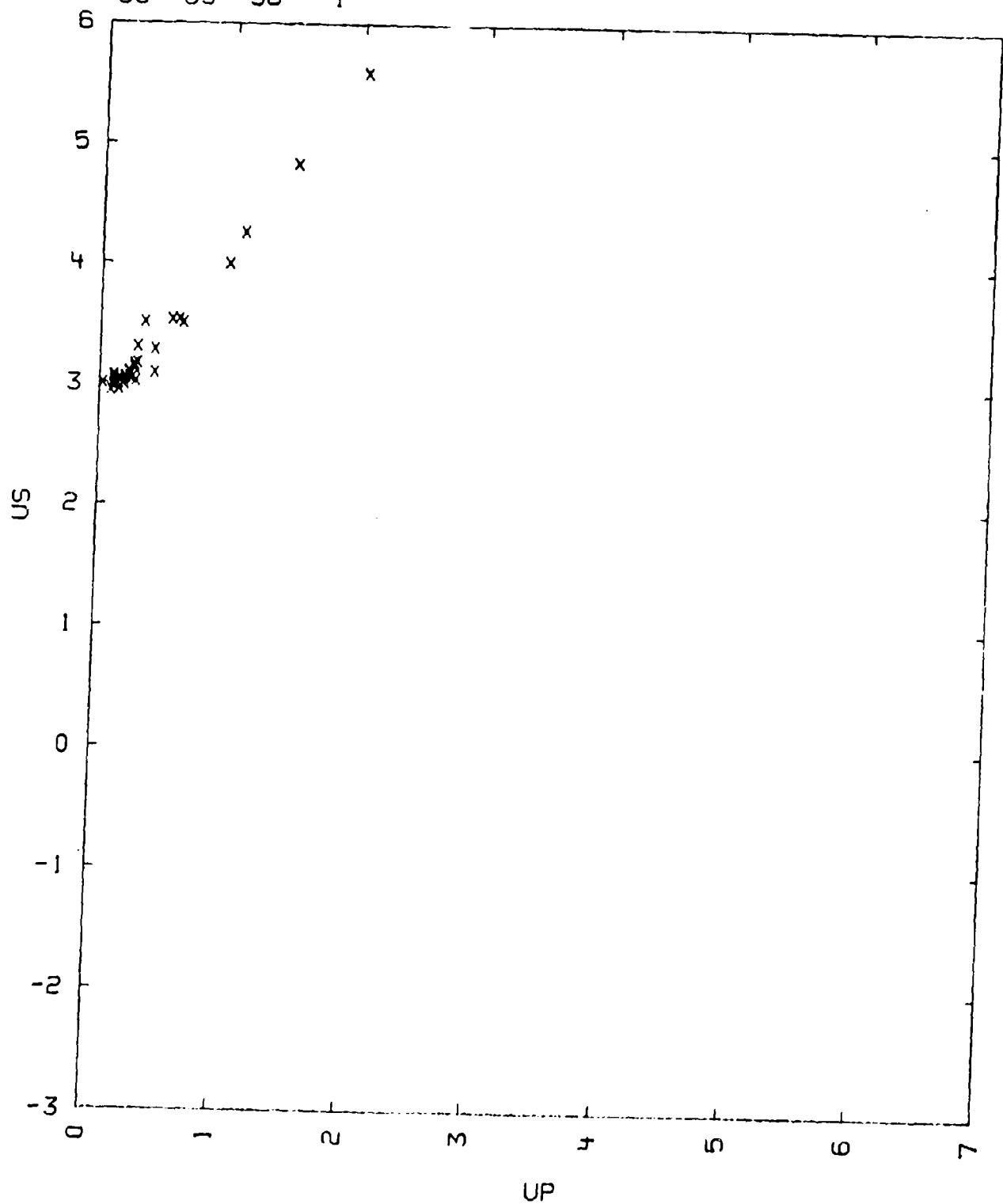
US =

## COMMENTS:

- 1) SOURCE: GUST W.N. AND ROYCE E.B.  
SHOCK COMPRESSION OF THE STAINLESS URANIUM ALLOY MULBERRY  
LAWRENCE LIVERMORE LABORATORY REPORT UCRL 50888 (1970)  
A KUSBOV - S DIVISION  
LAWRENCE LIVERMORE LABORATORY REPORT STN 183 (1968)
- 2) EXPERIMENTAL TECHNIQUE AS SHOWN IN TABLE.  
DATA REDUCTION METHODS: C, A, B, B FOR THE EXP. METHODS 12, A, C3, B RESPECTIVELY.
- 3) THE SAMPLE THICKNESS USED FOR UFS IN THE B EXPERIMENTS WAS 3.2 MM.
- 4) THE VALUES OF CL, CS AND CO ARE AVERAGES OF 34 MEASUREMENTS ON THE SAMPLES THAT ALSO GAVE THE DATA CORRESPONDING TO EXP. = 12 AND C3.  
SIG. CL = .0374 KM/SEC, SIG. CS = .0242 KM/SEC AND SIG. CO = .0365.
- 5) THE CO VALUE WITH  $1/V(DV/DT)P = 3.9E-5$  KM/SEC AND  $(DH/DT)P = CP = .04$  CAL/G. YIELD A GRUNEISEN CONSTANT = 1.7 (C.A.W. PETERSON AND W.E. ELKINGTON UCRL 14724) LARGER VALUES (1.8 - 2.0) HAVE BEEN CALCULATED (M. GUINAN ETAL, PRIVATE COMM.)
- 6) VOI IS CALCULATED FROM THE LATTICE CONSTANTS OF MATERIAL QUENCHED FROM 800 DEG. C. AND ANNEALED FOR 2 HRS AT 150 DEG. C., TO YIELD THE B.C. TETRAGONAL PHASE (GAMMAO) (H.L. YAKEL - J. NUCL MATS. V33, P. 286 (1969))
- 7) DATA SCATTER MAY BE DUE IN PART TO PRESENCE OF VARIABLE AMOUNTS OF AN ALPHA PHASE AND POSSIBLE INTERNAL STRAINS. DATA OBTAINED WITH METHOD 12, A AND B ARE FROM A SEPARATE BATCH OF SAMPLES. NOTE DENSITY DIFFERENCE.
- 8) A NARROW ELASTIC-PLASTIC DOUBLE WAVE REGION IS SUGGESTED BY SOME OF THE HIGHER DENSITY SAMPLES AND CONFIRMED BY TWO MANGANIN WAVE PROFILES (HEL = 70-80KB J.A. CHAREST REPORT E.O.G. 1183-2245, UCRL 13473 (1970))

TABLE I

MULBERRY  
88--55--58---1





92--29---1  
 LOCKALLOY (BERYLLIUM ALLOY)

BE 68 PERCENT BY WEIGHT  
 AI 32 PERCENT -

VO = 0.480 CC/G  
 VOI = 0.4769 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC.  
 AND PRESSURE IN KILOBARS.

TABLE

| ----- SAMPLE ----- |       |      |     |       | BASE PLATE |
|--------------------|-------|------|-----|-------|------------|
| RHO0               | US    | UP   | P   | V/VO  | P          |
| 2.090              | 10.04 | 2.55 | 535 | 0.746 | 721        |
| 2.090              | 7.33  | 0.53 | 80  | 0.928 | 85         |

US =

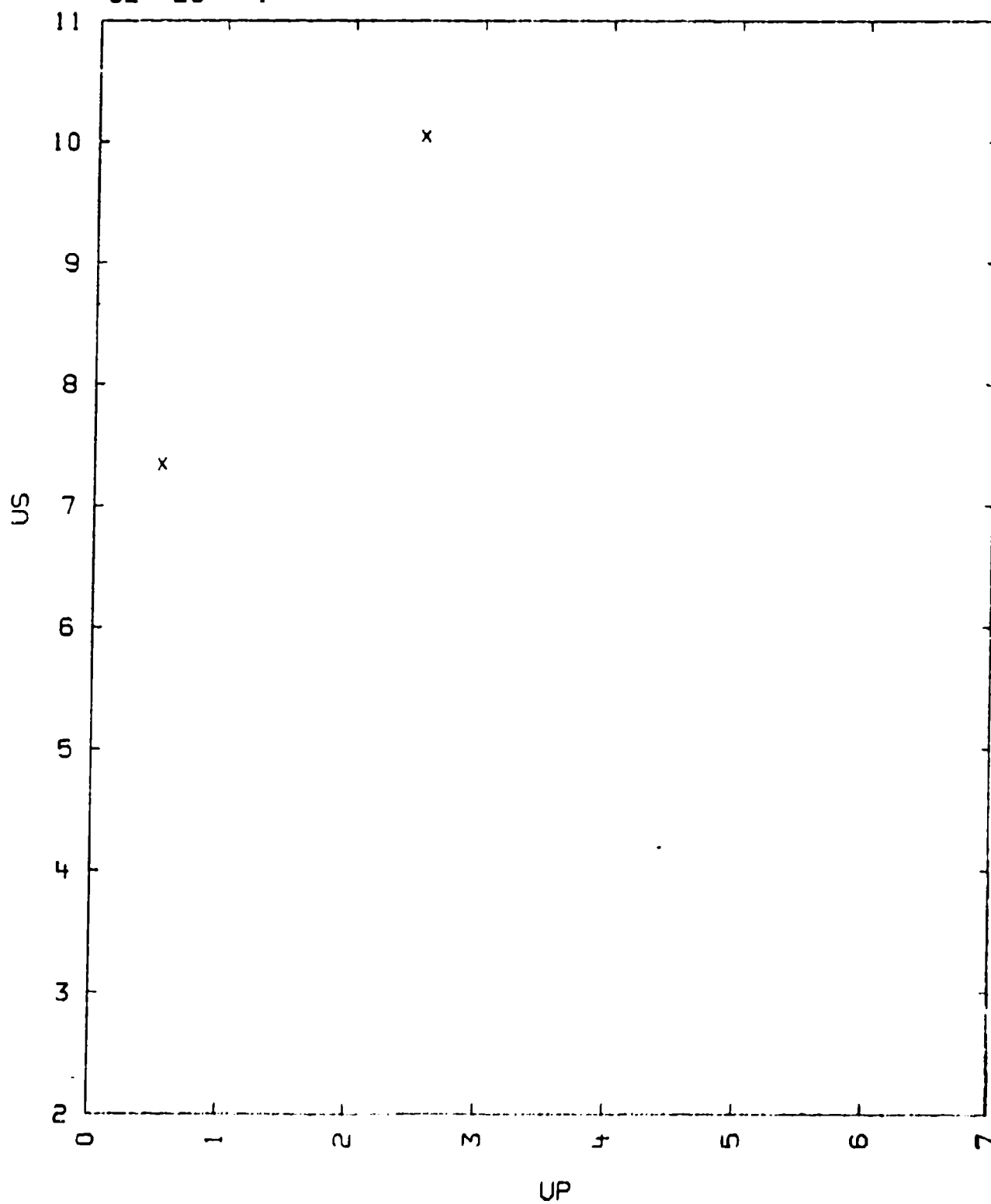
## COMMENTS:

- 1) SOURCE: COMPILER  
 L.R.L. EQUATION OF STATE FILE  
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE B. (ALUMINUM STANDARD BASE PLATE)  
 DATA REDUCTION TECHNIQUE B.
- 3) THE VALUE OF VOI WAS CALCULATED BY ASSUMING ADDITIVITY OF THE VOLUMES  
 OF COMPONENTS. THE VOLUMES OF THE COMPONENTS WERE OBTAINED FROM  
 A. TAYLOR AND BRENDA J. KAGLE, CRYSTALLOGRAPHIC DATA ON METAL AND  
 ALLOY STRUCTURES (DOVER PUBLICATIONS, INC., NEW YORK, N. Y., 1963).
- 4) LOCKALLOY WAS MANUFACTURED BY LOCKHEED MISSILES AND SPACE CO.
- 5) PHYSICAL PROPERTIES:  
 SPECIFIC HEAT 0.39 CAL/GM/DEG K  
 THERMAL CONDUCTIVITY 0.49 (CAL)/CM SEC DEG K  
 THERMAL EXPANSION 16.6 E-6 PER DEG K (25-145 DEG C)

TABLE I

LOCKALLOY (BERYLLIUM ALLOY)

92--29---1



93--22--34--1  
MAGNESIUM-BISMUTH ALLOY

MG-BI-CD

MG 40 PERCENT BY WEIGHT  
BI 40 PERCENT -  
CD 20 PERCENT -

$V_0 = 0.291 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC.  
AND PRESSURE IN KILOBARS.

TABLE

| ----- SAMPLE ----- |      |      |      |     |       | BASE PLATE |
|--------------------|------|------|------|-----|-------|------------|
| RH00               | US   | UFS  | UP   | P   | V/V0  | P          |
| 3.490              | 4.54 | 1.99 | 1.00 | 158 | 0.779 | 172        |
| 3.456              | 4.86 | 2.69 | 1.32 | 221 | 0.729 | 240        |
| 3.379              | 6.05 | 3.16 | 1.54 | 314 | 0.746 | 317        |

$US = 1.72 + 2.67 UP \text{ KM/SEC}$   
 $SIGMA US = 0.467 \text{ KM/SEC}$

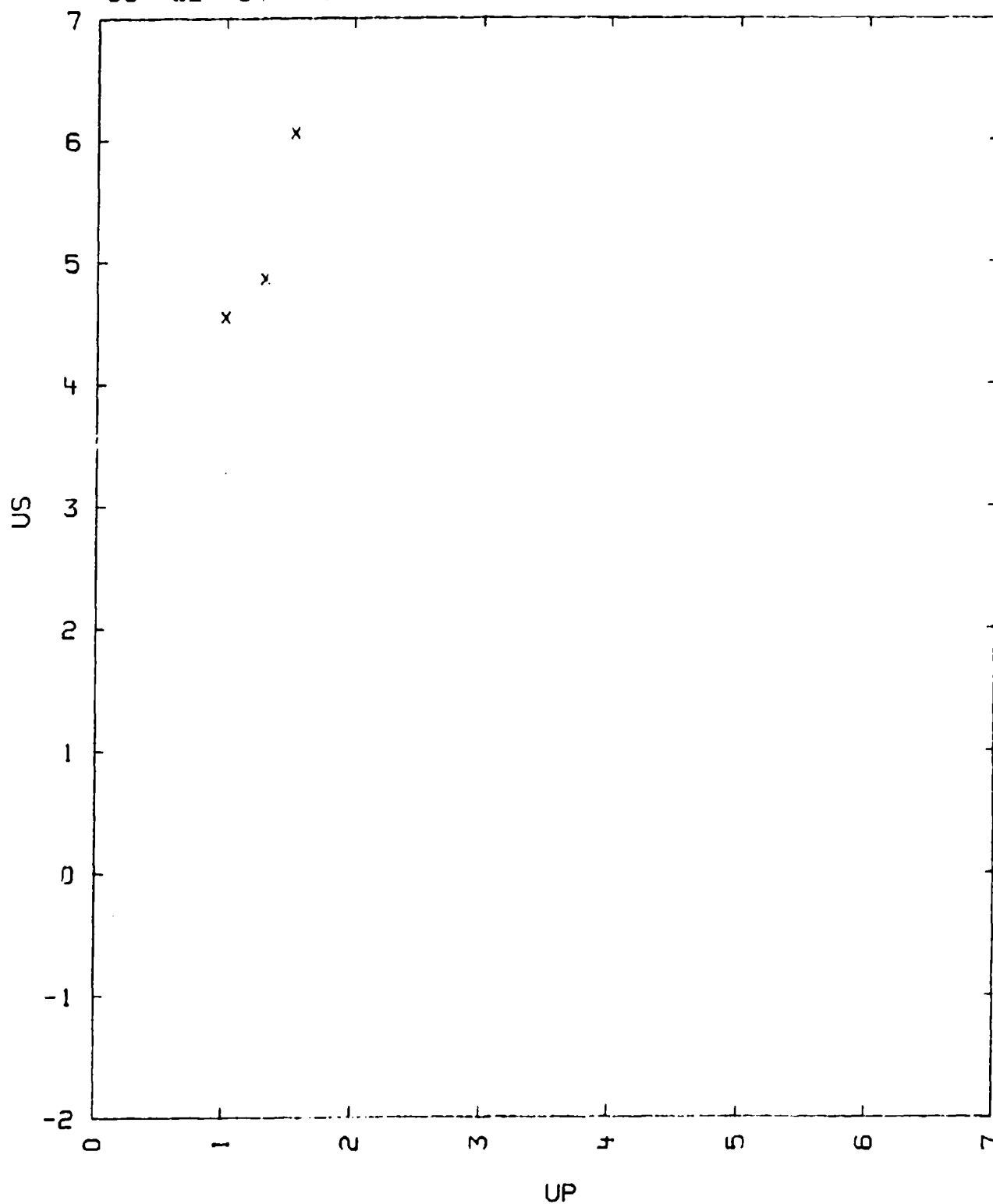
COMMENTS:

- 1) SOURCE: COMPILER  
L.R.L. EQUATION OF STATE FILE  
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE B. (ALUMINUM STANDARD BASE PLATE)  
DATA REDUCTION TECHNIQUE B.
- 3) SOME OF THE VARIATION IN RH00 MAY BE DUE TO A LACK OF UNIFORMITY  
IN THE ORIGINAL BATCH FROM WHICH THE SAMPLES WERE DERIVED.  
THE ABOVE COMPOSITION OF THE ALLOY IS THE AVERAGE BATCH COMPOSITION.
- 4) THIS ALLOY IS PROBABLY A TWO PHASE SYSTEM:
  - A) A SOLUTION OF CD IN MG
  - B) A MG3-BI2 PHASE (F. FULTON, METALLURGY L.R.L.)

TABLE I

MAGNESIUM-BISMUTH ALLOY

93--22--34---1



93-24-1--41-24-1---1  
DUNITE TWIN SISTERS MT. (SILICATE ROCK)

| OLIVENE:    |                   |     | 92.5 VOLUME PERCENT |   |   |
|-------------|-------------------|-----|---------------------|---|---|
| FORSTERITE  | MG2-S1-04         | 81  | -                   | - | - |
| FAYALITE    | FE2-S1-04         | 11  | -                   | - | - |
| PYROXENE:   |                   |     | 7                   | - | - |
| ENSTATITE   | MG2-S12-06        | 6.0 | -                   | - | - |
| FERROSILITE | FE2-S12-06        | 1.0 | -                   | - | - |
| SERPENTINE  | MG6-S14-010(0-H)8 |     | 0.5                 | - | - |

V0 = 0.301 CC/G      CL = 8.55 KM/SEC.  
V01 = 0.298 CC/G

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 3.32 | 7.31 | 0.76 | 185. | 0.896 | 6.54   |
| 3.32 | 7.32 | 0.78 | 190. | 0.893 | 6.56   |
| 3.32 | 7.27 | 0.78 | 189. | 0.893 | 6.56   |
| 3.32 | 7.35 | 0.84 | 205. | 0.886 | 6.64   |
| 3.32 | 7.32 | 0.84 | 204. | 0.885 | 6.64   |
| 3.32 | 7.29 | 0.84 | 204. | 0.885 | 6.64   |
| 3.32 | 7.62 | 1.05 | 265. | 0.862 | 6.95   |
| 3.32 | 7.48 | 1.06 | 264. | 0.858 | 6.97   |
| 3.32 | 7.61 | 1.09 | 276. | 0.857 | 7.02   |
| 3.32 | 7.57 | 1.11 | 280. | 0.853 | 7.04   |
| 3.32 | 7.59 | 1.22 | 307. | 0.839 | 7.18   |
| 3.32 | 7.69 | 1.25 | 319. | 0.837 | 7.23   |
| 3.32 | 7.94 | 1.54 | 405. | 0.806 | 7.64   |
| 3.32 | 8.00 | 1.56 | 415. | 0.805 | 7.68   |
| 3.32 | 7.93 | 1.57 | 412. | 0.802 | 7.67   |
| 3.32 | 7.87 | 1.64 | 429. | 0.792 | 7.76   |
| 3.32 | 8.10 | 1.65 | 442. | 0.796 | 7.79   |
| 3.32 | 8.10 | 1.65 | 442. | 0.796 | 7.79   |
| 3.32 | 8.11 | 1.75 | 472. | 0.784 | 7.93   |
| 3.32 | 8.15 | 1.98 | 536. | 0.757 | 8.23   |
| 3.32 | 8.13 | 2.01 | 542. | 0.753 | 8.26   |
| 3.32 | 8.17 | 2.12 | 576. | 0.741 | 8.41   |
| 3.32 | 8.22 | 2.22 | 607. | 0.730 | 8.53   |
| 3.32 | 8.24 | 2.23 | 610. | 0.729 | 8.54   |
| 3.32 | 8.22 | 2.23 | 609. | 0.729 | 8.54   |
| 3.32 | 8.33 | 2.38 | 657. | 0.714 | 8.73   |
| 3.32 | 8.28 | 2.41 | 662. | 0.709 | 8.77   |
| 3.32 | 8.31 | 2.42 | 668. | 0.709 | 8.78   |
| 3.32 | 8.28 | 2.43 | 669. | 0.707 | 8.79   |
| 3.32 | 8.24 | 2.44 | 668. | 0.704 | 8.80   |
| 3.32 | 8.39 | 2.64 | 734  | 0.686 | 9.05   |
| 3.32 | 8.31 | 2.65 | 730  | 0.682 | 9.05   |
| 3.32 | 8.75 | 2.86 | 831  | 0.674 | 9.38   |
| 3.32 | 8.66 | 2.90 | 847  | 0.667 | 9.40   |

## DUNITE TWIN SISTERS MT. (SILICATE ROCK)

| RH00 | US   | UP   | P    | V/V0  | US(51) |
|------|------|------|------|-------|--------|
| 3.32 | 8.73 | 2.91 | 844  | 0.667 | 9.44   |
| 3.32 | 8.69 | 2.93 | 844  | 0.663 | 9.45   |
| 3.32 | 8.77 | 2.95 | 858  | 0.664 | 9.49   |
| 3.32 | 8.75 | 2.95 | 857  | 0.663 | 9.49   |
| 3.32 | 9.15 | 3.10 | 941  | 0.661 | 9.73   |
| 3.32 | 9.12 | 3.10 | 940  | 0.660 | 9.73   |
| 3.32 | 9.25 | 3.28 | 1007 | 0.646 | 9.56   |
| 3.32 | 9.55 | 3.37 | 1070 | 0.647 | 10.13  |
| 3.32 | 9.45 | 3.39 | 1063 | 0.641 | 10.12  |
| 3.32 | 9.49 | 3.39 | 1068 | 0.642 | 10.13  |
| 3.32 | 9.69 | 3.49 | 1123 | 0.641 | 10.28  |

US =  $6.65 + 0.825 \cdot UP$  KM/SEC. FOR UP FROM 0.7 TO 1.65 KM/SEC.  
 SIGMA US = 0.06 KM/SEC.

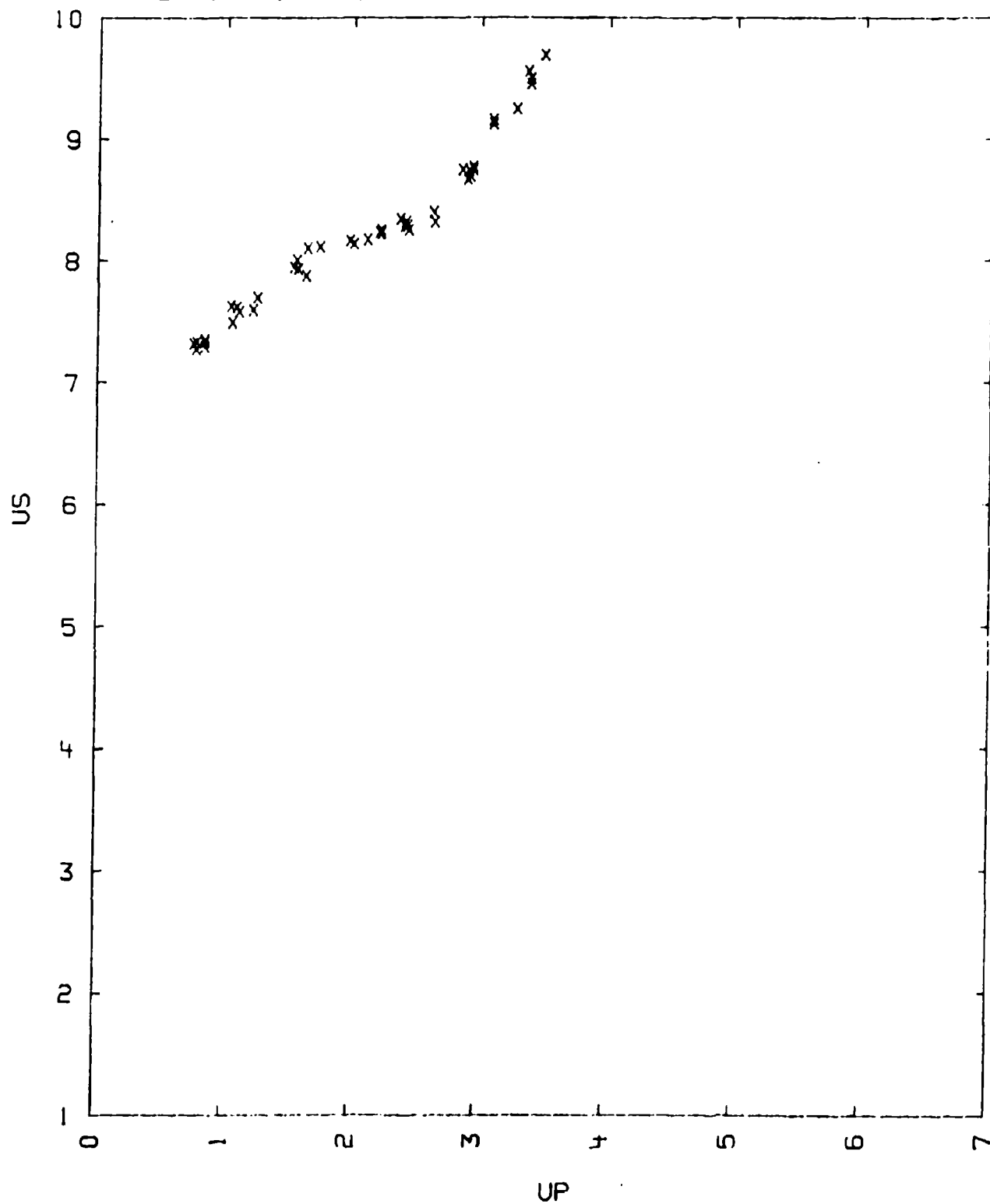
US =  $7.63 + 0.268 \cdot UP$  KM/SEC. FOR UP FROM 1.65 TO 2.5 KM/SEC.  
 SIGMA US = 0.03 KM/SEC.

US =  $4.140 + 1.582 \cdot UP$  KM/SEC. FOR UP FROM 2.6 TO 3.5 KM/SEC.  
 SIGMA US = 0.07 KM/SEC.

## COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.  
 PRIVATE COMMUNICATION  
 LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VOI WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA  
 DETERMINATIVE TABLES (AMERICAN CRYST. ASSN. 1963) 2ND ED.,  
 AND ASSUMING A DENSITY OF 2.2 AND 3.3 FOR SERPENTINE AND  
 THE REMAINING 0.5 PERCENT OF MATERIAL RESPECTIVELY
- 4) THE MODAL ANALYSIS OF THESE SAMPLES WHICH WERE OBTAINED FROM BIRCH  
 WAS TAKEN FROM : F. BIRCH, J. GEOPHYS. RES., NO. 65, P 1083, (1960)
- 5) FURTHER WORK IS IN PROGRESS.

TABLE I  
 DUNITE TWIN SISTERS MT. (SILICATE ROCK)  
 93-24-1--41-24-1---1



93-24-1--41-24-1--2

BRONZITITE, BUSHVELD COMPLEX, TRANSVAAL (SILICATE ROCK)

| PLAGIOCLASE: |                                         |      | 4  | VOL. PERCENT |   |
|--------------|-----------------------------------------|------|----|--------------|---|
| ANORTHITE    | CA-AL2-S12-08                           | 3.2  | -  | -            | - |
| ALBITE       | NA-AL-S13-08                            | 0.8  | -  | -            | - |
| PYROXENE:    |                                         |      | 92 | -            | - |
| ENSTATITE    | MG2-S12-06                              | 82.8 | -  | -            | - |
| FERROSILITE  | FE2-S12-06                              | 9.2  | -  | -            | - |
| HORNBLende   | CA-NA(MG,FE)4(AL,FE,TI)3-S18-022(0,OH)2 | 2    | -  | -            | - |

VO = 3.03 CC/G

CL = 7.7 KM/SEC

VOI = 3.121 CC/G

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 3.30 | 6.74 | 0.52 | 116. | 0.923 | 6.16   |
| 3.30 | 6.68 | 0.80 | 176. | 0.880 | 6.54   |
| 3.30 | 6.98 | 1.11 | 254. | 0.841 | 6.97   |
| 3.29 | 7.31 | 1.64 | 394. | 0.776 | 7.68   |
| 3.30 | 7.31 | 1.64 | 397. | 0.776 | 7.69   |
| 3.30 | 7.35 | 1.70 | 413. | 0.769 | 7.76   |
| 3.30 | 7.57 | 2.20 | 551  | 0.708 | 8.41   |
| 3.29 | 7.92 | 2.50 | 649  | 0.685 | 8.80   |
| 3.30 | 8.65 | 2.93 | 836  | 0.661 | 9.44   |
| 3.30 | 8.90 | 3.14 | 923  | 0.647 | 9.73   |

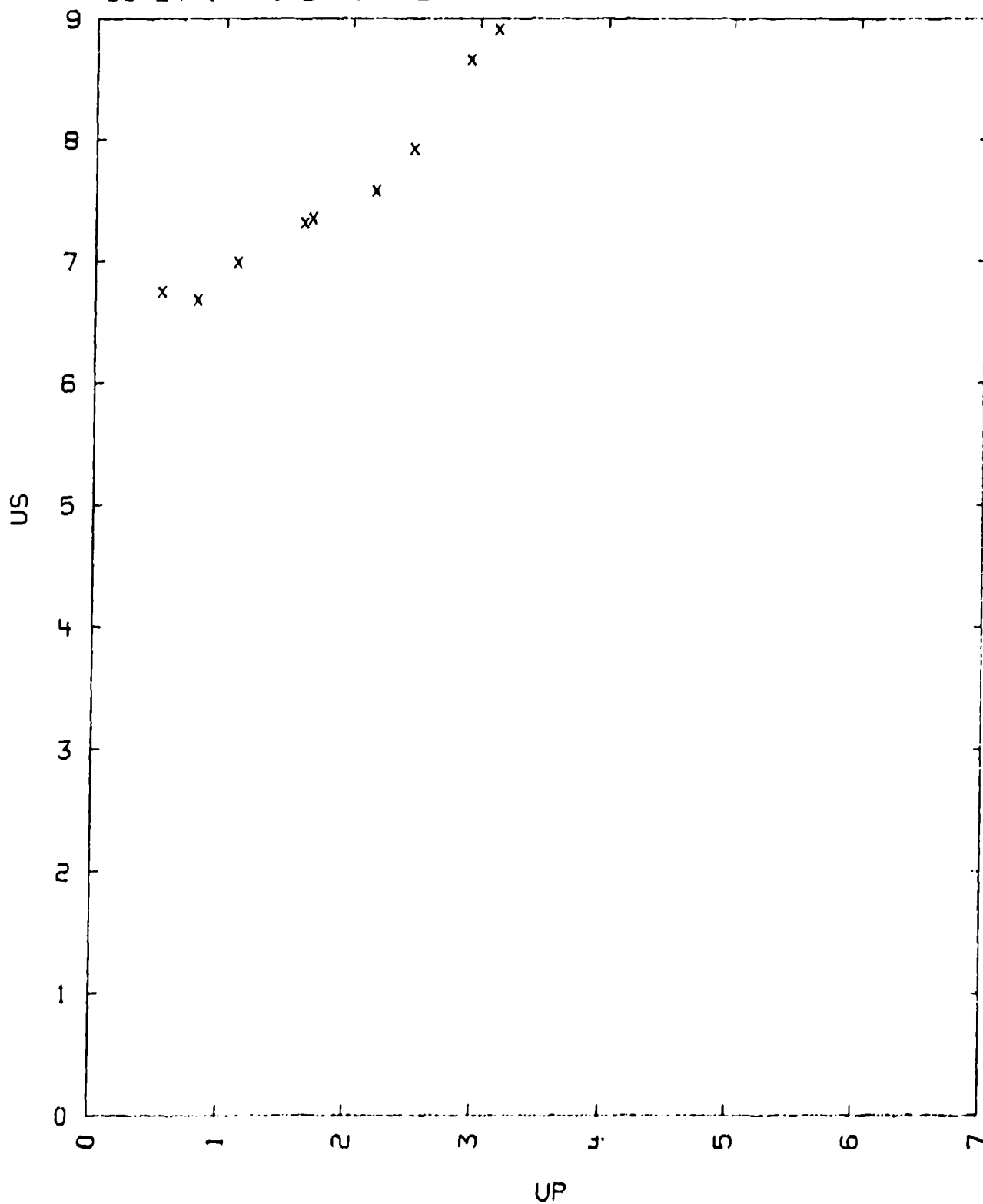
US =  $4.322 + 1.462 \cdot UP$  KM/SEC. FOR UP FROM 2.2 TO 3.2 KM/SEC.  
 SIGMA US = 0.056 KM/SEC.

## COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.  
 PRIVATE COMMUNICATION  
 LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VOI WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYST. ASSN. 1963) 2ND. ED., AND A HORNBLende DENSITY OF 3.20 G/CC
- 4) THE MODAL ANALYSIS OF THESE SAMPLES (OBTAINED THROUGH F. BIRCH), WAS TAKEN FROM: F. BIRCH, J. GEOPHYS. RES., VOL. 65, P. 1083 (1960)
- 5) FURTHER WORK IS IN PROGRESS.



TABLE I  
BRONZITITE, BUSHVELD COMPLEX, TRANSVAAL (SILICATE  
93-24-1--41-24-1---2



93-24-1--41-24-1---3  
OLIVINITE 1 (SILICATE ROCK)

|                 |                            |    |                |
|-----------------|----------------------------|----|----------------|
| OLIVINE:        |                            | 90 | VOLUME PERCENT |
| FORSTERITE      | MG2-SI-04                  | 81 | -              |
| FAYALITE        | FE2-SI-04                  | 9  | -              |
| BIOTITE         | K-(MG,FE)3AL-SI3-O10-(OH)2 | 7  | -              |
| TITANOMAGNETITE |                            | 3  | -              |

VO = 0.302 CC/G

VOI = 0.298 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBR5. PLEX INDICATES PLEXIGLAS, AL-ALUMINUM, MG-MAGNESIUM AND FE-IRON.

TABLE

| SAMPLE |       |      |      |       | STANDARD |      |
|--------|-------|------|------|-------|----------|------|
| RH00   | US    | UP   | P    | V/VO  | MTRL     | UP   |
| 3.31   | 6.98  | 0.59 | 136  | 0.915 | AL       | 0.69 |
| -      | 7.40  | 1.00 | 245  | 0.865 | AL       | 1.14 |
| -      | 7.77  | 1.33 | 342  | 0.829 | AL       | 1.50 |
| -      | 8.60  | 2.65 | 755  | 0.692 | AL       | 2.82 |
| -      | 8.19  | 1.70 | 461  | 0.792 | PLEX     | 3.05 |
| -      | 8.17  | 2.04 | 551  | 0.750 | MG       | 2.79 |
| -      | 9.78  | 3.59 | 1162 | 0.633 | FE       | 2.92 |
| -      | 12.48 | 5.81 | 2400 | 0.534 | FE       | 4.56 |
| -      | 16.83 | 9.07 | 5050 | 0.461 | FE       | 7.11 |

US = 5.08 + 1.287\*UP KM/SEC, FOR UP FROM 2.2 TO 9.5 KM/SEC.

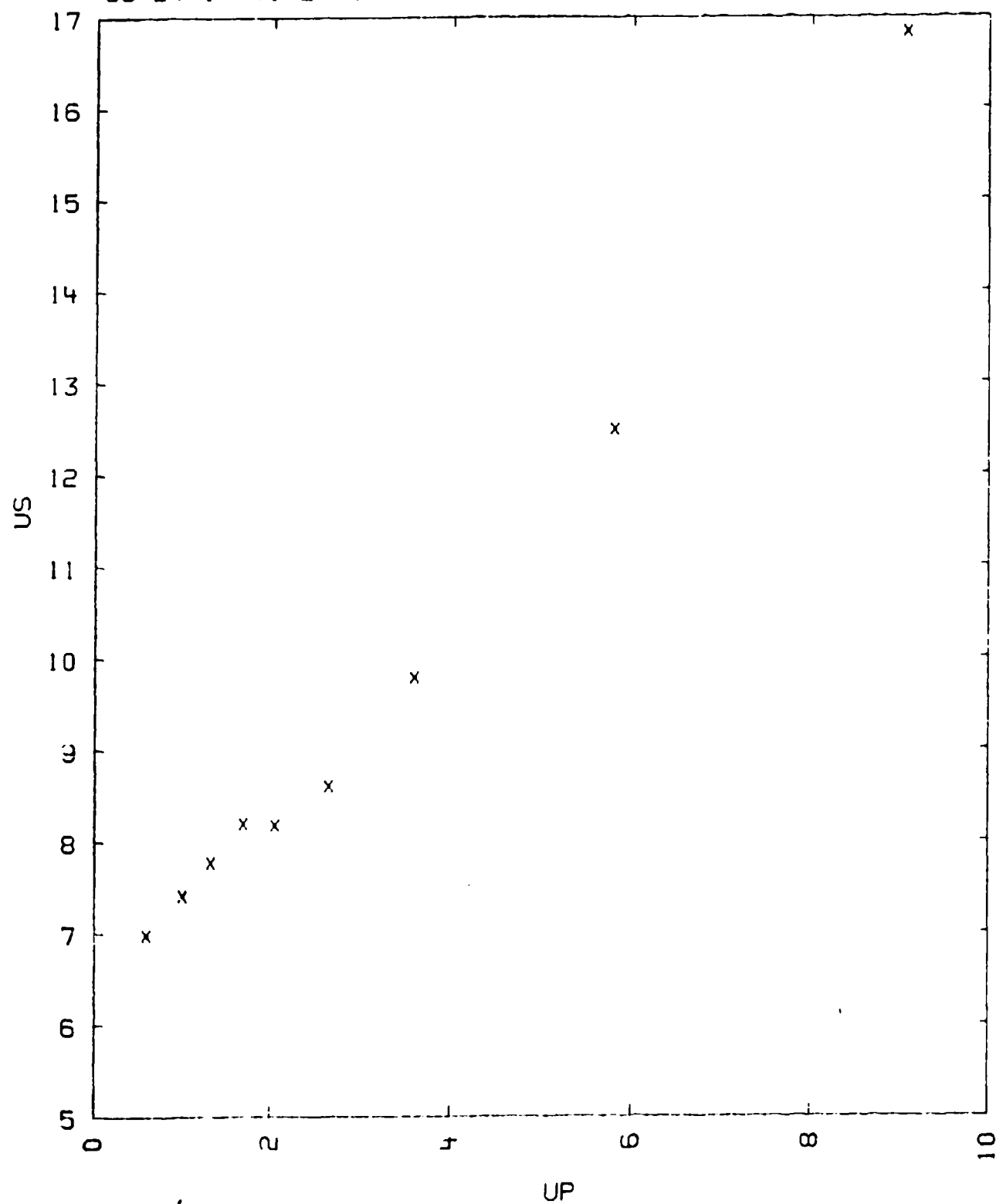
## COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
IZV. AKADEMII NAUK SSSR, FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
DATA REDUCTION METHOD B, (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4) A DISCONTINUITY IN THE HUGONIOT IS OBSERVED AT US = 9.2 KM/SEC.
- 5) VOI WAS OBTAINED FROM ASSUMED BIOTITE AND TITANOMAGNETITE DENSITIES OF 2.9 AND 5.1 G/CC RESPECTIVELY AND THE OLIVINE LATTICE PARAMETERS GIVEN IN: CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYST. ASSN. 1963) 2ND. ED.

TABLE I

OLIVINITE I (SILICATE ROCK)

93-24-1--41-24-1---3



93-24-1--41-24-1---4  
PYROXINITE (ENSTATITE) (SILICATE ROCK)

|              |               |     |    |                |   |
|--------------|---------------|-----|----|----------------|---|
| HYPERSTENE:  |               |     | 95 | VOLUME PERCENT |   |
| ENSTATITE    | MG2-SI2-O6    | 81  | -  | -              | - |
| FERROSILITE  | FE2-SI2-O6    | 14  | -  | -              | - |
| OLIVINE:     |               |     | 3  | -              | - |
| FORSTERITE   | MG2-SI-O4     | 2.7 | -  | -              | - |
| FAYALITE     | FE2-SI-O4     | 0.3 | -  | -              | - |
| LABRADORITE: |               |     | 2  | -              | - |
| ANORTHITE    | CA-AL2-SI2-O9 | 1.2 | -  | -              | - |
| ALBITE       | NA-AL-SI3-O8  | 0.8 | -  | -              | - |

V0 = 0.304 CC/G

V01 = 0.3002 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KBARS. PLEX INDICATES PLEXIGLAS, AL -ALUMINUM, CU -COPPER AND FE -IRON.

TABLE

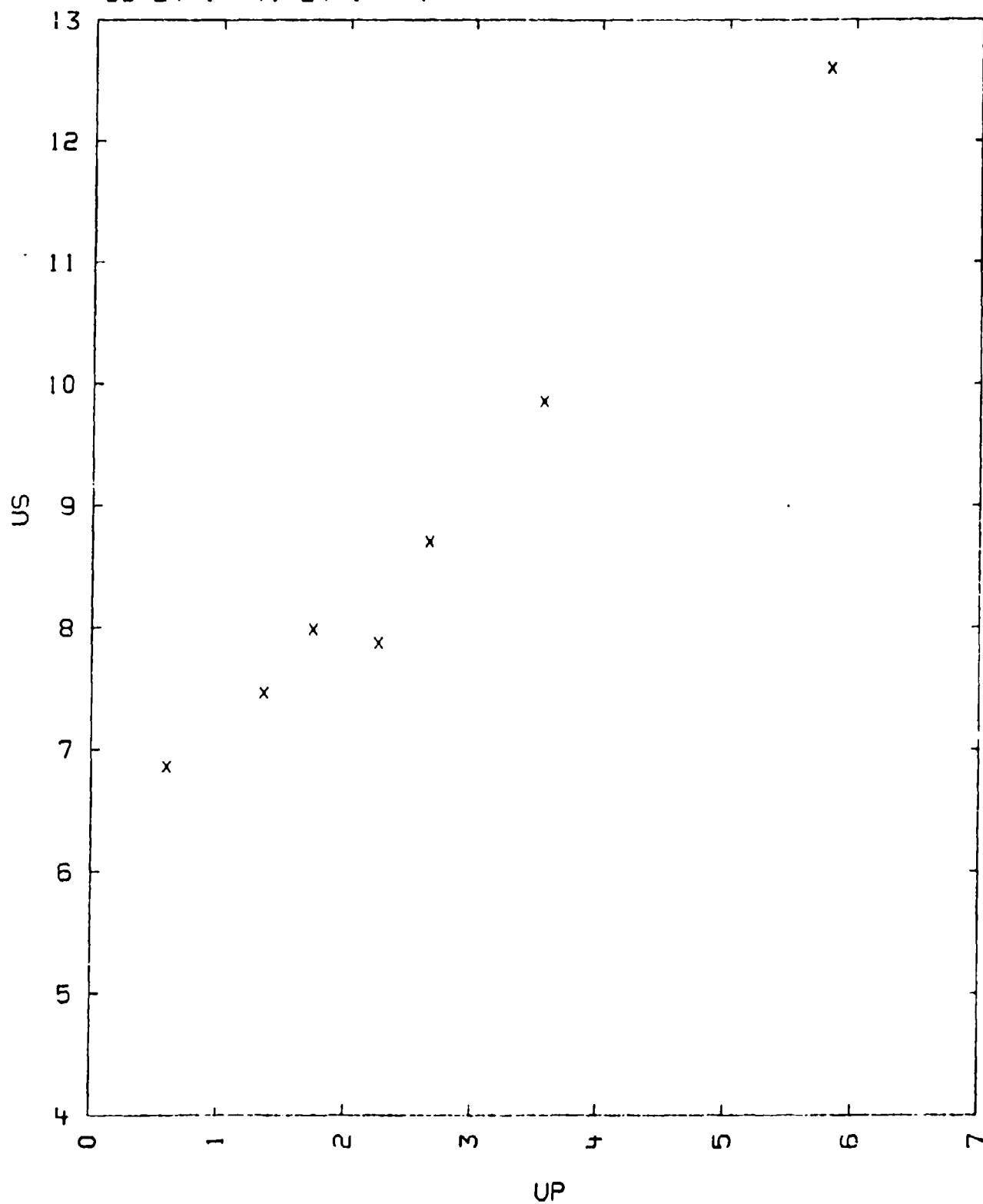
| SAMPLE |       |      |      |       | STANDARD |      |
|--------|-------|------|------|-------|----------|------|
| RH00   | US    | UP   | P    | V/V0  | MTRL     | UP   |
| 3.29   | 6.86  | 0.60 | 136  | 0.913 | AL       | 0.69 |
| -      | 7.46  | 1.36 | 334  | 0.818 | AL       | 1.50 |
| -      | 9.70  | 2.66 | 761  | 0.694 | AL       | 2.82 |
| -      | 7.98  | 1.74 | 457  | 0.782 | PLEX     | 3.05 |
| -      | 7.87  | 2.26 | 584  | 0.713 | CU       | 1.71 |
| -      | 9.85  | 3.56 | 1154 | 0.639 | FE       | 2.80 |
| -      | 12.60 | 5.80 | 2400 | 0.50  | FE       | 4.56 |

US = 5.30 + 1.265\*UP KM/SEC. FOR UP FROM 2.3 TO 6.0 KM/SEC.

## COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
IZV. AKADEMII NAUK SSSR. FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
DATA REDUCTION METHOD B, (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4) A DISCONTINUITY IN THE HUGONIOT OCCURS AT US = 7.9 KM/SEC.
- 5) V01 WAS OBTAINED FROM LATTICE PARAMETERS LISTED IN: CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYST. ASSN. 1963) 2ND. ED

TABLE 1  
PYROXINITE (ENSTATITE) (SILICATE ROCK)  
93-24-1--41-24-1---4



93-24-1--41-24-1--5  
 PERIDOTITE (OLIVINITE)

|                 |              |               | 75 | PERCENT BY VOLUME |   |   |
|-----------------|--------------|---------------|----|-------------------|---|---|
| OLIVINE:        | FORSTERITE   | MG2-SI-04     | 56 | -                 | - | - |
|                 | FAYALITE     | FE2-SI-04     | 19 | -                 | - | - |
| DIALLAGE:       | ENSTATITE    | MG-SI-03      | 5  | -                 | - | - |
|                 | HOLLASTONITE | CA-SI-03      | 5  | -                 | - | - |
| LABRADORITE:    | ANORTHITE    | CA-AL2-SI2-08 | 6  | -                 | - | - |
|                 | ALBITE       | NA-AL-SI3-08  | 4  | -                 | - | - |
| TITANOMAGNETITE |              |               | 5  | -                 | - | - |

$V_0 = 0.310 \text{ CC/G}$

$V_{01} = 0.286 \text{ CC/G}$

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| SAMPLE |       |      |      |       | STANDARD |      |
|--------|-------|------|------|-------|----------|------|
| RHO0   | US    | UP   | P    | V/V0  | MTRL     | UP   |
| 3.22   | 7.08  | 1.40 | 319  | 0.802 | AL       | 1.5  |
| -      | 8.32  | 2.73 | 732  | 0.672 | AL       | 2.82 |
| -      | 9.57  | 3.61 | 1110 | 0.623 | FE       | 2.80 |
| -      | 12.60 | 5.84 | 2369 | 0.537 | FE       | 4.56 |

$US = 4.50 + 1.400 \cdot UP \text{ KM/SEC, FOR UP FROM 2.7 TO 6.0 KM/SEC.}$

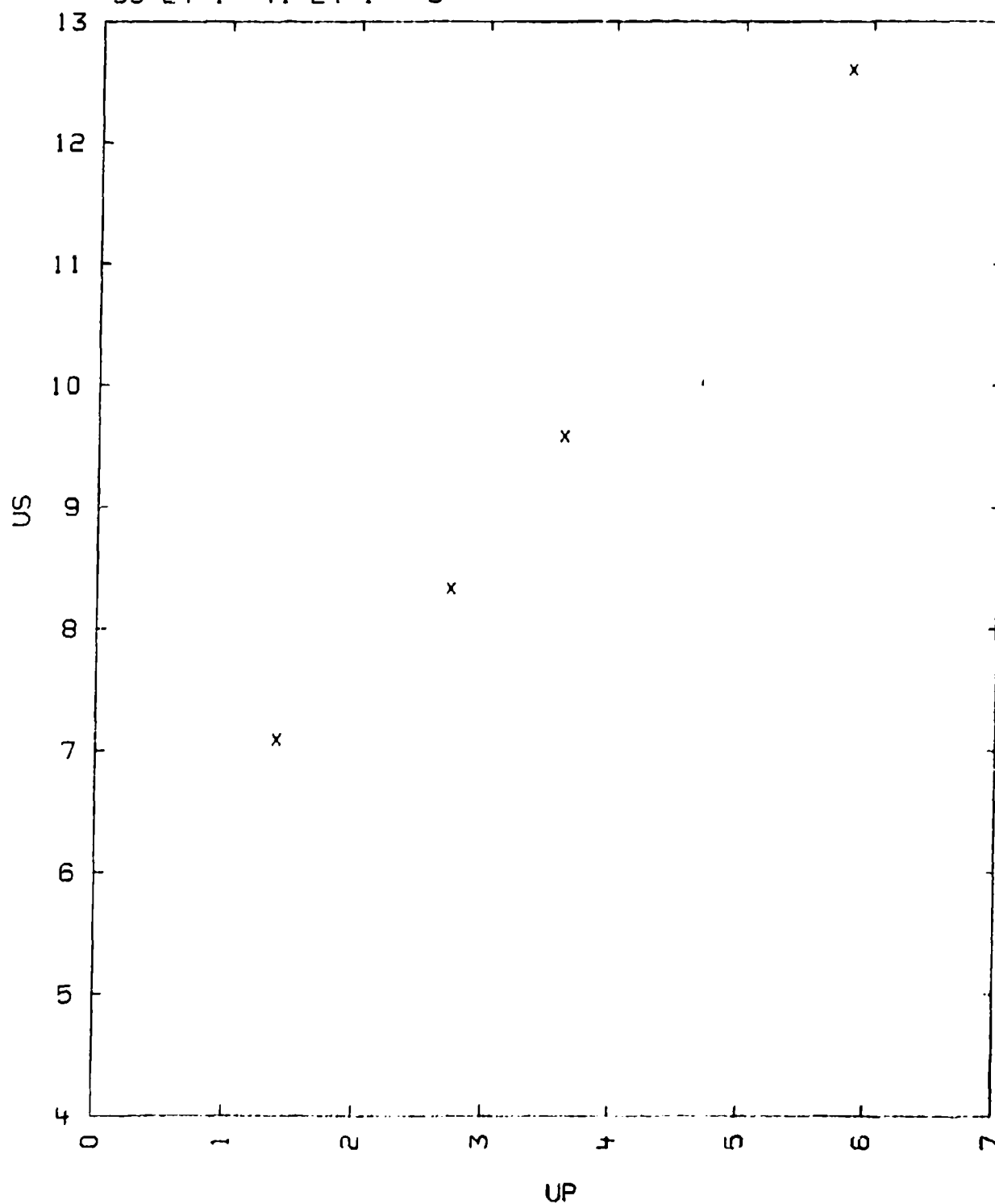
## COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
 IZV. AKADEMII NAUK SSSR. FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
 DATA REDUCTION METHOD 9, (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4)  $V_{01}$  WAS OBTAINED FROM THE LATTICE PARAMETERS GIVEN IN: CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYST. ASSN., WASH. 1963) 2ND ED., AND A TITANOMAGNETITE DENSITY OF 5.1 G/CC.

TABLE 1

PERIDOTITE (OLIVINITE)

93-24-1--41-24-1---5



93-24-1--41-24-1---6

## BRONZITE, STILLWATER COMPLEX, MONTANA (SILICATE ROCK)

| BRONZITE    |            |      | 94 VOLUME PERCENT |   |   |
|-------------|------------|------|-------------------|---|---|
| ENSTATITE   | MG-SI-03   | 84.6 | -                 | - | - |
| FERROSILITE | FE-SI-03   | 9.4  | -                 | - | - |
| HORNBLende  | (SEE NOTE) | 4    | -                 | - | - |
| OLIVENE:    |            | 2    | -                 | - | - |
| FORSTERITE  | H02-SI-04  | 1.72 | -                 | - | - |
| FAYALITE    | FE2-SI-04  | .28  | -                 | - | - |

V0 = 0.305 CC/G

CL = 7.66 KM/SEC

V01 = 0.3034 CC/G

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 3.28 | 6.84 | 0.52 | 117. | 0.924 | 6.16   |
| 3.27 | 6.87 | 0.79 | 178. | 0.885 | 6.54   |
| 3.27 | 6.99 | 0.86 | 197. | 0.877 | 6.64   |
| 3.29 | 7.02 | 0.87 | 202. | 0.876 | 6.66   |
| 3.28 | 7.24 | 1.09 | 259. | 0.849 | 6.97   |
| 3.28 | 7.17 | 1.09 | 257. | 0.848 | 6.97   |
| 3.27 | 7.14 | 1.12 | 261. | 0.843 | 6.99   |
| 3.28 | 7.44 | 1.28 | 312. | 0.828 | 7.23   |
| 3.28 | 7.45 | 1.32 | 321. | 0.823 | 7.28   |
| 3.30 | 7.53 | 1.43 | 354. | 0.810 | 7.44   |
| 3.28 | 7.54 | 1.55 | 384. | 0.794 | 7.60   |
| 3.22 | 7.54 | 1.56 | 380. | 0.793 | 7.59   |
| 3.27 | 7.56 | 1.59 | 394. | 0.790 | 7.65   |
| 3.28 | 7.63 | 1.60 | 402. | 0.790 | 7.67   |
| 3.27 | 7.59 | 1.61 | 401. | 0.788 | 7.68   |
| 3.28 | 7.54 | 1.62 | 402. | 0.785 | 7.69   |
| 3.28 | 7.61 | 1.63 | 406. | 0.786 | 7.70   |
| 3.27 | 7.51 | 1.69 | 416. | 0.775 | 7.76   |
| 3.28 | 7.62 | 1.70 | 426. | 0.777 | 7.79   |
| 3.28 | 7.65 | 1.72 | 432. | 0.775 | 7.82   |
| 3.28 | 7.64 | 1.89 | 472. | 0.753 | 8.02   |
| 3.28 | 7.73 | 2.10 | 531. | 0.728 | 8.29   |
| 3.28 | 7.79 | 2.15 | 549. | 0.724 | 8.37   |
| 3.23 | 7.72 | 2.15 | 537. | 0.722 | 8.34   |
| 3.28 | 7.76 | 2.19 | 557. | 0.718 | 8.41   |
| 3.28 | 7.89 | 2.32 | 601  | 0.707 | 8.59   |
| 3.27 | 7.93 | 2.33 | 606  | 0.706 | 8.61   |
| 3.29 | 7.96 | 2.39 | 626  | 0.700 | 8.68   |
| 3.28 | 8.04 | 2.44 | 643  | 0.696 | 8.75   |
| 3.28 | 8.08 | 2.47 | 655  | 0.695 | 8.79   |
| 3.28 | 8.20 | 2.57 | 692  | 0.686 | 8.93   |
| 3.28 | 8.32 | 2.63 | 718  | 0.683 | 9.02   |
| 3.28 | 8.60 | 2.89 | 817  | 0.663 | 9.30   |
| 3.28 | 8.63 | 2.95 | 836  | 0.657 | 9.45   |
| 3.28 | 8.93 | 3.10 | 908  | 0.653 | 9.67   |



## BRONZITITE, STILLWATER COMPLEX, MONTANA (SILICATE R

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 3.28 | 8.88 | 3.11 | 904  | 0.651 | 9.67   |
| 3.28 | 8.94 | 3.15 | 922  | 0.648 | 9.73   |
| 3.28 | 8.98 | 3.27 | 963  | 0.636 | 9.88   |
| 3.28 | 9.40 | 3.42 | 1055 | 0.636 | 10.13  |
| 3.28 | 9.17 | 3.46 | 1040 | 0.624 | 10.13  |
| 3.27 | 9.33 | 3.54 | 1082 | 0.619 | 10.25  |
| 3.28 | 9.36 | 3.55 | 1090 | 0.621 | 10.27  |

US =  $6.08 + 1.03 \cdot UP$  KM/SEC. FOR UP FROM 0.8 TO 1.3 KM/SEC.  
 SIGMA US = 0.05 KM/SEC

US =  $7.06 + 0.320 \cdot UP$  KM/SEC. FOR UP FROM 1.4 TO 2.2 KM/SEC.  
 SIGMA US = 0.04 KM/SEC.

US =  $5.113 + 1.204 \cdot UP$  KM/SEC. FOR UP FROM 2.3 TO 3.6 KM/SEC.  
 SIGMA US = 0.064 KM/SEC

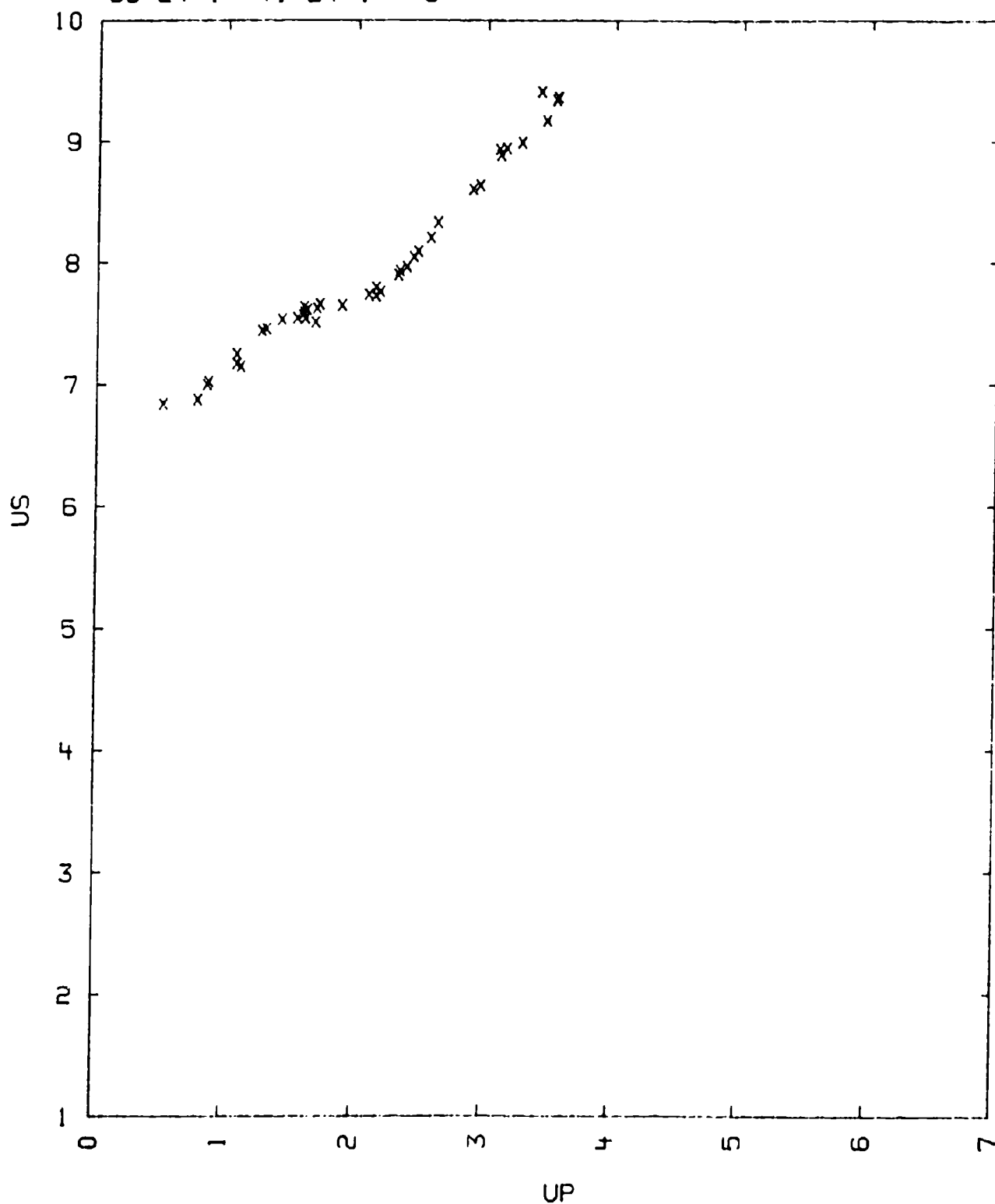
## COMMENTS :

- 1) SOURCE: MCQUEEN R. G. AND MARSH S. P.  
 PRIVATE COMMUNICATION  
 LOS ALAMOS SCIENTIFIC LABORATORY  
 LOS ALAMOS, NEW MEXICO
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VOI WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA  
 DETERMINATIVE TABLES (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION MONOGRAPH  
 5, 1963) 2ND ED - AND FROM THE MODAL ANALYSIS OF F. BIRCH, J. GEOPHYS  
 RES., VOL. 65, P. 1083 (1960), AND HESS AND PHILLIPS, AMERICAN MINERA  
 LOGIST, VOL. 25, P 277 (1940).  
 A HORNBLENDE DENSITY OF 3.2 G/CC WAS ASSUMED
- 4) SAMPLES OBTAINED THROUGH F. BIRCH FROM STILLWATER COMPLEX, MONTANA.
- 5) FURTHER WORK IN PROGRESS
- 6) CL ALSO OBTAINED FROM BIRCH (1960) BY LINEAR EXTRAPOLATION OF HIS  
 HIGH PRESSURE POINTS TO P=0 BAR.
- 7) AN ANALYSIS GIVEN BY HESS YIELDED THE FOLLOWING WEIGHT PERCENTAGES:

SI-02, AL2-03, FE2-03, FE-0, MG-0, CA-0, NA2-0, K2-0, H2-0, TI-02  
 54.68 1.80 0.50 9.19 30.19 2.22 0.04 0.03 0.51 0.11

P2-05, CR2-03, MN-0 TOTAL  
 0.02 0.47 0.21 99.97

TABLE 1  
BRONZITITE, STILWATER COMPLEX, MONTANA (SILICATE R  
93-24-1--41-24-1---6



95-24-1--94-24-1---7  
OLIVINE

FORSTERITE MG2-SI-04 91 +OR-1 WT PERCENT  
FAYALITE FE2-SI-04 9 +OR-1 - -

V0 = 0.3040-0.3017 CC/G  
V01 = 0.3008-0.3039 -

THE TABLES LIST DENSITY IN G/CC VELOCITY IN KM/SEC. AND PRESSURE IN KBAR  
D IS SAMPLE THICKNESS IN MM AND MAT IS THE BASE PLATE MATERIAL.

TABLE I

| ----- SAMPLE ----- |      |       |      |        |      |       |      |      |       |      | STANDARD |      |
|--------------------|------|-------|------|--------|------|-------|------|------|-------|------|----------|------|
| RH00               | US1  | UP1   | P1   | V1/V0  | US2  | UP2   | UFS  | P2   | V2/V0 | D    | MAT      | UFS  |
| 3.289              | 8.45 | 0.323 | 90.1 | 0.9618 | 6.58 | 0.665 | 1.24 | 163. | 0.909 | 8.90 | AL       | 1.55 |
| 3.315              | 8.72 | 0.323 | 93.4 | 0.963  | 8.21 | 1.59  | 3.37 | 437. | 0.808 | 4.81 | -        | 3.60 |

US =

TABLE II

| ----- SAMPLE ----- |      |       |       |      |       |      |     | STANDARD |  |
|--------------------|------|-------|-------|------|-------|------|-----|----------|--|
| RH00               | US   | UP    | UFS   | P    | V/V0  | D    | STM | UFS      |  |
| 3.289              | 8.45 | 0.272 | 0.544 | 75.  | .9678 | 8.90 | AL  | 1.55     |  |
| 3.289              | 8.39 | 2.19  | 4.22  | 604. | .739  | 4.82 | AL  | 4.80     |  |
| 3.289              | 8.48 | 2.80  | 5.41  | 781. | .670  | 4.83 | BR  | 4.40     |  |

US =

#### COMMENTS:

- 1) SOURCE: AHRENS T.J., ROSENBERG J.T., RUDERMAN M.H.  
DYNAMIC PROPERTIES OF ROCKS  
PROJECT FGU-4816. REPORT NO. DASA-1868 (SEPT. 30 1966)  
STANFORD RESEARCH INSTITUTE  
MENLO PARK, CALIF., USA
- 2) EXPERIMENTAL TECHNIQUE: C1 (INCLINED MIRROR) AND D (UFS)  
DATA REDUCTION METHOD: B AND D (FOR UP1)
- 3) V01 WAS ESTIMATED FROM THE ORTHORHOMBIC UNIT CELL CONSTANTS  
5.99 10.246 4.756 A FOR A FE/MG MOLE RATIO OF: 0.0/1.0 TO .04/96  
6.010 10.271 4.773 A FOR A FE/MG MOLE RATIO OF: .13/.87 TO .14/.86  
6.014 10.357 4.768 A FOR A FE/MG MOLE RATIO OF: .22/.78 TO .23/.77

TABLE I

OLIVINE

93-24-1--94-24-1---7

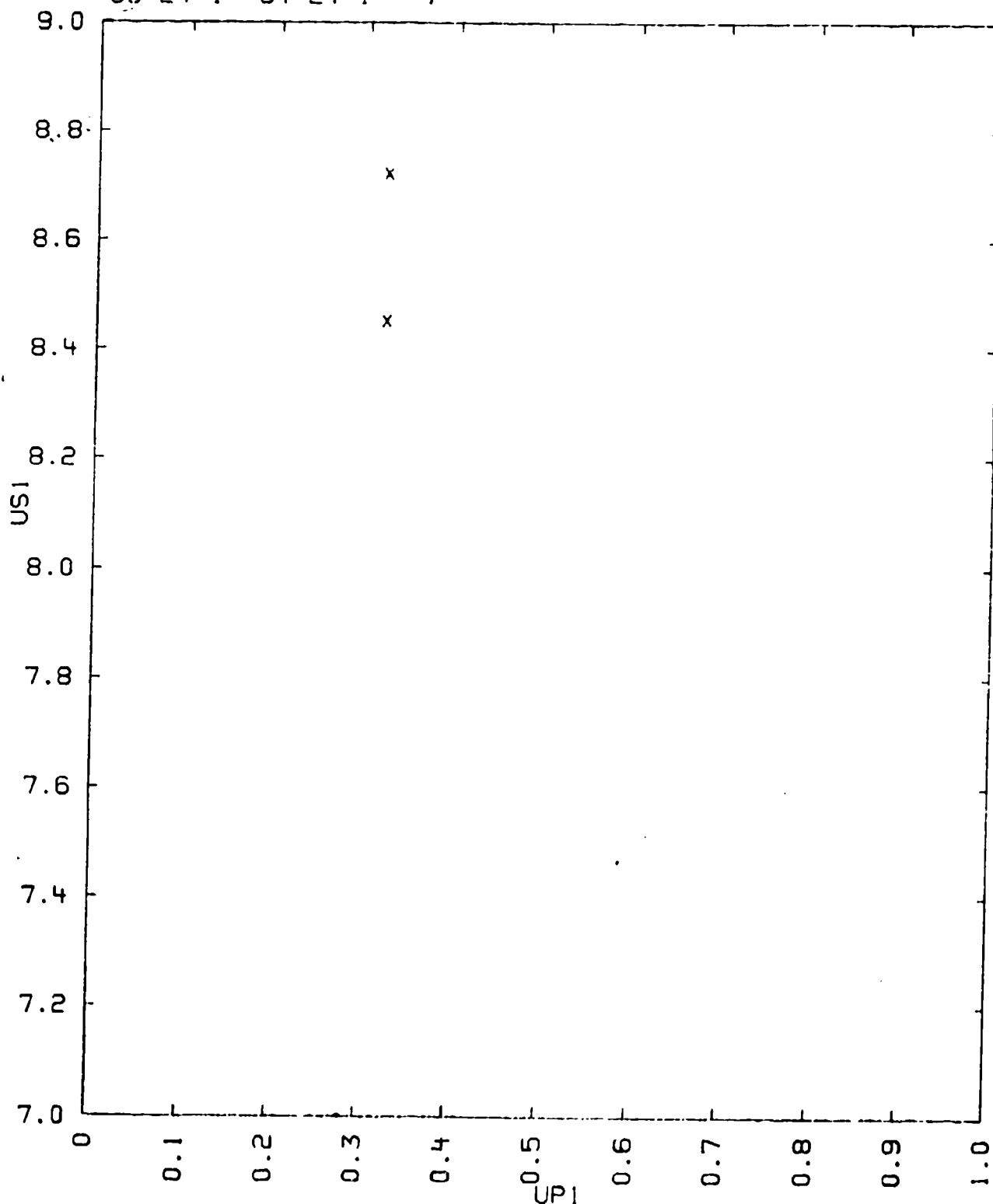


TABLE I

OLIVINE

93-24-1--94-24-1---7

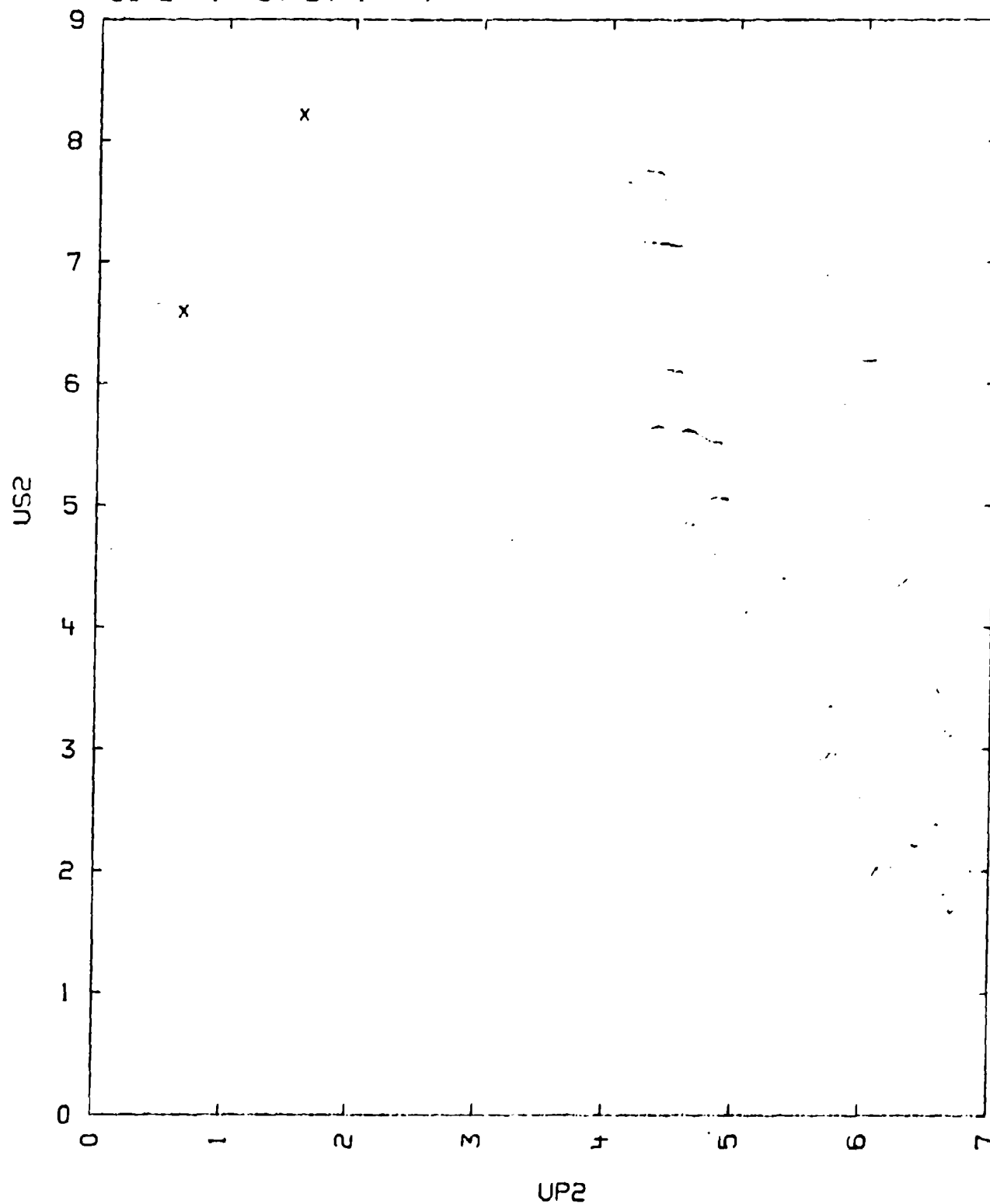
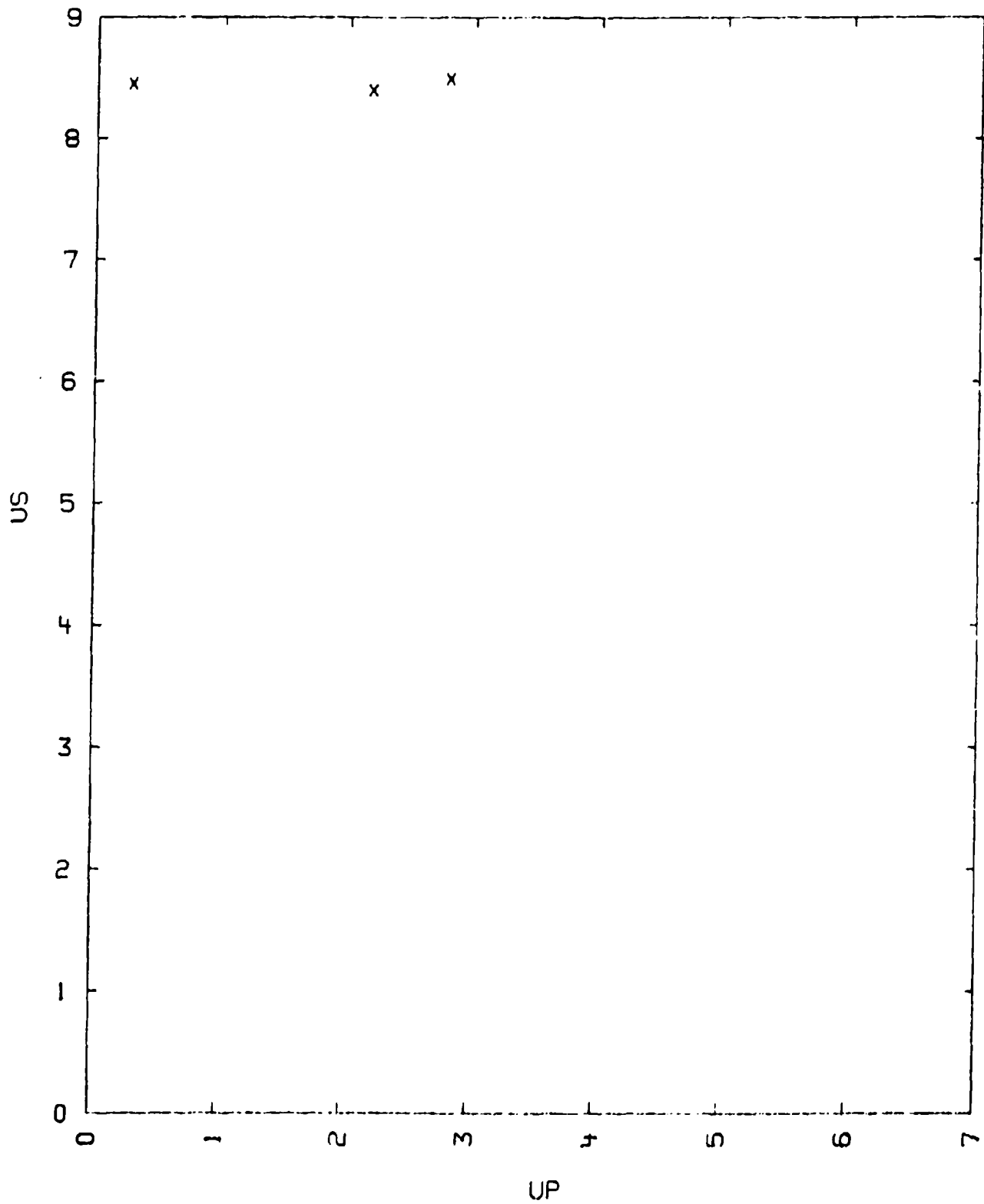


TABLE II

OLIVINE

93-24-1--94-24-1---7



93-24-1--41-24-1--41-57-1---1  
OLIVINITE II (SILICATE ROCK)

| OLIVINE:        |                   |      | 85 PERCENT BY VOLUME |   |   |   |
|-----------------|-------------------|------|----------------------|---|---|---|
| FORSTERITE      | MG2-SI-04         | 59.5 | -                    | - | - | - |
| FAYALITE        | FE2-SI-04         | 25.5 | -                    | - | - | - |
| TITANOMAGNETITE |                   |      | 7                    | - | - | - |
| SERPENTINE      | MG6-SI4-O10(O-H)8 |      | 5                    | - | - | - |
| TALC            | MG3-SI4-O10(O-H)2 |      | 3                    | - | - | - |

V0 = 0.312 CC/G

V01 = 0.277 CC/G

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC AND PRESSURE KBARS.

TABLE

| SAMPLE |       |      |      |       | STANDARD |      |
|--------|-------|------|------|-------|----------|------|
| RH00   | US    | UP   | P    | V/V0  | MTRL.    | UP   |
| 3.21   | 7.39  | 1.38 | 327  | 0.813 | AL       | 1.5  |
| -      | 8.55  | 2.70 | 741  | 0.684 | AL       | 2.82 |
| -      | 9.85  | 3.58 | 1133 | 0.637 | FE       | 2.80 |
| -      | 12.56 | 5.85 | 2360 | 0.534 | FE       | 4.56 |

US =  $5.23 + 1.270 \cdot UP$  KM/SEC, FOR UP FROM 2.7 TO 6.0 KM/SEC

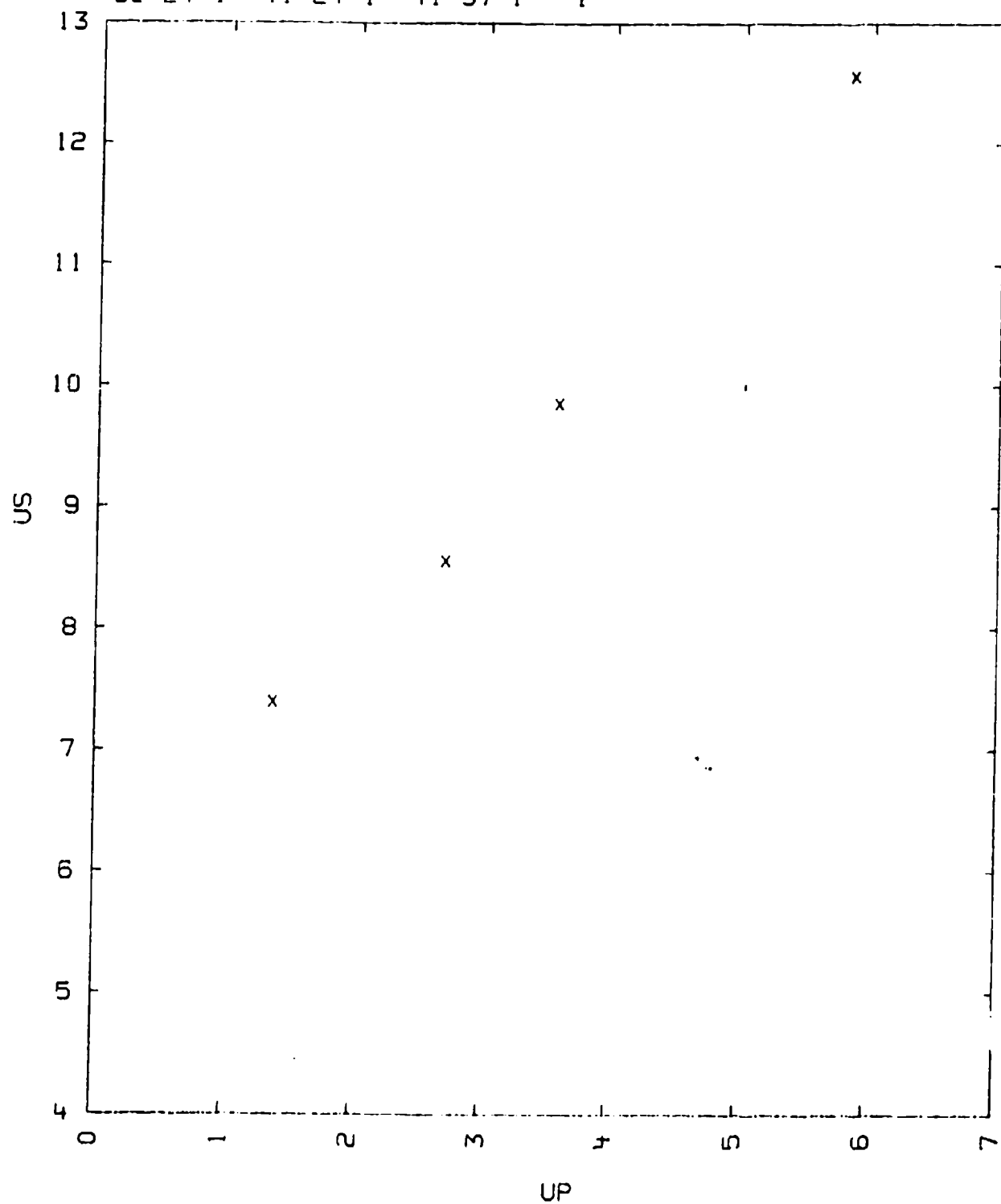
## COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
IZV. AKADEMII NAUK SSSR, FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
DATA REDUCTION METHOD B. (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4) V01 WAS OBTAINED FROM ASSUMED DENSITIES OF 5.1, 2.6 AND 2.8 G/CC FOR TITANOMAGNETITE, SERPENTINE, AND TALC. FOR OLIVINE THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYST. ASSN. 1963) 2ND. ED.

TABLE 1

OLIVINITE II (SILICATE ROCK)

93-24-1--41-24-1--41-57-1---1





93-24-1--41-24-1--41-57-1--2  
 ORE-OLIVENITE (OLIVINITE) (SILICATE ROCK)

|                 |           |    |                      |
|-----------------|-----------|----|----------------------|
| OLIVINE:        |           |    | 80 PERCENT BY VOLUME |
| FORSTERITE      | MG2-SI-O4 | 56 | -                    |
| FAYALITE        | FE2-SI-O4 | 24 | -                    |
| TITANOMAGNETITE |           | 20 | -                    |

V0 = 0.271 CC/G

V01 = 0.257 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBARS.

TABLE

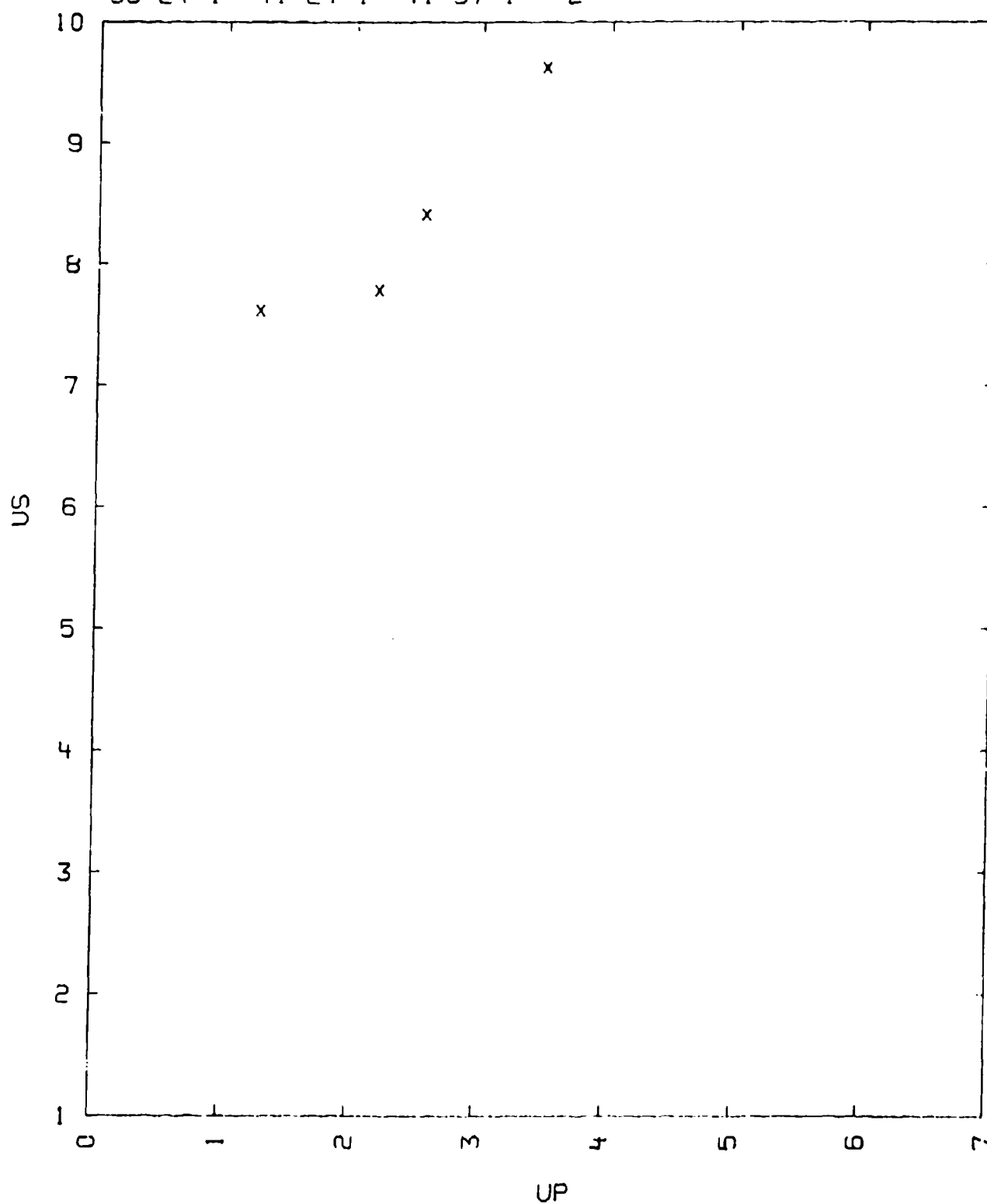
| - - - - - SAMPLE - - - - - |      |      |      |       | STANDARD |      |
|----------------------------|------|------|------|-------|----------|------|
| RH00                       | US   | UP   | P    | V/V0  | MTRL     | UP   |
| 3.69                       | 7.61 | 1.27 | 356  | 0.833 | AL       | 1.5  |
| -                          | 8.40 | 2.56 | 793  | 0.695 | AL       | 2.82 |
| -                          | 7.78 | 2.20 | 631  | 0.717 | CU       | 1.71 |
| -                          | 9.62 | 3.49 | 1239 | 0.637 | FE       | 2.82 |

US = 4.96 + 1.324\*UP KM/SEC, FOR UP FROM 2.2 TO 3.5 KM/SEC.

## COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
 IZV. AKADEMII NAUK SSSR, FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
 DATA REDUCTION METHOD B, (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4) A DISCONTINUITY OBSERVED IN THE US VERSUS UP PLOT OCCURS BELOW US = 7.7 KM/SEC.
- 5) V01 WAS OBTAINED FROM AN ASSUMED DENSITY OF 5.1 G/CC FOR TITANOMAGNETITE AND OLIVINE LATTICE CONSTANTS GIVEN IN: CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYST. ASSN. 1963) 2ND. ED.

TABLE 1  
ORE-OLIVENITE (OLIVINITE) (SILICATE ROCK)  
93-24-1--41-24-1--41-57-1---2



93-24-1--41-24-1--93-24-2-1---1  
DUNITE 1 (SILICATE ROCK)

|            |                   |    |    |                   |
|------------|-------------------|----|----|-------------------|
| OLIVINE:   |                   |    | 50 | PERCENT BY VOLUME |
| FORSTERITE | MG2-SI-04         | 25 | -  | -                 |
| FAYALITE   | FE2-SI-04         | 25 | -  | -                 |
| SERPENTINE | MG6-SI4-O10(O-H)8 |    | 40 | -                 |
| CHROMITE   | FE-CR2-O4         |    | 10 | -                 |

$V_0 = 0.345 \text{ CC/G}$

$V_{01} = 0.288 \text{ CC/G}$

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| SAMPLE |      |      |      |       | STANDARD |      |
|--------|------|------|------|-------|----------|------|
| RH00   | US   | UP   | P    | V/V0  | MTRL     | UP   |
| 2.9    | 6.85 | 1.50 | 298  | 0.801 | AL       | 1.5  |
| -      | 8.28 | 2.85 | 684  | 0.760 | AL       | 2.82 |
| -      | 9.39 | 3.75 | 1021 | 0.728 | FE       | 2.82 |

$US = 4.59 + 1.290 \cdot UP \text{ KM/SEC, FOR UP FROM 2.8 TO 3.8 KM/SEC.}$

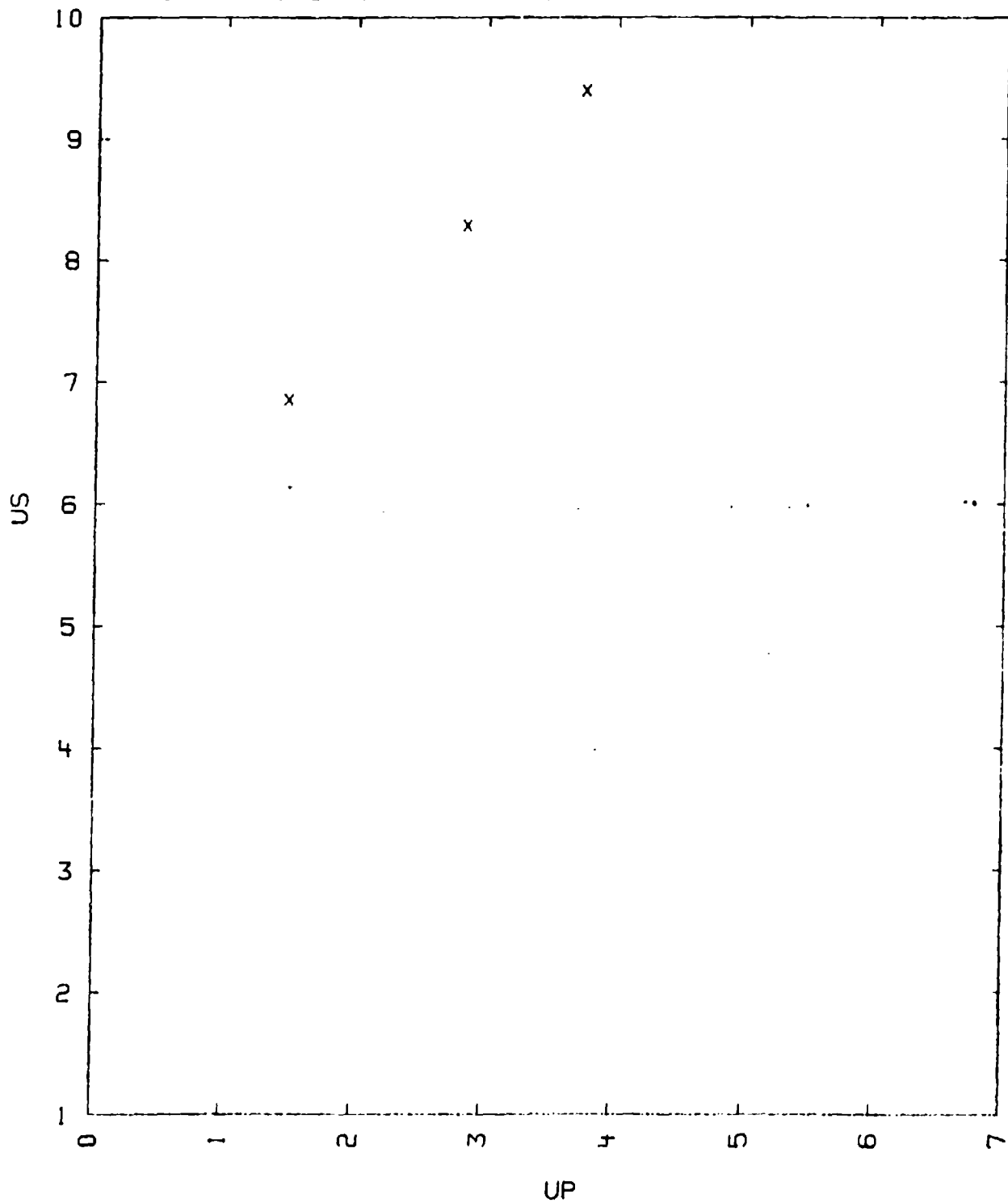
## COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
IZV. AKADEMII NAUK SSSR, FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
DATA REDUCTION METHOD B, (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4)  $V_{01}$  WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN: CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYST ASSN., WASH. 1963) 2ND. ED., AND A SERPENTINE DENSITY OF 2.65 G/CC.

TABLE 1

DUNITE 1 (SILICATE ROCK)

93-24-1--41-24-1--93-24-2-1---



93-24-1--41-24-1--94-24-1--94-29-24-1--99-29-24-1---1  
 DOLERITE (TRAP) (SILICATE ROCK)

|                  |               |       |    |                |
|------------------|---------------|-------|----|----------------|
| PIGEONITE-AUGITE |               |       | 55 | VOLUME PERCENT |
| ENSTATITE        | MG-SI-03      | 14.25 | -  | -              |
| FERROSILITE      | FE-SI-03      | 14.25 | -  | -              |
| WOLLASTONITE     | CA-SI-03      | 16.5  | -  | -              |
| LABRADORITE:     |               |       | 30 | -              |
| ANORTHITE        | CA-AL2-SI2-08 | 16.5  | -  | -              |
| ALBITE           | NA-AL-SI3-08  | 13.5  | -  | -              |
| TITANOMAGNETITE  |               |       | 10 | -              |
| OLIVENE:         |               |       | 5  | -              |
| FORSTERITE       | MG2-SI-04     | 3.    | -  | -              |
| FAYALITE         | FE2-SI-04     | 2.    | -  | -              |

$V_0 = 0.328 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KBARS.

| TABLE  |       |      |      |       |          |      |
|--------|-------|------|------|-------|----------|------|
| SAMPLE |       |      |      |       | STANDARD |      |
| RH00   | US    | UP   | P    | V/V0  | MTRL     | UP   |
| 3.05   | 5.80  | 0.67 | 119  | 0.884 | AL       | 0.69 |
| -      | 6.21  | 1.53 | 290  | 0.754 | -        | 1.5  |
| -      | 7.95  | 2.84 | 688  | 0.643 | -        | 2.82 |
| -      | 9.01  | 3.74 | 1028 | 0.585 | FE       | 2.82 |
| -      | 12.09 | 5.99 | 2209 | 0.505 | -        | 4.56 |

$US = 4.10 + 1.325 \cdot UP \text{ KM/SEC, FOR UP FROM 1.5 TO 6.0 KM/SEC.}$

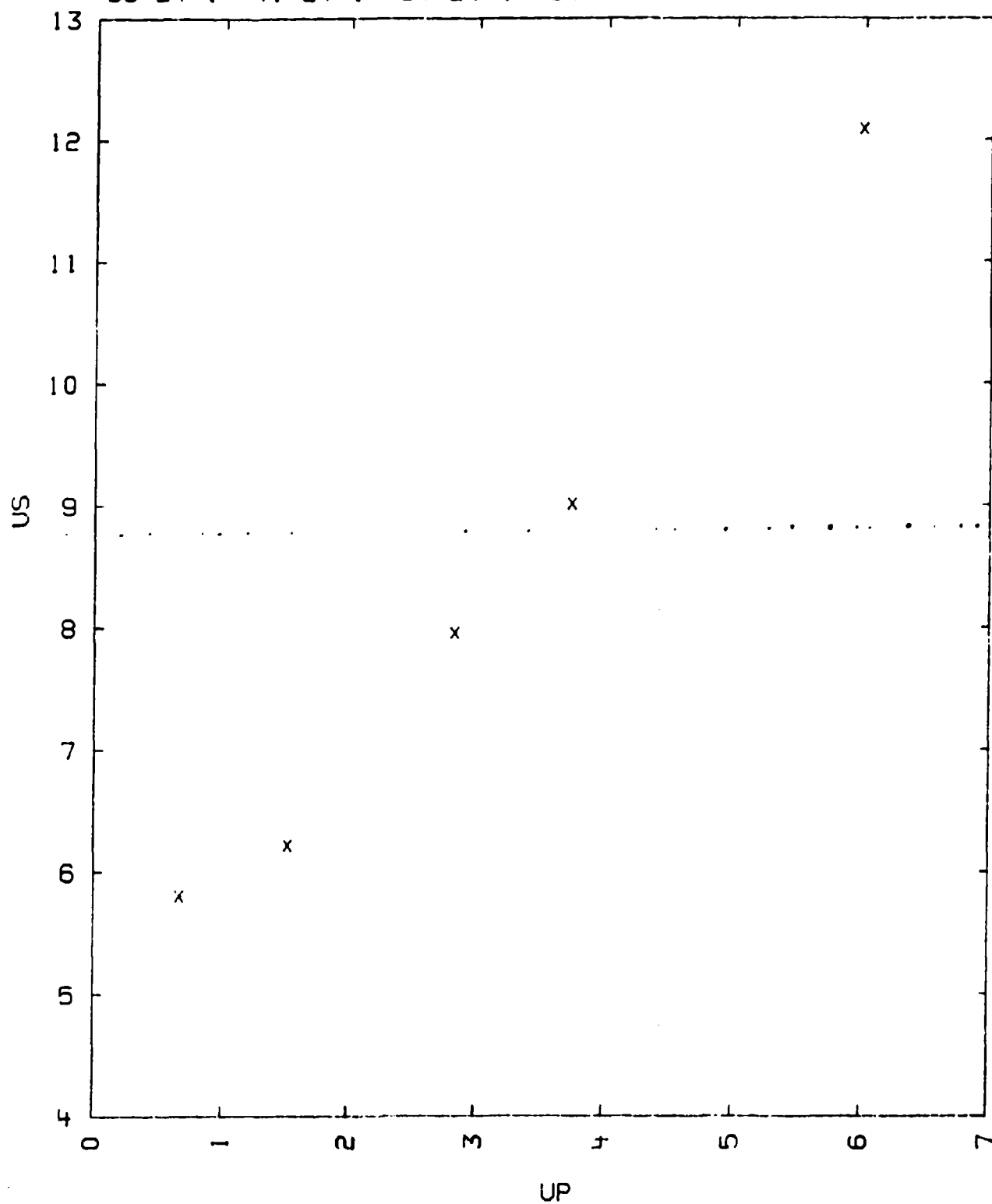
#### COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
 IZV. AKADEMII NAUK SSSR. FIZIKA ZEMLI, VOL. 9, 1965. P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
 DATA REDUCTION METHOD B, (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4) A DISCONTINUITY IN THE HUGONIOT IS OBSERVED AT  $US = 6.0 \text{ KM/SEC.}$

TABLE 1

DOLERITE (TRAP) (SILICATE ROCK)

93-24-1--41-24-1--94-24-1--94-



93-24-1--93-24-2-1---1  
DUNIT 11 (SILICATE ROCK)

| OLIVINITE: |                  |      | 65 PERCENT BY VOLUME |   |   |
|------------|------------------|------|----------------------|---|---|
| FORSTERITE | MG2-SI-OJ        | 60.5 | -                    | - | - |
| FAYALITE   | FE2-SI-OJ        | 4.5  | -                    | - | - |
| SERPENTINE | MG6-SI4-O10(OH)8 |      | 30                   | - | - |
| CHROMITE   | FE-CR2-O4        |      | 5                    | - | - |

$V_0 = 0.338 \text{ CC/G}$

$V_{01} = 0.312 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KBARS.

TABLE

| - - - - - |       | SAMPLE |      | - - - - - |      | STANDARD |  |
|-----------|-------|--------|------|-----------|------|----------|--|
| RH00      | US    | UP     | P    | V/V0      | MTRL | UP       |  |
| 2.96      | 7.08  | 1.46   | 307  | 0.790     | AL   | 1.5      |  |
| -         | 8.51  | 2.80   | 706  | 0.748     | AL   | 2.82     |  |
| -         | 12.70 | 5.95   | 2240 | 0.532     | FE   | 4.56     |  |

$US = 4.54 + 1.370 \cdot UP \text{ KM/SEC FOR UP FROM 2.8 TO 6.0 KM/SEC.}$

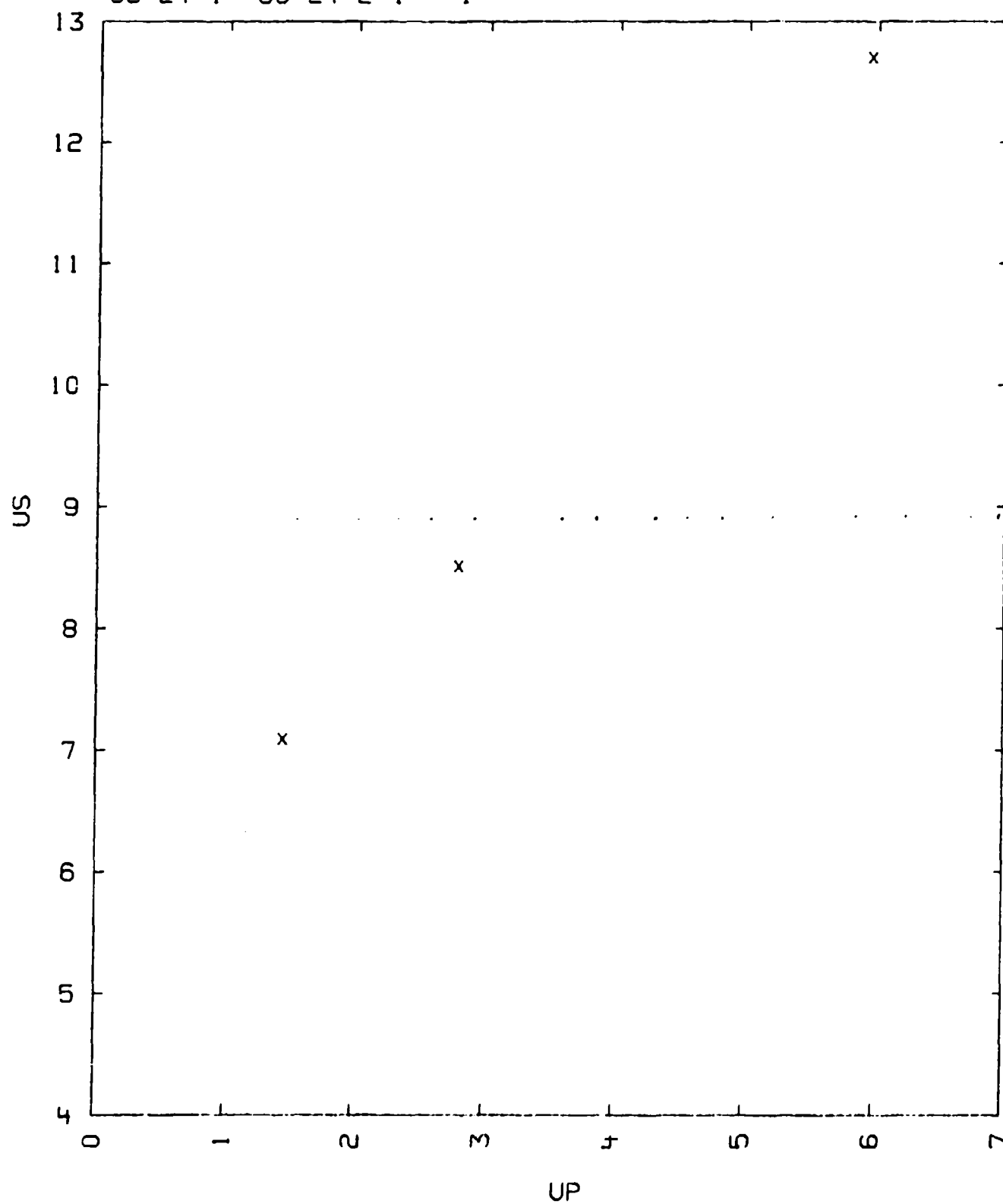
COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
IZV. AKADEMII NAUK SSSR. FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
DATA REDUCTION METHOD B. (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4)  $V_{01}$  WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN: CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYST. ASSN., WASH. 1963) 2ND ED., AND A SERPENTINE DENSITY OF 2.65 G/CC.

TABLE I

DUNITE II (SILICATE ROCK)

93-24-1--93-24-2-1---1





93-24-1--94-24-1--93-24-2-1---1  
DIOPSIDITE (SILICATE ROCK)

|                 |                   |    |                      |
|-----------------|-------------------|----|----------------------|
| DIALLAGE:       |                   |    | 70 PERCENT BY VOLUME |
| ENSTATITE       | MG-SI-03          | 42 | - - -                |
| WOLLASTONITE    | CA-SI-03          | 28 | - - -                |
| SERPENTINE      | MG6-SI4-O10(O-H)8 |    | 25 - - -             |
| TITANOMAGNETITE |                   |    | 5 - - -              |

$V_0 = 3.32 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBARS.

TABLE

| SAMPLE |      |      |      |       | STANDARD |      |
|--------|------|------|------|-------|----------|------|
| RH00   | US   | UP   | P    | V/V0  | MTRL     | UP   |
| 3.01   | 7.33 | 1.43 | 316  | 0.805 | AL       | 1.50 |
| -      | 8.47 | 2.79 | 709  | 0.671 | AL       | 2.82 |
| -      | 9.39 | 3.72 | 1052 | 0.604 | FE       | 2.82 |

$US = 5.33 + 1.120 \cdot UP \text{ KM/SEC, FOR UP FROM 2.7 TO 3.8 KM/SEC.}$

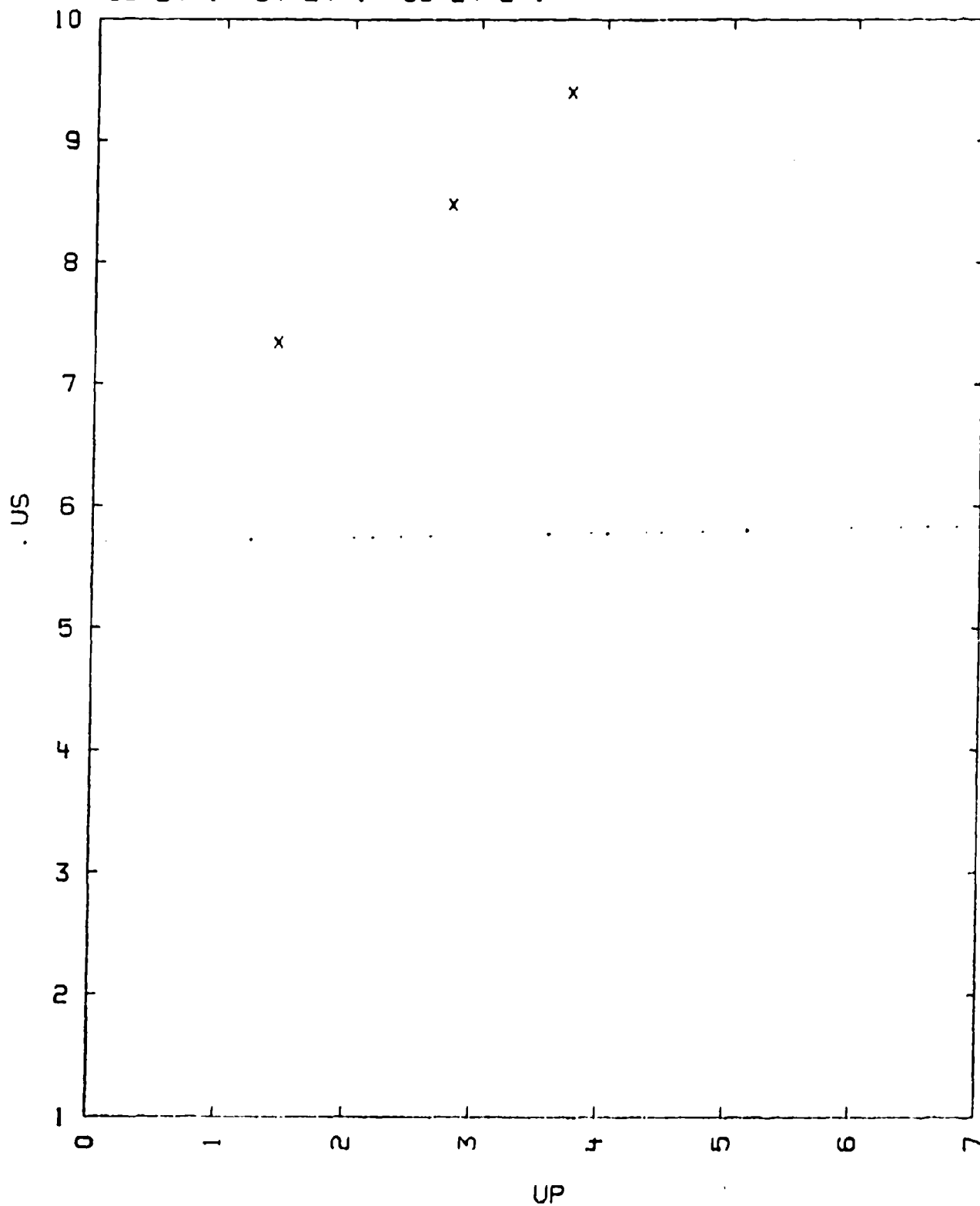
COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. Z., SIMAKOV, G. V. AND GALDIN, N. E.  
IZV. AKADEMII NAUK SSSR. FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
DATA REDUCTION METHOD B, (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.

TABLE I

DIOPSITITE (SILICATE ROCK)

93-24-1--94-24-1--93-24-2-1---



93-24-1--94-24-1--99-29-24-1--1  
ENSTATITIC GABBRO (SILICATE ROCK)

| BRONZITE:    |               |      | 60 | PERCENT BY VOLUME |   |   |
|--------------|---------------|------|----|-------------------|---|---|
| ENSTATITE    | MG2-S12-06    |      | -  | -                 | - |   |
| FERROSILITE  | FE2-S12-06    | 6    | -  | -                 | - |   |
| LABRADORITE: |               |      | 35 | -                 | - | - |
| ALBITE       | NA-AL-S13-08  |      | -  | -                 | - |   |
| ANORTHITE    | CA-AL2-S12-08 | 24.5 | -  | -                 | - |   |
| OLIVINE:     |               |      | 5  | -                 | - | - |
| FORSTERITE   | MG2-S1-04     | 2.5  | -  | -                 | - |   |
| FAYALITE     | FE2-S1-04     | 2.5  | -  | -                 | - |   |

$V_0 = 0.317 \text{ CC/G}$

$V_{01} = 0.321 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBARS.

TABLE

| SAMPLE |       |      |      |       | STANDARD |      |
|--------|-------|------|------|-------|----------|------|
| RHO0   | US    | UP   | P    | V/V0  | MTRL     | UP   |
| 3.15   | 6.92  | 1.44 | 314  | 0.792 | AL       | 1.5  |
| -      | 8.39  | 2.74 | 724  | 0.673 | AL       | 2.82 |
| -      | 9.55  | 3.63 | 1091 | 0.620 | FE       | 2.80 |
| -      | 12.56 | 5.88 | 2325 | 0.532 | FE       | 4.56 |

$US = 4.66 + 1.355 \cdot UP \text{ KM/SEC, FOR UP FROM 2.7 TO 6.0 KM/SEC.}$

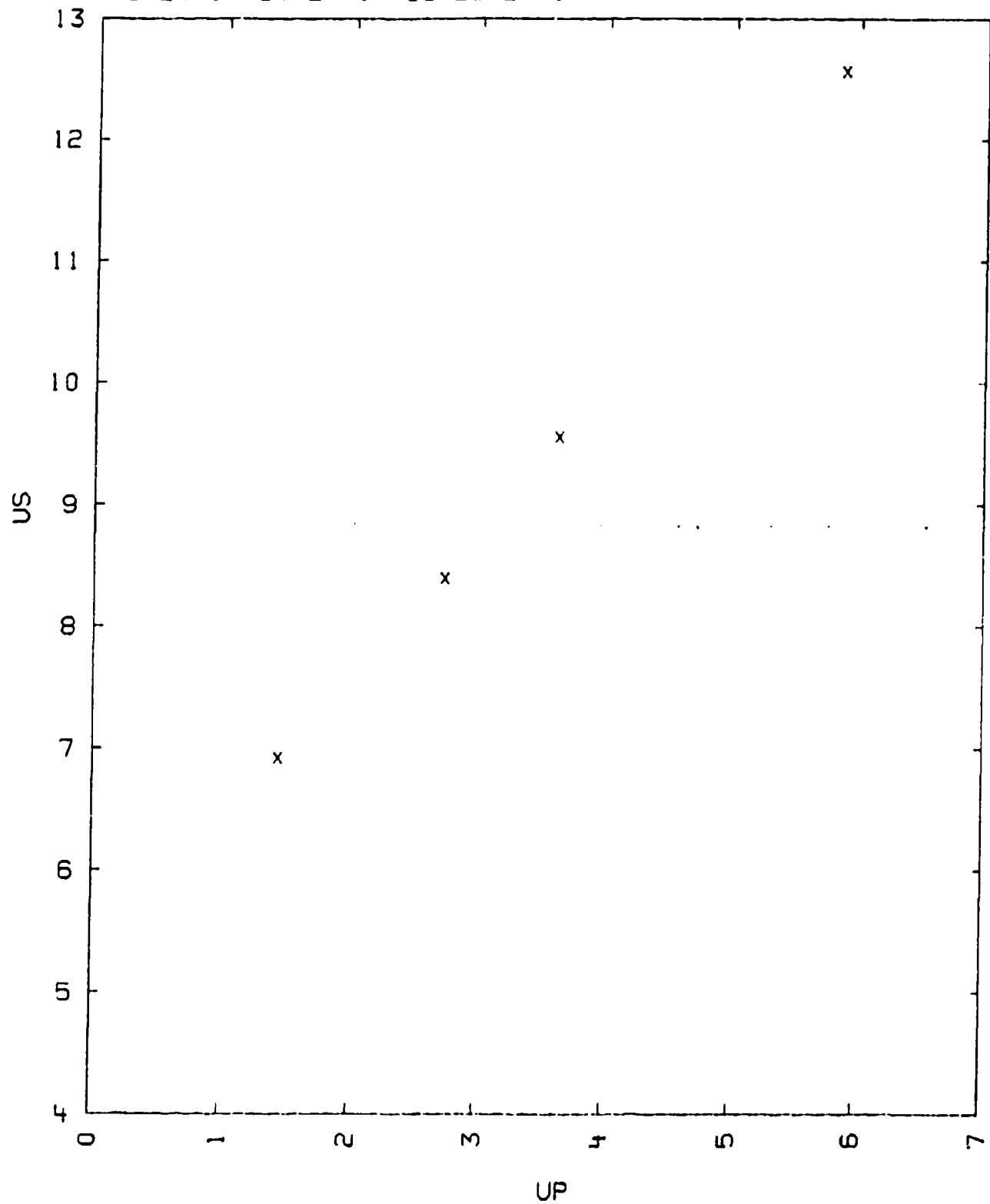
## COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
IZV. AKADEMII NAUK SSSR, FIZIKA ZEMLI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE, A  
DATA REDUCTION METHOD B. (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4)  $V_{01}$  WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN: CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYST. ASSN. 1963) 2ND. ED

TABLE 1

ENSTATITIC GABBRO (SILICATE ROCK)

93-24-1--94-24-1--99-29-24-1--



94-29-24-1--99-29-24-1--93-24-1--41-24-1--1  
 OLIVINITE (DIABASE) (SILICATE ROCK)

|                   |               |     |  |    |                |   |
|-------------------|---------------|-----|--|----|----------------|---|
| LABRADORITE:      |               |     |  | 50 | VOLUME PERCENT |   |
| ANORTHITE         | CA-AL2-S12-08 | 30  |  | -  | -              |   |
| ALBITE            | NA-AL-S13-08  | 20  |  | -  | -              |   |
| OLIVINE:          |               |     |  | 25 | -              | - |
| FORSTERITE        | MG2-S1-04     | 19  |  | -  | -              |   |
| FAYALITE          | FE2-S1-04     | 6   |  | -  | -              |   |
| PIGEONITE-AUGITE: |               |     |  | 15 | -              | - |
| ENSTATITE         | MG-S1-03      | 7.5 |  | -  | -              |   |
| WOLLASTONITE      | CA-S1-03      | 4.5 |  | -  | -              |   |
| FERROSILITE       | FE-S1-03      | 3.0 |  | -  | -              |   |
| TITANOMAGNETITE   |               |     |  | 10 | -              | - |

$V_0 = 0.319$

THE TABLE LISTS DENSITY IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KBARS.

TABLE

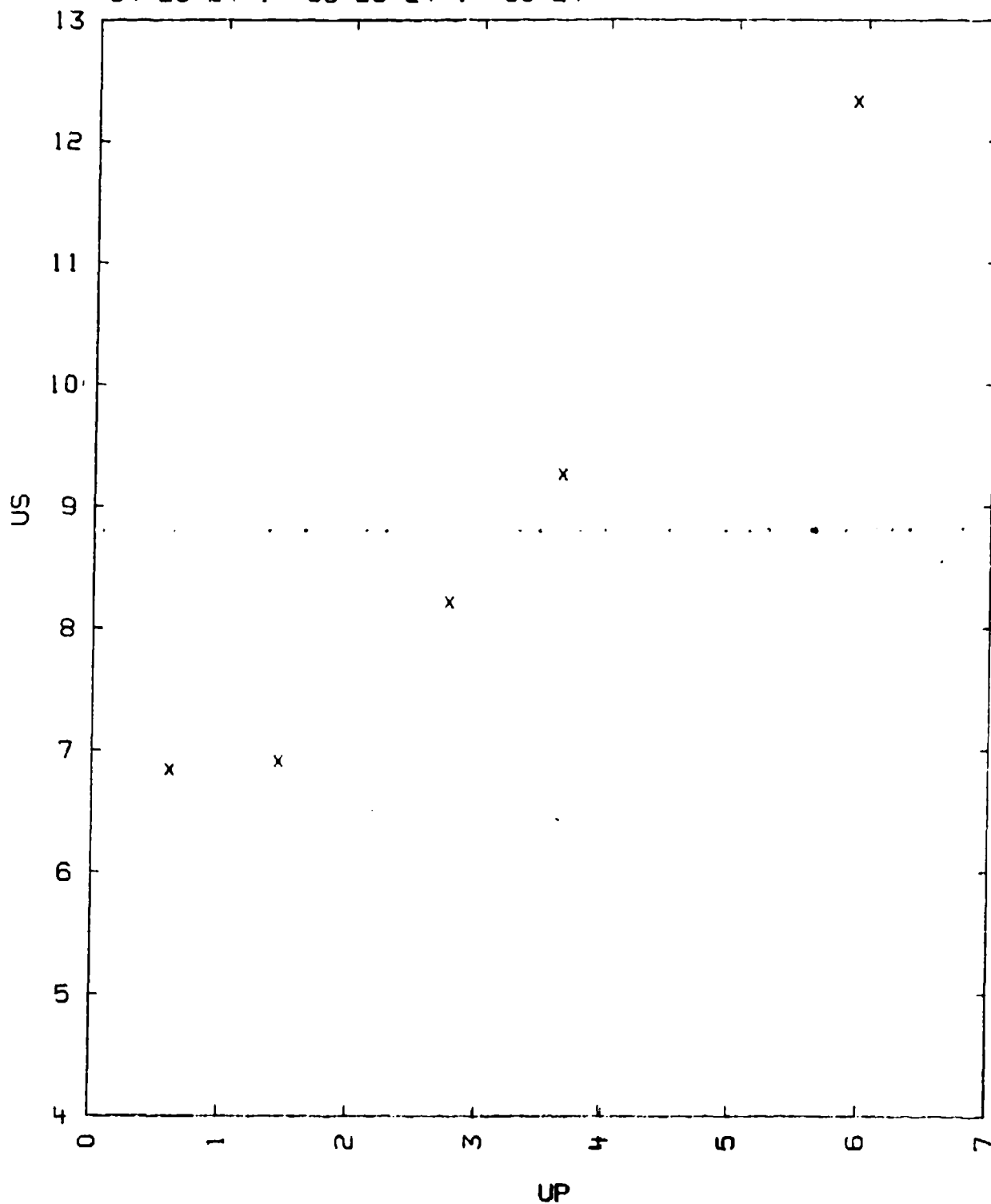
| SAMPLE |       |      |      |       | STANDARD |      |
|--------|-------|------|------|-------|----------|------|
| RH00   | US    | UP   | P    | V/V0  | MTRL     | UP   |
| 3.13   | 6.83  | 0.61 | 131  | 0.911 | AL       | 0.69 |
|        | 6.90  | 1.45 | 313  | 0.790 | AL       | 1.50 |
|        | 8.21  | 2.78 | 714  | 0.661 | AL       | 2.82 |
|        | 9.26  | 3.66 | 1061 | 0.605 | FE       | 2.80 |
|        | 12.32 | 5.92 | 2280 | 0.519 | FE       | 4.56 |

$US = 4.48 + 1.326 \cdot UP$  KM/SEC FOR UP FROM 1.6 TO 6.0 KM/SEC.

## COMMENTS:

- 1) SOURCE: TRUNIN, R. F., GON'SHAKOVA, V. I., SIMAKOV, G. V. AND GALDIN, N. E.  
 IZV. AKADEMII NAUK SSSR. FIZIKA TVERI, VOL. 9, 1965, P. 1-12.
- 2) EXPERIMENTAL TECHNIQUE A.  
 DATA REDUCTION METHOD B. (STANDARD MATERIAL INDICATED IN THE TABLE).
- 3) THE SHOCK VELOCITY WAS MEASURED WITH AN ACCURACY OF 1.5 PERCENT UP TO 700 KBAR AND WITH 2 PERCENT ACCURACY AT HIGHER PRESSURE.
- 4) A DISCONTINUITY IN THE HUGONIOT IS OBSERVED AT  $US = 6.9$  KM/SEC.

TABLE 1  
OLIVINITE (DIABASE) (SILICATE ROCK)  
94-29-24-1--99-29-24-1--93-24-



94-29-24-1--99-94-93-41-29-24-1---1  
DIABASE, CENTERVILLE, VA. (SILICATE ROCK)

|            |                              |     |                |   |
|------------|------------------------------|-----|----------------|---|
| ANORTHITE  | CA-AL2-SI2-O8                | 45  | VOLUME PERCENT |   |
| AUGITE     | (CA,NA)(MG,FE,AL)(SI,AL)2-O6 | 45  | -              | - |
| BIOTITE    | K(MG,FE)3-AL-SI3-O10(O-H)2   | 1.8 | -              | - |
| QUARTZ     | SI-O2                        | 1.8 | -              | - |
| MICROCLINE | K-AL-SI3-O8                  | 3   | -              | - |

V0 = 0.335 CC/G

CL = 6.73 KM/SEC.

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

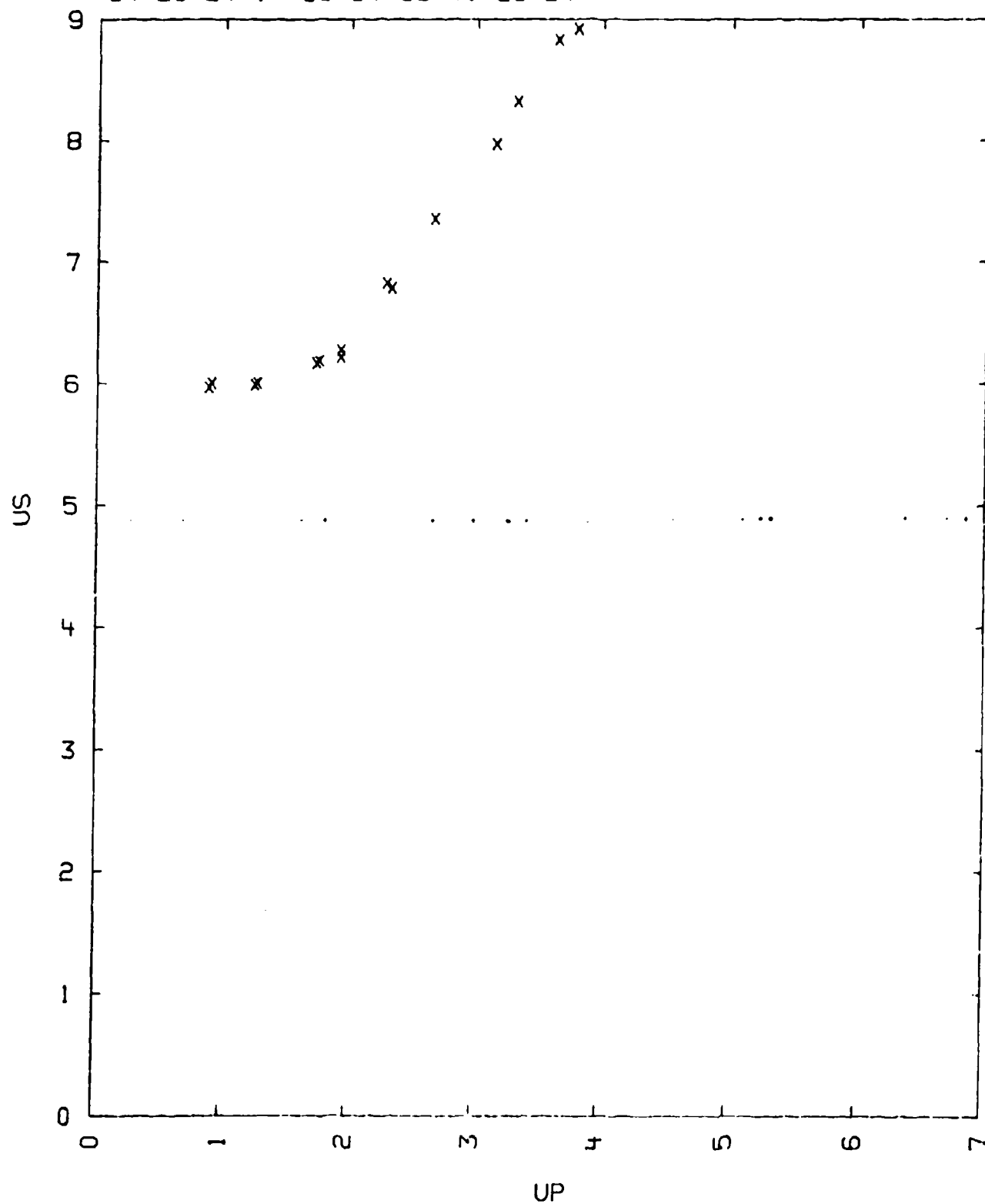
| RHO0 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 2.99 | 5.96 | 0.89 | 160. | 0.851 | 6.55   |
| 3.00 | 6.00 | 0.91 | 164. | 0.848 | 6.57   |
| 2.99 | 5.98 | 1.25 | 223. | 0.791 | 6.97   |
| 2.99 | 5.99 | 1.27 | 226. | 0.788 | 6.99   |
| 2.99 | 6.16 | 1.75 | 322. | 0.716 | 7.58   |
| 2.98 | 6.18 | 1.77 | 326. | 0.714 | 7.60   |
| 2.97 | 6.27 | 1.94 | 361  | 0.691 | 7.80   |
| 2.97 | 6.21 | 1.94 | 358  | 0.688 | 7.79   |
| 2.98 | 6.81 | 2.29 | 466  | 0.664 | 8.28   |
| 2.99 | 6.78 | 2.34 | 475  | 0.654 | 8.33   |
| 2.98 | 7.35 | 2.67 | 585  | 0.637 | 8.78   |
| 2.98 | 7.96 | 3.15 | 747  | 0.604 | 9.42   |
| 2.99 | 8.31 | 3.32 | 825  | 0.602 | 9.68   |
| 2.98 | 8.82 | 3.65 | 961  | 0.585 | 10.13  |
| 3.01 | 8.91 | 3.80 | 1019 | 0.573 | 10.33  |

US = 3.403 1.466\*UP KM/SEC. FOR UP FROM 1.9 TO 3.8 KM/SEC  
SIGMA US = 0.056 KM/SEC.

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.  
PRIVATE COMMUNICATION  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) THE MODAL ANALYSIS OF THESE SAMPLES WHICH WERE OBTAINED FROM BIRCH  
WAS TAKEN FROM: F. BIRCH, J. GEOPHYS. RES., VOL. 65, P. 1083 (1960)
- 4) FURTHER WORK IS IN PROGRESS.

TABLE 1  
 DIABASE, CENTERVILLE, VA. (SILICATE ROCK)  
 94-29-24-1--99-94-93-41-29-24-





94-93-23-1--24-1---1  
LIMESTONE, KAIBAB, ALPHA MEMBER

|                                             |              |                   |
|---------------------------------------------|--------------|-------------------|
| DOLOMITE                                    | CA-MG(C-03)2 | 75 VOLUME PERCENT |
| QUARTZ                                      | SI-O2        | 20 - -            |
| CALCITE, FELDSPAR, CLAY MINERALS, HEMATITE, |              |                   |
| GOETHITE AND HEAVY MINERALS                 | 5 - -        |                   |
| POROSITY                                    |              | 20.3-23.8 PERCENT |

V0 = 0.450 - 0.472 CC/G  
V01 = 0.355 - 0.347 CC/G.

C0 = 2.845 KM/SEC

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES ARE IN KM/SEC.  
AND PRESSURE IN KILOBARS

TABLE

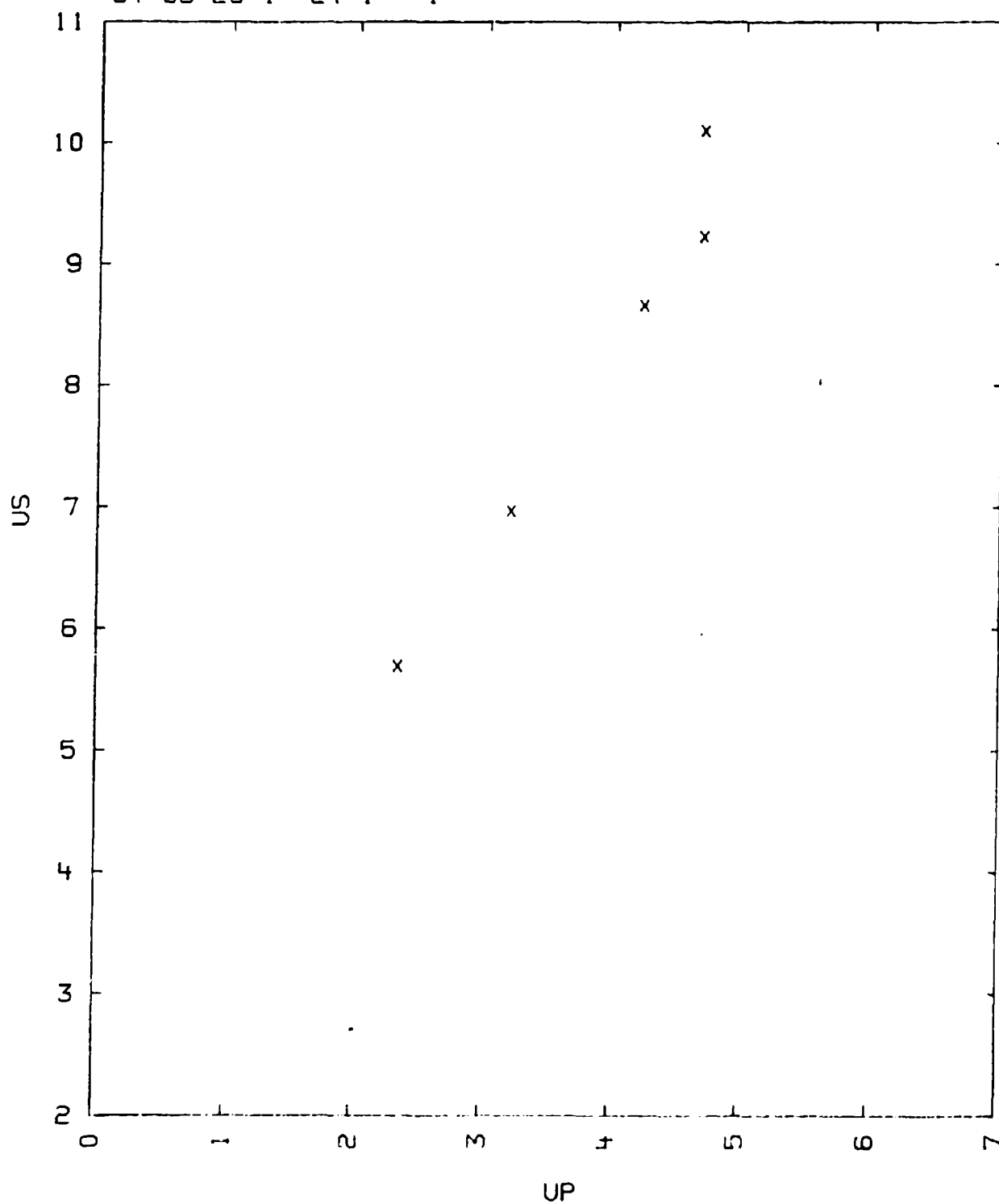
| RH00 | US    | UP    | P     |       |
|------|-------|-------|-------|-------|
| 2.22 | 5.69  | 2.35  | 297.  | 0.587 |
| -    | 6.96  | 3.20  | 494.  | 0.541 |
| -    | 8.65  | 4.23  | 812.  | 0.511 |
| -    | 9.22  | 4.69  | 961.  | 0.491 |
| -    | 10.10 | 5.05* | 1131. | 0.500 |

US = 1.89 + 1.597\*UP KM/SEC. SIGMA US = 0.13 KM/SEC.

COMMENTS:

- 1) SOURCE: JONES, A. H., ISBELL, W. M., SHIPMAN, F. H., PERKINS, R. D., GREEN, S. J. AND MAIDEN, C. J.  
INTERIM REPORT, CONTRACT NAS2-3427, 1968  
GENERAL MOTORS TECH. CENTER, WARREN, MICHIGAN 48090
- 2) EXPERIMENTAL TECHNIQUE A:  
DATA REDUCTION TECHNIQUE A  
STANDARD MATERIALS: OFHC COPPER AND FANSTEEL-77 ALLOY. THE COPPER STANDARD US-UP HUGONOT RELATIONSHIP IS GIVEN BY:  
US = 3.96 + 1.497\*UP KM/SEC. RH00 = 8.93 G/CC  
THE FANSTEEL US-UP HUGONOT IS GIVEN BY:  
US = 3.96 + 1.295\*UP KM/SEC. RH00 = 17.01 G/CC
- 3) THESE PRESSURES WERE ACHIEVED BY USING A TWO-STAGE LIGHT GAS GUN. THE PROJECTILE IMPACT VELOCITY AND TILT WERE MEASURED BY TWO TIMED FLASH X-RAY SHADOWGRAPHS OF THE PROJECTILE.
- 4) THE UNCONFINED CRUSHING STRENGTH IS 3.50 - 4.30 (10\*\*8) DYNES/(CM\*\*2)
- 5) THE ESTIMATED EXPERIMENTAL ERROR IN MEASURING US IS 1 - 2 PERCENT  
THE UNCERTAINTY IN UP IS ABOUT 0.2 PERCENT EXCEPT FOR A 5 PERCENT UNCERTAINTY IN THE LAST ENTRY
- 6) V01 WAS CALCULATED FROM THE ABOVE COMPOSITION AND THE DENSITIES LISTED BY: HURLBUT, DANAS MANUAL OF MINERALOGY (JOHN WILEY AND SONS INC., NEW YORK, 1963) 17TH ED.

TABLE I  
LIMESTONE, KAIBAB, ALPHA MEMBER  
94-93-23-1--24-1---1



96-18-1--23-18-2-117-3-5-6)---1  
 BARATOL, CAST (EXPLOSIVE)

BARIUM NITRATE  $\text{Ba(NO}_3)_2$  76 WT PERCENT  
 TRINITROTOLUENE  
 $-\text{C}(\text{C}-\text{H}_3)-\text{C}(\text{N}-\text{O}_2)(-\text{C}(\text{H})-\text{C}(\text{N}-\text{O}_2)-) = \text{C}_7-\text{N}_3-\text{H}_5-\text{O}_6$  24 - -

$V_0 = 0.388 \text{ CC/G}$   
 $V_{01} = 0.409 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

| RH00  | US   | UP   | P    | V/V0  |
|-------|------|------|------|-------|
| 2.580 | 2.92 | 0.36 | 27.1 | 0.877 |
| -     | 3.02 | 0.35 | 27.3 | 0.884 |
| -     | 3.00 | 0.41 | 31.7 | 0.863 |
| -     | 3.00 | 0.41 | 31.7 | 0.863 |
| -     | 4.17 | 0.86 | 92.5 | 0.794 |
| -     | 3.35 | 0.44 | 38.0 | 0.869 |
| -     | 3.67 | 0.58 | 54.9 | 0.842 |
| -     | 3.19 | 0.45 | 24.4 | 0.859 |
| -     | 4.15 | 0.87 | 61.4 | 0.790 |
| -     | 4.34 | 0.85 | 95.2 | 0.804 |
| -     | 3.71 | 0.70 | 67.0 | 0.811 |
| -     | 3.77 | 0.74 | 72.0 | 0.804 |
| -     | 4.13 | 0.72 | 76.7 | 0.826 |

$US = 2.11 + 2.45 \cdot UP \text{ KM/SEC}$   
 $SIGMA US = 0.13 \text{ KM/SEC}$

## COMMENTS:

- 1) SOURCE: BOYLE, V. M.  
 PRIVATE COMMUNICATION  
 BALLISTIC RESEARCH LABORATORIES, AMXDR-ID  
 ABERDEEN PROVING GROUND, MARYLAND 21005.
- 2) EXPERIMENTAL TECHNIQUE: THE SHOCK VELOCITY IN THE SAMPLE WAS MEASURED BY A SHEAR CAMERA THAT SWEEPED THE SHADOWGRAPH OF A TRANSPARENT CHANNEL IN THE SAMPLE ACROSS THE FILM PLANE. THE CHANNEL WAS MADE BY SPLITTING THE SAMPLE IN TWO ALONG THE SHOCK DIRECTION AND SEPARATING THE TWO HALVES BY A THIN (0.127 MM) TRANSPARENT PLASTIC SHEET (EXTRUDED ACETATE).

## DATA REDUCTION TECHNIQUE: B

STANDARD MATERIALS USED:  
 ALUMINUM, 2024-T4,  $US = 5.360 + 1.351 \cdot UP \text{ KM/SEC}$   
 $RHO = 2.785 \text{ G/CC}$   
 PLEXIGLASS,  $US = 2.702 + 1.544 \cdot UP, \text{ KM/SEC}, RHO = 1.184 \text{ G/CC}$   
 $UP = 1/2 UFS$  WAS ASSUMED FOR THE STANDARD MATERIALS SO THAT

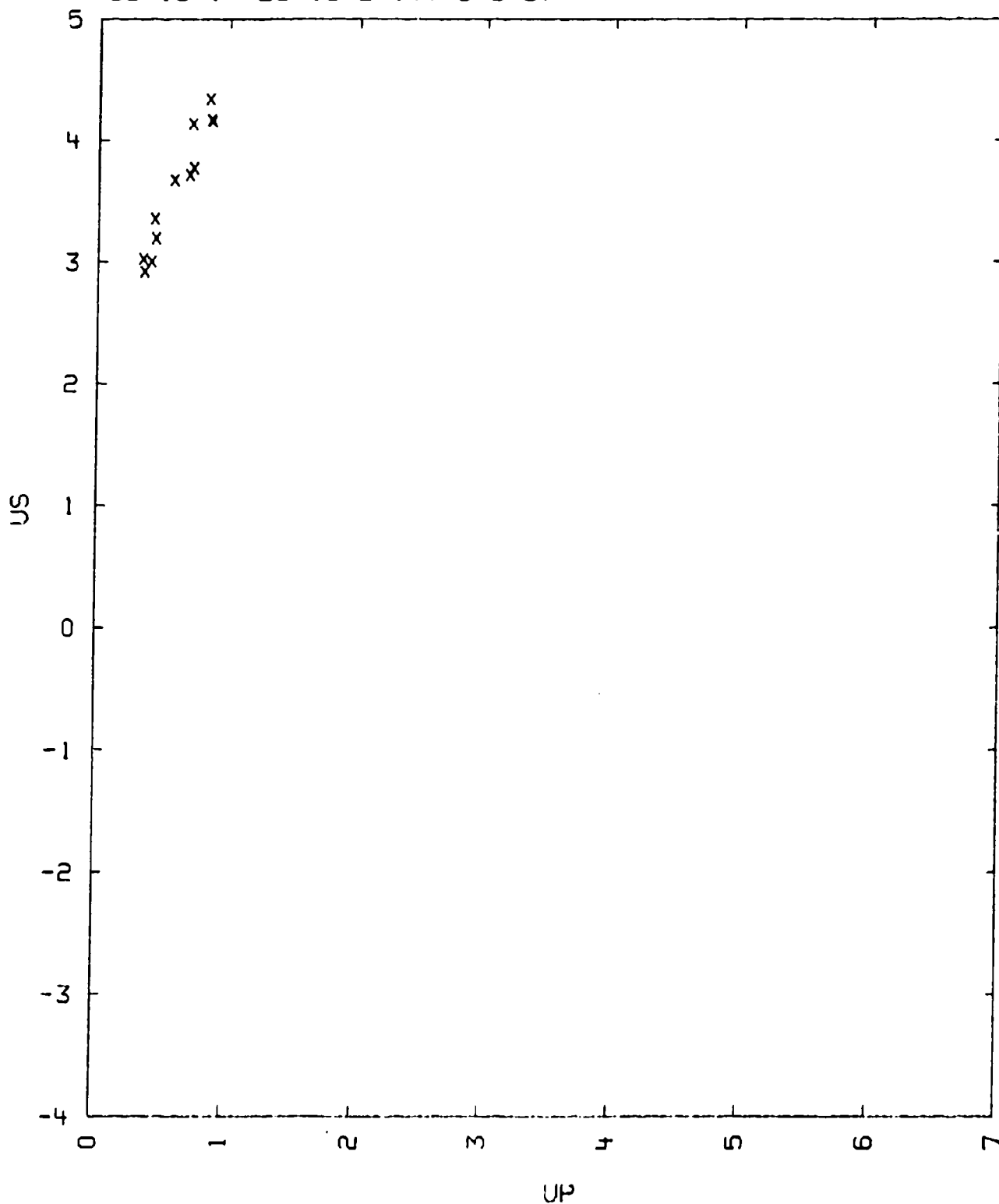
THE PRESSURE ISENTROPE COULD BE OBTAINED BY REFLECTING THE  
P VS. UP HUGONIOT IN THE LINE  $UP = 1/2 UFS$ .

- 3) THE DEGREE TO WHICH THE RESULTS MAY BE AFFECTED BY CHEMICAL REACTION  
OF THE SHOCKED EXPLOSIVE SAMPLE HAS NOT BEEN DETERMINED AT THIS TIME.
- 4) VOI WAS CALCULATED ASSUMING VOLUME ADDITIVITY OF THE COMPONENTS:  
VOI(TNT) = 0.6046 CC/G, HANDBOOK OF CHEM. AND PHYS. (CHEM. RUBBER  
PUBL. CO. 1964) 45TH ED.  
VOI(BA-N2-O6) = 0.3073 CC/G, WYCKOFF, CRYSTAL STRUCTURES, VOL. 2  
(INTERSCIENCE PUBL., N. Y., 1964).

TABLE I

BARATOL, CAST (EXPLOSIVE)

96-18-1--23-18-2-1(7-3-5-6)---



98-28-1--23-18-2-1(200-10-286-33)---1

LITHIUM TETRABORATE-EPOXY

LITHIUM TETRABORATE L12-B4-07-(H2-O)5  
EPOXY (C200-N10-H286-033)N90 WT PERCENT  
10 WT PERCENT

V0 = 0.458 - 0.460 CC/G

CL = 4.40 KM/SEC

C0 = 3.14 KM/SEC

CS = 2.67

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |      |
|------------------|------|------|------|--------|--------------------|------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |      |
| 2.174            | 5.54 | 1.07 | 129. | 0.8069 | 2024 AL            | 6.54 |
| 2.181            | 5.56 | 1.08 | 131. | 0.8058 | 2024 AL            | 6.55 |
| 2.177            | 6.09 | 1.39 | 184. | 0.7718 | 2024 AL            | 6.92 |
| 2.175            | 6.09 | 1.40 | 185. | 0.7701 | 2024 AL            | 6.93 |
| 2.188            | 6.81 | 1.87 | 279. | 0.7254 | 2024 AL            | 7.51 |
| 2.181            | 6.83 | 1.88 | 280. | 0.7247 | 2024 AL            | 7.52 |
| 2.177            | 7.09 | 2.07 | 320. | 0.7080 | 2024 AL            | 7.75 |
| 2.179            | 7.42 | 2.48 | 401. | 0.6658 | 2024 AL            | 8.22 |
| 2.176            | 7.45 | 2.49 | 404. | 0.6658 | 2024 AL            | 8.23 |
| 2.178            | 8.04 | 2.91 | 510. | 0.6381 | 2024 AL            | 8.75 |
| 2.176            | 8.23 | 2.92 | 523. | 0.6452 | 2024 AL            | 8.79 |
| 2.178            | 8.00 | 2.93 | 511. | 0.6337 | 2024 AL            | 8.76 |
| 2.173            | 9.22 | 3.78 | 757. | 0.5900 | 2024 AL            | 9.82 |
| 2.172            | 9.32 | 3.85 | 779. | 0.5869 | 2024 AL            | 9.91 |

US = 4.052 + 1.486\*UP - 0.033\*UP\*\*2 KM/SEC

SIGMA US = 0.094 KM/SEC

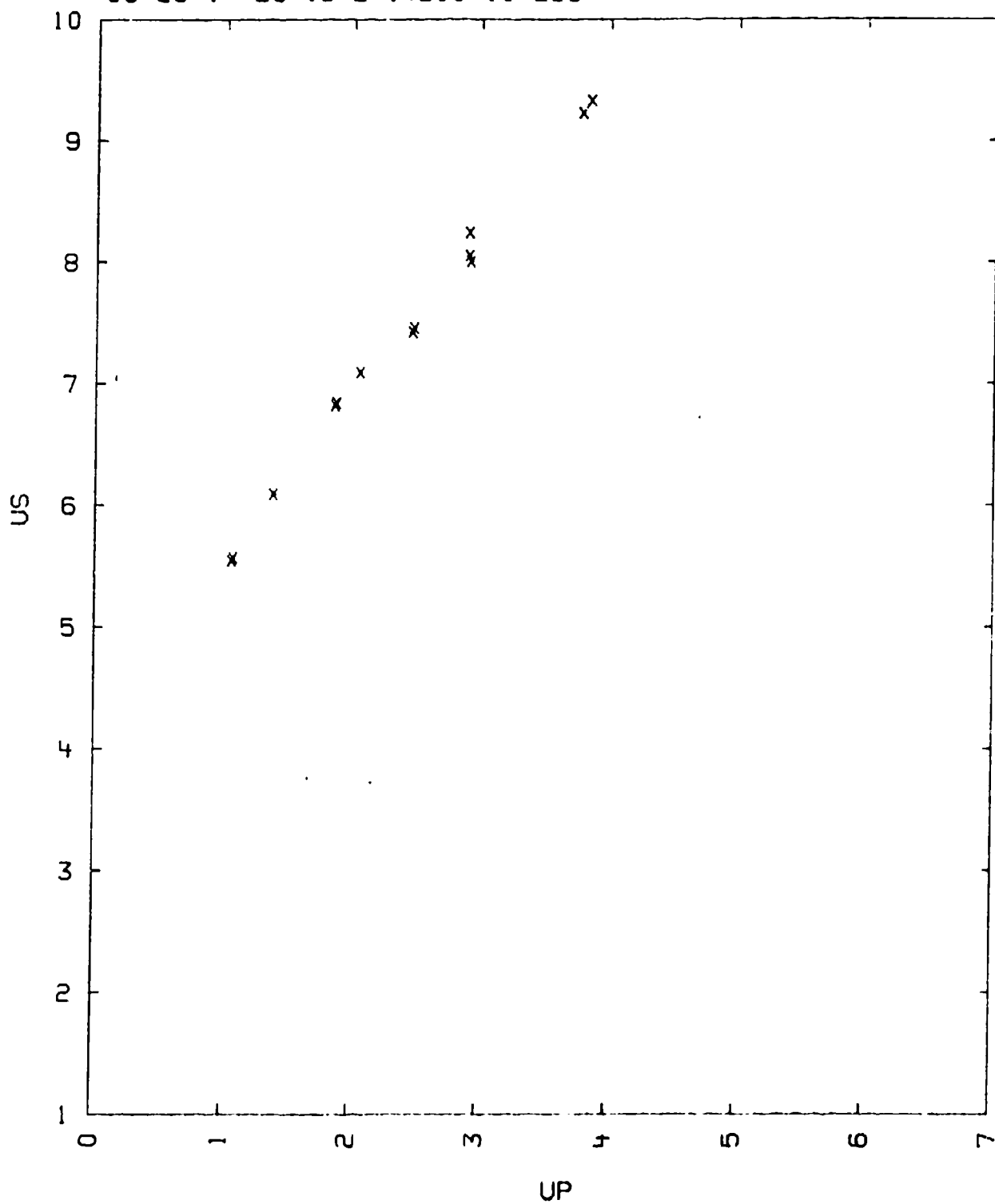
## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) THE EPOXY COMPOSITION WAS ASSUMED TO BE THAT OF EPOXY B15, APPLICABL  
TO ENTRY 36-1--23-18-2-1(200-10-286-33)---1 (COPPER OXIDE EPOXY)

TABLE I

LITHIUM TETRABORATE-EPOXY

98-28-1--23-18-2-1(200-10-286-



98-29-24-1--23-18-2-1(200-10-286-33)---1  
 ZERIFAC- EPOXY

|                 |                          |               |
|-----------------|--------------------------|---------------|
| ZERIFAC         | L1-AL-S1-04              | 71 WT PERCENT |
| EPOXY           | C200-N10-H286-033        | 29 WT PERCENT |
| EPON 815        | C200-H261-036,           | 90 WT PERCENT |
| DIETHYLTRIAMINE | H-N(-C(H2)-C(H2)-N-H2)2, | 10 WT PERCENT |

$V_0 = 0.563$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
 AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |       |
|------------------|------|------|------|--------|--------------------|-------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |       |
| 1.777            | 4.41 | 1.27 | 100. | 0.7120 | 2024 AL            | 6.56  |
| 1.776            | 5.42 | 2.19 | 211. | 0.5959 | 2024 AL            | 7.54  |
| 1.776            | 6.82 | 3.15 | 382. | 0.5381 | 2024 AL            | 8.62  |
| 1.774            | 6.82 | 3.44 | 416. | 0.4956 | 2024 AL            | 8.89  |
| 1.775            | 7.83 | 3.96 | 550. | 0.4943 | 2024 AL            | 9.53  |
| 1.775            | 8.35 | 4.48 | 664. | 0.4635 | 2024 AL            | 10.10 |

$US = 2.765 + 1.247 \cdot UP$  KM/SEC  
 $SIGMA US = 0.156$  KM/SEC

COMMENTS:

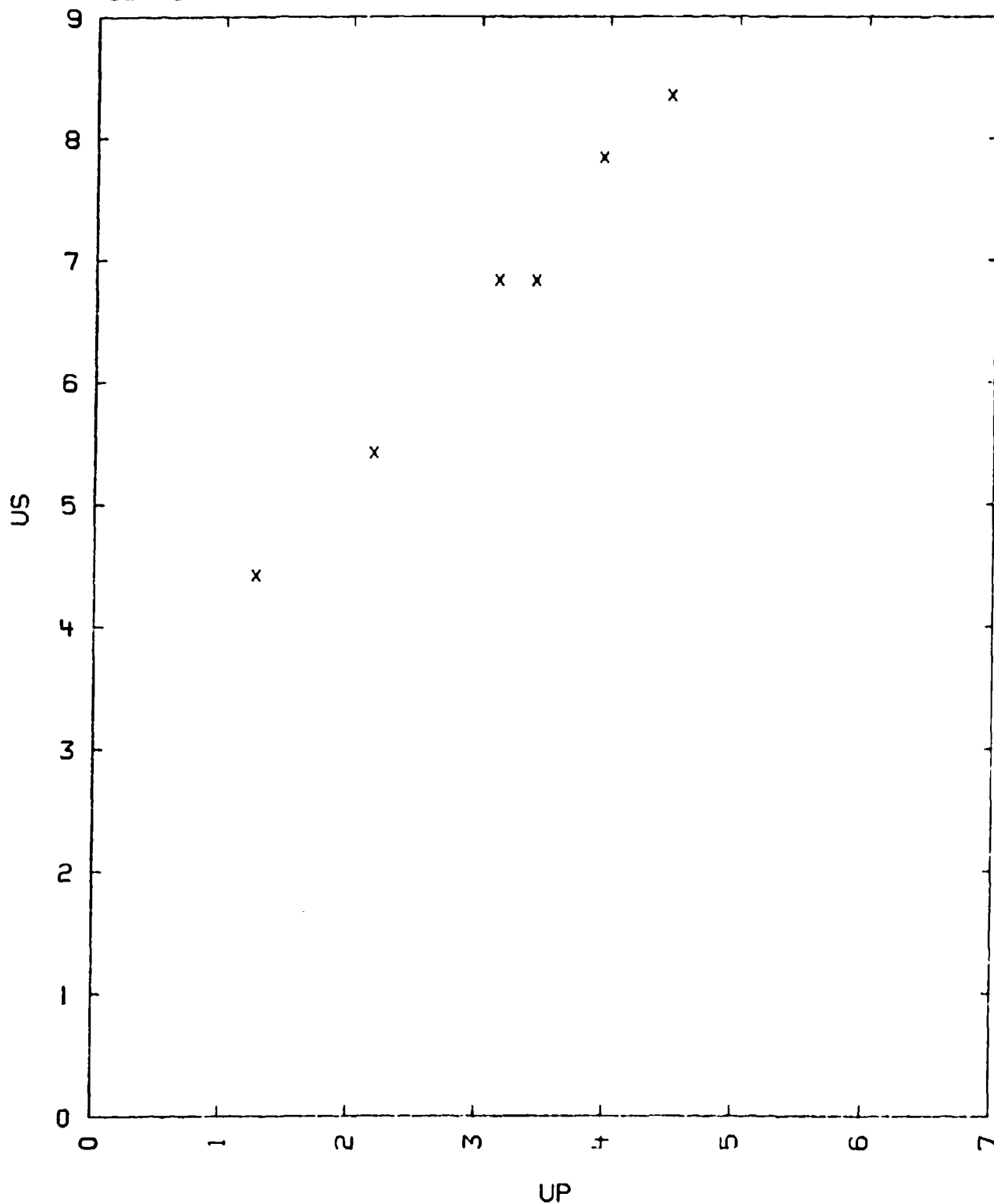
- 1) SOURCE: MC QUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.  
 AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
 DATA REDUCTION TECHNIQUE: B
- 3) EPON 815 COMPOSITION. PRIVATE COMMUNICATION, P. FLEMING (LLL,  
 LIVERMORE, CA, 1975), SE ALSO MODERN PLASTICS ENCYCLOPEDIA (MC GRAW  
 HILL, N.Y., 1975) VOL. 51



TABLE I

ZERIFAC- EPOXY

98-29-24-1--23-18-2-1(200-10-2



98-29-24-1--23-18-2-1(200-16-286-79)---1  
 ZERIFAC- POLYURETHANE FOAM

ZERIFAC  
 POLYURETHANE

L1-AL-SI-04  
 C200-N18-H286-079

50 WT PERCENT  
 50 WT PERCENT

$V_0 = 1.39-1.43 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
 AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |        |
|------------------|------|------|------|--------|--------------------|--------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL           | US(ST) |
| 0.702            | 2.58 | 1.62 | 29.  | 0.3721 | 2024 AL            | 6.53   |
| 0.699            | 2.71 | 1.63 | 31.  | 0.3985 | 2024 AL            | 6.55   |
| 0.705            | 3.30 | 2.06 | 48.  | 0.3758 | 2024 AL            | 6.91   |
| 0.712            | 3.72 | 2.39 | 63.  | 0.3575 | 2024 AL            | 7.18   |
| 0.703            | 4.35 | 2.79 | 85.  | 0.3586 | 2024 AL            | 7.53   |
| 0.708            | 4.43 | 2.82 | 88.  | 0.3634 | 2024 AL            | 7.56   |
| 0.721            | 4.33 | 2.86 | 89.  | 0.3395 | 2024 AL            | 7.59   |
| 0.709            | 4.53 | 3.01 | 97.  | 0.3355 | 2024 AL            | 7.71   |
| 0.707            | 5.69 | 3.67 | 148. | 0.3550 | 2024 AL            | 8.32   |
| 0.706            | 5.52 | 3.67 | 143. | 0.3351 | 2024 AL            | 8.30   |
| 0.709            | 5.71 | 3.98 | 161. | 0.3030 | 2024 AL            | 8.56   |
| 0.705            | 6.19 | 4.13 | 180. | 0.3328 | 2024 AL            | 8.72   |
| 0.708            | 6.33 | 4.45 | 199. | 0.2970 | 2024 AL            | 8.98   |
| 0.701            | 6.48 | 4.47 | 203. | 0.3102 | 2024 AL            | 9.01   |
| 0.704            | 6.43 | 4.51 | 204. | 0.2986 | 2024 AL            | 9.03   |
| 0.707            | 6.39 | 4.52 | 204. | 0.2926 | 2024 AL            | 9.04   |
| 0.704            | 6.77 | 4.62 | 220. | 0.3176 | 2024 AL            | 9.16   |
| 0.706            | 7.79 | 5.38 | 296. | 0.3094 | 2024 AL            | 9.86   |
| 0.703            | 7.91 | 5.45 | 303. | 0.3110 | 2024 AL            | 9.93   |
| 0.717            | 8.06 | 5.79 | 335. | 0.2816 | 2024 AL            | 10.23  |

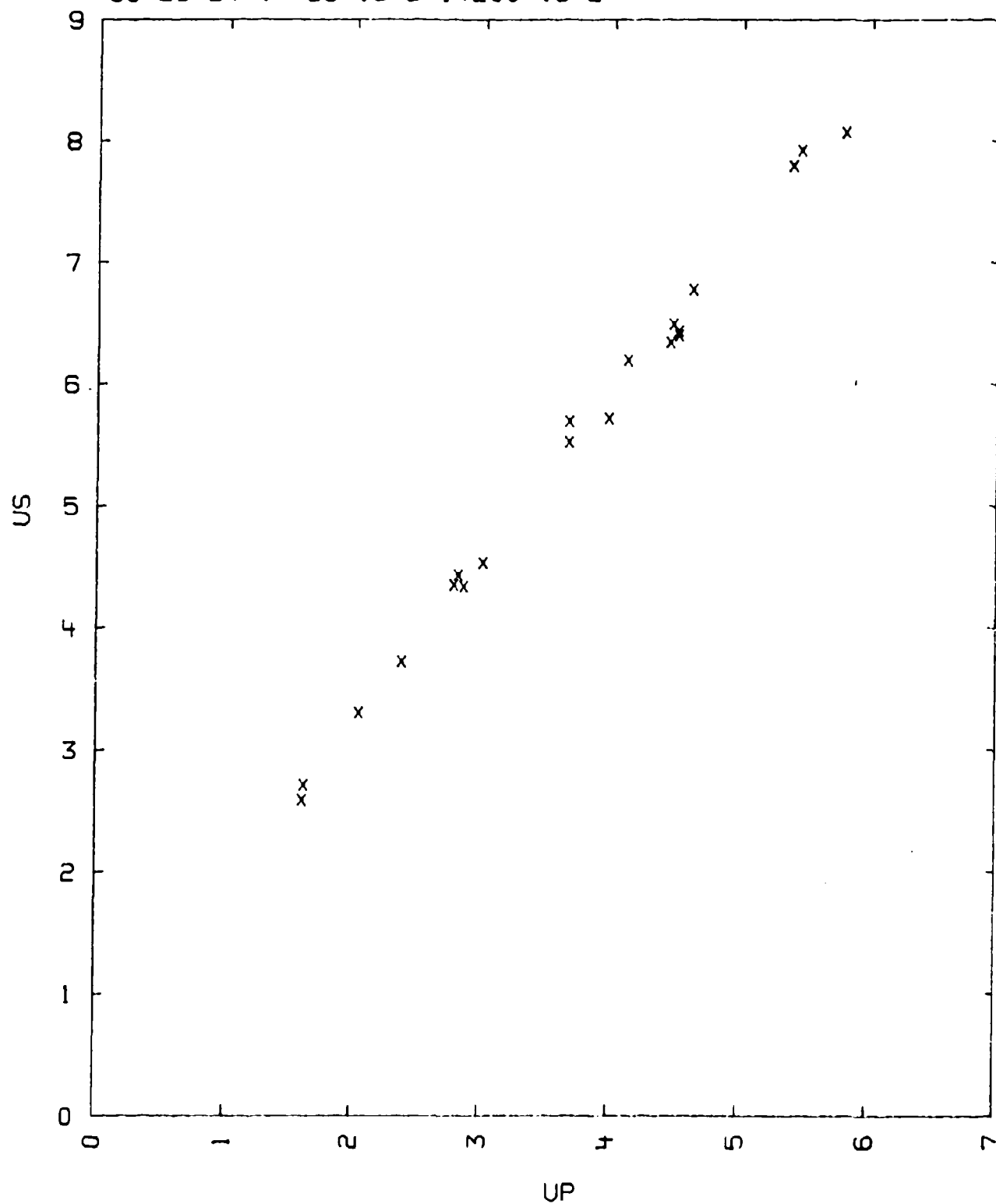
$US = 0.327 + 1.479 \cdot UP - 0.021 \cdot UP^2$   
 $SIGMA \text{ US} = 0.124 \text{ KM/SEC}$

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
 AND CARTER, W.J.  
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
 DATA REDUCTION TECHNIQUE: B
- 3) THE POLYURETHANE COMPOSITION WAS ASSUMED TO BE THE SAME AS ENTRY  
 23-18-2-1(200-16-286-79)---1

TABLE I

ZERIFAC- POLYURETHANE FOAM  
98-29-24-1--23-18-2-1 (200-16-2)



99-29-24-1--94-29-24-1---1  
ANORTHOSITE, TAHAWUS N.Y.

|             |                              |    |                |
|-------------|------------------------------|----|----------------|
| PLAGIOCLASE |                              | 90 | VOLUME PERCENT |
| ANORTHITE   | CA-AL2-S12-08                | 44 | -              |
| ALBITE      | NA-AL-S13-08                 | 46 | -              |
| AUGITE      | (NA,CA)(MG,FE,AL)(SI,AL)2-06 | 10 | -              |

V0 = 0.362 TO 0.370 CC/G CL = 6.94 KM/SEC  
V01 = 0.364 CC/G

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 2.72 | 5.93 | 0.92 | 148. | 0.845 | 6.52   |
| 2.71 | 5.94 | 1.31 | 210. | 0.779 | 6.97   |
| 2.73 | 5.88 | 1.32 | 213. | 0.776 | 6.99   |
| 2.73 | 5.92 | 2.05 | 331  | 0.655 | 7.79   |
| 2.71 | 5.93 | 2.05 | 330  | 0.655 | 7.80   |
| 2.73 | 6.63 | 2.45 | 442  | 0.630 | 8.33   |
| 2.73 | 6.46 | 2.47 | 435  | 0.618 | 8.33   |
| 2.72 | 7.02 | 2.81 | 538  | 0.599 | 8.78   |
| 2.73 | 7.06 | 2.82 | 542  | 0.601 | 8.79   |
| 2.75 | 7.84 | 3.27 | 704  | 0.584 | 9.42   |
| 2.76 | 8.25 | 3.44 | 782  | 0.584 | 9.68   |
| 2.73 | 8.25 | 3.50 | 788  | 0.576 | 9.73   |
| 2.75 | 8.39 | 3.68 | 849  | 0.561 | 9.96   |
| 2.79 | 8.68 | 3.76 | 913  | 0.566 | 10.12  |
| 2.73 | 8.49 | 3.84 | 888  | 0.549 | 10.13  |
| 2.70 | 8.80 | 3.94 | 937  | 0.552 | 10.28  |
| 2.72 | 8.81 | 3.97 | 952  | 0.548 | 10.33  |

US = 2.775 + 1.536\*UP KM/SEC. FOR UP FROM 2.05 TO 4.0 KM/SEC  
SIGMA US = 0.10 KM/SEC.

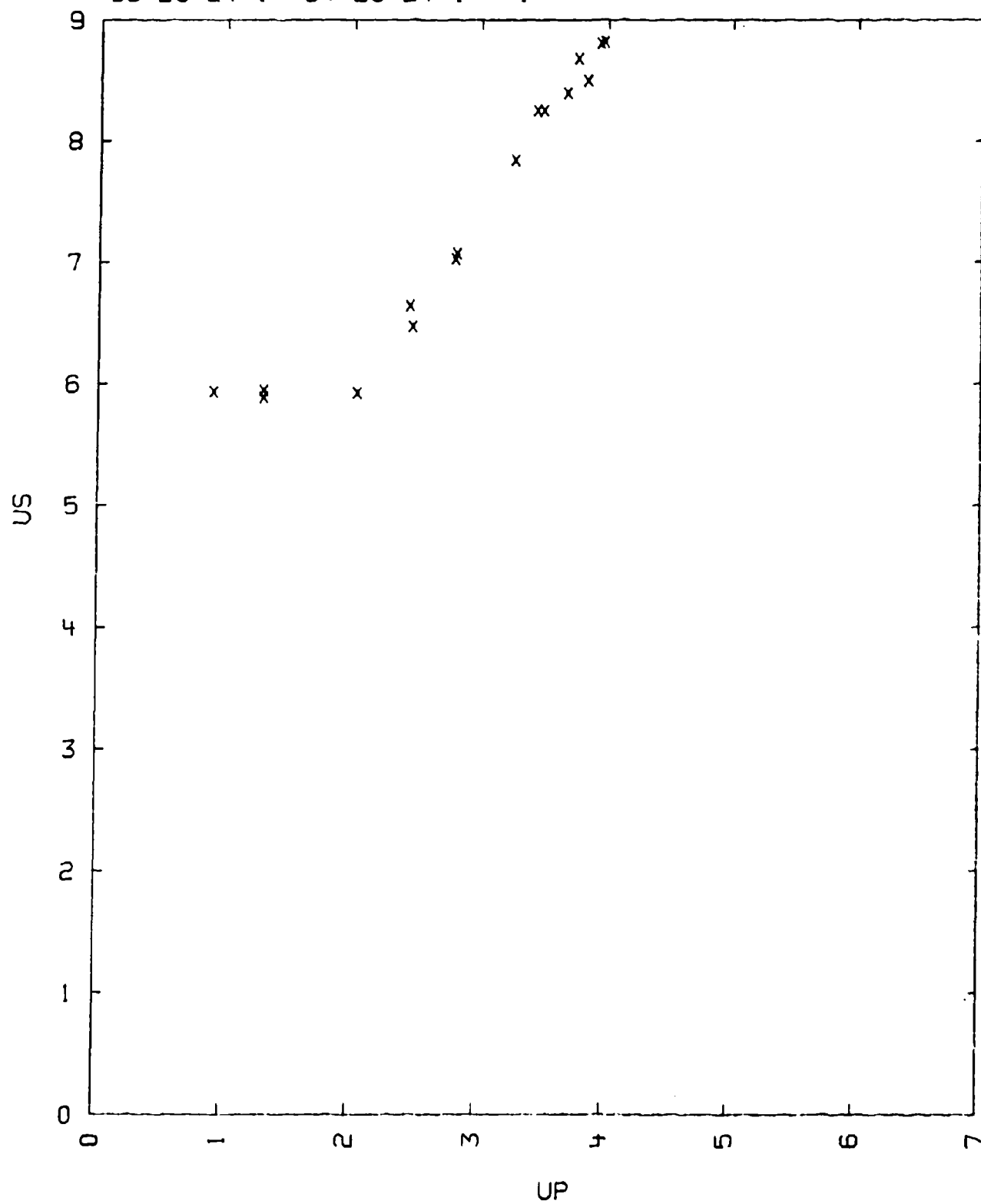
## COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.  
PRIVATE COMMUNICATION  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED FOR PLAGIOCLASE  
IN CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYST. ASSN. 1963) 2ND  
ED. AND AN ASSUMED AUGITE DENSITY OF 3.2 G/CC
- 4) THE MODAL ANALYSIS OF THESE SAMPLES WHICH WERE OBTAINED THROUGH BIRCH  
WAS TAKEN FROM: F. BIRCH, J. GEOPHYS. RES., VOL. 65, P.1083 (1960)
- 5) FURTHER WORK IN PROGRESS
- 6) CL WAS ALSO LISTED IN THE ABOVE BIRCH PAPER

TABLE I

ANORTHOSITE, TAHAWUS N.Y.

99-29-24-1--94-29-24-1---1



99-29-24-1--94-29-24-1---2  
ALBITITE, SYLMAR, PENN. (SILICATE ROCK)

| OLIGOCLASE: |                            |    | 98 VOL. PERCENT |   |
|-------------|----------------------------|----|-----------------|---|
| ALBITE      | NA-AL-S13-08               | 86 | -               | - |
| ANORTHITE   | CA-AL2-S12-08              | 12 | -               | - |
| ACTINOLITE  | CA2-(MG,FE)5-S18-022-(OH)2 | 2  | -               | - |

V0 = 0.383 CC/G  
V01 = 0.3773 CC/G

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 2.61 | 5.66 | 0.92 | 136. | 0.837 | 6.49   |
| 2.61 | 5.56 | 1.34 | 195. | 0.759 | 6.95   |
| 2.61 | 5.82 | 1.89 | 287. | 0.675 | 7.58   |
| 2.61 | 5.90 | 1.97 | 303. | 0.666 | 7.67   |
| 2.61 | 5.94 | 2.08 | 322. | 0.650 | 7.79   |
| 2.61 | 6.31 | 2.43 | 410  | 0.606 | 8.28   |
| 2.61 | 6.96 | 2.88 | 524  | 0.587 | 8.80   |
| 2.61 | 7.75 | 3.35 | 677  | 0.567 | 9.42   |
| 2.61 | 8.09 | 3.54 | 747  | 0.563 | 9.68   |
| 2.61 | 8.14 | 3.70 | 786  | 0.546 | 9.86   |
| 2.61 | 8.65 | 3.95 | 892  | 0.544 | 10.21  |
| 2.61 | 8.69 | 3.98 | 904  | 0.541 | 10.23  |

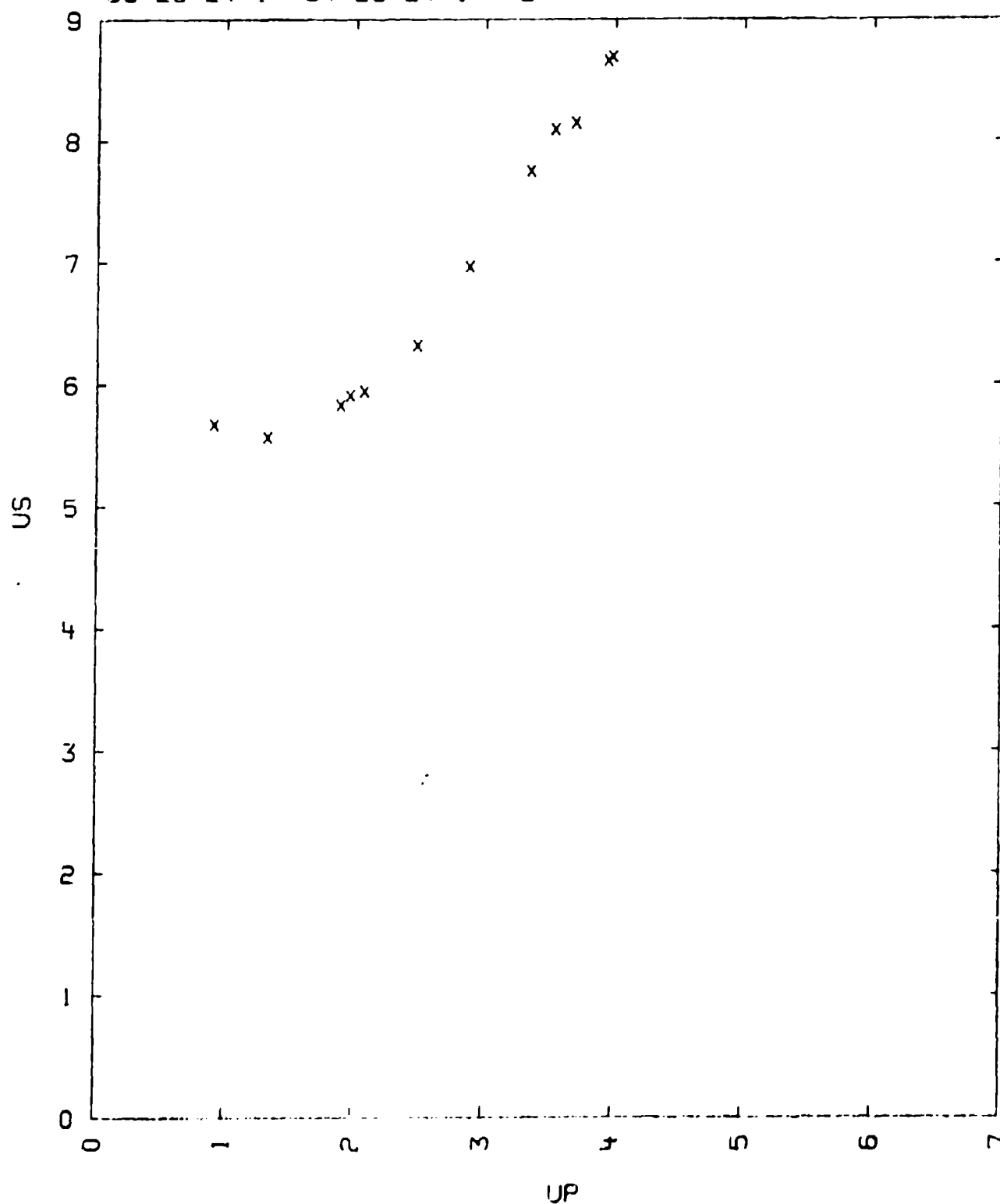
US = 5.32 + 0.280\*UP KM/SEC. FOR UP FROM 0.9 TO 2.1 KM/SEC.  
SIGMA US = 0.1 KM/SEC

US = 2.404 + 1.581\*UP KM/SEC. FOR UP FROM 2.5 TO 4.0 KM/SEC.  
SIGMA US = 0.07 KM/SEC

## COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.  
PRIVATE COMMUNICATION  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYST. ASSN. 1963) 2ND ED., AND A ACTINOLITE DENSITY OF 3.1 G/CC.
- 4) THE MODAL ANALYSIS OF THESE SAMPLES WHICH WERE OBTAINED THROUGH BIRCH WAS TAKEN FROM F. BIRCH, J. GEOPHYS. RES., VOL. 65, P. 1083 (1960)
- 5) FURTHER WORK IS IN PROGRESS.
- 6) THE DATA SUGGEST A PHASE TRANSITION AT US = 8.2 KM/SEC.

TABLE 1  
ALBITITE, SYLMAR, PENN. (SILICATE ROCK)  
99-29-24-1--94-29-24-1---2



99-29-24-1-94-29-24-1---3  
 ANDESITE (ANORTHOSITE) (SILICATE ROCK)

ANDESINE: 98 VOLUME PERCENT 1-8MM GRAINS  
 ALBITE NA-AL-SI3-O8 70-50 - -  
 ANORTHITE CA-AL2-SI2-O8 30-50 - -  
 APATHITE CA5(F,CL,O-H)(P-OY)3 REMAINDER 0.01-0.03 MM GRAINS  
 ZIRCON ZR-SI-O4 - - - -  
 CHLORITE MG3(SI4-O10)(O-H)2-MG3(O-H)6 - - - -  
 HORNBLende - - - -

VO = 0.375-0.362  
 VOI = 0.373-0.369 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURES IN KILOBARS. AL = 2024 ALUMINUM, BR = 356 BRASS, PLE = PLEXIGLAS

TABLE I

| - - - - - SAMPLE - - - - - |      |       |      |       |      |       |      |      |       | STANDARD |     |
|----------------------------|------|-------|------|-------|------|-------|------|------|-------|----------|-----|
| RH00                       | US1  | UP1   | P    | V1/VO | US2  | UP2   | UFS2 | P2   | V2/VO | UFS      | MAT |
| 2.662                      | 5.66 | 0.286 | 43.  | 0.950 | 3.71 | 0.406 |      | 55.  | 0.915 | 1.404    | PLE |
| -                          | 5.67 | 0.293 | 44.  | 0.948 |      |       |      |      |       | 1.404    | PLE |
| -                          | 5.86 | 0.317 | 49.  | 0.946 | 5.28 | 0.812 |      | 111. | 0.851 | 1.560    | AL  |
| -                          | 5.40 | 0.403 | 58.  | 0.925 | 5.18 | 1.029 |      | 144. | 0.804 | 1.97     | AL  |
| -                          | 5.77 | 0.378 | 58.  | 0.935 | 5.38 | 0.852 |      | 126. | 0.846 | 1.97     | AL  |
| 2.76                       | 6.69 | 0.280 | 51.8 | 0.951 | 5.25 | 0.82  | 1.12 | 130  | 0.853 | 1.55     | AL  |
| 2.76                       | 6.56 | 0.158 | 28.6 | 0.976 | 5.62 | 0.835 | 1.14 | 132  | 0.855 | 1.58     | AL  |
| 2.75                       | 6.80 | 0.300 | 57.2 | 0.955 | 6.10 | 1.94  |      | 330  | 0.718 | 3.57     | AL  |
| 2.73                       | 7.76 | 0.290 | 61.5 | 0.961 | 6.50 | 1.88  |      | 344  | 0.742 | 3.57     | AL  |
| 2.763                      | 7.22 | 0.290 | 57.8 | 0.959 | 6.14 | 1.94  | 3.84 | 335  | 0.689 | 3.58     | AL  |
| 2.75                       | 6.59 | 0.290 | 52.5 | 0.956 | 6.22 | 2.37  | 4.65 | 405  | 0.621 | 3.34     | BR  |
| 2.75                       | 6.81 | 0.290 | 54.3 | 0.957 | 6.31 | 2.36  | 4.38 | 412  | 0.628 | 3.34     | BR  |
| 2.75                       | 7.03 | 290   | 56.1 | 0.959 | 6.56 | 2.38  | 4.87 | 432  | 0.639 | 4.41     | AL  |
| 2.75                       |      | 290   | 57.6 | 0.960 | 6.71 | 2.57  | 5.24 | 476  | 0.619 | 4.78     | AL  |

US =

TABLE II

| RH00  | US   | UP    | UFS  | P   | V/V0  | UFS   | MAT |
|-------|------|-------|------|-----|-------|-------|-----|
| 2.662 | 5.63 | 1.517 |      | 227 | 0.730 | 2.955 | AL  |
| -     | 5.59 | 1.320 |      | 197 | 0.764 | 2.955 | AL  |
| -     | 5.34 | 0.858 |      |     |       | 1.560 | AL  |
| 2.72  | 6.45 | 2.27  | 4.43 | 400 | 0.647 | 3.23  | BR  |
| 2.75  | 6.45 | 2.40  | 4.77 | 427 | 0.628 | 4.41  | AL  |
| 2.76  | 6.73 | 2.33  |      | 433 | 0.652 | 3.36  | BR  |
| 2.75  | 6.73 | 2.57  | 5.33 | 478 | 0.618 | 4.78  | AL  |
| 2.75  | 7.33 | 3.10  | 6.04 | 622 | 0.577 | 4.45  | BR  |
| 2.75  | 7.35 | 3.10  | 5.98 | 623 | 0.579 | 4.45  | BR  |



RH00 US UP UFS P V/V0

UFS MAT

US =

## COMMENTS

- 1) SOURCE: AHRENS, T. J. AND GREGSON JR, V. G.  
J. GEOPHYS. RES., VOL. 69, P. 4839 (1964)  
AHRENS, T. J. AND ROSENBERG, T. J.  
POULTER LABORATORIES, MENLO PARK, CALIF. USA.  
CONFERENCE ON SHOCK METAMORPHISM, APRIL 14-18 (1966)  
AHRENS T.J., ROSENBERG J.T. AND RUDERMAN M.H.  
STANFORD RESEARCH INSTITUTE REPORT DASA 1068 (1966)  
POULTER LABORATORIES, MENLO PARK, CALIF. 94025, USA
- 2) EXPERIMENTAL TECHNIQUE: C2  
DATA REDUCTION METHOD: B. D WITH UFS1=2UP1 (ELASTIC WAVE ONLY)  
STANDARDS: 2024 ALUMINUM, PLEXIGLAS  
AND 356 BRASS.
- 3) VOI WAS OBTAINED FROM AN AVERAGE IMPURITY DENSITY AND THE DENSITY RANGE LISTED IN: HURLBUT, C. S., DANAS MANUAL OF MINERALOGY (JOHN WILEY AND SONS INC., NEW YORK 1963) 17TH ED.
- 4) TWO SINGLE CRYSTALS OF PURE PLAGIOCLASE WERE SHOCKED IN THIS WORK AND GAVE THE FOLLOWING RESULTS:
- |                            |               |                            |               |
|----------------------------|---------------|----------------------------|---------------|
| LABRADORITE (AN50-AN70)    |               | ALBITE (AB100-AB90)        |               |
| RH00 = 2.69 G/CC           |               | RH00 = 2.59 G/CC           |               |
| US1 = 6.62                 | UP1 = 0.273   | US1 = 6.60                 | UP1 = 0.188   |
| P1 = 49.                   | V1/V0 = 0.959 | P1 = 32                    | V1/V0 = 0.972 |
| US2 = 5.27                 | UP2 = 0.803   | US2 = 4.80                 | UP2 = 0.802   |
| P2 = 123.                  | V2/V0 = 0.857 | P2 = 107                   | V2/V0 = 0.842 |
| NOTE RHO(DANA) = 2.72-2.69 |               | NOTE RHO(DANA) = 2.62-2.64 |               |
- ALL UNITS AS IN THE TABLE.
- 5) SEVERAL POINTS ON THE RELEASE ISENTROPE WERE ALSO MEASURED BY ALLOWING THE WAVE EMERGING FROM THE SAMPLE TO COMPRESS ANOTHER MATERIAL (BUFFER) OR ACCELERATE A THIN BRASS SHIM (BS). THE BUFFERS ARE MAGNESIUM (MG), GLYCEROL (GL), ETHANOL (ET) AND ETHYLETHER (ETE). RELEASE WAVE PRESSURE (P) AND VELOCITIES (UR) FROM SOME OF THE ABOVE HUGONIOT POINTS (PH) ARE:

|        |       |       |       |       |       |       |       |       |        |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|--------|
| PH     | 129.5 | 132.0 | 400.0 | 400.0 | 433.0 | 433.0 | 433.0 | 433.0 | KBAR   |
| P      | 114.0 | 31.0  | 101.0 | 77.5  | 332.0 | 210.0 | 111.0 | 168.0 | KBAR   |
| UR     | 1.11  | 1.18  | 3.24  | 3.77  | 2.51  | 2.59  | 2.76  | 3.20  | KM/SEC |
| BUFFER | MG    | ET    | BS    | BS    | MG    | GL    | ETC   | ET    |        |

USING THE ABOVE AND OTHER DATA THE RIEMAN INTEGRAL, ALLOWS CALCULATION OF P.V. RELEASE PATHS SHOWING A LARGE HYSTERESIS. SOME SPECIFIC VOLUMES CALCULATED AT P=0 FROM THE CORRESPONDING HUGONIOT POINTS (2ND REF.) ARE:

|    |                |       |                |                |      |
|----|----------------|-------|----------------|----------------|------|
| P  | 54.0           | 132   | 335            | 424            | KBAR |
| V0 | 0.344 TO 0.356 | 0.319 | 0.355 TO 0.542 | 0.414 TO 0.534 | CC/G |

6) THE RELATIVELY LARGE SCATTER IN THE DATA POINTS IS PROBABLY DUE TO

LACK OF UNIFORMITY IN THE SAMPLES AND RELAXATION EFFECTS.  
FURTHER WORK IN PROGRESS

TABLE 1  
 ANDESITE (ANORTHOSITE) (SILICATE ROCK)  
 99-29-24-1--94-29-24-1---3

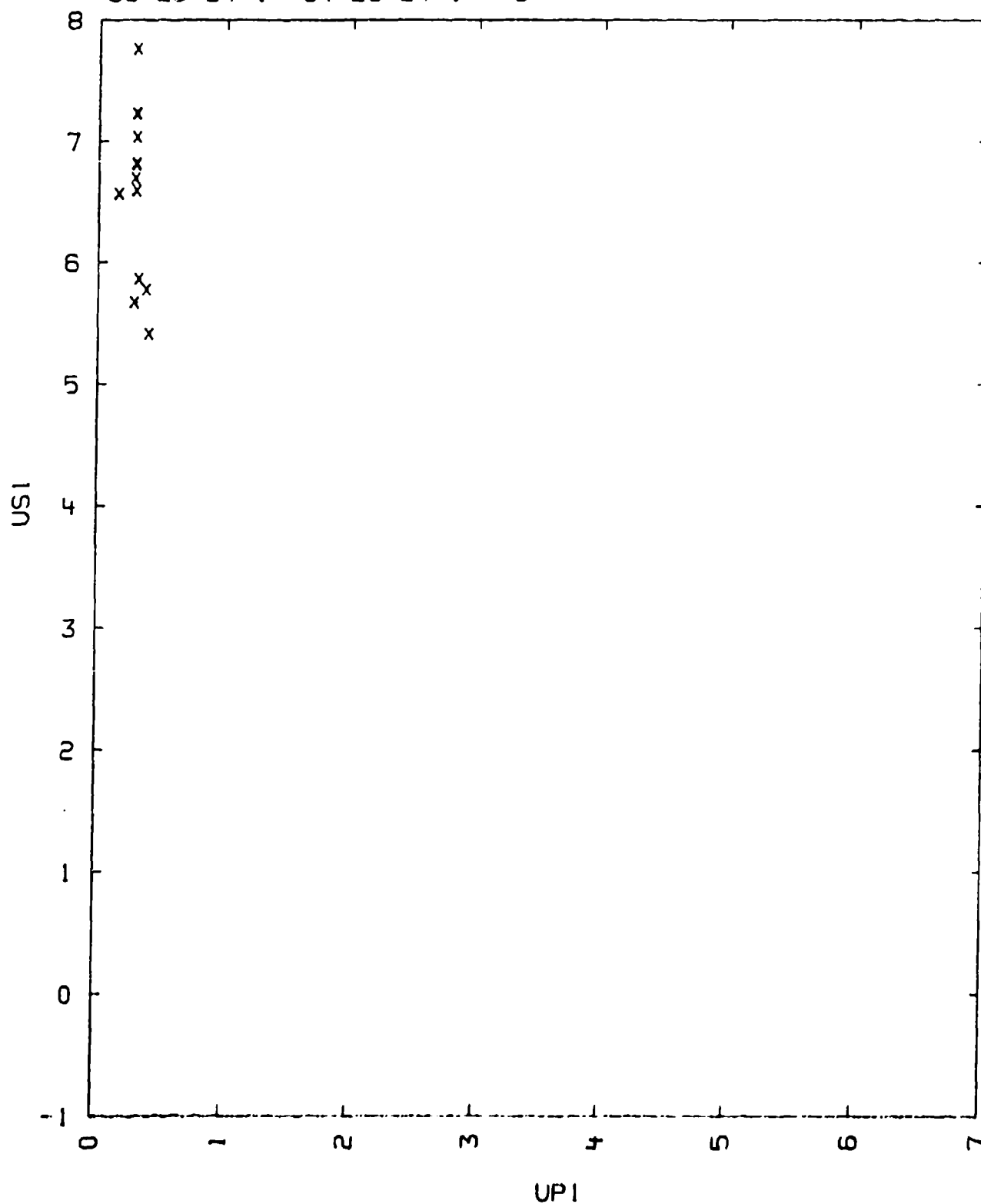


TABLE 1  
ANDESITE (ANORTHOSITE) (SILICATE ROCK)  
99-29-24-1--94-29-24-1---3

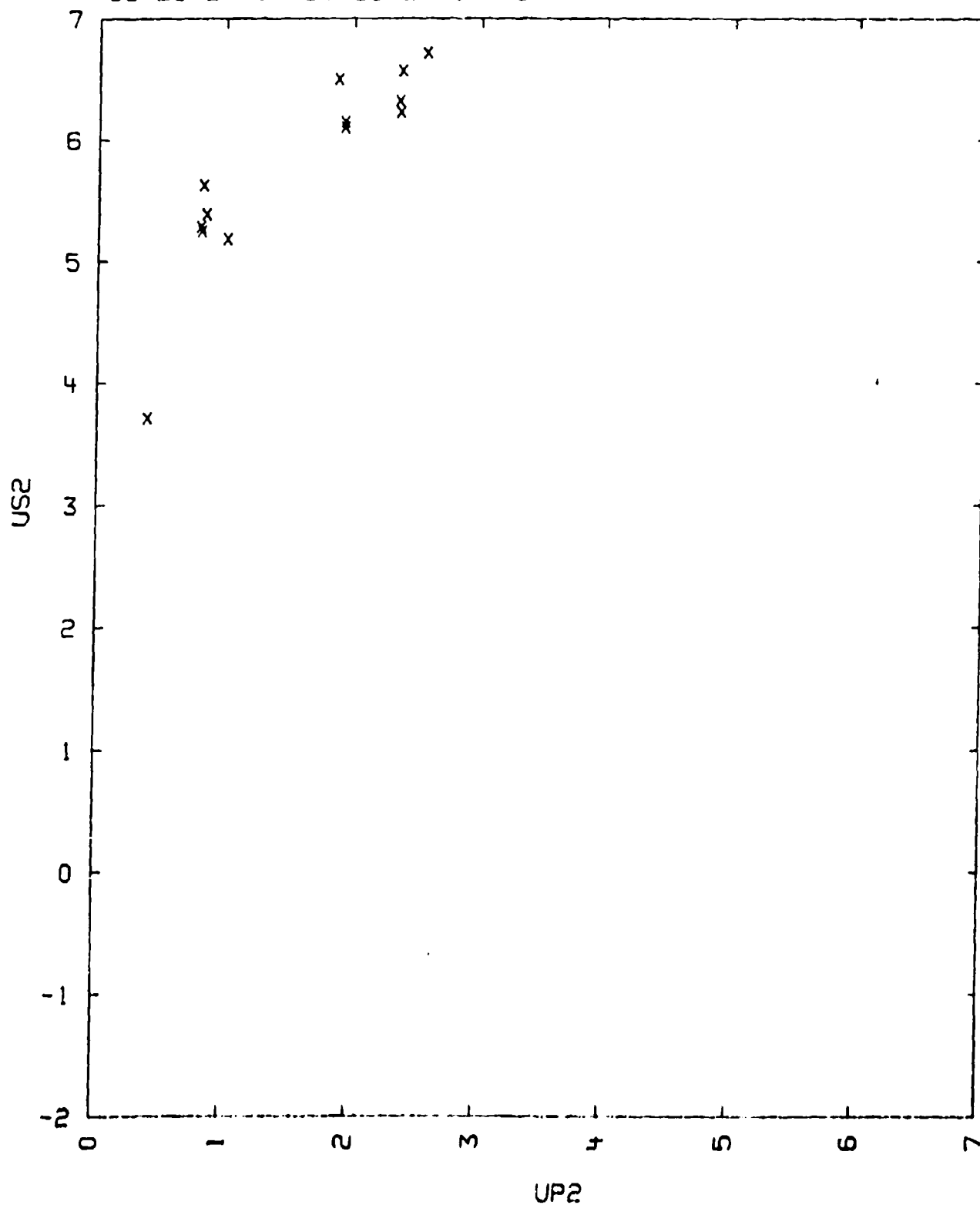
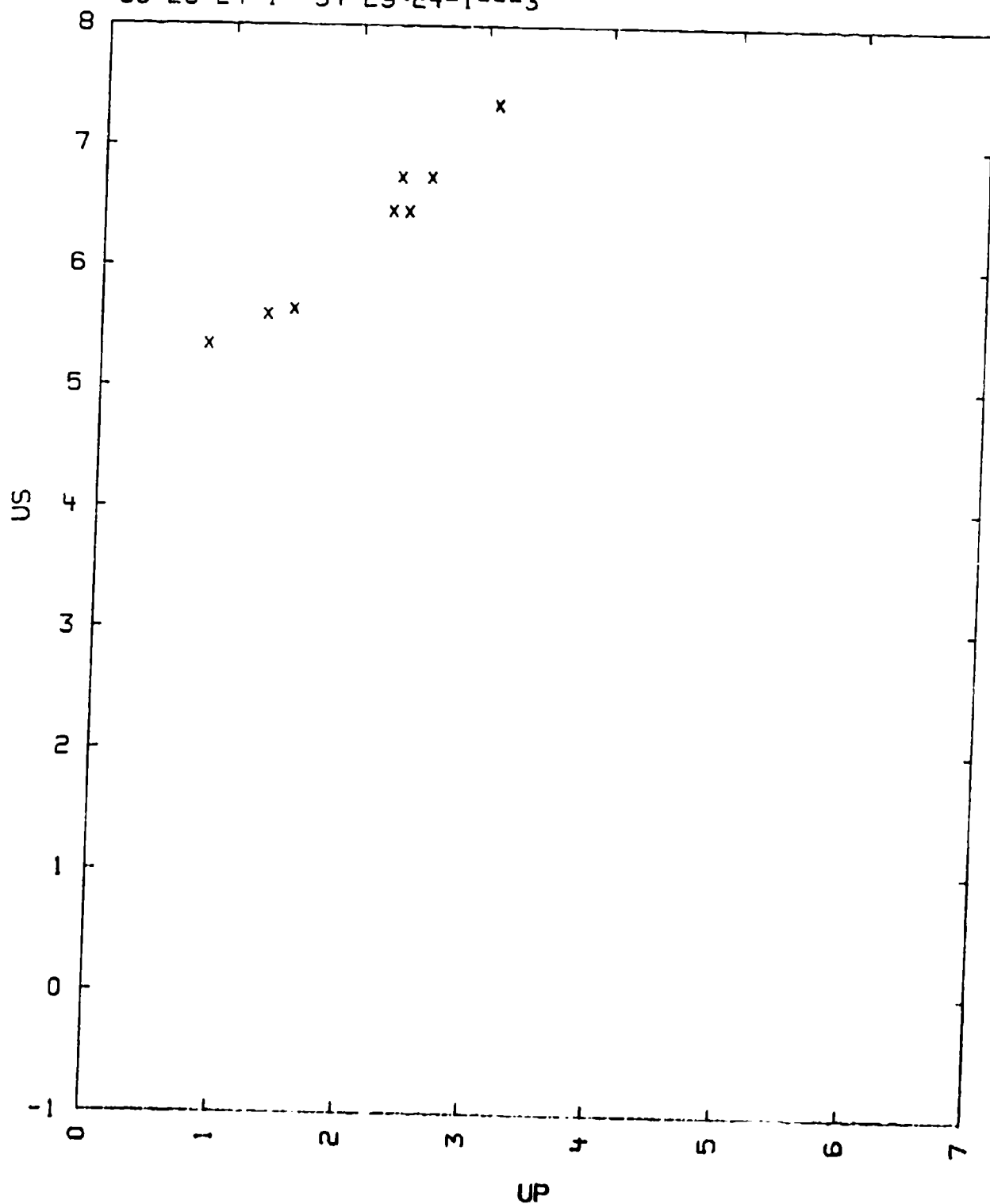


TABLE 11  
 ANDESITE (ANORTHOSITE) (SILICATE ROCK)  
 99-29-24-1--94-29-24-1---3



99-29-24-1--94-29-24-1---4  
OLIGOCLASE (PLAGIOCLASE MUSKAWA)

|                  |               |            |              |
|------------------|---------------|------------|--------------|
| ALBITE           | NA-AL-S13-08  | 75.        | MOLE PERCENT |
| ANORTITE         | CA-AL2-S12-08 | 19.        |              |
| ORTHOCLASE       | K-AL-S13-08   | 5.         |              |
| MINOR IMPURITIES |               | SEE NOTE 4 |              |

$V_0 = 0.379-0.380$  CC/G

TABLE I LISTS  $\rho_{00}$  IN G/CC, VELOCITIES IN KM/SEC AND PRESSURES IN KBARS. D IS SAMPLE THICKNESS IN MM. MAT IS THE STANDARD(DRIVER) MATERIAL: AL = DURALUMINUM, BR = 3% BRASS.

TABLE I

| - - - - - SAMPLE - - - - - |      |       |      |          |      |      |      |          |      | STANDARD |  |     |
|----------------------------|------|-------|------|----------|------|------|------|----------|------|----------|--|-----|
| $\rho_{00}$                | US1  | UP1   | P1   | $V1/V_0$ | US2  | UP2  | P2   | $V2/V_0$ | US   | D        |  | MAT |
| 2.64                       | 7.30 | 0.196 | 38.  | 0.9768   | 4.80 | 1.36 | 183. | 0.       | 2.58 | 6.472    |  | AL  |
| 2.63                       | 7.14 | 0.195 | 37.  | 0.9727   | 4.91 | 1.28 | 177. |          | 2.50 | 3.190    |  | -   |
| 2.64                       | 7.05 | 0.231 | 43.  | 0.9672   | 5.42 | 1.85 | 272. |          | 3.39 | 6.378    |  | -   |
| 2.63                       | 6.82 | 0.25  | 44.  | 0.963    | 5.42 | 1.88 | 275. |          |      | 3.228    |  | -   |
| 2.63                       | 7.24 | 0.20  | 38.  | 0.972    | 5.76 | 1.84 | 285. |          |      | 3.188    |  | -   |
| 2.63                       | 7.61 | 0.20  | 40.  | 0.974    | 5.38 | 1.88 | 275. |          | 3.68 | 3.188    |  | -   |
| 2.64                       | 7.07 | 0.30  | 56.  | 0.958    | 6.30 | 2.44 | 410. |          | 4.74 | 5.911    |  | -   |
| 2.64                       | 7.33 | 0.28  | 55.  | 0.962    | 6.37 | 2.45 | 417. |          |      | 6.416    |  | -   |
| 2.64                       | 7.24 | 0.29  | 55.  | 0.960    | 6.34 | 2.48 | 420. |          |      | 3.185    |  | -   |
| 2.63                       | 7.24 | 0.29  | 55.  | 0.960    | 6.43 | 2.47 | 422. |          |      | 3.200    |  | -   |
| 2.625                      | 7.22 | 0.29  | 55.  | 0.960    | 6.30 | 2.49 | 417. |          | 4.79 | 3.175    |  | -   |
| 2.64                       | 7.13 | 0.30  | 56.  | 0.958    | 6.74 | 2.60 | 464. |          | 5.27 | 5.911    |  | -   |
| 2.63                       | 7.76 | 3.30  | 674. | 0.575    |      |      |      |          | 6.78 | 3.181    |  | BR  |

US =

TABLE II LISTS STATES ON SEVERAL RELEASE WAVE PROFILES P U. THE LARGEST P AND SMALLEST U VALUE OF EACH SET OF 2-4 POINTS IS ON THE HUGONOT.

TABLE II

| P    | U    | P    | U    | P    | U    |
|------|------|------|------|------|------|
| 183. | 1.36 | 272. | 1.85 | 417. | 2.45 |
| 114. | 1.76 | 173. | 2.28 | 254. | 2.94 |
| 0.   | 2.58 | 112. | 2.56 | 187. | 3.42 |
| 177. | 1.28 | 0.   | 3.39 | 420. | 2.48 |
| 150. | 1.39 | 275. | 1.88 | 346. | 2.59 |
| 0.   | 2.50 | 216. | 1.84 | 422. | 2.47 |
| 182. | 1.24 | 285. | 1.84 | 345. | 2.59 |
| 87.  | 1.82 | 213. | 1.81 |      |      |
| 270. | 1.80 | 410. | 2.44 |      |      |
| 171. | 2.30 | 260. | 2.95 |      |      |
| 109. | 2.42 | 166. | 3.26 |      |      |

## COMMENTS:

- 1) SOURCE: AHRENS T.J., PETERSEN C.F. AND ROSENBERG J.T.  
J. GEOPHYS. RES., NO.74, P.2727 (1969)
- 2) EXPERIMENTAL TECHNIQUE: C1 AND D  
DATA REDUCTION METHOD : D (UP1) AND B (UP2)  
STANDARDS USED TO OBTAIN THE RELEASE WAVE  
STATES ARE MAGNESIUM, GLYCERIN, ETHANOL AND  
WATER. THE SHOCK WAS PASSED THROUGH THE DRIVER  
, THE SAMPLE AND INTO THE LIQUID WHERE AN IM-  
MERSED FOIL YIELDED VALUES FOR US AND UP LI-  
QUID. (EXP. TECH. D)
- 3) COMPARISON WITH OTHER FELDSPARS (99-29-24-1---1(2 AND3), 100-29-24-1-  
--1 AS WELL AS ANORTHOSITE (AHRENS SECTION E)) SHOWS A TRANSFORMATION  
REGION BETWEEN ABOUT 150. AND 400 KBARS.  
PHASE COMPOSITIONS AND TEMPERATURE ON THE HUGONIOT AS WELL AS ISEN.  
TROPEES AND ISOTHERMS HAVE ALSO BEEN CALCULATED BY THE AUTHORS
- 4) CHEMICAL ANALYSIS INDICATES ABOUT 1 PERCENT OF IRON SILICATE PLUS  
SOME HYDRATE: SI-O2 63.02, K2-O 0.05, TI-O2 0.01 WT-PERCENT  
AL2-O3 27.93, FE2-O3 0.22, MN-O 0.001 - -  
NA2-O 8.55, H2-O 0.13, MG-O 0.07 - -  
CA-O 3.89, - -  
IN ADDITION 0.03 WT PERCENT OF ADSORBED WATER WAS DRIVEN OFF AT 110  
DEG. C.

TABLE I

OLIGOCLASE (PLAGIOCLASE MUSKAWA)

99-29-24-1--94-29-24-1---4

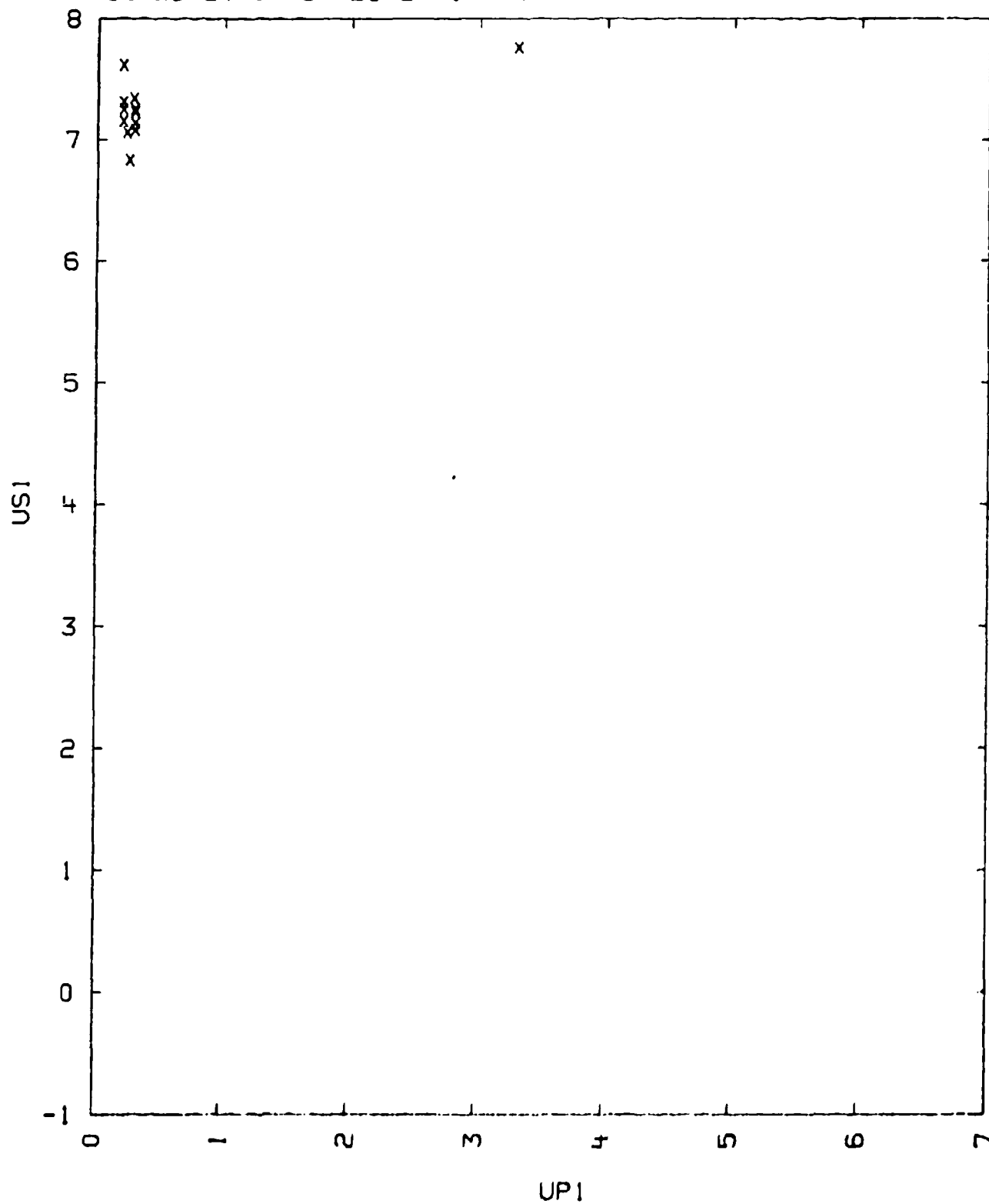
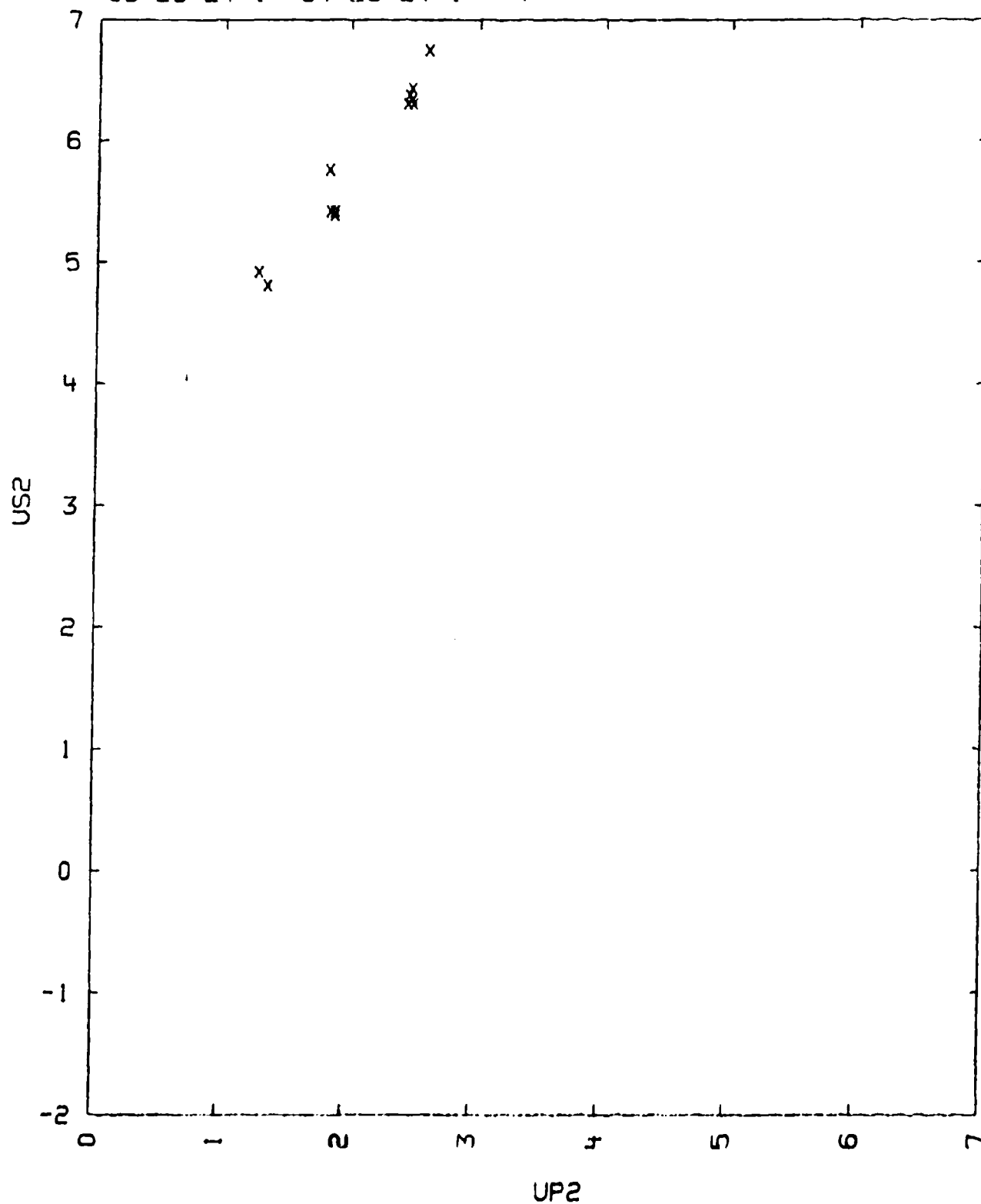




TABLE I

OLIGOCLASE (PLAGIOCLASE MUSKAWA)

99-29-24-1--94-29-24-1---4



99-29-24-1--94-29-24-1--24-1---1  
GRANITE, SHOAL

|                |             |                    |
|----------------|-------------|--------------------|
| PLAGIOCLASE    | (AN)X-(AB)Y | 41.0 PERCENT BY WT |
| QUARTZ         | SI-O2       | 26.8 PERCENT       |
| ORTHOCLASE     | K-AL-SI3-O8 |                    |
| AND MICROCLINE |             | 17.7 PERCENT       |
| BIOTITE        |             | 9.1 PERCENT        |
| MICROPERTHITE  |             | 5.4 PERCENT        |

$V_0 = 0.375 \text{ CC/G}$

THE TABLES LISTS SHOCK AND PARTICLE VELOCITIES IN KM/SEC. PRESSURE IN KBARS AND DENSITY IN G/CC.

TABLE I

| RH00 | US   | UP   | P     | V/V0      |
|------|------|------|-------|-----------|
| 2.66 | 5.95 | 0.00 | 0.010 | 0.9999894 |
| 2.66 | 6.10 | -    | 0.011 | 0.9999889 |
| 2.74 | 6.30 | -    | 0.020 | 0.9999816 |
| 2.65 | 6.30 | -    | 0.031 | 0.9999705 |
| 2.61 | 6.30 | -    | 0.057 | 0.9999449 |
| 2.66 | 5.95 | -    | 0.074 | 0.9999215 |
| 2.66 | 5.95 | -    | 0.075 | 0.9999205 |
| 2.72 | 5.30 | -    | 0.125 | 0.9998364 |
| 2.7  | 5.92 | 0.19 | 26.5  | 0.978     |
| 3.0  | 5.74 | 0.11 | 18.0  | 0.982     |
| 2.4  | 6.30 | 0.23 | 38.0  | 0.960     |

US =

TABLE II

| RH00 | US1  | UP1  | P1   | V1/V0 | US2   | UP2   | P2    | V2/V0 |
|------|------|------|------|-------|-------|-------|-------|-------|
| 2.82 | 5.80 | 0.25 | 38.0 | 0.960 | 4.75  | 0.26  | 41.5  | 0.954 |
| 2.65 | 5.98 | 0.24 | 38.0 | 0.960 | 3.566 | 0.870 | 94.7  | 0.779 |
| -    | -    | -    | -    | -     | 3.932 | 0.898 | 103.8 | 0.790 |
| -    | -    | -    | -    | -     | 3.993 | 0.985 | 113.9 | 0.770 |
| -    | -    | -    | -    | -     | 4.054 | 0.916 | 107.8 | 0.791 |
| -    | -    | -    | -    | -     | 4.481 | 1.171 | 145.6 | 0.750 |
| -    | -    | -    | -    | -     | 4.572 | 1.128 | 142.8 | 0.764 |
| -    | -    | -    | -    | -     | 4.663 | 1.195 | 152.4 | 0.752 |
| -    | -    | -    | -    | -     | 4.663 | 1.291 | 164.9 | 0.732 |
| -    | -    | -    | -    | -     | 4.968 | 1.500 | 200.9 | 0.705 |
| -    | -    | -    | -    | -     | 5.029 | 1.471 | 193.9 | 0.722 |
| -    | -    | -    | -    | -     | 5.182 | 1.481 | 205.6 | 0.719 |
| -    | -    | -    | -    | -     | 5.334 | 1.471 | 209.5 | 0.728 |
| -    | -    | -    | -    | -     | 5.425 | 1.965 | 283.3 | 0.641 |
| -    | -    | -    | -    | -     | 5.791 | 2.047 | 313.2 | 0.648 |
| -    | -    | -    | -    | -     | 5.882 | 1.672 | 257.0 | 0.714 |
| -    | -    | -    | -    | -     | 6.035 | 1.296 | 205.1 | 0.785 |
| -    | -    | -    | -    | -     | 6.126 | 2.380 | 384.1 | 0.611 |

GRANITE, SHOAL

RH00 US1 UP1 P1 V1/V0 US2 UP2 P2 V2/V0

US =

## COMMENTS:

- 1) SOURCE: DENNEN, R.S.  
J.APPL.PHYS., VOL.40 P.3326 (1969)  
J.APPL.PHYS., VOL.41 P.5309 (1970)
- 2) EXPERIMENTAL TECHNIQUE: A FOR PRESSURES BELOW 42 KBAR  
FOR PRESSURES ABOVE 50 KBAR A SHADOWGRAPH  
OF THE FREE SURFACE OF A WEDGE SHAPED SAMPLE WAS USED.  
DATA REDUCTION TECHNIQUE: A FOR PRESSURES BELOW 42 KBAR  
D FOR PRESSURES ABOVE 50 KBAR  
C FOR PRESSURES BELOW 0.13 KBAR
- 3) THE POINTS BELOW 0.13 KBAR WERE OBTAINED WITH A SHOCK TUBE AND A GAS  
STANDARD
- 4) POISSON'S RATIO FOR GRANITE WAS USED TO CALCULATE UP FROM THE FREE  
SURFACE MOTIONS OF THE WEDGE. THE VALUE USED WAS FROM F.BIRCH,  
J.GEOL. VOL.48,P.752 (1940)
- 5) PETROGRAPHIC COMPOSITION OF SHOAL GRANITE WAS REFERENCED AS A PRIVATE  
COMMUNICATION FROM R.S.YOUNG.
- 6) NO DATA ON GRAIN SIZE REPORTED
- 7) RH00 WAS NOT LISTED BY AUTHOR BUT RECALCULATED FROM HIS DATA

TABLE I

GRANITE, SHOAL

99-29-24-1--94-29-24-1--24-1--

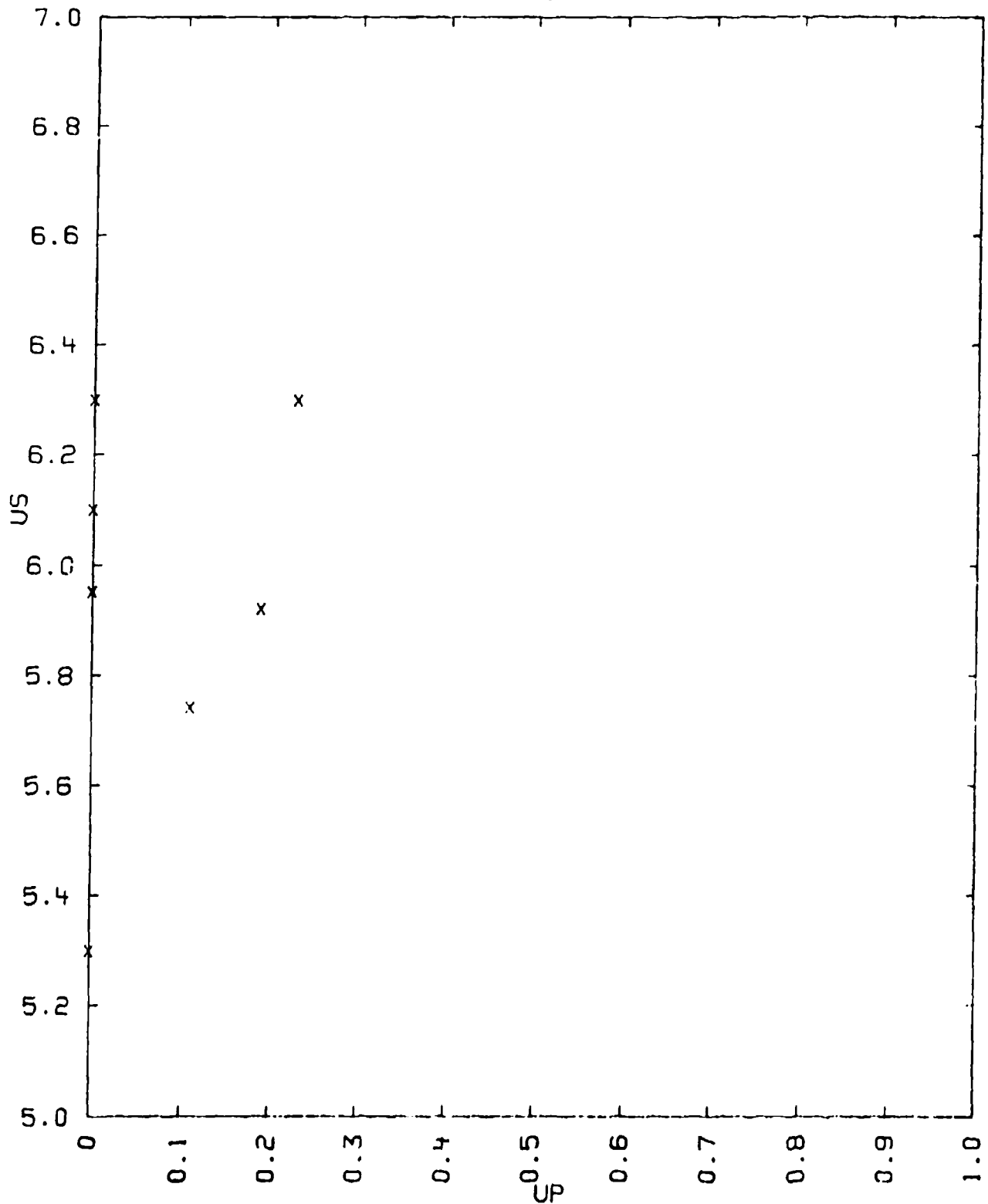


TABLE II

GRANITE, SHOAL

99-29-24-1--94-29-24-1--24-1--

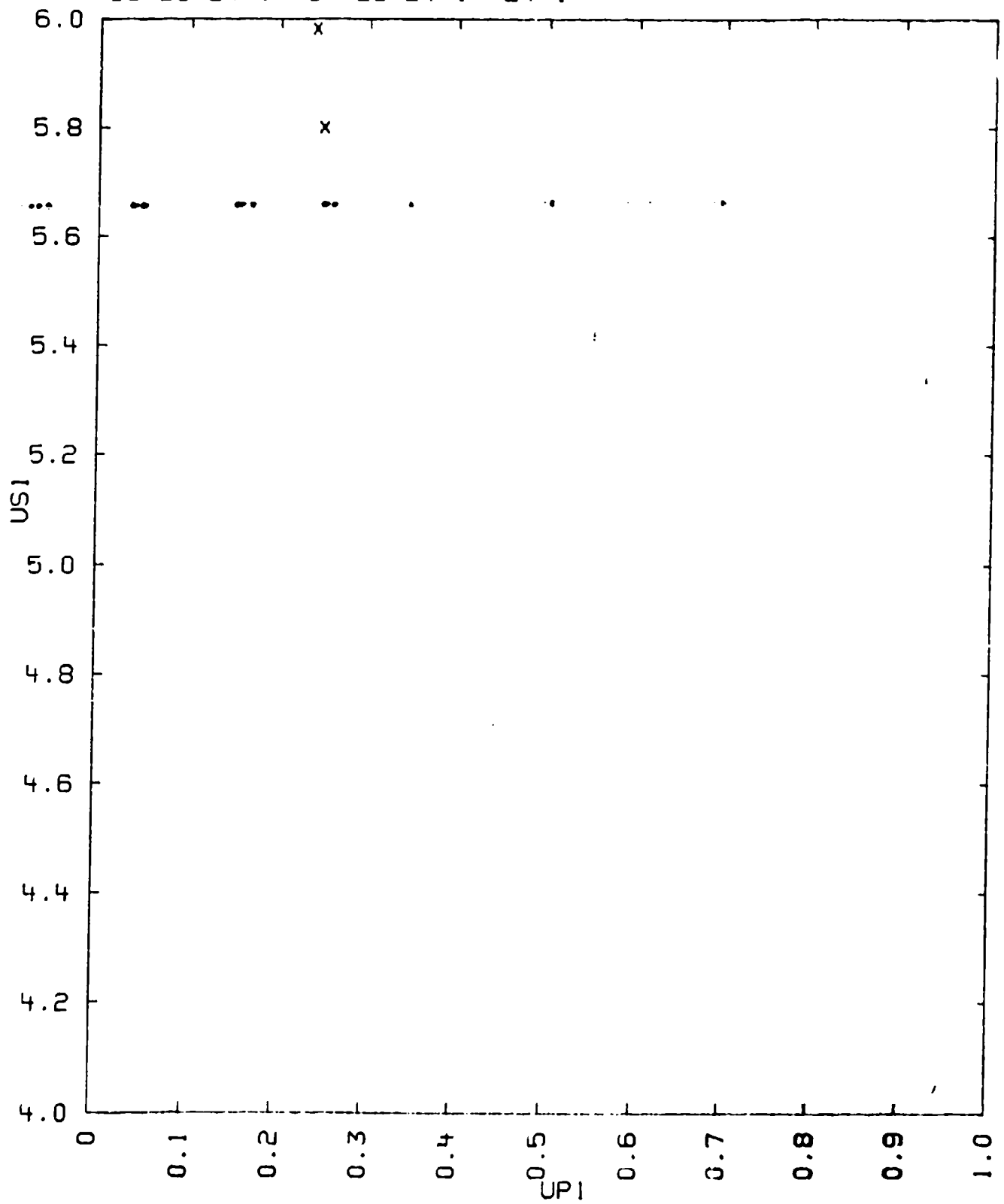
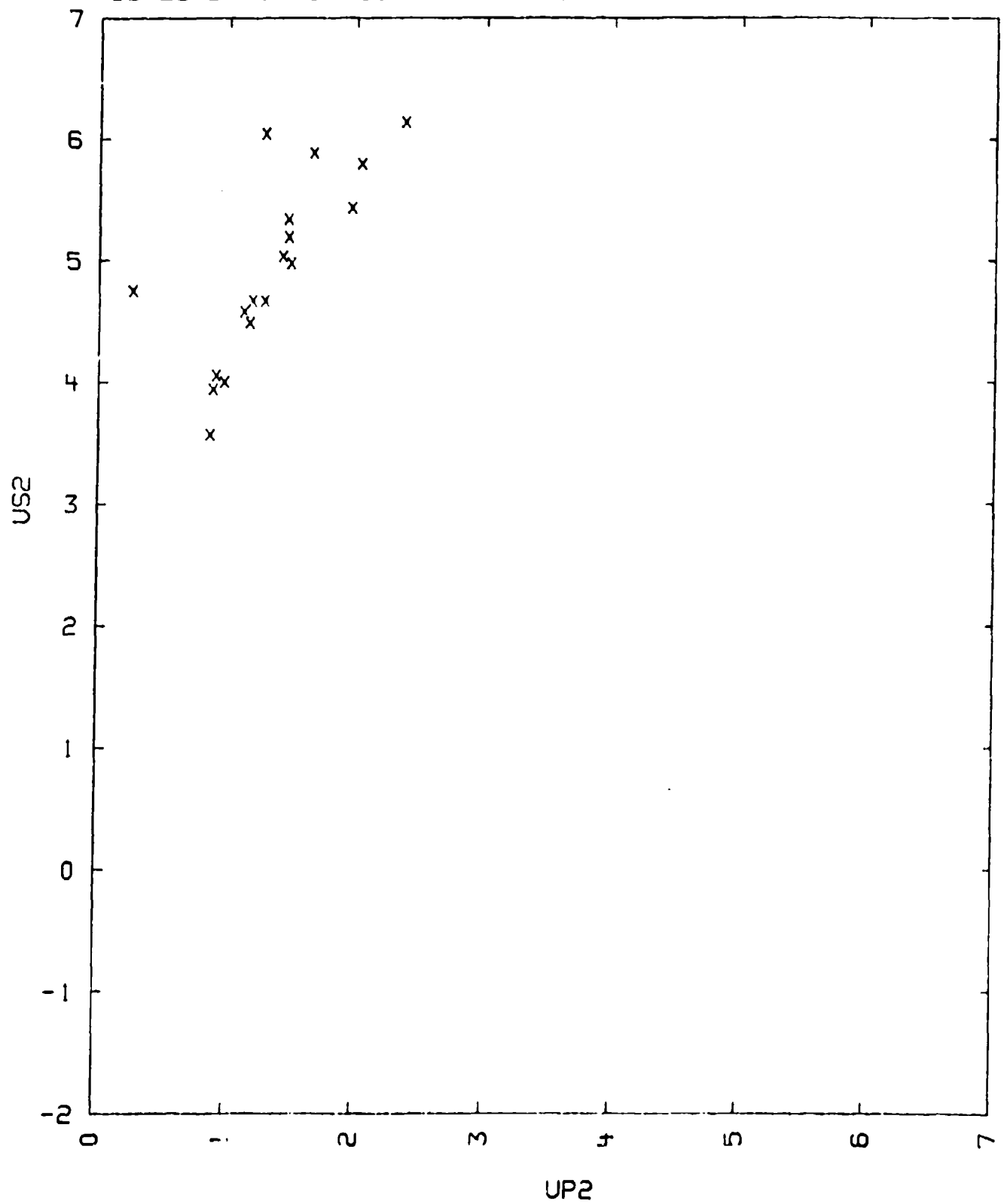


TABLE II

GRANITE, SHOAL

99-29-24-1--94-29-24-1--24-1--



99-29-24-1--94-29-24-1--24-1--100-29-24-1---1  
GRANITE

|             |                               |      |               |
|-------------|-------------------------------|------|---------------|
| PLAGIOCLASE | (AB)X-(AN)Y                   | 46.7 | VOL. PERCENT. |
| QUARTZ      | SI-O2                         | 21.1 | -             |
| ORTHOCLASE  | K-AL-SI3-O8                   | 20.3 | -             |
| BIOTITE     | K(MG,FE)3-(AL-SI3-O10)-(O-H)2 | 4.9  | -             |
| CHLORITE    | MG3(SI4-O10)-(O-H)2-MG3(O-H)6 | 6.5  | -             |
| OPAQUES     | FE, O AND S                   | 0.5  | -             |
| POROSITY    |                               | 0.9  | -             |

V0 = 0.373 CC/G

V01 =

THE TABLE LISTS VELOCITIES IN KM/SEC, PRESSURE IN KBAR, AND DENSITY IN G/CC.

TABLE

| SAMPLE |       |      |       |       | STANDARD |
|--------|-------|------|-------|-------|----------|
| RHO0   | US    | UP   | P     | V/V0  | MAT.     |
| 2.68   | 11.93 | 6.01 | 1921. | 0.496 | FANSTEEL |
| -      | 10.67 | 5.21 | 1480. | 0.510 | -        |
| -      | 10.22 | 4.90 | 1340. | 0.521 | -        |
| -      | 10.11 | 4.86 | 1327. | 0.519 | -        |
| -      | 9.00  | 4.05 | 986.  | 0.550 | CU       |
| -      | 8.66  | 4.01 | 930.  | 0.537 | -        |
| -      | 7.27  | 3.17 | 627.  | 0.564 | -        |

US = 2.22 + 1.625\*UP KM/SEC.

SIG.US = 0.11 KM/SEC.

#### COMMENTS:

1) SOURCE: ISBELL, W.M.

PAPER PRESENTED AT DASA SPONSORED MEETING  
AT THE RAND CORPORATION, SANTA MONICA, CALIFORNIA,  
OCTOBER 26-28 (1965)

CONTRACT DA-49-146-XZ-429

GENERAL MOTORS TECHNICAL CENTER, WARREN, MICH., U. S. A.

2) EXPERIMENTAL TECHNIQUE: A. FOR SHOCK VELOCITY MEASUREMENTS. TWO TIMED  
X-RAY FLASHES DETERMINE VELOCITY OF THE PRO-  
JECTILE.

DATA REDUCTION METHOD: A. STANDARD PROJECTILES: FANSTEEL-77 AND  
OXYGEN FREE HIGH CONDUCTIVITY COPPER

3) THE MODAL ANALYSIS OF ROCK SAMPLES FROM THE SAME LOCATION GIVEN ABOVE  
WAS MADE BY:

H. BARNES TECHNICAL LETTER: NTS-185, JUNE 21 (1967), ALSO  
PRIVATE COMMUNICATION 1968

U. S. DEP. OF THE INTERIOR, GEOLOGICAL SURVEY  
FEDERAL CENTER, DENVER, COLORADO 80225, U. S. A.

4) THIS SAME REPORT LISTS FOR A DUPLICATE ROCK WITH SIMILAR COMPOSITION  
BULK MODULUS (ISOTHERMAL) 0.355 MBAR

SHEAR -  
POISSONS RATIO

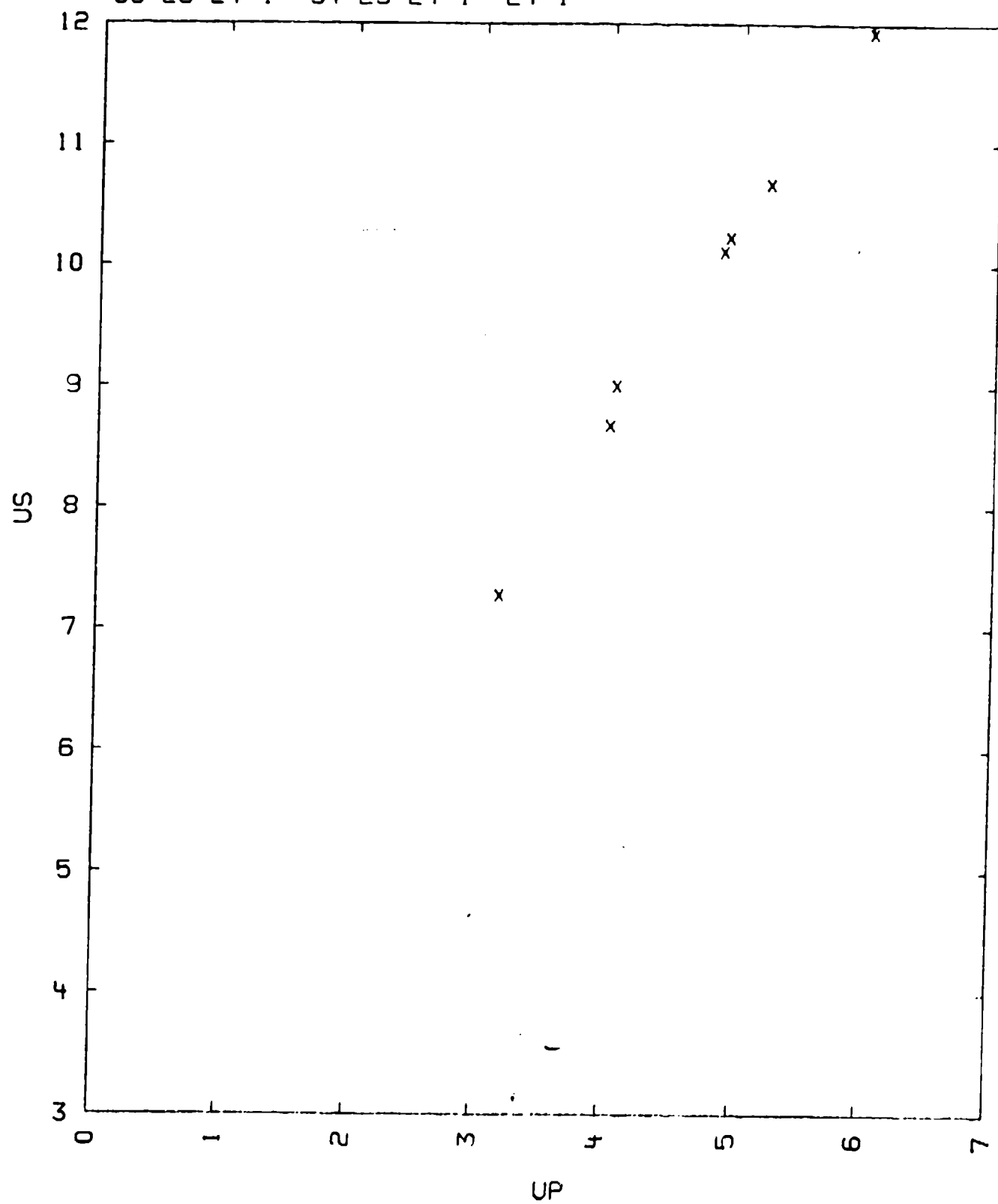
0.244 MBAR  
0.22



TABLE 1

GRANITE

99-29-24-1--94-29-24-1--24-1--



99-29-24-1--94-29-24-1--93-41-24-1---1  
 BASALT

|                       |                |                     |
|-----------------------|----------------|---------------------|
| PLAGIOCLASE           | (AN)X-(ABIY    | 70.0 PERCENT BY WT. |
| OLIVINE               | (MG-FE)2-SI-O4 | 24.5 PERCENT        |
| MAGNETITE AND OPAQUES | FE3-O4 +       | 5.5 PERCENT         |
| POROSITY (MEASURED)   |                | 4.9 PERCENT         |
| PARTICLE SIZE         |                | UP TO 0.5 MM        |

V0 = 0.374 CC/G      CL = 5.36 KM/SEC  
 CS = 3.10 KM/SEC

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC.  
 AND PRESSURE IN KILOBARS.

TABLE

| RH00  | US   | UFS  | UP   | P   | V/V0  |
|-------|------|------|------|-----|-------|
| 2.667 | 7.79 | 6.10 | 3.29 | 684 | 0.578 |
| 2.673 | 4.87 | 1.59 | 0.79 | 103 | 0.837 |
| 2.668 | 5.24 | 3.02 | 1.67 | 233 | 0.681 |
| 2.654 | 8.59 | 6.71 | 3.50 | 797 | 0.593 |
| 2.682 | 5.25 | 2.71 | 1.53 | 215 | 0.709 |
| 2.693 | 5.70 | 3.83 | 2.10 | 322 | 0.633 |
| 2.688 | 6.93 | 5.54 | 2.86 | 533 | 0.588 |

US =

## COMMENTS:

- 1) SOURCE: COMPILER  
 L. R. L. EQUATION OF STATE FILE  
 S DIVISION REPORT STN 71, AUG 1964  
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION TECHNIQUE B  
 (STANDARD MATERIAL 2024 ALUMINUM)
- 3) THE TABLE LISTS RESULTS FOR TWO TYPES OF BASALT FROM NATIONAL TEST SITE, NEVADA.  
 THE FIRST FOUR POINTS CORRESPOND TO SAMPLES FROM BUCKBOARD HOLE NO. 3 AT 36 FOOT DEPTH.  
 THE OTHER THREE POINTS CORRESPOND TO SAMPLES FROM AREA 18 IN THE VICINITY OF BUCKBOARD DRILL CORE.
- 4) A MORE EXTENSIVE DISCUSSION OF THIS MATERIAL MAY BE FOUND IN REPORT UOPK B 64-2 JAN 1964 BY L. ROGERS, LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 5) BOTH TYPES OF BASALT HAVE THE SAME PARTICLE VS. SHOCK VELOCITY DEPENDENCE WITHIN EXPERIMENTAL ERROR.
- 6) CHEMICAL ANALYSIS  
 SILICA                      51.88 PERCENT BY WEIGHT  
 FERRIC OXIDE              9.57 PERCENT  
 ALUMINUM OXIDE            17.56 PERCENT

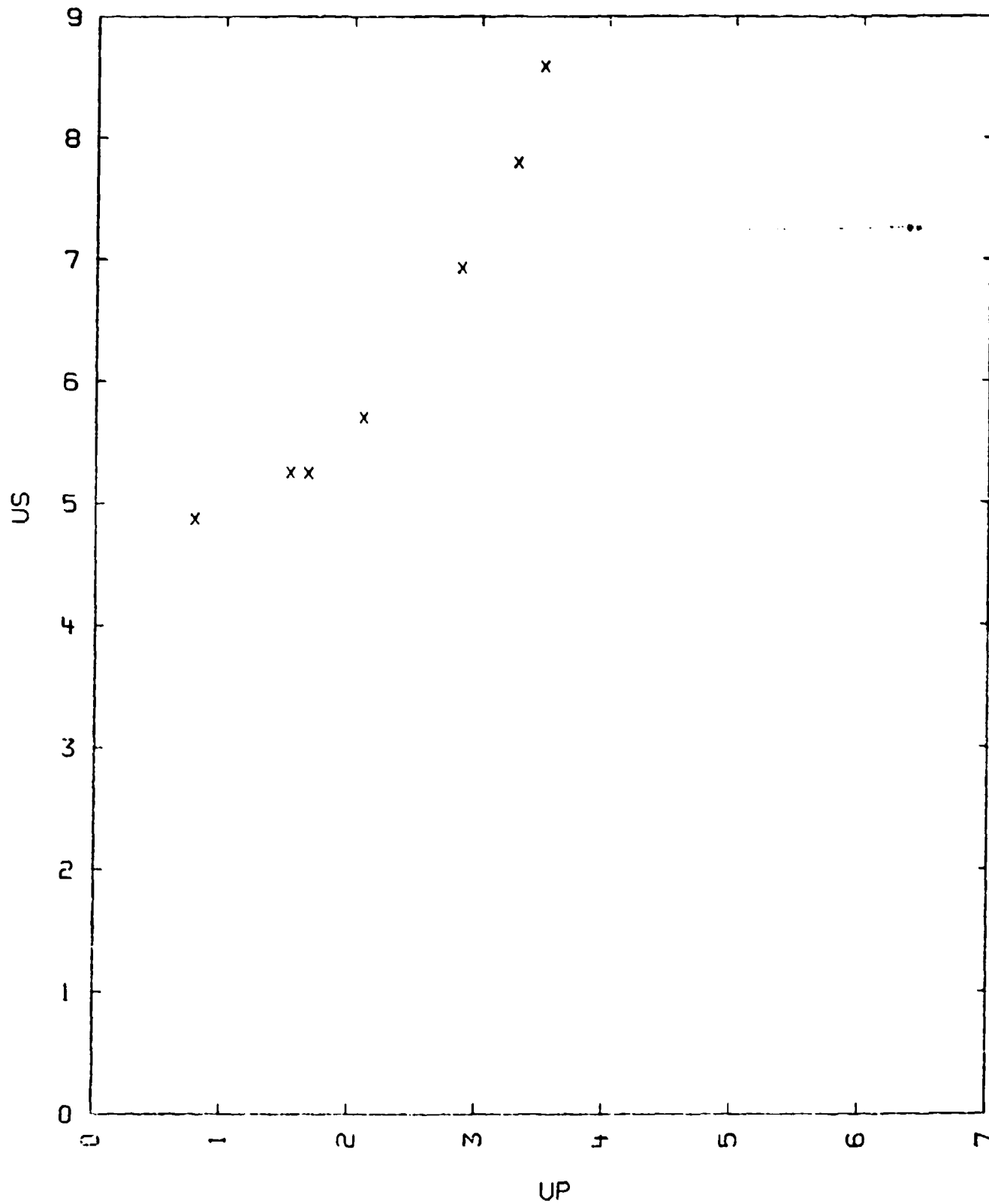
|                  |              |
|------------------|--------------|
| CALCIUM OXIDE    | 6.74 PERCENT |
| MAGNESIUM OXIDE  | 5.54 PERCENT |
| SODIUM OXIDE     | 4.26 PERCENT |
| POTASSIUM OXIDE  | 2.34 PERCENT |
| TITANIUM DIOXIDE | 1.32 PERCENT |
| BARIUM OXIDE     | 0.42 PERCENT |
| WATER            | 0.18 PERCENT |

- 7) THE CHEMICAL ANALYSIS INDICATES THAT THE PLAGIOCLASE CAN BE IDENTIFIED AS ANDESINE.
- 8) MINERALOGICAL AND CHEMICAL ANALYSIS COMPARE QUITE FAVORABLY TO EACH OTHER PROVIDING THAT THE OPAQUES CONSIST OF MINERALS THAT ARE PARTIALLY COMPOSED OF POTASSIUM, TITANIUM, BARIUM, AND HYDROGEN, SINCE THESE ELEMENTS ARE NOT PART OF PLAGIOCLASE, CLIVINE, OR MAGNETITE, WHICH ACCOUNT FOR 74.5 PERCENT OF MINERALOGICAL ANALYSIS.

TABLE I

BASALT

99-29-24-1--94-29-24-1--93-41-



99-29-24-1--94-29-24-1--99-94-93-41-29-24-1---1  
 BASALT, VACAVILLE (SILICATE ROCK)

|                    |                              |       |                   |
|--------------------|------------------------------|-------|-------------------|
| ANDESINE:          |                              |       | 53 VOLUME PERCENT |
| ANORTHITE          | CA-AL2-SI2-O8                | 24-28 | -                 |
| ALBITE             | NA-AL-SI3-O8                 | 29-25 | -                 |
| AUGITE             | (CA,NA)(MG-FE-AL)(SI,AL)2-O6 | 31    | -                 |
| MAGNETITE-ILMENITE | FE2-O3 - FE-TI-O3            | 9     | -                 |
| CELADONITE         | K(MG-FE)(AL-FE)-SI4-O10(OH)2 | 5     | -                 |
| APATITE            | Ca5(F,CL,O-H)(P-O4)3         | 2     | -                 |
| GRAIN SIZE:        |                              |       | 0.01-0.2 MM.      |

V0 = 0.355 CC/G  
 V01 = 0.329-0.315 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURES IN KBARS.

TABLE

| - - - - - SAMPLE - - - - - |      |       |    |       |      |       |     |       |        | STANDARD |
|----------------------------|------|-------|----|-------|------|-------|-----|-------|--------|----------|
| RH00                       | US1  | UP1   | P1 | V0/V0 | US2  | UP2   | P2  | V2/V0 | UFS    |          |
| 2.82                       |      |       |    |       | 5.31 | 0.964 | 145 | 0.820 | 1.958  |          |
| -                          | 5.43 | 0.328 | 50 | 0.940 | 5.19 | 0.906 | 134 | 0.828 | -      |          |
| -                          |      |       |    |       | 5.06 | 0.798 | 116 | 0.845 | (1.64) |          |
| -                          | 5.33 | 0.291 | 44 | 0.945 | 5.12 | 0.764 | 112 | 0.854 | -      |          |
| -                          |      |       |    |       | 5.44 | 1.232 | 189 | 0.775 | (2.61) |          |
| -                          | 5.55 | 0.323 | 50 | 0.942 | 5.40 | 1.124 | 172 | 0.793 | -      |          |

US =

## COMMENTS:

- 1) SOURCE: AHRENS, T. J. AND GREGSON JR, V. G.  
 J. GEOPHYS. RES., VOL. 69, P. 4839 (1964)
- 2) EXPERIMENTAL METHOD C2  
 DATA REDUCTION TECHNIQUE B AND D WITH 2UP=UFS FOR THE FIRST WAVE
- 3) V01 WAS OBTAINED FROM THE DENSITY RANGES GIVEN BY HURLBUT, C. S.,  
 DANAS MANUAL OF MINERALOGY (JOHN WILEY, N.Y. 1963) 17TH ED.
- 4) SOME TABULATED LINES SHOW NO FIRST WAVE. HERE THE FIRST WAVE OF THE  
 FOLLOWING LINE WAS USED IN THE CALCULATION OF P2 AND V2/V0, SINCE  
 THAT LINE WAS OBTAINED IN THE SAME EXPERIMENT.

TABLE 1

BASALT, VACAVILLE (SILICATE ROCK)

99-29-24-1--94-29-24-1--99-94-

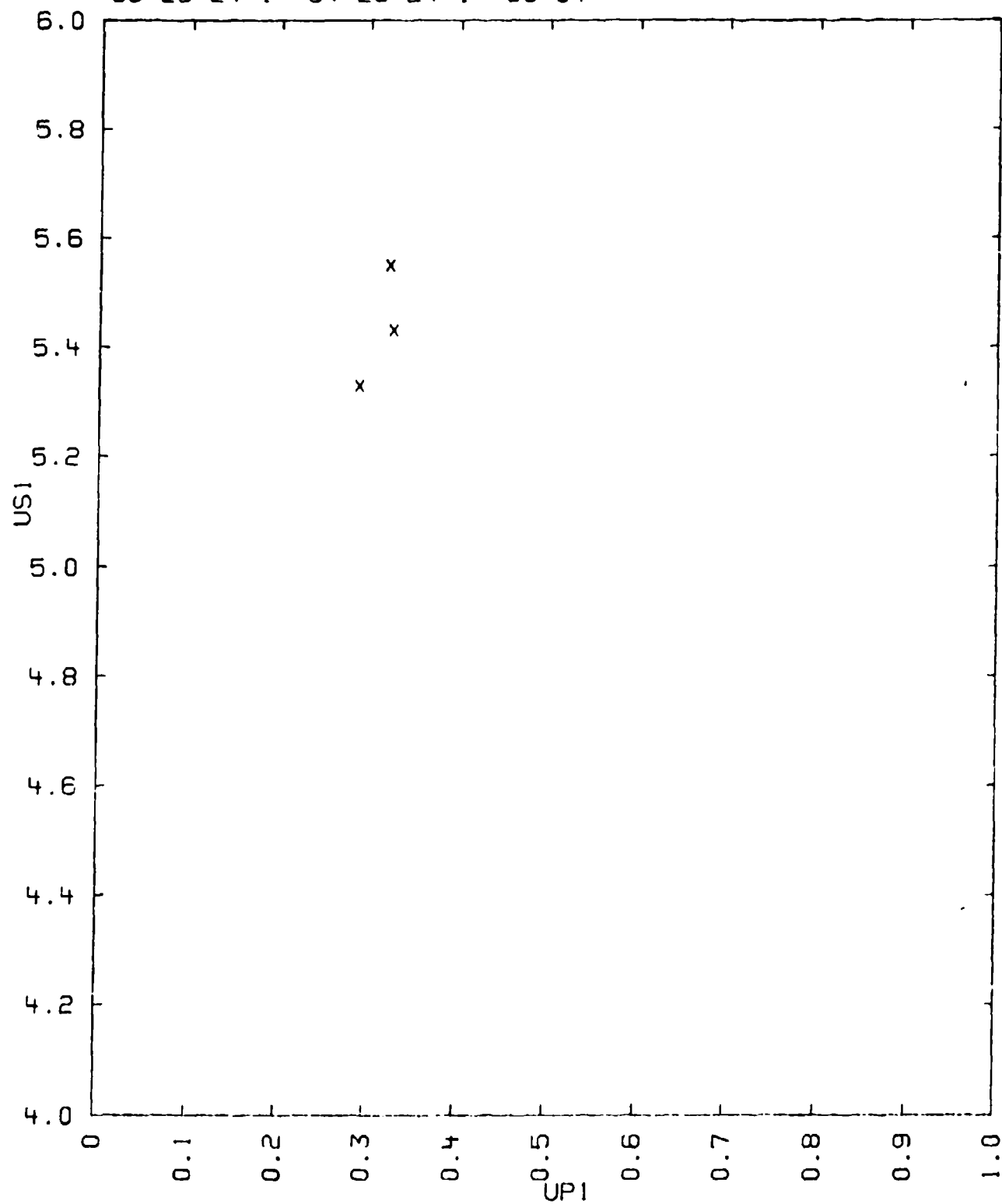
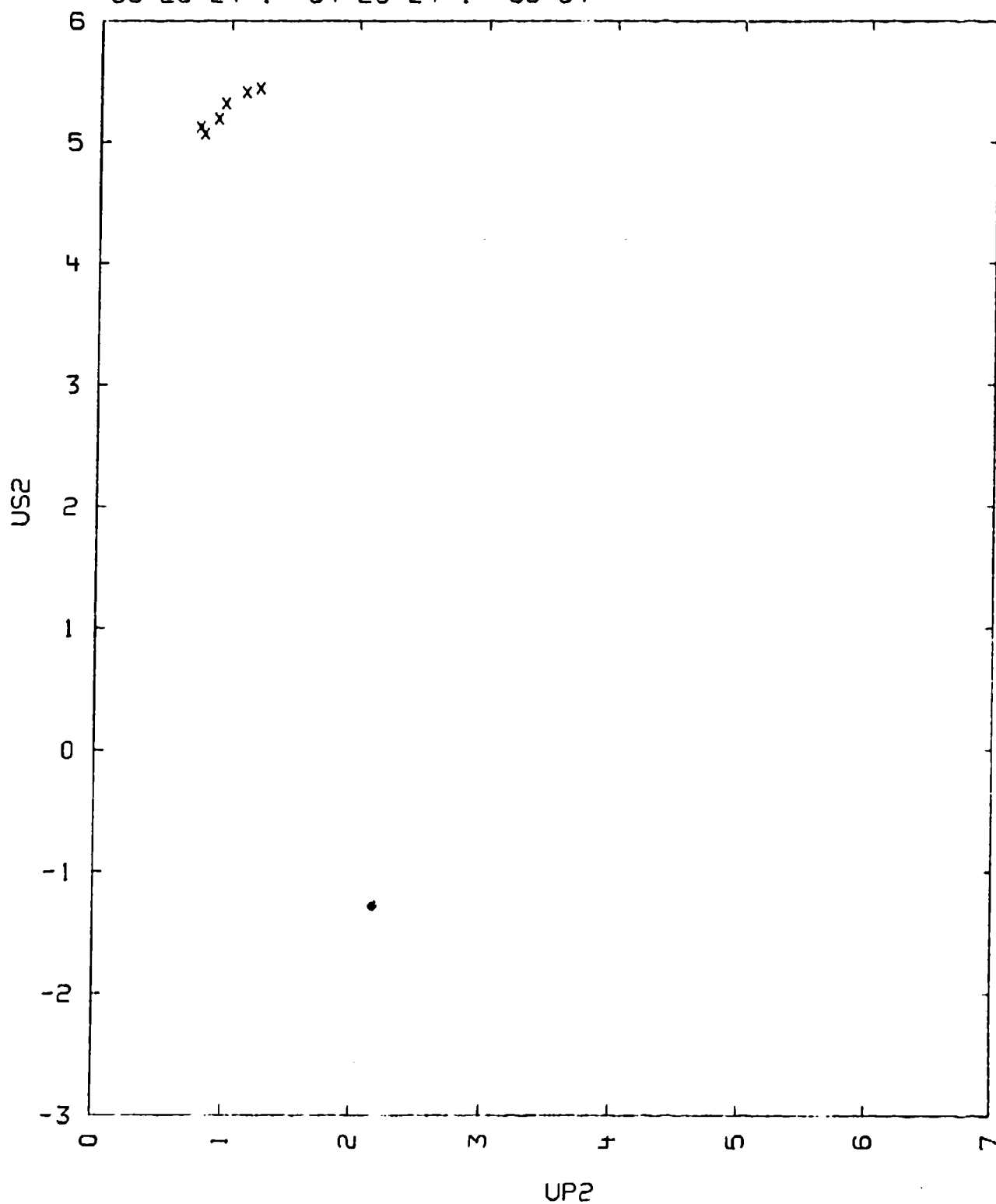


TABLE 1

BASALT, VACAVILLE (SILICATE ROCK)

99-29-24-1--94-29-24-1--99-94-



99-29-24-1--94-29-24-1--99-94-93-41-29-24-1--2  
 BASALT, VACAVILLE

|                                          |             |                |
|------------------------------------------|-------------|----------------|
| PLAGIOCLASE FELDSPAR:                    | 53          | VOLUME PERCENT |
| ANORTHITE CA-AL2-SI2-O8                  | -           | -              |
| ALBITE NA-AL-SI3-O8                      | -           | -              |
| AUGITE (CA,NA)(MG,FE-FE,AL)(SI,AL)2-O6   | 31          | -              |
| MAGNETITE: FE2-O3 AND ILMENITE: FE-TI-O3 | 9           | -              |
| CELADONITE K(MG-FE)(AL-FE)-SI4-O10(OH)2  | 5           | -              |
| APATITE CA5-O-H-(P-O4)3                  | 2           | -              |
| GRAIN SIZE                               | 0.3 - 0.003 | MM             |
| POROSITY                                 | 2.0         | PERCENT        |

VO = 0.346 CC/G  
 VOI = 0.329 - 0.315 CC/G.

CO = 2.306 KM/SEC.

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES ARE IN KM/SEC.  
 AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US    | UP    | P     | V/VO  |
|------|-------|-------|-------|-------|
| 2.86 | 5.88  | 2.10  | 353.  | 0.643 |
| -    | 6.77  | 2.76  | 534.  | 0.592 |
| -    | 7.59  | 3.24  | 703.  | 0.573 |
| -    | 8.31  | 3.94* | 936.  | 0.526 |
| -    | 9.19  | 4.25  | 1117. | 0.538 |
| -    | 9.01  | 4.33* | 1116. | 0.520 |
| -    | 9.91  | 4.64  | 1315. | 0.532 |
| -    | 10.60 | 5.01  | 1519. | 0.529 |
| -    | 10.63 | 5.20  | 1581. | 0.511 |
| -    | 12.04 | 5.94  | 2046. | 0.507 |

US = 2.31 + 1.615\*UP KM/SEC. SIGMA US = 0.20 KM/SEC.

COMMENTS:

- 1) SOURCE: JONES, A. H., ISBELL, W. M., SHIPMAN, F. H., PERKINS, R. D.,  
 GREEN, S. J. AND MAIDEN, C. J.  
 INTERIM REPORT, CONTRACT NAS2-3427, 1968  
 GENERAL MOTORS TECH. CENTER, WARREN, MICHIGAN 48090
- 2) EXPERIMENTAL TECHNIQUE A:  
 DATA REDUCTION TECHNIQUE A  
 STANDARD MATERIALS: OFHC COPPER AND FANSTEEL-77 ALLOY. THE  
 COPPER STANDARD US-UP HUGONIOT RELATIONSHIP IS  
 GIVEN BY:  
 $US = 3.96 + 1.497 \cdot UP$  KM/SEC. RH00 = 8.93 G/CC  
 THE FANSTEEL US-UP HUGONIOT IS GIVEN BY:  
 $US = 3.96 + 1.295 \cdot UP$  KM/SEC. RH00 = 17.01 G/CC
- 3) THESE PRESSURES WERE ACHIEVED BY USING A TWO-STAGE LIGHT GAS GUN  
 THE PROJECTILE IMPACT VELOCITY AND TILT WERE MEASURED BY TWO TIMED  
 FLASH X-RAY SHADOWGRAPHS OF THE PROJECTILE.
- 4) THE CHEMICAL COMPOSITION IN WEIGHT PERCENT IS:



|                      |                    |                     |
|----------------------|--------------------|---------------------|
| SI-O2 = 50.3 PERCENT | CA-O = 7.7 PERCENT | TI-O2 = 2.4 PERCENT |
| AL2-O3 = 13.8 -      | NA2-O = 3.3 -      | P2-O5 = 1.2 -       |
| FE2-O3 = 3.5 -       | K2-O = 1.6 -       | MN-O = 0.24 -       |
| FE-O = 9.1 -         | H2O- = 1.0 -       | CO2 = 0.05 -        |
| MG-O = 4.4 -         | H2O+ = 1.5 -       |                     |

5) OTHER STRENGTH PARAMETERS MEASURED BY THE AUTHORS ARE LISTED BELOW:

|                        | AVERAGE | RANGE     | UNITS               |
|------------------------|---------|-----------|---------------------|
| COMPRESSIVE STRENGTH   | 2.56    | 1.56-3.69 | 10**9 DYNES/(CM**2) |
| SHEAR STRENGTH (CALC.) | 8.6     |           | 10**8               |
| TENSILE STRENGTH       | 1.42    | 0.90-2.32 | 10**8               |

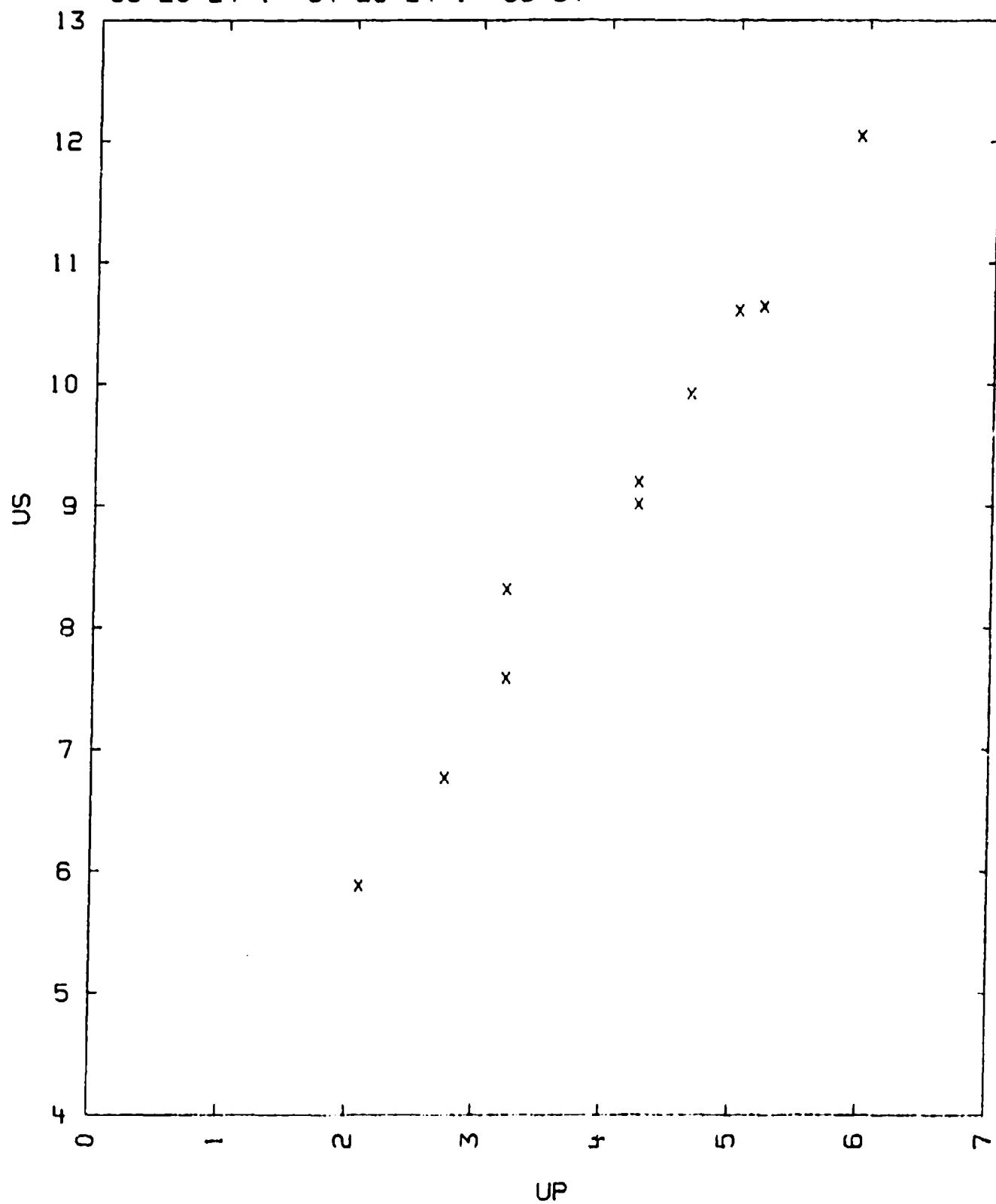
6) THE ESTIMATED EXPERIMENTAL ERROR IN MEASURING US IS 1 - 4 PERCENT  
THE UNCERTAINTY IN THE PARTICLE VELOCITIES IS 0.2 PERCENT EXCEPT  
FOR THE TWO VALUES INDICATED WITH A \*, WHICH HAVE AN UNCERTAINTY  
OF 3 PERCENT.

7) VDI WAS ASSUMED TO BE EQUAL TO VACAVILLE BASALT ENTRY ---1

TABLE 1

BASALT, VACAVILLE

99-29-24-1--94-29-24-1--99-94-



99-29-24-1--100-29-24-1--24-1  
 GRANITE (GRANODIORITE, HARDHAT)

|                    |                                              |       |                |
|--------------------|----------------------------------------------|-------|----------------|
| ORTHOCLASE         | K-AL-S13-08                                  |       | 26 WT. PERCENT |
| PLAGIOCLASE        |                                              |       | 37 - -         |
|                    | NA-AL-S13-08                                 | 90-80 | - -            |
|                    | CA-AL2-S12-08                                | REST  | - -            |
| QUARTZ             | S1-02                                        |       | 29 - -         |
| BIOTITE            | K-(MG,FE)3-AL-S13-010-(O-H)2                 |       | 6 - -          |
| HORNBLENDE         | CA2-NA-(MG,FE)4-(AL,FE,TI)3-S16-022-(O,O-H)2 |       | 1 - -          |
| ACCESSORY MINERALS |                                              |       | REST           |
| PARTICLE SIZE.     |                                              |       | 0.2 TO 5.0 MM. |

V0 = 0.3738 CC/G

V01 = 0.376 CC/G

TABLE I LISTS SAMPLE THICKNESS IN MM. AND THE SHOCK- AND PARTICLE VELOCITIES OF THE TWO-WAVE SYSTEM, IN KM/SEC. TABLE II LISTS INITIAL DENSITY IN G/CC., PRESSURE IN KBAR AND COMPRESSION.

TABLE I

| NO  | X     | US1  | UP1  | US2  | UP2  | UFS  |
|-----|-------|------|------|------|------|------|
| *1A | 6.38  | 5.96 | 0.28 | 5.19 | 0.85 | 1.65 |
| 1B  | 12.38 | 5.95 | 0.27 | 5.21 | 0.85 | 1.60 |
| 2A  | 6.36  | 5.90 | 0.29 | 5.68 | 1.53 | 2.92 |
| *2B | 12.73 | 5.96 | 0.28 | 5.55 | 1.54 | 2.71 |
| *3A | 6.88  | 5.99 | 0.28 | 5.37 | 0.87 |      |
| *3B | 12.72 | 5.98 | 0.28 | 5.25 | 0.88 | 1.64 |
| 4A  | 6.37  | 6.04 | 0.28 | 5.50 | 1.54 | 2.92 |
| 4B  | 12.68 | 5.97 | 0.27 | 5.50 | 1.54 | 2.87 |
| 5A  | 6.24  | 6.02 | 0.34 | 5.51 | 1.22 | 2.38 |
| 5B  | 25.77 | 5.94 | 0.20 | 5.40 | 1.23 | 1.99 |
| 6B  | 25.76 | 6.05 | 0.29 | 5.45 | 1.25 | 2.00 |
| 7   | 6.37  | 6.08 | 0.29 | 5.44 | 1.26 | 2.30 |
| *8  | 6.18  | 5.98 | 0.28 | 5.71 | 1.82 | 3.40 |
| 9   |       |      |      | 7.04 | 3.00 | 5.90 |

US =

TABLE II

| NO | RH00  | P1  | V1/V0  | P2   | V2/V0 |
|----|-------|-----|--------|------|-------|
| 1A | 2.675 | 45. | 0.9530 | 123. | 0.842 |
| 1B | -     | 43. | 0.9514 | 124. | 0.840 |
| 2A | -     | 46. | 0.9508 | 233. | 0.732 |
| 2B | -     | 45. | 0.9530 | 231. | 0.725 |
| 3A | -     | 45. | 0.9532 | 130. | 0.843 |
| 3B | -     | 45. | 0.9532 | 128. | 0.838 |
| 4A | -     | 46. | 0.9536 | 230. | 0.723 |
| 4B | -     | 42. | 0.9548 | 229. | 0.723 |
| 5A | 2.674 | 54. | 0.9435 | 183. | 0.783 |
| 5B | 2.675 | 31. | 0.9663 | 180. | 0.775 |

|    |       |      |        |      |       |
|----|-------|------|--------|------|-------|
| 68 | 2.67  | 47.  | 0.9521 | 186. | 0.775 |
| 7  | 2.700 | 48.  | 0.9523 | 189. | 0.773 |
| 8  | 2.701 | 45.* | 0.9532 | 284. | 0.683 |
| 9  | 2.675 |      |        | 565. | 0.574 |

## COMMENTS:

- 1) SOURCE: PETERSEN, C. F., MURRI, W. J. ANDERSON, G. D. AND ALLEN C. F.  
S.R.I. INTERIM TECH. REPORT, PROJECT PGU-6618 (1968)  
STANFORD RES. INST., MENLO PARK, CALIF., U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: C1 AND D: HERE A REFLECTING FOIL IS PLACED  
A KNOWN DISTANCE FROM THE SAMPLE SURFACE  
IN GLYCEROL OR ETANOL).  
DATA REDUCTION TECHNIQUE: B AND D (FIRST WAVE)
- 3) EXP. TECHN. D MEASURED PARTICLE VELOCITY AND PRESSURE OF THE PARTIAL-  
LY DECOMPRESSED SAMPLE YIELDING THE FOLLOWING RELEASE STATE POINTS

|              | P    | UP   | P    | UP   |
|--------------|------|------|------|------|
| HUG. POINT   | 189. | 1.26 | 284. | 1.82 |
| REL. STATE 1 | 111. | 1.73 | 170. | 2.28 |
| - - 2        | 0.   | 2.30 | 122. | 2.64 |
| - - 3        |      |      | 0.   | 3.40 |

- 4) THE UP1 VALUES FOR THE POINTS MARKED WITH \* ARE THE AVERAGE OF THE  
REMAINING POINTS. THE US1 AND UP1 VALUES FOR THE POINT MARKED \*\* ARE  
ALSO THE AVERAGE OF THE REMAINING POINTS.  
SINCE THE MEASURED VELOCITIES WERE OF RELATIVELY LOW ACCURACY,  
SINCE THE EXPERIMENTAL QUANTITIES MEASURED ARE US AND UP, THE FINAL  
STATE IS INSENSITIVE TO THE VALUES SELECTED FOR THE FIRST WAVE.
- 5) THE ABOVE COMPOSITION WAS TAKEN FROM THE LITERATURE  
SHORT, M. M. J. GEOPHYS. RES., VOL. 71, P. 1195, (1966)  
HOUSER, F. N. AND POOLE, F. G.  
U.S. GEOLOGICAL SURVEY, REPT. TEM-836A (1959)
- 6) V01 IS THE SUM OF THE QUANTITIES (WT. PERCENT)/(100\*RHO) FOR ALL  
THE MINERALS LISTED. RHO IS GIVEN BY DANAS MANUAL OF MINERALOGY  
REVISED BY C.S. HURLBUT JR. (JOHN WILEY AND SONS INC., N.Y., 1959).

TABLE 1

GRANITE (GRANODIORITE, HARDHAT)

99-29-24-1--100-29-24-1--24-1

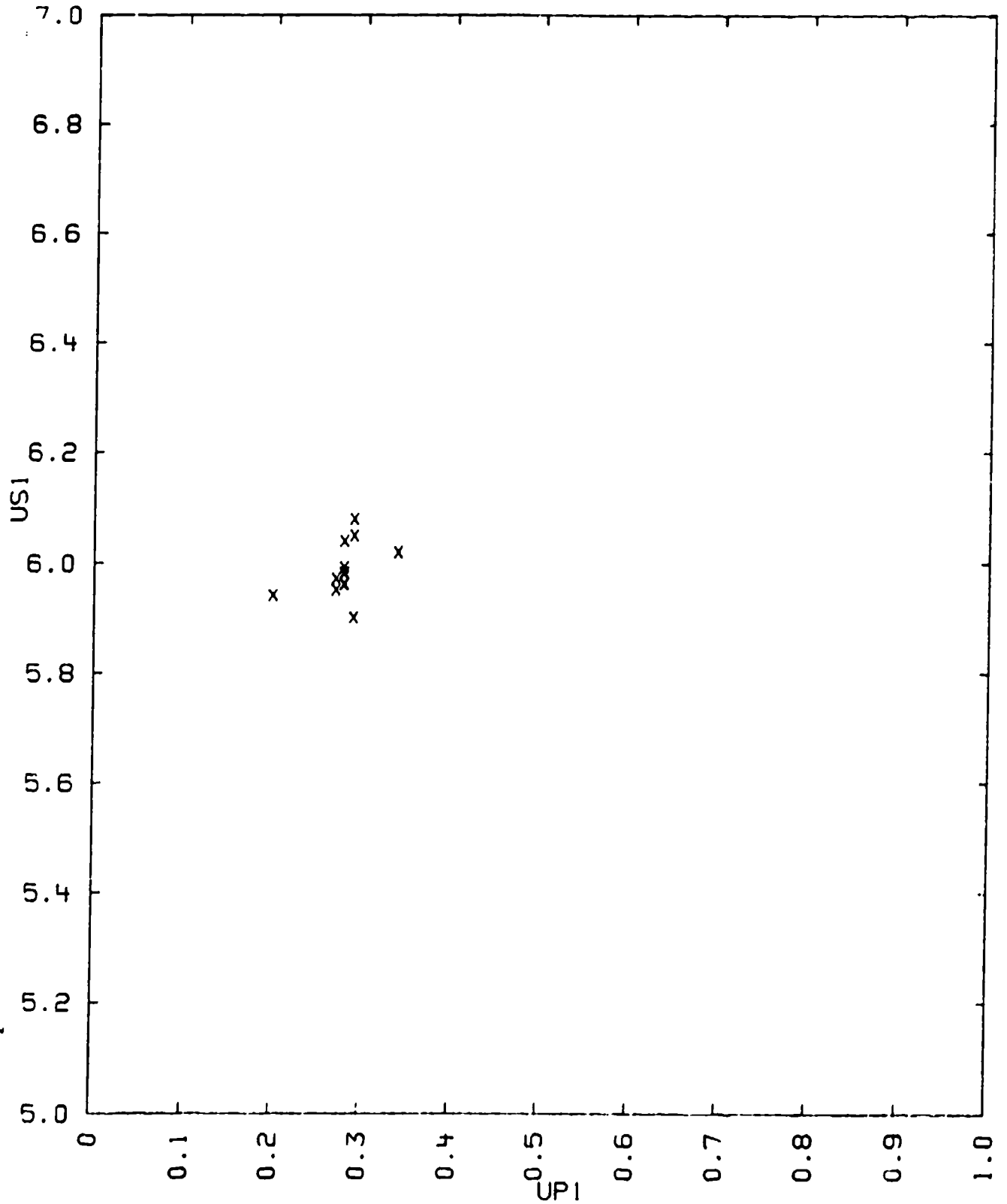
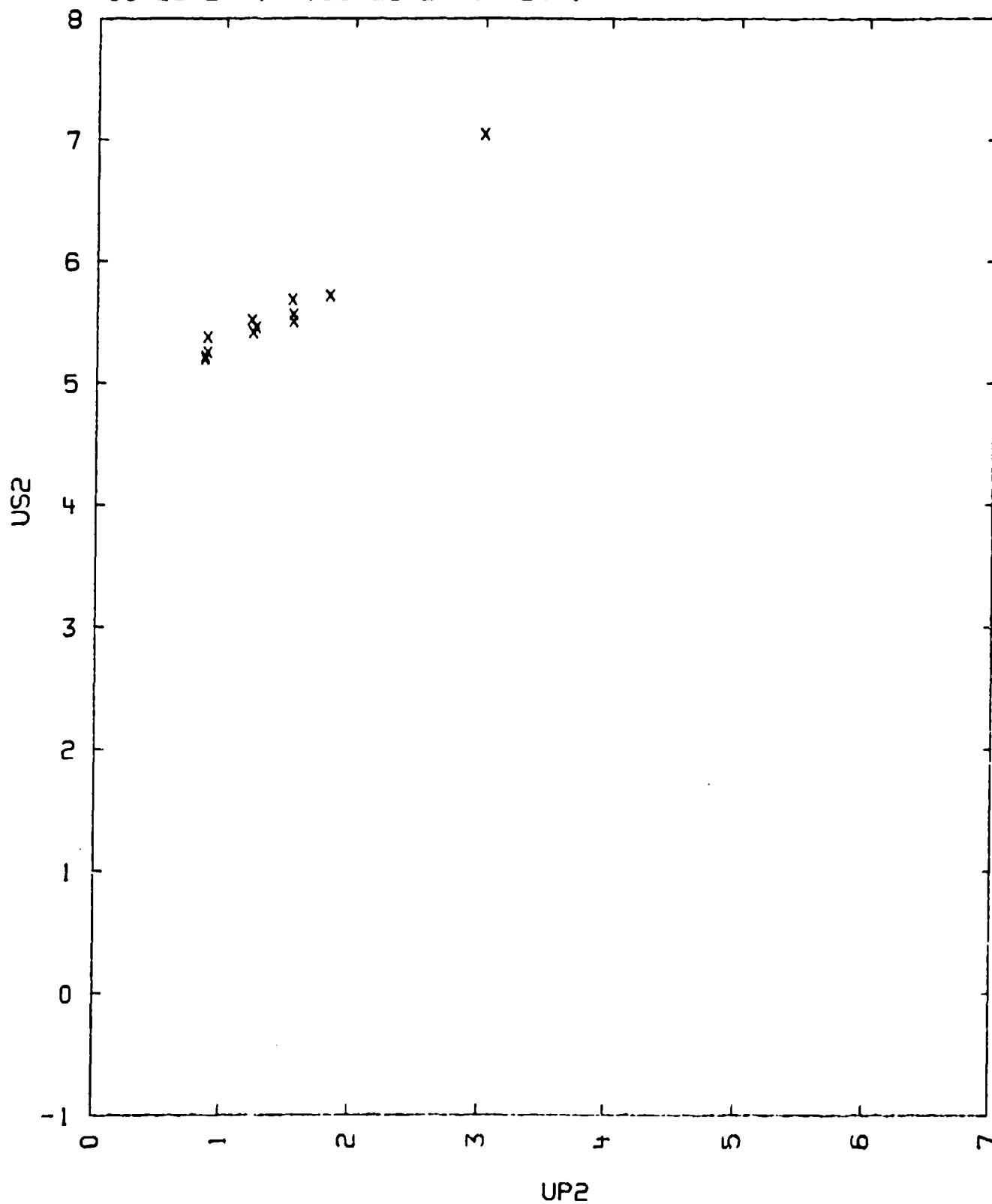


TABLE 1

GRANITE (GRANODIORITE, HARDHAT)

99-29-24-1--100-29-24-1--24-1



99-94-29-24-1--99-94-93-41-24-1---1  
 DIABASE, MARYLAND (SILICATE ROCK)

|              |                              |    |    |
|--------------|------------------------------|----|----|
| PYROXENE:    |                              | 49 |    |
| AUGITE       | (NA,CA)(MG,FE,AL)(SI,AL)2-06 |    | 24 |
| HYPERSTHENE  | (FE,MG)SI-03                 |    | 25 |
| PLAGIOCLASE: |                              | 48 |    |
| ANORTHITE    | CA-AL2-SI2-08                |    | 32 |
| ALBITE       | NA-AL-SI3-08                 |    | 16 |
| OLIVINE      | (MG,FE)2-SI-04               | 1  |    |
| MICA         |                              | 1  |    |

V0 = 0.332 CC/G CL = 6.82 KM/SEC.

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 3.01 | 6.00 | 0.89 | 161. | 0.852 | 6.55   |
| 3.01 | 6.11 | 0.96 | 177. | 0.843 | 6.64   |
| 3.01 | 6.05 | 1.22 | 223. | 0.798 | 6.95   |
| 3.01 | 6.05 | 1.24 | 225. | 0.795 | 6.97   |
| 3.01 | 5.98 | 1.28 | 231. | 0.786 | 7.02   |
| 3.01 | 6.15 | 1.63 | 301. | 0.735 | 7.44   |
| 3.02 | 6.22 | 1.74 | 326  | 0.722 | 7.58   |
| 3.01 | 6.29 | 1.81 | 344  | 0.710 | 7.67   |
| 3.01 | 6.39 | 1.91 | 368  | 0.702 | 7.80   |
| 3.01 | 6.89 | 2.27 | 472  | 0.669 | 8.28   |
| 3.01 | 6.90 | 2.31 | 481  | 0.663 | 8.33   |
| 3.01 | 7.38 | 2.65 | 590  | 0.640 | 8.78   |
| 3.01 | 7.39 | 2.66 | 593  | 0.639 | 8.80   |
| 3.02 | 7.99 | 3.13 | 754  | 0.609 | 9.42   |
| 3.02 | 8.08 | 3.14 | 765  | 0.613 | 9.45   |
| 3.01 | 8.36 | 3.30 | 832  | 0.604 | 9.68   |
| 3.02 | 8.75 | 3.65 | 963  | 0.584 | 10.13  |
| 3.01 | 9.04 | 3.78 | 1029 | 0.581 | 10.33  |

US = 3.778 + 1.371\*UP KM/SEC FOR UP FROM 1.9 TO 3.8 KM/SEC.  
 SIGMA US = 0.050 KM/SEC.

## COMMENTS :

- 1) SOURCE: MCQUEEN R. G. AND MARSH S. P.  
 PRIVATE COMMUNICATION (1966)  
 LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) THE MODAL ANALYSIS ON THESE SAMPLES WHICH WERE OBTAINED FROM BIRCH  
 WAS TAKEN FROM F. BIRCH, J. GEOPHYS. RES., NO. 65, P. 1083 (1960)

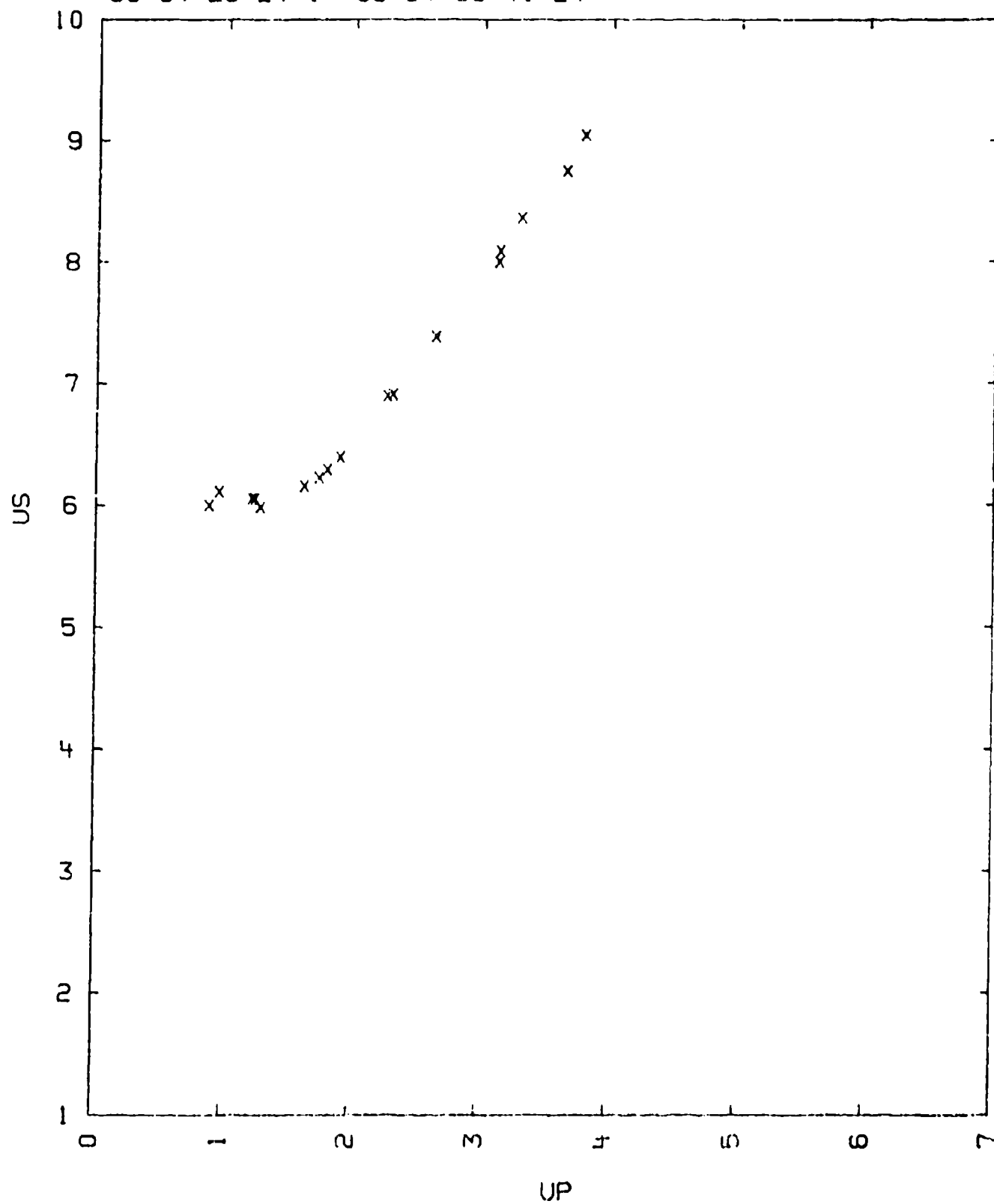
ALSO PRIVATE COMMUNICATION (1966)  
4) FURTHER WORK IS IN PROGRESS.



TABLE I

DIABASE, MARYLAND (SILICATE ROCK)

99-94-29-24-1--99-94-93-41-24-



99-94-93-29-24-1--41-29-24-1---1  
ECLOGITE, HEALDSBURG, CALIF. (SILICATE ROCK)

| GARNET:      |                 |      | 24 | VOLUME PERCENT |   |
|--------------|-----------------|------|----|----------------|---|
| ALMANDITE    | FE3-AL2(SI-04)3 | 14   | -  | -              | - |
| PYROPE       | MGS-AL2(SI-04)3 | 3    | -  | -              | - |
| GROSSULARITE | CA3-AL2(SI-04)3 | 4.5  | -  | -              | - |
| ANDRADITE    | CA3-FE2(SI-04)3 | 2.4  | -  | -              | - |
| SPESSARTITE  | MN3-AL2(SI-04)3 | 0.5  | -  | -              | - |
| OMPHASITE:   |                 |      | 72 |                |   |
| DIOPSIDE     | CA-MG(SI2-06)   | 39.7 | -  | -              | - |
| JADEITE      | NA-AL(SI2-06)   | 20.4 | -  | -              | - |
| ACMITE       | NA-FE(SI2-06)   | 8.6  | -  | -              | - |
| REST         | UNKNOWN         | 3.3  | -  | -              | - |
|              |                 |      | 4  | -              | - |

V0 = 0.295 TO 0.288 CC/G      CL = 7.84 KM/SEC  
V01 = 0.288 CC/G

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/V0  | US(ST) |
|------|------|------|------|-------|--------|
| 3.35 | 6.52 | 0.53 | 115. | 0.919 | 6.16   |
| 3.45 | 7.03 | 0.76 | 183. | 0.892 | 6.53   |
| 3.38 | 6.92 | 0.78 | 182. | 0.887 | 6.54   |
| 3.47 | 7.30 | 1.05 | 265. | 0.856 | 6.96   |
| 3.38 | 7.20 | 1.08 | 262. | 0.850 | 6.97   |
| 3.45 | 7.62 | 1.23 | 324. | 0.839 | 7.23   |
| 3.46 | 7.72 | 1.38 | 368. | 0.821 | 7.44   |
| 3.42 | 7.71 | 1.44 | 381. | 0.813 | 7.52   |
| 3.42 | 7.77 | 1.48 | 392. | 0.810 | 7.56   |
| 3.43 | 7.84 | 1.56 | 418. | 0.801 | 7.68   |
| 3.44 | 7.74 | 1.57 | 418. | 0.797 | 7.69   |
| 3.43 | 7.83 | 1.58 | 425. | 0.798 | 7.71   |
| 3.44 | 7.88 | 1.61 | 438. | 0.796 | 7.76   |
| 3.38 | 8.29 | 2.09 | 587. | 0.748 | 8.41   |
| 3.43 | 8.43 | 2.17 | 627. | 0.743 | 8.53   |
| 3.45 | 8.56 | 2.36 | 697. | 0.724 | 8.79   |
| 3.40 | 8.60 | 2.37 | 694. | 0.724 | 8.80   |
| 3.40 | 8.41 | 2.38 | 681. | 0.717 | 8.78   |
| 3.36 | 8.56 | 2.66 | 764. | 0.689 | 9.12   |
| 3.41 | 8.60 | 2.76 | 817  | 0.677 | 9.30   |
| 3.39 | 8.79 | 2.87 | 859  | 0.673 | 9.44   |
| 3.40 | 8.79 | 2.94 | 877  | 0.667 | 9.51   |
| 3.41 | 9.06 | 3.07 | 951  | 0.661 | 9.73   |
| 3.47 | 9.41 | 3.25 | 1062 | 0.655 | 10.03  |
| 3.43 | 9.33 | 3.37 | 1078 | 0.640 | 10.13  |

US = 5.86 + 1.36\*UP KM/SEC. FOR UP FROM 0.5 TO 1.4 KM/SEC.  
SIGMA = 0.10 KM/SEC.

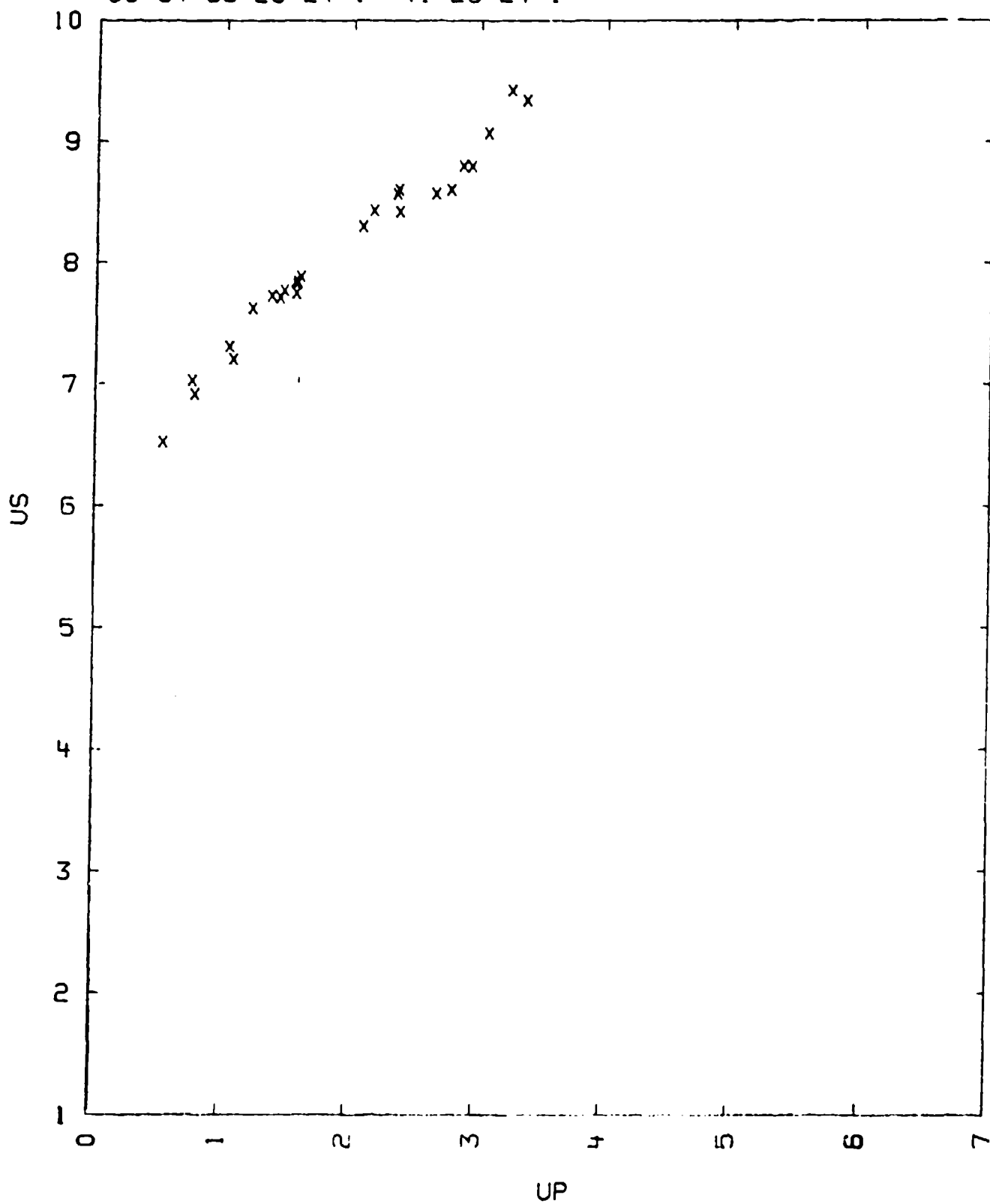
$US = 6.56 + 0.812 \cdot UP$  KM/SEC. FOR UP FROM 1.4 TO 2.7 KM/SEC.  
SIGMA US = 0.09 KM/SEC.

$US = 4.808 + 1.375 \cdot UP$  KM/SEC. FOR UP FROM 2.78 TO 3.4 KM/SEC  
SIGMA US = 0.096 KM/SEC.

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.  
PRIVATE COMMUNICATION  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) THE MODAL ANALYSIS OF THESE SAMPLE WHICH WERE OBTAINED THROUGH BIRCH  
WAS TAKEN FROM: BIRCH F., J. GEOPHYS. RES., VOL. 65, P. 1083 (1960)  
ALSO PRIVATE COMMUNICATION  
SEE ALSO: I. BORG, BULL. GEOL. SOC. AMER., VOL. 67, P. 1563, (1956).
- 4) FURTHER WORK IN PROGRESS.
- 5) CL ALSO WAS OBTAINED FROM BIRCHS 1960 PAPER.
- 6) VOI WAS CALCULATED BY ASSUMING VOLUME ADDITIVITY OF THE COMPONENTS.  
DIOPSIDE AND JADEITE DENSITIES WERE FROM: CRYSTAL DATA DETERMINATIVE  
TABLES (AM. CRYST. ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN,  
N.Y., 1963) 2ND ED. THE OTHER DENSITIES WERE TAKEN FROM: C.S. HURLBUT  
DANAS MANUAL OF MINERALOGY. (JOHN WILEY AND SONS, N.Y. 1963) 17 ED.

TABLE I  
 ECLOGITE, HEALDSBURG, CALIF. (SILICATE ROCK)  
 99-94-93-29-24-1--41-29-24-1--



99-94-93-29-24-1--41-29-24-1--93-29-24-1---1  
ECLOGITE, NORWAY (SILICATE ROCK)

|           |                                                                    |    |              |   |
|-----------|--------------------------------------------------------------------|----|--------------|---|
| OMPHASITE | (AL-NA,MG-CA)Si <sub>2</sub> O <sub>6</sub>                        | 52 | VOL. PERCENT |   |
| GARNET:   |                                                                    | 42 | -            | - |
| ALMANDITE | FE <sub>3</sub> -AL <sub>2</sub> (Si-04) <sub>3</sub>              | 25 | -            | - |
| PYROPE    | MG <sub>3</sub> -AL <sub>2</sub> (Si-04) <sub>3</sub>              | 17 | -            | - |
| BIOTITE   | K(ING,FE) <sub>3</sub> (AL-Si <sub>3</sub> -010)(O-H) <sub>2</sub> | 6  | -            | - |

V<sub>0</sub> = 0.287 TO 0.279 CC/G CL = 7.4 KM/SEC

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P     | V/V <sub>0</sub> | US(ST) |
|------|------|------|-------|------------------|--------|
| 3.59 | 6.80 | 0.50 | 121.  | 0.926            | 6.16   |
| 3.53 | 7.02 | 0.75 | 187.  | 0.893            | 6.54   |
| 3.56 | 7.10 | 0.77 | 195.  | 0.892            | 6.57   |
| 3.57 | 7.40 | 1.02 | 270.  | 0.862            | 6.95   |
| 3.60 | 7.39 | 1.03 | 273.  | 0.861            | 6.97   |
| 3.51 | 7.31 | 1.07 | 274.  | 0.854            | 6.99   |
| 3.53 | 7.63 | 1.22 | 328.  | 0.840            | 7.23   |
| 3.55 | 7.86 | 1.35 | 376.  | 0.828            | 7.44   |
| 3.56 | 8.04 | 1.51 | 432.  | 0.812            | 7.68   |
| 3.58 | 7.92 | 1.51 | 428.  | 0.809            | 7.67   |
| 3.48 | 7.84 | 1.61 | 439.  | 0.795            | 7.76   |
| 3.52 | 7.99 | 1.61 | 453.  | 0.798            | 7.80   |
| 3.51 | 7.83 | 1.63 | 448.  | 0.792            | 7.79   |
| 3.59 | 8.37 | 2.03 | 609.  | 0.757            | 8.41   |
| 3.58 | 8.81 | 2.27 | 718.  | 0.741            | 8.78   |
| 3.54 | 8.72 | 2.31 | 713.  | 0.734            | 8.79   |
| 3.56 | 8.88 | 2.55 | 805.  | 0.712            | 9.12   |
| 3.57 | 9.11 | 2.72 | 886.  | 0.701            | 9.38   |
| 3.53 | 9.24 | 2.76 | 902.  | 0.700            | 9.44   |
| 3.52 | 9.36 | 2.99 | 984.  | 0.681            | 9.73   |
| 3.56 | 9.22 | 2.99 | 983.  | 0.676            | 9.73   |
| 3.55 | 9.72 | 3.26 | 1125. | 0.664            | 10.13  |

US = 6.15 + 1.21\*UP KM/SEC. FOR UP FROM 0.5 TO 1.4 KM/SEC.  
SIGMA US = 0.07 KM/SEC.

US = 6.40 + 0.997\*UP KM/SEC. FOR UP FROM 1.5 TO 3.3 KM/SEC.  
SIGMA US = 0.11 KM/SEC.

## COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.  
PRIVATE COMMUNICATION  
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B

DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM.

- 3) THE MODAL ANALYSIS OF THESE SAMPLES WHICH WERE OBTAINED THROUGH BIRCH WAS TAKEN FROM F. BIRCH, J. GEOPHYS. RES., VOL. 65, P. 1083 (1960)
- 4) FURTHER WORK IS IN PROGRESS
- 5) THE GARNET COMPOSITION LISTED BY BIRCH IS:  
 SI-02, AL2-03, FE-0, TI-02, FE2-03, MN-0, MG-0, CA-0, H2-0  
 36.30 20.18 32.01 2.45 0.07 1.74 4.75 2.02 0.27 WT PERCENT
- 6) NO DETAILED ANALYSIS OF THE OMPHACITE EXISTS. ANOTHER SAMPLE FROM THIS GENERAL LOCALITY IN ESCOLA HAS THE COMPOSITION:

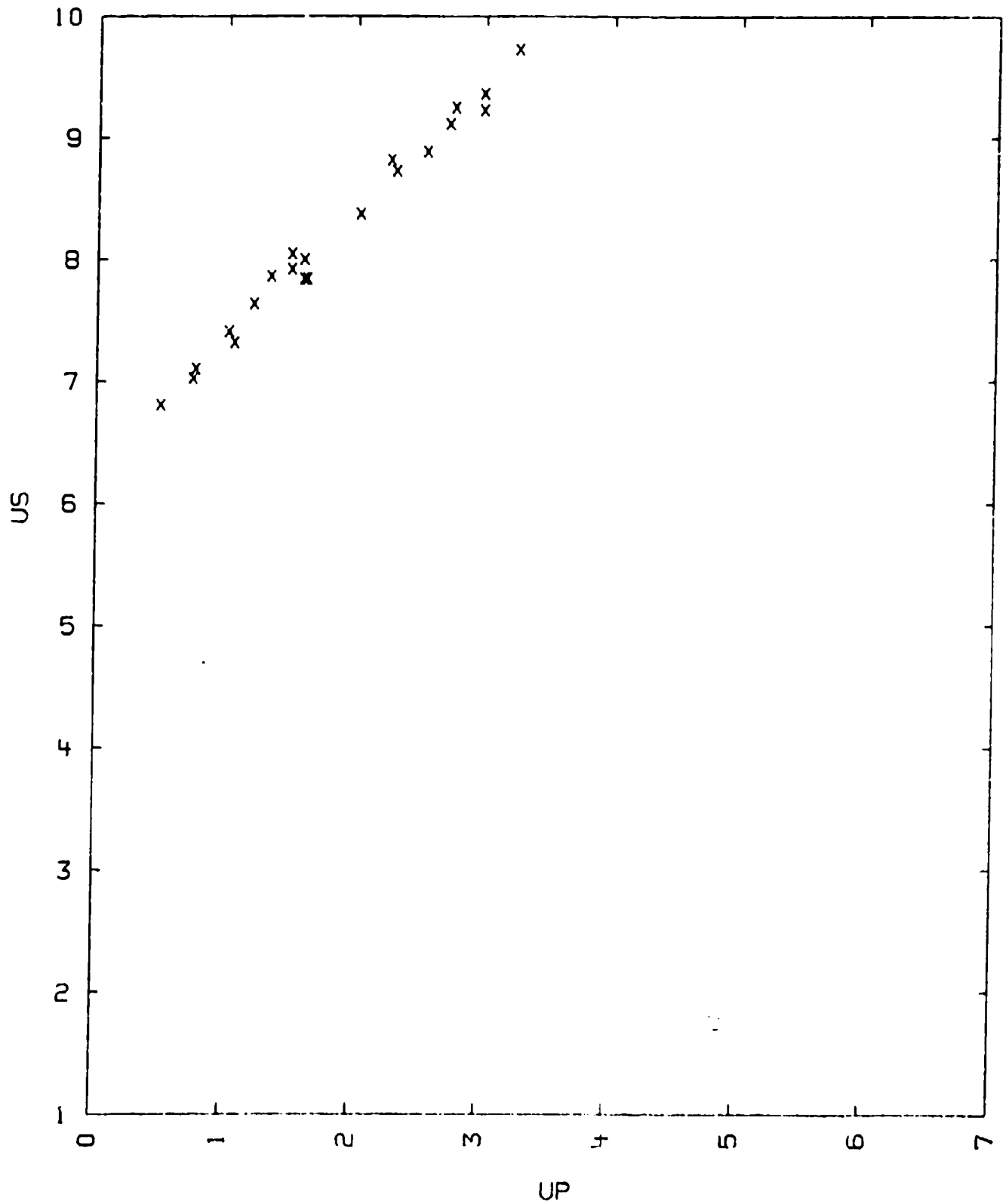
|                     |       |
|---------------------|-------|
| DIOPSIDE            | 83.48 |
| JADEITE             | 7.38  |
| ENSTATITE           | 4.67  |
| TSCHERMAKS SILICATE | 4.12  |
| UNACCOUNTED FOR     | 0.73  |

F. BIRCH, PRIVATE COMMUNICATION (1967)

TABLE 1

ECLOGITE, NORWAY (SILICATE ROCK)

99-94-93-29-24-1--41-29-24-1--



100-29-24-1--99-29-24-1--24-1---1  
 GRANITE, WESTERLY, R. I. (SILICATE ROCK)

|            |              |      |                |   |
|------------|--------------|------|----------------|---|
| MICROCLINE | K-AL-S13-08  | 35.4 | VOLUME PERCENT |   |
| ALBITE     | NA-AL-S13-08 | 25.1 | -              | - |
| ANORTHITE  | CA-AL-S13-08 | 6.3  | -              | - |
| QUARTZ     | SI-02        | 27.5 | -              | - |
| MICA       |              | 3.2  | -              | - |

VO = 0.3817 CC/G      CL = 6.1 KM/SEC  
 VOI = 0.3811 CC/G

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

| RH00 | US   | UP   | P    | V/VO  | US(ST) |
|------|------|------|------|-------|--------|
| 2.63 | 5.29 | 1.00 | 138. | 0.811 | 6.55   |
| 2.63 | 5.31 | 1.01 | 141. | 0.810 | 6.57   |
| 2.63 | 5.45 | 1.35 | 193. | 0.752 | 6.95   |
| 2.63 | 5.46 | 1.37 | 196. | 0.749 | 6.97   |
| 2.63 | 5.42 | 1.39 | 198. | 0.744 | 6.99   |
| 2.63 | 5.45 | 1.43 | 205. | 0.738 | 7.04   |
| 2.63 | 5.60 | 1.91 | 281. | 0.659 | 7.58   |
| 2.63 | 5.61 | 1.93 | 285. | 0.656 | 7.60   |
| 2.63 | 5.67 | 1.99 | 297. | 0.649 | 7.67   |
| 2.62 | 5.78 | 2.10 | 318. | 0.637 | 7.80   |
| 2.62 | 5.69 | 2.11 | 315. | 0.629 | 7.79   |
| 2.63 | 6.19 | 2.50 | 406  | 0.596 | 8.28   |
| 2.63 | 6.18 | 2.55 | 414  | 0.588 | 8.33   |
| 2.63 | 6.83 | 2.88 | 517  | 0.578 | 8.78   |
| 2.63 | 7.58 | 3.37 | 671  | 0.557 | 9.42   |
| 2.63 | 7.99 | 3.54 | 744  | 0.557 | 9.68   |
| 2.63 | 8.49 | 3.89 | 868  | 0.542 | 10.13  |
| 2.63 | 8.41 | 3.90 | 861  | 0.537 | 10.12  |
| 2.63 | 8.62 | 4.05 | 919  | 0.530 | 10.33  |

US = 4.93 + 0.372\*UP KM/SEC. FOR UP BETWEEN 1.0 AND 2.1  
 SIGMA US = 0.03 KM/SEC.

US = 2.103 + 1.629\*UP KM/SEC FOR UP BETWEEN 2.5 AND 4.1  
 SIGMA US = 0.074 KM/SEC.

## COMMENTS :

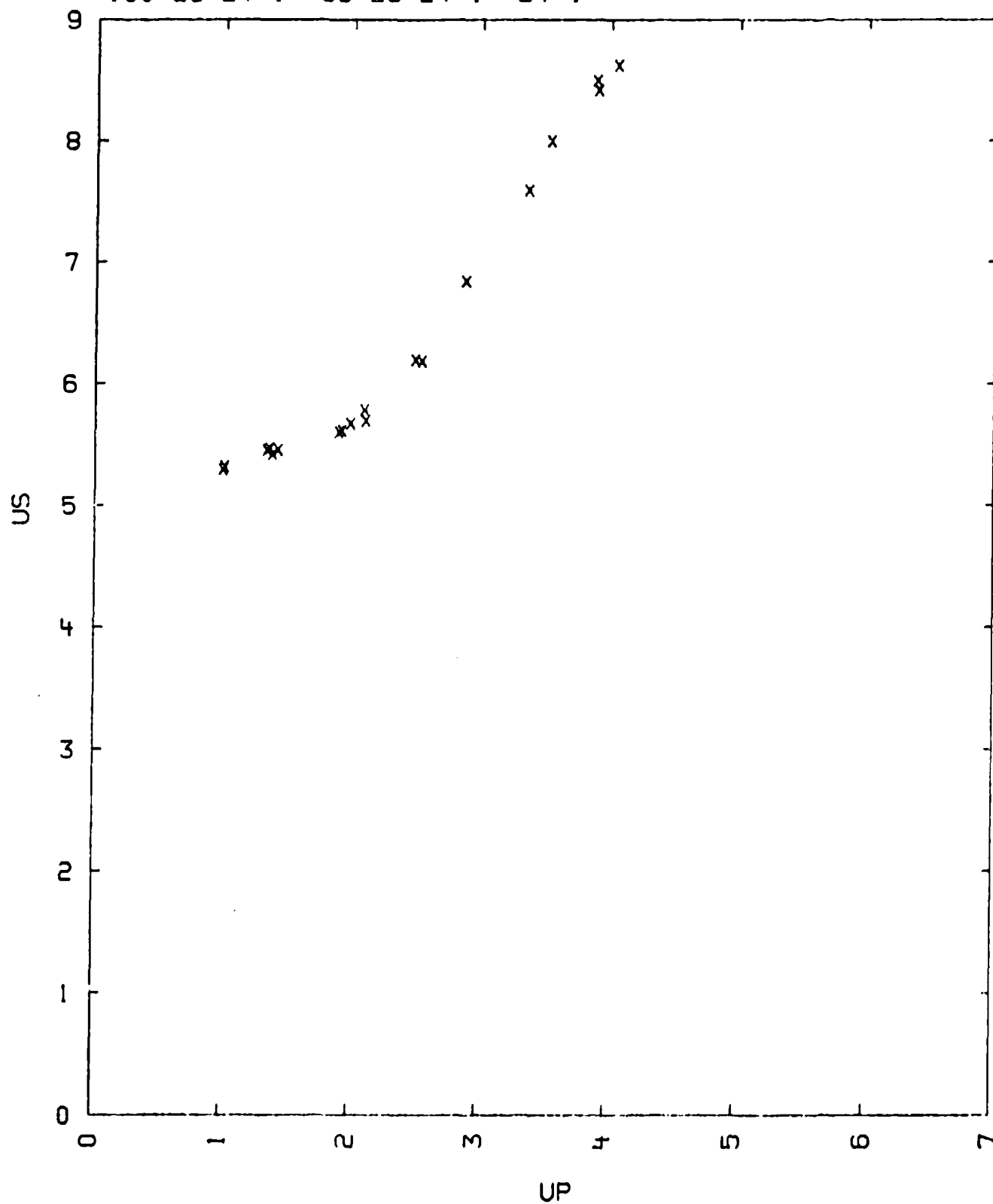
- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.  
 PRIVATE COMMUNICATION  
 LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VOI WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA



DETERMINATIVE TABLES (AMERICAN CRYST. ASSN. 1953) 2ND ED., AND A MICA  
DENSITY OF 2.80 G/CC

- 4) THE MODAL ANALYSIS OF THESE SAMPLES WHICH WERE OBTAINED THROUGH BIRCH  
WAS TAKEN FROM: F. BIRCH, J. GEOPHYS. RES., VOL. 65, P. 1083 (1960)  
VO IS THE SPECIFIC VOLUME REPORTED BY BIRCH.
- 5) FURTHER WORK IS IN PROGRESS.

TABLE 1  
 GRANITE, WESTERLY, R. I. (SILICATE ROCK)  
 100-29-24-1--99-29-24-1--24-1-



100-29-24-1--99-29-24-1--94-29-24-1---1  
 GRANITE

|                     |                                             |                       |
|---------------------|---------------------------------------------|-----------------------|
| ORTHOCLASE          | K-AL-S13-08                                 | 47.0 PERCENT BY WT.   |
| PLAGIOCLASE         | (AN)X-(AB)Y                                 | 26.5 PERCENT          |
| QUARTZ              | SI-02                                       | 19.5 PERCENT          |
| MICA                |                                             | 5.0 PERCENT           |
| HORNBLENDE          | CA2-NA-(MG,FE)4-(AL,FE,TI)3-SI6-O22-(O,OH)2 | 1.5 PERCENT           |
| OPAQUES             |                                             | LESS THAN 1.0 PERCENT |
| POROSITY (MEASURED) |                                             | 0.8 PERCENT           |
| PARTICLE SIZE       |                                             | UP TO 5.0 MM          |

V0 = 0.374 CC/G      CL = 5.64 KM/SEC  
 CS = 3.53 KM/SEC

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,  
 AND PRESSURE IN KILOBARS.

TABLE

| RH00  | US   | UFS  | UP   | P   | V/V0  |
|-------|------|------|------|-----|-------|
| 2.669 | 5.38 | 2.04 | 0.99 | 142 | 0.816 |
| 2.669 | 5.66 | 3.09 | 1.63 | 246 | 0.712 |
| 2.660 | 5.19 |      | 0.49 | 68  | 0.906 |
| 2.680 | 7.58 | 6.38 | 3.35 | 680 | 0.558 |
| 2.690 | 5.52 | 1.99 | 0.96 | 143 | 0.826 |
| 2.686 | 6.32 | 4.87 | 2.57 | 436 | 0.593 |
| 2.674 | 5.59 | 3.33 | 1.72 | 257 | 0.693 |
| 2.674 | 8.27 | 7.98 | 3.87 | 856 | 0.532 |
| 2.679 | 5.66 | 1.13 | 0.49 | 74  | 0.914 |
| 2.680 | 5.59 | 1.73 | 0.82 | 123 | 0.853 |
| 2.690 | 5.65 | 3.05 | 1.63 | 247 | 0.712 |
| 2.675 | 5.68 | 3.74 | 2.11 | 319 | 0.629 |
| 2.672 | 6.92 | 5.59 | 2.88 | 533 | 0.584 |
| 2.612 | 5.37 | 2.60 | 1.31 | 184 | 0.756 |
| 2.614 | 5.83 | 4.25 | 2.22 | 337 | 0.619 |
| 2.618 | 5.37 | 2.06 | 1.00 | 140 | 0.814 |
| 2.614 | 5.38 |      | 0.49 | 68  | 0.909 |

US = 2.52 + 1.50 UP KM/SEC      ABOVE UP = 2. KM/SEC.  
 SIG.US = 0.06

## COMMENTS:

- 1) SOURCE: COMPILER  
 L. R. L. EQUATION OF STATE FILE  
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA  
 S DIVISION REPORT STN 71, AUG 1964
- 2) EXPERIMENTAL TECHNIQUE B  
 DATA REDUCTION TECHNIQUE B  
 (STANDARD MATERIAL 2024 ALUMINUM)
- 3) THE TABLE LISTS THE RESULTS OF FOUR TYPES OF GRANITE OBTAINED FROM

AREA 15 AT THE NATIONAL TEST SITE IN NEVADA.

THE FIRST FOUR POINTS CORRESPOND TO SAMPLES FROM 1005 FEET EXPLORATORY CORE.

THE TWO FOLLOWING POINTS CORRESPOND TO SAMPLES FROM HARDHAT TUNNEL.

THE LAST FOUR POINTS CORRESPOND TO SAMPLES THAT CAN BE VISUALLY CHARACTERIZED AS PINK GRANITE.

4) ALL OF THESE SAMPLES HAVE THE SAME SHOCK VS. PARTICLE VELOCITY DEPENDENCE WITHIN EXPERIMENTAL ERROR.

5) CHEMICAL ANALYSIS (GREY GRANITE AREA 15 NTS NEVADA)

|                  |                      |
|------------------|----------------------|
| SILICA           | 71.94 PERCENT BY WT. |
| FERRIC OXIDE     | 4.25 PERCENT         |
| ALUMINUM OXIDE   | 13.68 PERCENT        |
| CALCIUM OXIDE    | 2.96 PERCENT         |
| MAGNESIUM OXIDE  | 0.63 PERCENT         |
| SODIUM OXIDE     | 2.94 PERCENT         |
| POTASSIUM OXIDE  | 1.44 PERCENT         |
| TITANIUM DIOXIDE | 0.26 PERCENT         |
| WATER            | 1.38 PERCENT         |

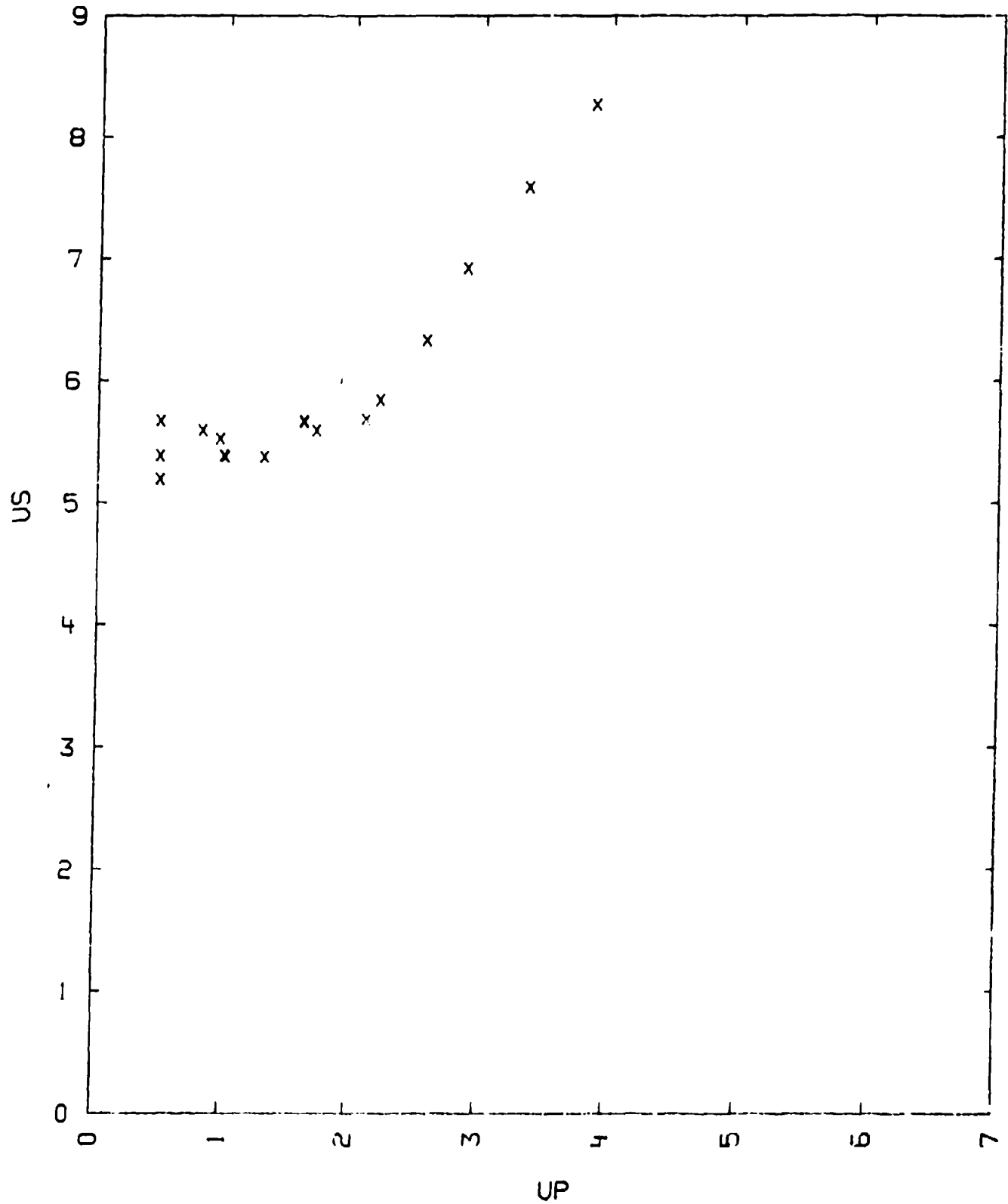
6) MINERALOGICAL AND CHEMICAL ANALYSIS AGREE TO 2 PERCENT.

7) THE CHEMICAL ANALYSIS INDICATES THAT THE PLAGIOCLASE CONSISTS MOSTLY OF ALBITE.

TABLE I

GRANITE

100-29-24-1--99-29-24-1--94-29



UNCL

BOX V72 PLTR

10:26:28 06/15/77U

XEROX+F ILM

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 09:55:29U 06/15

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 09:55:29U 06/15



EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 09:55:29U 06/15

237 FRAMES PLOTTED

UNCL

BOX V72 PLTR

10:27:38 06/15/77U

XEROX+F ILM

S E C T I O N E  
- - - - -

MIXTURES AND SOLUTIONS  
WITHOUT  
CHEMICAL CHARACTERIZATION

94-93-41-29-24-1 ?

AUGITE

CA-(MG-FE-AL)-(AL-SI)2-O6

GRAIN SIZE ABOUT 0.5 MM.

V0 = 0.2877-0.2971 CC/G CL = 8.18-8.26 KM/SEC

V01 = 0.2944-0.2966 CC/G

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBAR. STM IS THE STANDARD BASE PLATE MATERIAL, AL=ALUMINUM AND BR=BRASS  
D=SAMPLE THICKNESS IN MM.

TABLE I

| - - - - - SAMPLE - - - - - |      |       |      |       |      |       |      |       |       |   | STANDARD |      |
|----------------------------|------|-------|------|-------|------|-------|------|-------|-------|---|----------|------|
| RH00                       | US1  | UP1   | P1   | V1/V0 | US2  | UP2   | UFS  | P2    | V2/V0 | D | STM      | UFS  |
| 3.463                      | 6.61 | 0.264 | 60.4 | 0.960 | 5.91 | 0.710 | 1.22 | 151.3 | 0.884 | 9 | AL       | 1.55 |
| 3.475                      | 7.67 | 0.13  | 34.6 | 0.983 | 6.25 | 0.670 | 1.34 | 151.5 | 0.896 | 9 | AL       | 1.51 |
| 3.473                      | 7.70 | 0.177 | 47.3 | 0.977 | 6.74 | 0.825 |      | 190.5 | 0.881 | 9 | AL       | 1.89 |
| 3.475                      | 7.27 | 0.13  | 32.8 | 0.982 | 6.68 | 0.945 | 1.91 | 221.7 | 0.860 | 6 | AL       | 2.11 |
| 3.366                      | 7.84 | 0.268 | 70.7 | 0.966 | 7.42 | 1.66  | 3.29 | 417.7 | 0.778 | 5 | AL       | 3.58 |
| 3.393                      | -    | 0.13  | 34.6 | 0.983 | 7.79 | 1.89  | 3.56 | 499.7 | 0.757 | 6 | BR       | 3.03 |

US =

TABLE II

| - - - - - SAMPLE - - - - - |      |       |      |      |      |      | STANDARD |      |
|----------------------------|------|-------|------|------|------|------|----------|------|
| RH00                       | US   | UP    | UFS  | P    | V/V0 | D    | STM      | UFS  |
| 3.393                      | 7.07 | 0.935 | 1.91 | 224. | .868 | 6.41 | AL       | 2.11 |
| 3.470                      | 7.26 | 1.26  | 2.41 | 317. | .826 | 8.67 | AL       | 2.82 |
| 3.475                      | 7.49 | 1.42  | 2.93 | 369. | .810 | 5.87 | AL       | 3.18 |
| 3.475                      | 7.88 | 1.87  | 3.67 | 512. | .763 | 6.40 | BR       | 3.03 |
| 3.463                      | 7.60 | 2.05  | 4.20 | 540. | .730 | 4.81 | AL       | 4.41 |
| 3.463                      | 7.73 | 2.10  | 4.40 | 562. | .728 | 4.83 | BR       | 3.34 |
| 3.393                      | 7.92 | 2.16  | 4.14 | 580. | .727 | 6.50 | BR       | 3.45 |
| 3.475                      | 7.94 | 2.15  | 4.41 | 593. | .729 | 6.06 | BR       | -    |
| 3.463                      | 7.65 | 2.22  | 4.66 | 586. | .710 | 4.83 | AL       | 4.78 |
| 3.393                      | 7.92 | 2.48  | 4.99 | 666. | .687 | 6.84 | BR       | 3.90 |
| 3.393                      | 8.31 | 2.44  | 4.85 | 688. | .706 | 4.97 | BR       | -    |
| 3.463                      | 8.01 | 2.84  | 6.03 | 788. | .645 | 4.83 | BR       | 4.45 |

US =

COMMENTS:

- 1) SOURCE: AHRENS T.J., ROSENBERG J.T., RUDERMAN M.H.  
 STANFORD RESEARCH INSTITUTE REPORT NO DASA 1868 (1966)  
 STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA 94550  
 U.S.A.
- 2) EXPERIMENTAL TECHNIQUE C1 (INCLINED MIRROR)  
 DATA REDUCTION METHOD B AND D1 (ELASTIC WAVES)
- 3) VOI IS CALCULATED FROM THE LATTICE CONSTANTS OF A NUMBER OF SAMPLES  
 FROM KANGERDLUGSSAUG FJORD, E GREENLAND :  
 COMPOSITION: FE 0.212 - 0.362 NA 0.024 - 0.036 MOLES/6 MOLES OF O  
                   AL 0.149 - 0.239 CR 0.0 - 0.022 - - - -  
                   CA 0.830 - 0.775 TI 0.021 - 0.039 - - - -  
                   MG 0.630 - 0.695 SI 1.819 - 1.893 - - - -  
 DEER AND ABBOTT, MINERAL MAG. 34 177 (1965)
- 4) THE VALUE OF VOI AND THE ABOVE COMPOSITION SUGGEST THAT THE SAMPLES  
 IN USED FOR THE HUGONIOT MEASUREMENTS WERE RICHER IN FE AND PERHAPS  
 IN AL TOO.

TABLE I

AUGITE  
94-93-41-29-24-1 ?

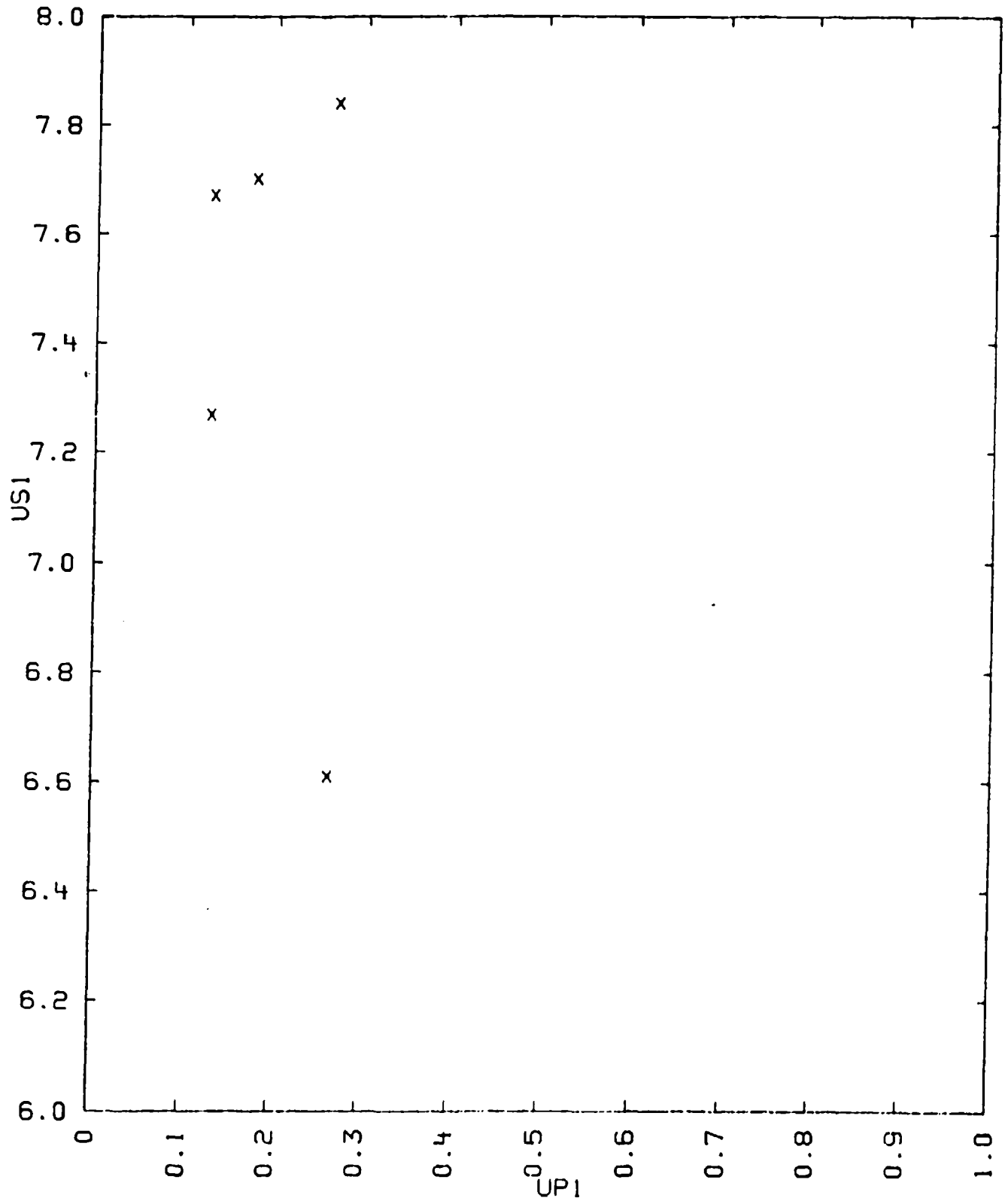


TABLE II

AUGITE

94-93-41-29-24-1 ?

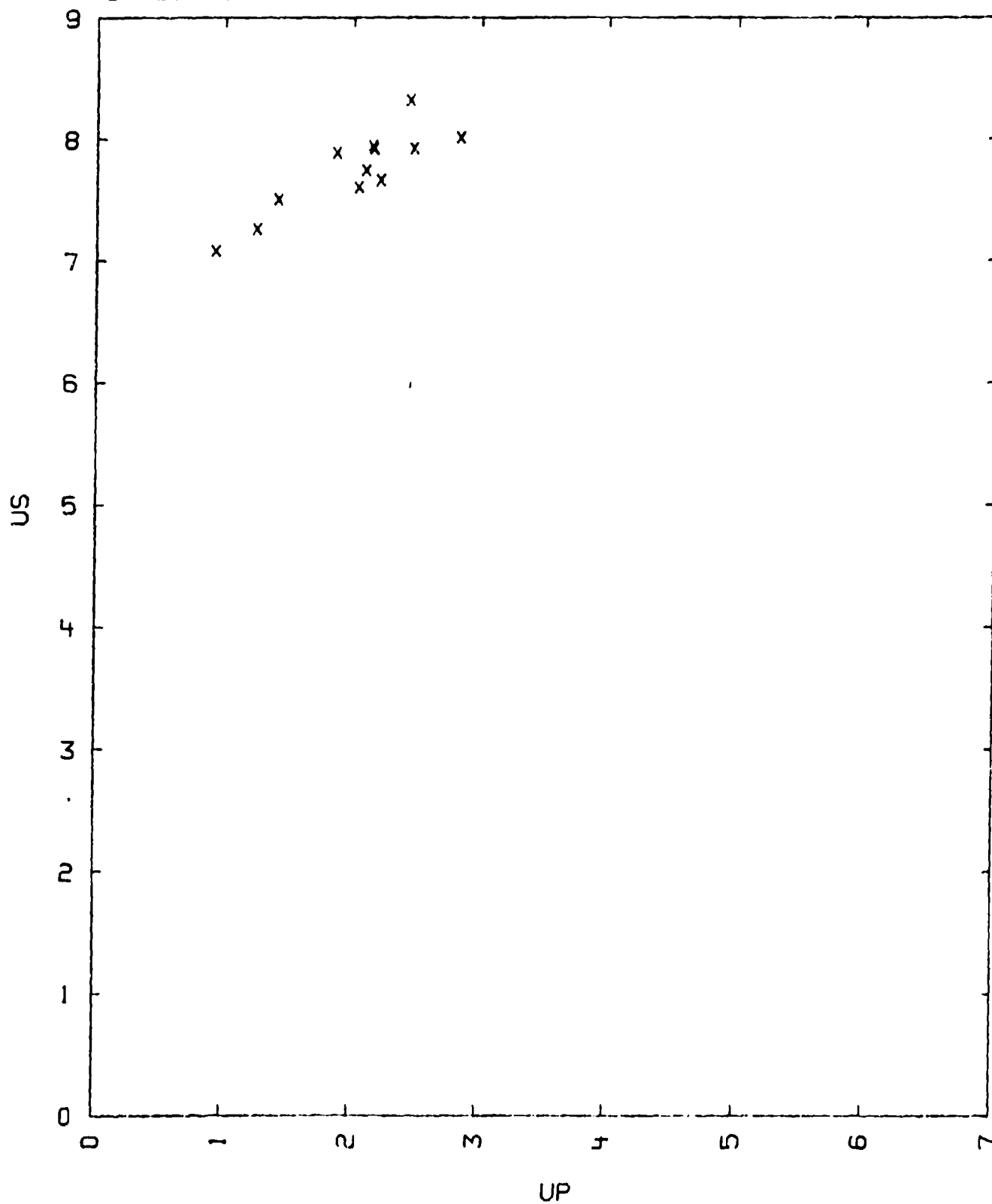
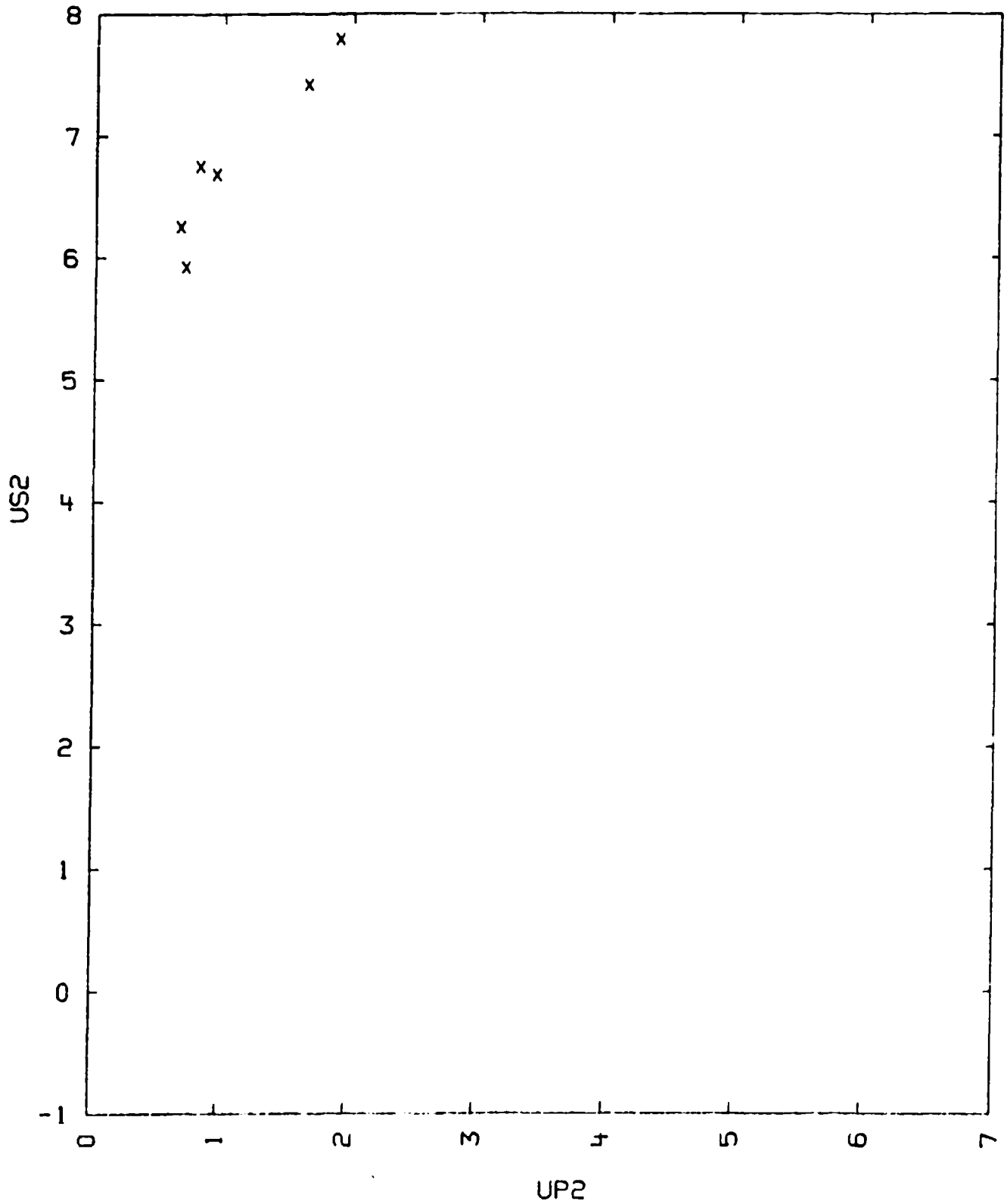


TABLE 1

AUGITE

94-93-41-29-24-1 ?





23--29-19-1 ?

CARBON CLOTH LAMINATE WITH ALUMINUM PHOSPHATE RESIN

|              |                       |            |
|--------------|-----------------------|------------|
| CARBON CLOTH | C (99.9 PERCENT PURE) | WT PERCENT |
| RESIN        | AL-P-04               | - -        |

V0 = 0.697 AND 0.96 CC/G.

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR

TABLE

| RH00  | US   | UP   | P    | V/V0 | MET |
|-------|------|------|------|------|-----|
| 1.435 | 2.91 | 0.93 | 39.  | 0.68 | A   |
| 1.435 | 4.01 | 1.75 | 100. | 0.56 | -   |
| 1.435 | 4.68 | 2.29 | 154. | 0.51 | -   |
| 1.435 | 5.01 | 2.68 | 192. | 0.47 | -   |
| 1.435 | 2.82 | 0.86 | 35.  | 0.70 | F   |
| 1.435 | 4.06 | 1.71 | 100. | 0.58 | -   |
| 1.435 | 4.72 | 2.22 | 150. | 0.53 | -   |
| 1.435 | 5.05 | 2.50 | 181. | 0.50 | -   |
| 1.435 | 5.00 | 2.58 | 185. | 0.48 | -   |
| 1.04  | 2.47 | 0.89 | 23.  | 0.64 | A   |
| 1.04  | 2.34 | 0.92 | 22.  | 0.61 | -   |
| 1.04  | 2.83 | 1.09 | 33.  | 0.61 | -   |
| 1.04  | 2.65 | 1.27 | 36.  | 0.52 | -   |
| 1.04  | 3.19 | 1.64 | 55.  | 0.48 | -   |
| 1.04  | 3.54 | 1.88 | 69.  | 0.47 | -   |
| 1.04  | 3.48 | 1.91 | 69.  | 0.45 | -   |
| 1.04  | 3.46 | 2.05 | 73.  | 0.41 | -   |
| 1.04  | 4.29 | 2.65 | 118. | 0.38 | -   |
| 1.04  | 4.65 | 2.82 | 131. | 0.39 | -   |

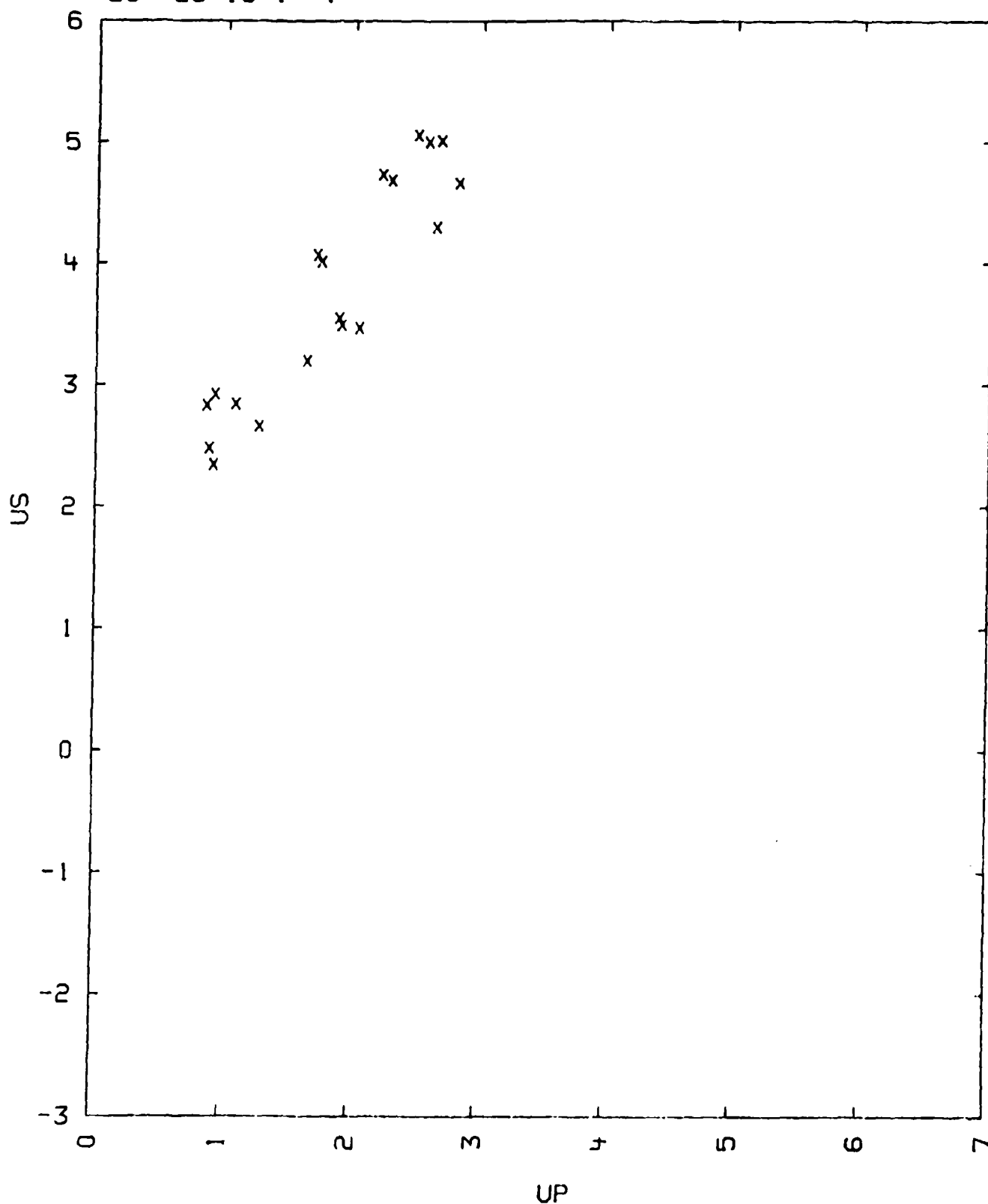
US = 1.412 + 1.097\*UP KM/SEC. FOR RH00 = 1.04

US = 1.778 + 1.270\*UP KM/SEC. FOR RH00 = 1.435

## COMMENTS:

- 1) SOURCE: MAY, R. P. AND KINSEY, C. H.  
SANDIA CORPORATION REPORT, SC-DR-67-2958, MARCH 1968  
SANDIA CORPORATION, ALBUQUERQUE, NEW-MEXICO, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE A AND F  
DATA REDUCTION METHOD B
- 3) THE SHOCK DIRECTION WAS PERPENDICULAR TO THE LAMINATIONS.  
NO TWO WAVE STRUCTURE WAS OBSERVED.

TABLE I  
 CARBON CLOTH LAMINATE WITH ALUMINUM PHOSPHATE RESI  
 23--29-19-1 ?



23-2 ?

CARBON PHENOLIC, FILAMENT WOUND AND PYROLYSED

V0 = 0.769 CC/G.

CL = 2.60 KM/SEC

THE TABLE LISTS DENSITY IN G/CC., VELOCITY IN KM/SEC. AND PRESSURE IN KBAR

TABLE

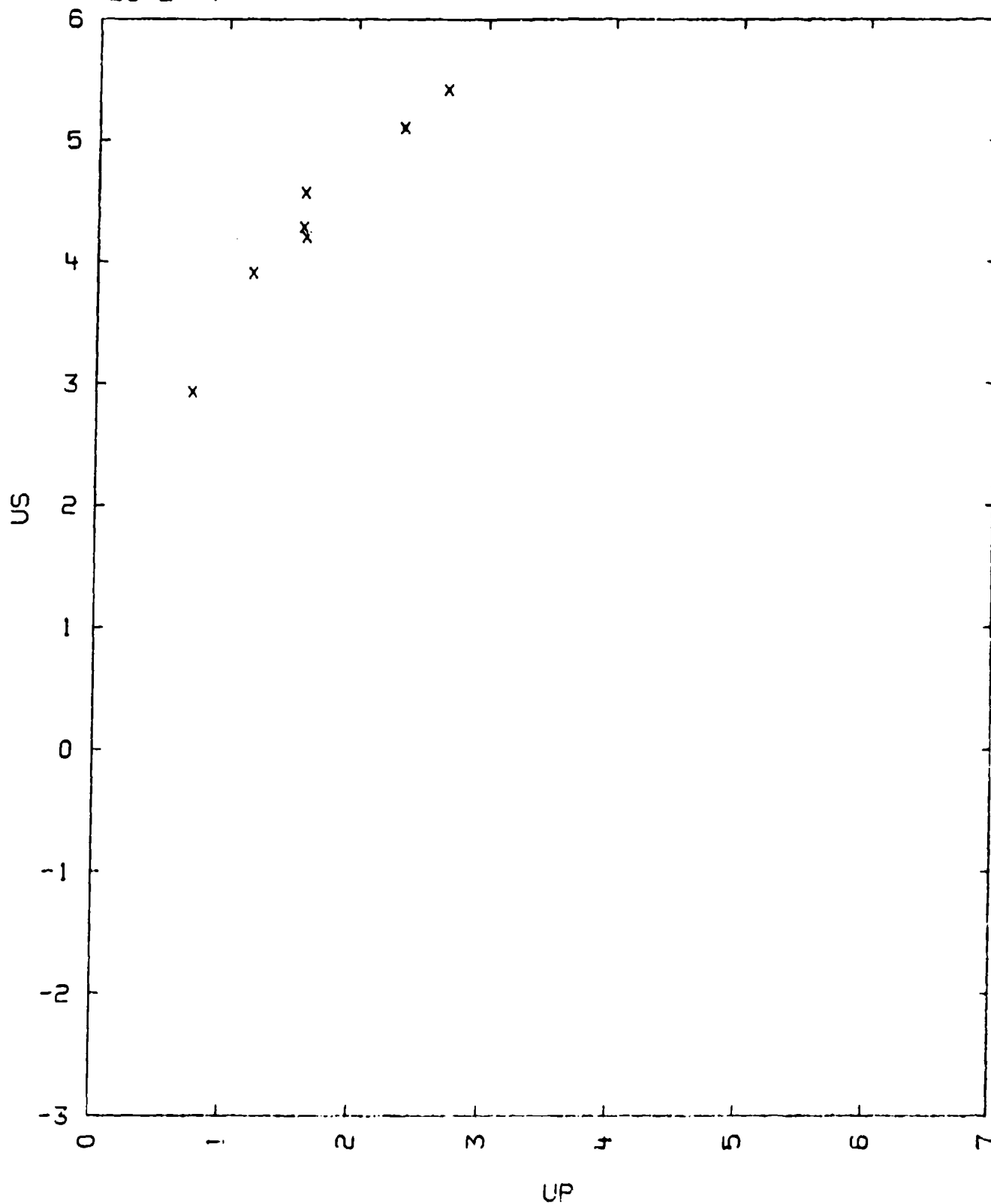
| RH00  | US   | UP   | P    | V/V0 |
|-------|------|------|------|------|
| 1.30  | 2.93 | 0.75 | 29.  | 0.74 |
| 1.30  | 3.90 | 1.21 | 61.  | 0.69 |
| 1.30  | 4.28 | 1.59 | 98.  | 0.63 |
| 1.345 | 4.20 | 1.62 | 92.  | 0.61 |
| 1.30  | 4.56 | 1.61 | 96.  | 0.65 |
| 1.30  | 5.10 | 2.36 | 156. | 0.54 |
| 1.30  | 5.42 | 2.69 | 190. | 0.52 |

$$US = 1.344 + 2.44 \cdot UP - 0.351 \cdot UP^2 \text{ KM/SEC.}$$

## COMMENTS:

- 1) SOURCE: MAY, R. P. AND KINSEY, C. H.  
SANDIA CORPORATION REPORT, SC-TM-67-737, OCT. 1967  
SANDIA LABORATORY, ALBUQUERQUE, NEW MEXICO, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION TECHNIQUE B
- 3) U.S. POLYMERIC FM 5215  
UNION CARBIDE VYB-105-1/5 CARBON YARN, UNIDIRECTIONAL, PARALLEL WOUND FIBERS  
EC 201 RESIN, 38 WT PERCENT PRIOR TO PYROLYSIS  
RESULTING MATERIAL IS SLIGHTLY POROUS
- 4) CL DETERMINED PERPENDICULAR TO LAMINATIONS BY T. GUESS SANDIA LABORATORY, ALBUQUERQUE, NEW MEXICO, PRIVATE COMMUNICATION.

TABLE I  
CARBON PHENOLIC, FILAMENT WOUND AND PYROLISED  
23-2 ?



$V_0 = 0.835 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KBAR.

TABLE

| RH00  | US   | UP   | P    | $V/V_0$ |
|-------|------|------|------|---------|
| 1.198 | 6.48 | 2.38 | 185. | 0.633   |
| -     | 6.48 | 2.36 | 183. | 0.636   |
| -     | 5.82 | 1.83 | 128. | 0.686   |
| -     | 5.73 | 1.90 | 130. | 0.668   |
| -     | 5.33 | 1.52 | 97.  | 0.715   |
| -     | 4.69 | 1.19 | 66.3 | 0.746   |
| -     | 4.07 | 0.78 | 38.0 | 0.808   |
| -     | 3.70 | 0.60 | 26.6 | 0.838   |

$US = 2.85 + 1.55 \cdot UP \text{ KM/SEC.}$   
 $SIG.US = 0.09 \text{ KM/SEC.}$

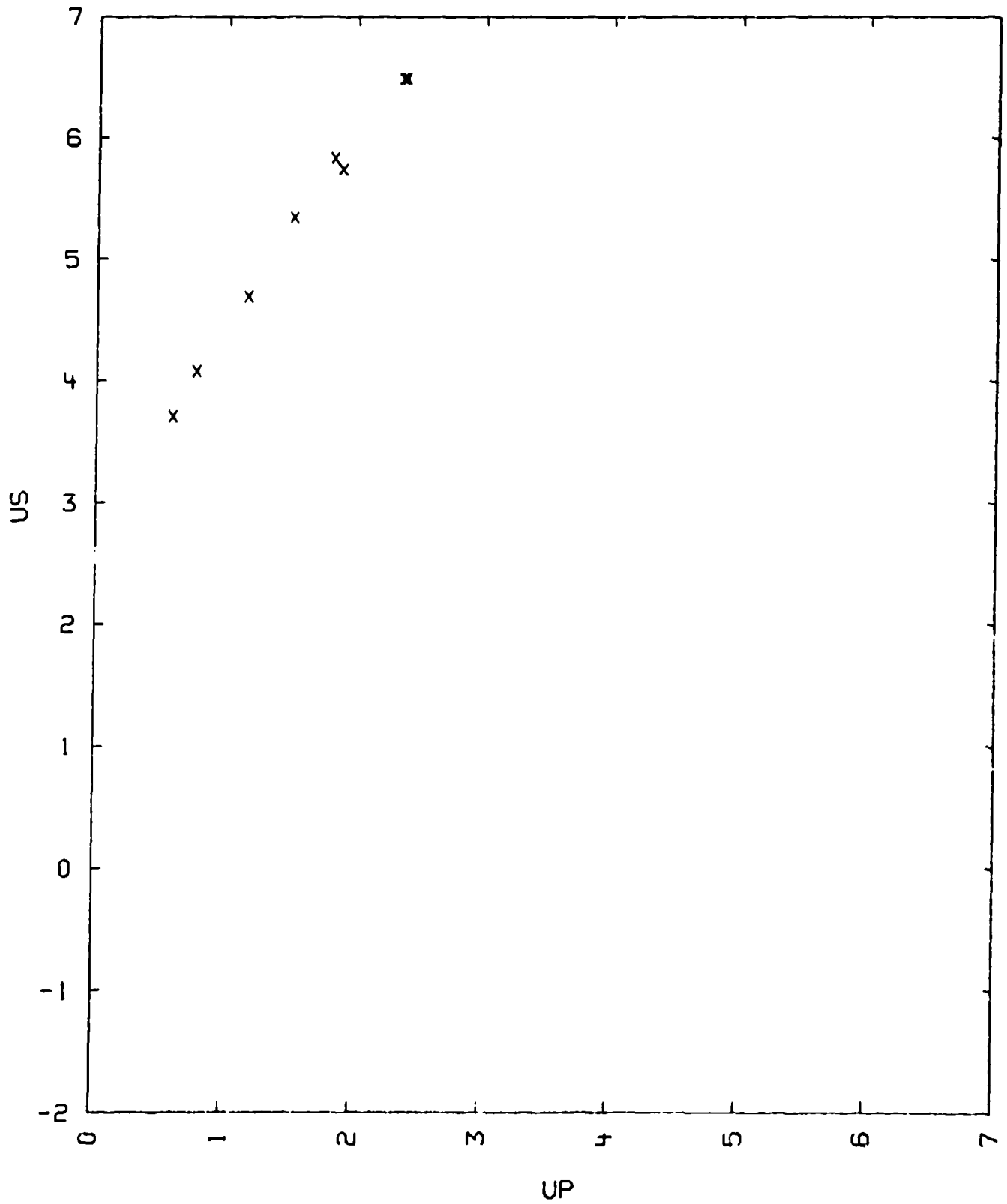
COMMENTS:

- 1) SOURCE: HAUVER, G. E. AND MELANI, A.  
PRIVATE COMMUNICATION, JAN. 1969.  
BALLISTICS RES. LAB., ABERDEEN PROVING GROUNDS  
MARLAND, USA.
- 2) EXPERIMENTAL TECHNIQUE: H  
DATA REDUCTION TECHNIQUE: B, STANDARDS AL AND PLEXIGLAS.
- 3) A PLEXIGLAS DISC (WITH  $US = 2.702 + 1.544 \cdot UP \text{ KM/SEC}$  AND  $RH00 = 1.18$ )  
WAS USED TO DETERMIN THE LOCATION OF THE AL CROSS CURVE IN THE P VS.  
UP PLANE NEEDED FOR THE ANALYSIS
- 4) RESIN PURCHASED IN EARLY 1968

TABLE I

EPOXY ARMSTRONG C-7 - ACTIVATOR A

23-18-2-1---1 ?



23-18-2-1---2 ?  
EPOXY ARMSTRONG C-7 - ACTIVATOR R

$V_0 = 0.830 \text{ CC/G}$

THE TABLE LISTS DENSITY IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KBAR.

TABLE

| RH00  | US   | UP   | P    | V/V0  |
|-------|------|------|------|-------|
| 1.205 | 6.50 | 2.35 | 184. | 0.638 |
| -     | 6.46 | 2.45 | 191. | 0.621 |
| -     | 6.46 | 2.42 | 188. | 0.625 |
| -     | 5.70 | 1.94 | 133. | 0.660 |
| -     | 5.38 | 1.66 | 108. | 0.691 |
| -     | 5.24 | 1.53 | 96.6 | 0.708 |
| -     | 4.64 | 1.18 | 66.0 | 0.746 |
| -     | 4.01 | 0.79 | 38.2 | 0.803 |
| -     | 3.69 | 0.60 | 26.6 | 0.837 |

$US = 2.83 + 1.52 \cdot UP \text{ KM/SEC}$

$SIG US = 0.07 \text{ KM/SEC.}$

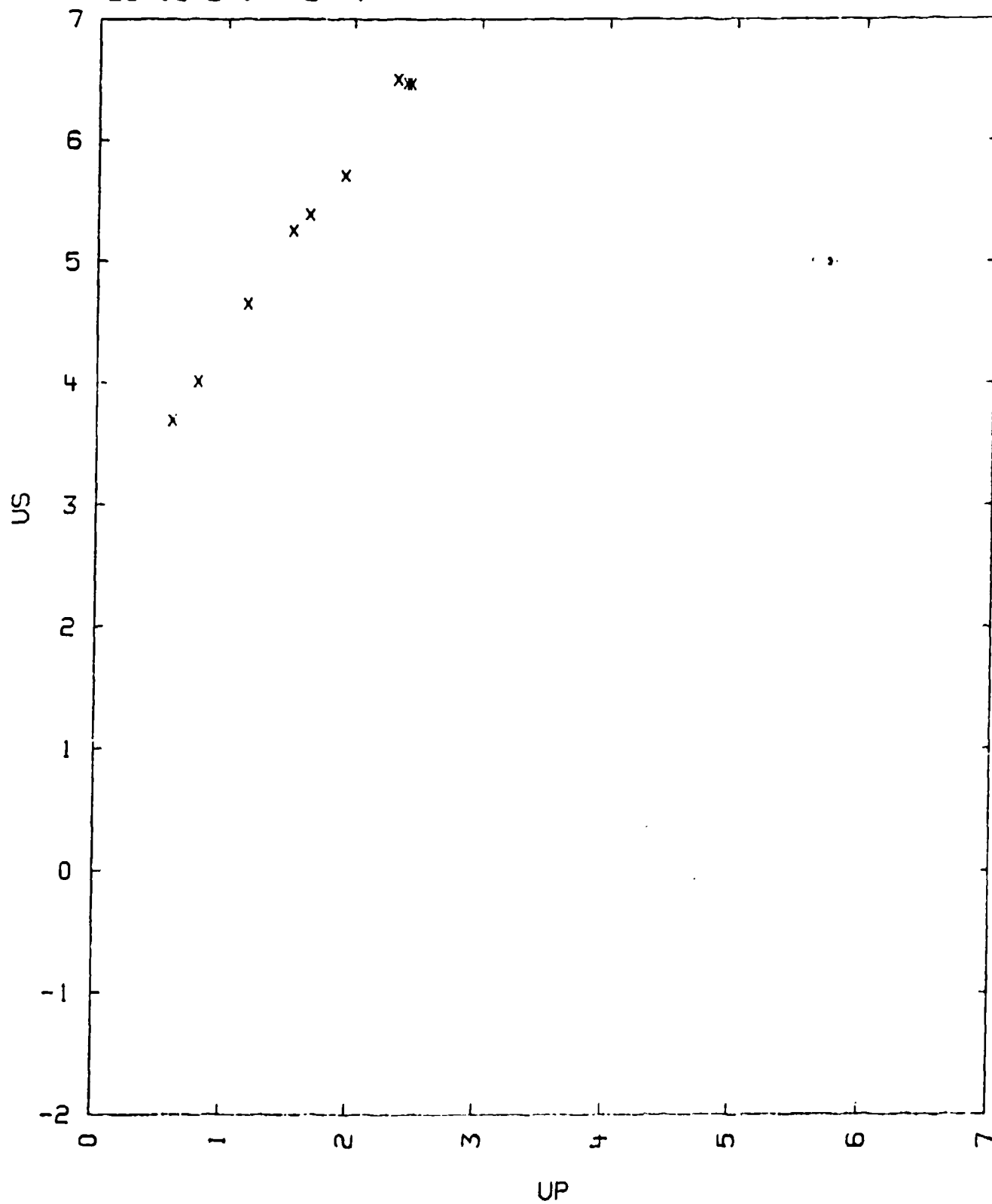
COMMENTS:

- 1) SOURCE: HAUVER, G. E. AND MELANI, A.  
PRIVATE COMMUNICATION (1969)  
BALLISTICS RESEARCH LABS., ABERDEEN PROVING GROUND, MARYLAND.
- 2) EXPERIMENTAL TECHNIQUE: H  
DATA REDUCTION TECHNIQUE: B, STANDARDS AL AND PLEXIGLAS.
- 3) A PLEXIGLAS DISC (WITH  $US = 2.702 + 1.544 \cdot UP \text{ KM/SEC}$  AND  $RH00 = 1.18$ )  
WAS USED TO DETERMINE THE LOCATION OF THE AL CROSS CURBE IN THE P VS.  
UP PLANE NEEDED FOR THE ANALYSIS
- 4) RESIN PURCHASED IN EARLY 1968

TABLE I

EPOXY ARMSTRONG C-7 - ACTIVATOR R

23-18-2-1---2 ?





23-10-2(2-1-3) ?  
EXON

POLYVINYLCHLORIDE       $(-CH_2)C-Cl(H)-n$       NOTE 4  
PLASTISIZERS                ?  
FILLERS                        ?

$V_0 = 0.5947 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |      |
|------------------|------|------|------|--------|--------------------|------|
| RHO0             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |      |
| 1.682            | 3.99 | 1.19 | 80.  | 0.7018 | 2024 AL            | 6.44 |
| 1.681            | 3.94 | 1.22 | 81.  | 0.6904 | 2024 AL            | 6.47 |
| 1.681            | 4.48 | 1.55 | 117. | 0.6540 | 2024 AL            | 6.82 |
| 1.681            | 5.33 | 2.02 | 181. | 0.6210 | 2024 AL            | 7.42 |

$US = 1.952 + 1.660 \cdot UP \text{ KM/SEC}$

$SIGMA \text{ US} = 0.063 \text{ KM/SEC}$

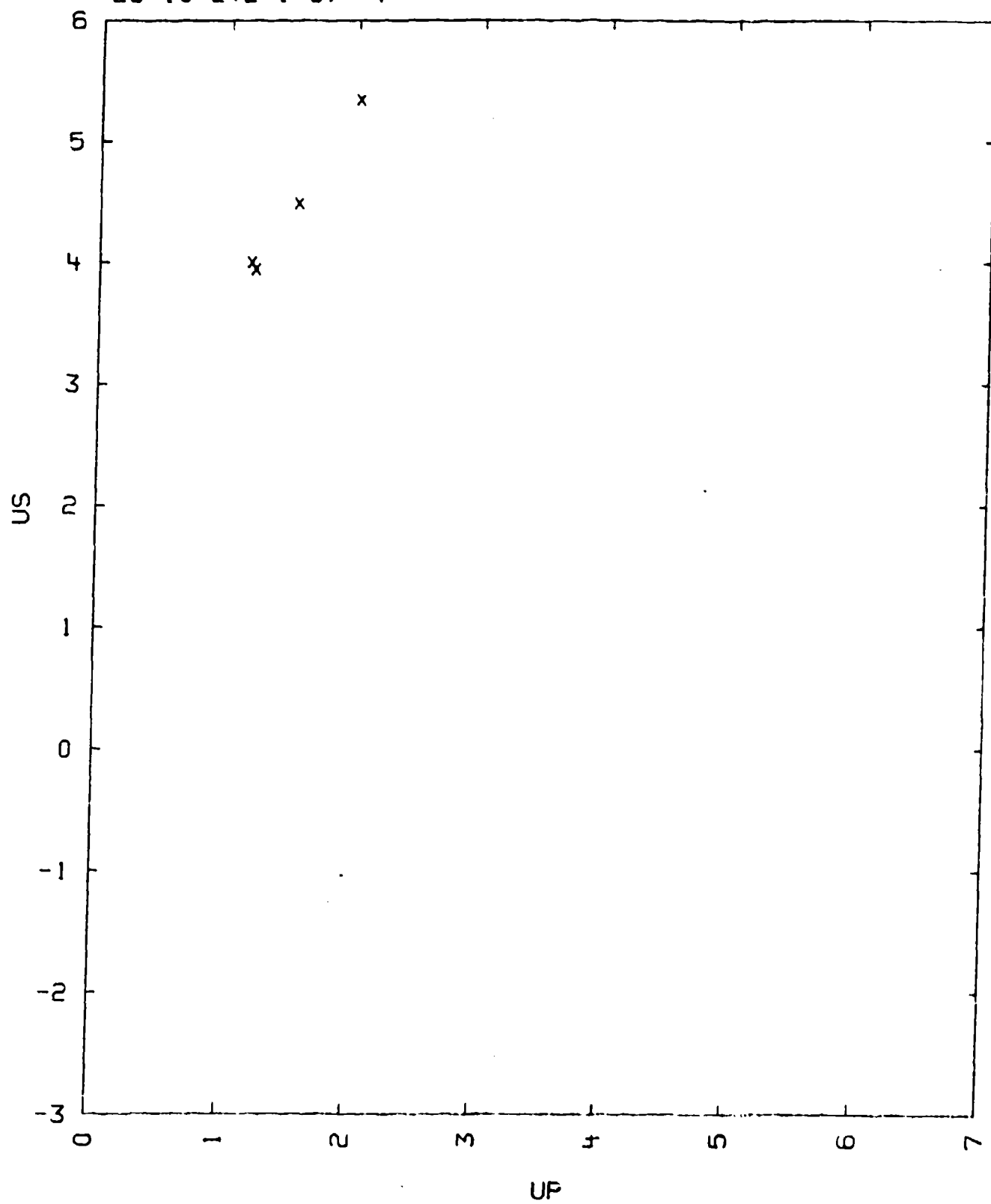
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3)  $V(DP/DE) = 0.87$
- 4) THE ABOVE MATERIAL IS DEFINED AS PVC (POLYVINYLCHLORIDE) WHICH BY  
1966 SPECS NEED ONLY BE 51 PERCENT PURE TO BE SO DESIGNATED.  
RIGID UNFILLED PVC CONTAINS A MINIMUM OF LUBRICANT OR SOLVENT AND  
HAS A DENSITY RANGE OF 1.35 - 1.45 G/CC. THE ABOVE DENSITY IMPLIES  
A SIGNIFICANT AMOUNT OF FILLER, PERHAPS TI-03 CA-03 AND CARBON BLACK  
PRIVATE COMMUNICATION, PHILIP G. FLEMING, LLL

TABLE I

EXON

23-10-2(2-1-3) ?



94-29-28-24--29-19-1---1 7

GLASS CLOTH 101 LAMINATE WITH ALUMINUM PHOSPHATE RESIN

## GLASS CLOTH:

|        |      |             |
|--------|------|-------------|
| SI-02  | 53.5 | WT. PERCENT |
| CA-02  | 20.4 | -           |
| AL2-03 | 14.9 | -           |
| B2-03  | 5.   | -           |

RESIN AL-P-04

V0 = 0.500 TO 0.584 CC/G

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR.

TABLE

| RH00  | US   | UP   | P    | V/V0 | MET |
|-------|------|------|------|------|-----|
| 2.00  | 3.18 | 0.87 | 55.  | 0.73 | A   |
| 2.00  | 3.48 | 1.15 | 80.  | 0.67 | -   |
| 2.00  | 4.84 | 2.2  | 209. | 0.54 | -   |
| 2.00  | 5.10 | 2.33 | 237. | 0.54 | -   |
| 1.869 | 3.10 | 0.85 | 49.  | 0.73 | -   |
| 1.869 | 3.84 | 1.71 | 123. | 0.56 | -   |
| 1.869 | 4.49 | 2.18 | 183. | 0.51 | -   |
| 1.869 | 4.85 | 2.47 | 224. | 0.49 | -   |
| 1.869 | 2.90 | 0.86 | 55.  | 0.70 | F   |
| 1.869 | 3.66 | 1.58 | 108. | 0.57 | -   |
| 1.869 | 4.02 | 1.78 | 134. | 0.56 | -   |
| 1.869 | 4.79 | 2.34 | 210. | 0.51 | -   |
| 1.711 | 2.49 | 0.73 | 31.  | 0.71 | A   |
| 1.711 | 2.53 | 0.89 | 39.  | 0.65 | F   |
| 1.711 | 4.60 | 2.45 | 193. | 0.47 | -   |
| 1.711 | 4.64 | 2.48 | 197. | 0.47 | -   |

US = 2.014 + 1.305\*UP KM/SEC., FOR RH00 = 2.00 G/CC.

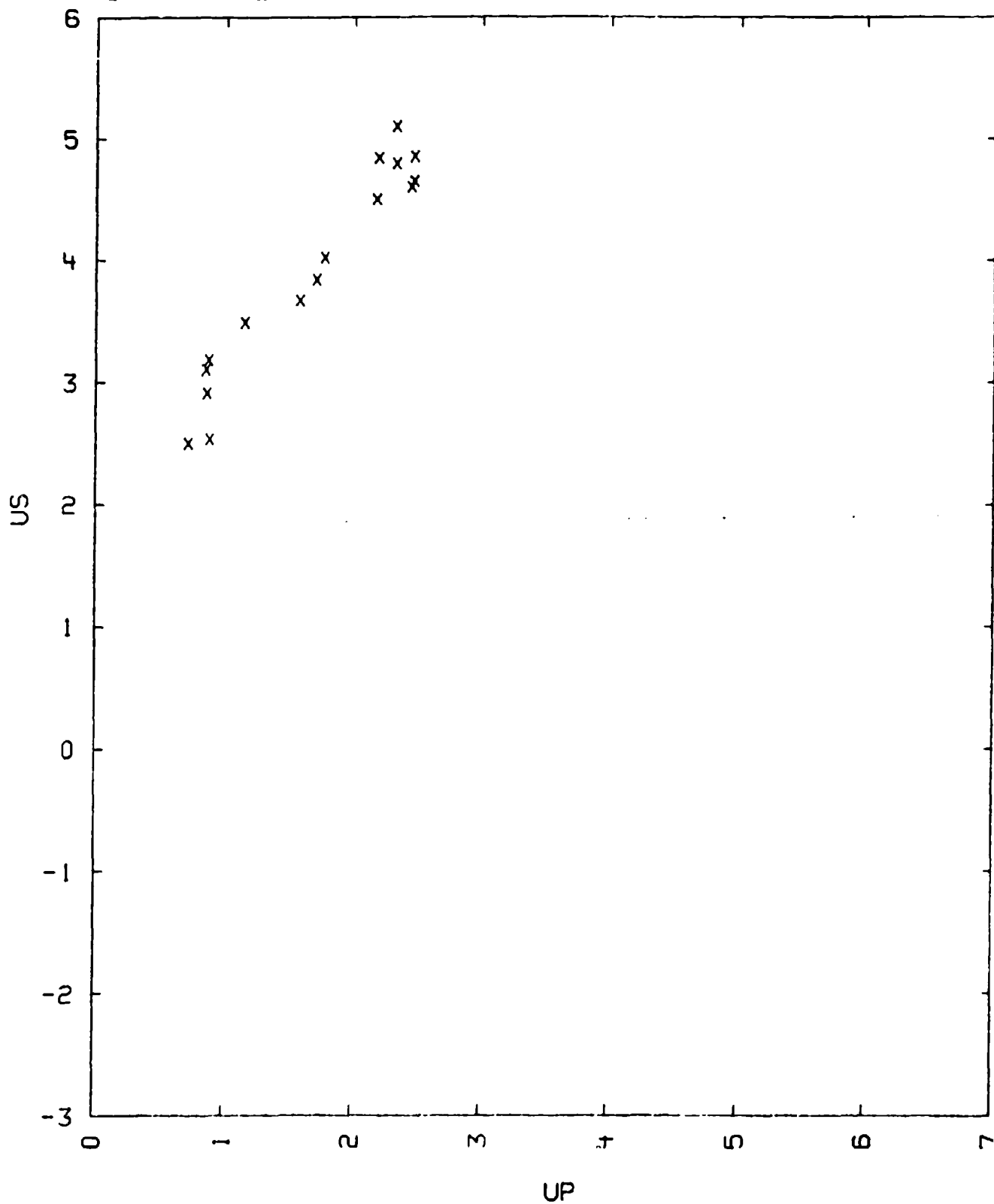
US = 1.919 + 1.190\*UP KM/SEC., FOR RH00 = 1.869 G/CC.

US = 1.485 + 1.270\*UP KM/SEC., FOR RH00 = 1.711 G/CC.

## COMMENTS:

- 1) SOURCE: MAY, R. P. AND KINSEY, C. H.  
SANDIA CORPORATION REPORT, SC-DR-67-2958, MARCH 1968  
SANDIA LABORATORY, ALBUQUERQUE, NEW MEXICO, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE A AND F  
DATA REDUCTION METHOD B
- 3) THE SHOCK DIRECTION WAS NORMAL TO THE LAMINATIONS.  
NO TWO WAVE SYSTEMS WERE OBSERVED.

TABLE 1  
GLASS CLOTH 181 LAMINATE WITH ALUMINUM PHOSPHATE R  
94-29-28-24--29-19-1---1 ?



23-18-2-1-- ?  
MELMAC

MELAMINEFORMALDEHYDE  
MELAMINE (C-N)3-(N-H2)3  
FORMALDEHYDE H2-C-O  
FILLER

$V_0 = 0.703 - 0.009 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |      |
|------------------|------|------|------|--------|--------------------|------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |      |
| 1.494            | 4.80 | 1.03 | 74.  | 0.7854 | 2024 AL            | 6.32 |
| 1.411            | 4.86 | 1.04 | 71.  | 0.7860 | 2024 AL            | 6.32 |
| 1.494            | 5.40 | 1.50 | 121. | 0.7222 | 2024 AL            | 6.80 |
| 1.494            | 5.31 | 1.52 | 121. | 0.7137 | 2024 AL            | 6.81 |
| 1.411            | 5.33 | 1.54 | 116. | 0.7111 | 2024 AL            | 6.80 |
| 1.411            | 5.13 | 1.56 | 113. | 0.6959 | 2024 AL            | 6.81 |
| 1.494            | 6.09 | 2.01 | 183. | 0.6700 | 2024 AL            | 7.33 |
| 1.411            | 6.00 | 2.05 | 174. | 0.6583 | 2024 AL            | 7.33 |

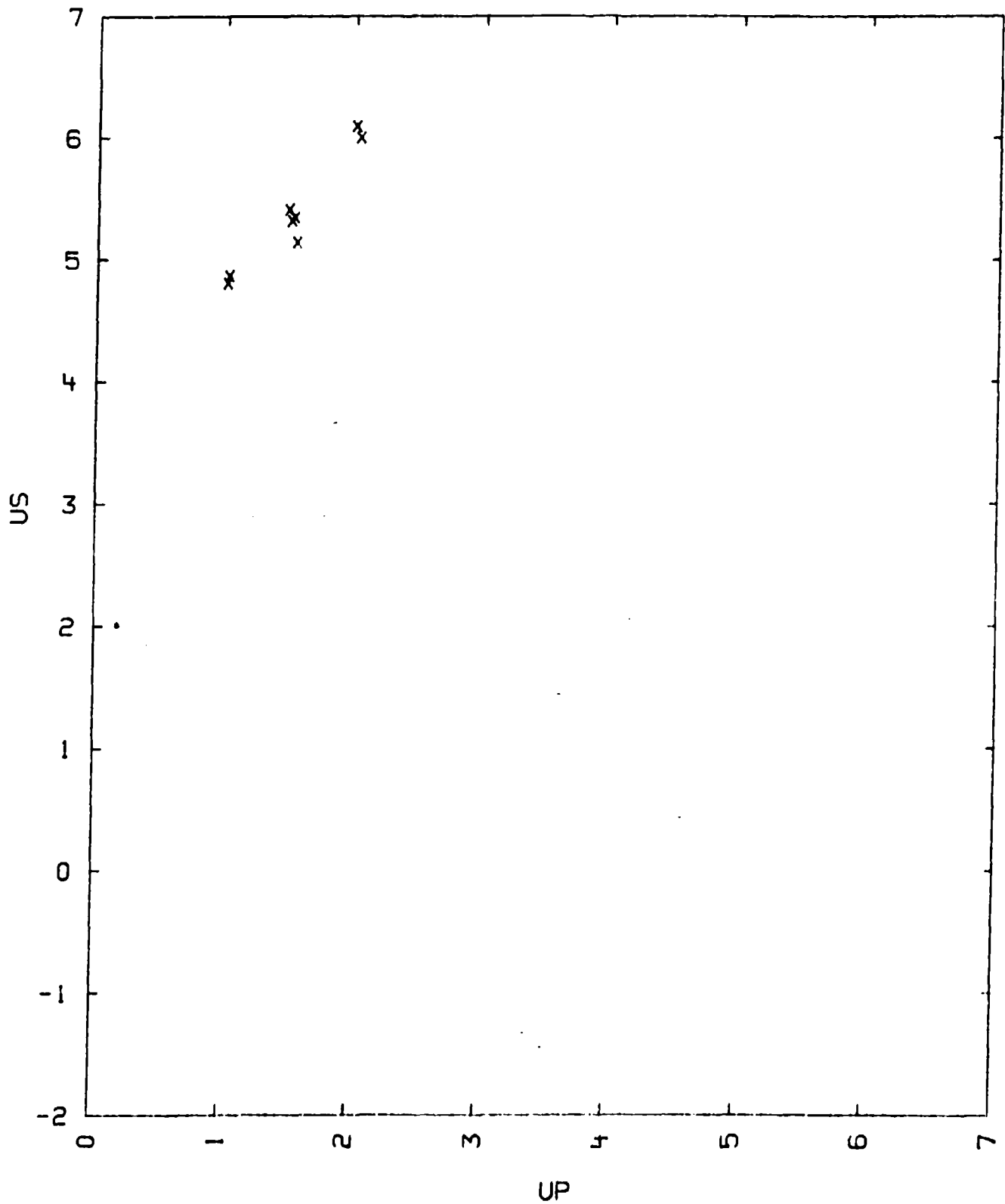
$US = 3.505 + 1.213 \cdot UP \text{ KM/SEC}$   
 $SIGMA \text{ US} = 0.137 \text{ KM/SEC}$

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES.  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) THE PRECISE COMPOSITION OF THIS SAMPLE IS NOT KNOWN
- 4)  $V(DP/DE) = 0.89$

TABLE 1

MELMAC  
23-18-2-1-- ?



$V_0 = 3.5 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |      |
|------------------|------|------|------|--------|--------------------|------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |      |
| 0.270            | 2.19 | 1.76 | 10.  | 0.1963 | 2024 AL            | 6.55 |
| 0.280            | 2.67 | 2.26 | 17.  | 0.1536 | 2024 AL            | 6.91 |
| 0.280            | 5.28 | 4.12 | 61.  | 0.2197 | 2024 AL            | 8.30 |
| 0.280            | 5.25 | 4.14 | 61.  | 0.2114 | 2024 AL            | 8.32 |
| 0.270            | 5.82 | 4.68 | 74.  | 0.1959 | 2024 AL            | 8.72 |
| 0.290            | 6.39 | 4.99 | 92.  | 0.2191 | 2024 AL            | 8.98 |
| 0.290            | 6.32 | 5.02 | 92.  | 0.2057 | 2024 AL            | 9.00 |
| 0.280            | 6.77 | 5.06 | 96.  | 0.2526 | 2024 AL            | 9.04 |
| 0.290            | 6.39 | 5.08 | 91.  | 0.2050 | 2024 AL            | 9.03 |
| 0.270            | 6.81 | 5.24 | 96.  | 0.2305 | 2024 AL            | 9.16 |
| 0.290            | 7.64 | 6.13 | 136. | 0.1976 | 2024 AL            | 9.86 |
| 0.280            | 8.29 | 6.19 | 144. | 0.2533 | 2024 AL            | 9.32 |

$US = -.257 + 1.333 \cdot UP \text{ KM/SEC}$   
 $SIGMA US = 0.180 \text{ KM/SEC}$

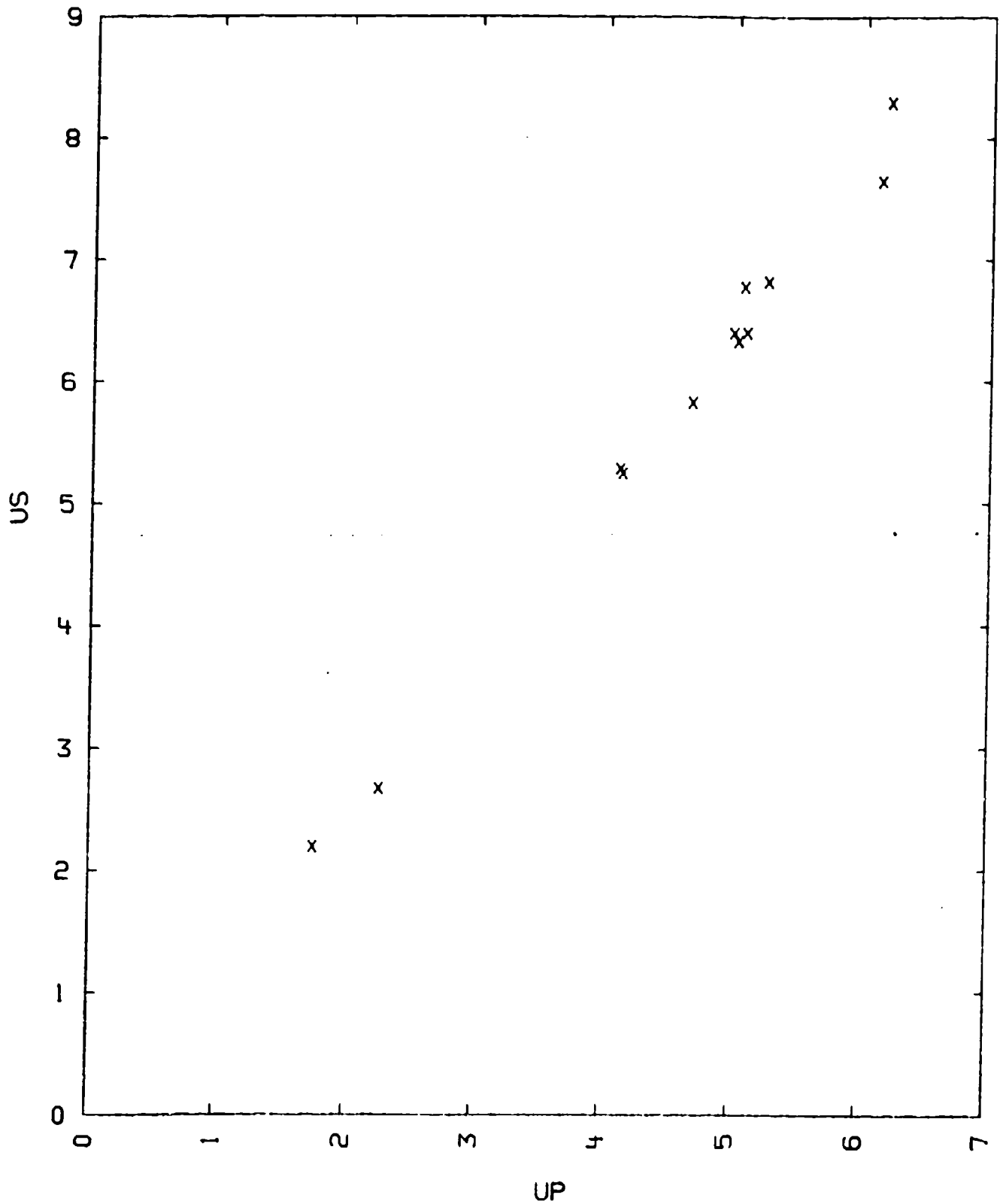
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES, HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B
- 3) MIN-K-2000 IS A VIBROUS INSULATING MATERIAL FROM THE JOHNS MANVILLE CO. THE CHEMICAL COMPOSITION IS UNDETERMINED

TABLE I

MIN-K-2000

24-1 ?





23-18-2-1 ?  
POLYRUBBER

$V_0 = 0.9814 - 1.30 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE I

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |      |
|------------------|------|------|------|--------|--------------------|------|
| RH00             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |      |
| 1.012            | 3.23 | 1.28 | 42.  | 0.6037 | 2024 AL            | 6.36 |
| 1.014            | 3.33 | 1.30 | 44.  | 0.6096 | 2024 AL            | 6.38 |
| 1.015            | 4.12 | 1.73 | 72.  | 0.5801 | 2024 AL            | 6.78 |
| 1.009            | 4.06 | 1.78 | 73.  | 0.5616 | 2024 AL            | 6.81 |
| 1.019            | 5.19 | 2.30 | 122. | 0.5568 | 2024 AL            | 7.33 |

$US = 0.854 + 1.865 \cdot UP \text{ KM/SEC}$   
 $SIGMA US = 0.080 \text{ KM/SEC}$

TABLE II

| -----SAMPLE----- |      |      |     |        | -----STANDARD----- |      |
|------------------|------|------|-----|--------|--------------------|------|
| RH00             | US   | UP   | P   | V/V0   | MATERIAL US(ST)    |      |
| 0.784            | 2.78 | 1.37 | 30. | 0.5072 | 2024 AL            | 6.37 |
| 0.771            | 2.80 | 1.38 | 30. | 0.5071 | 2024 AL            | 6.38 |
| 0.778            | 3.66 | 1.84 | 52. | 0.4973 | 2024 AL            | 6.78 |
| 0.775            | 3.64 | 1.90 | 54. | 0.4780 | 2024 AL            | 6.82 |
| 0.775            | 4.34 | 2.51 | 84. | 0.4217 | 2024 AL            | 7.33 |
| 0.775            | 4.56 | 2.52 | 89. | 0.4474 | 2024 AL            | 7.36 |
| 0.769            | 4.46 | 2.54 | 87. | 0.4305 | 2024 AL            | 7.37 |

$US = 0.891 + 1.423 \cdot UP \text{ KM/SEC}$   
 $SIGMA US = 0.105 \text{ KM/SEC}$

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B  
DATA REDUCTION TECHNIQUE: B (STANDARD BASE PLATE AS SHOWN)

TABLE I

POLYRUBBER  
23-18-2-1 ?

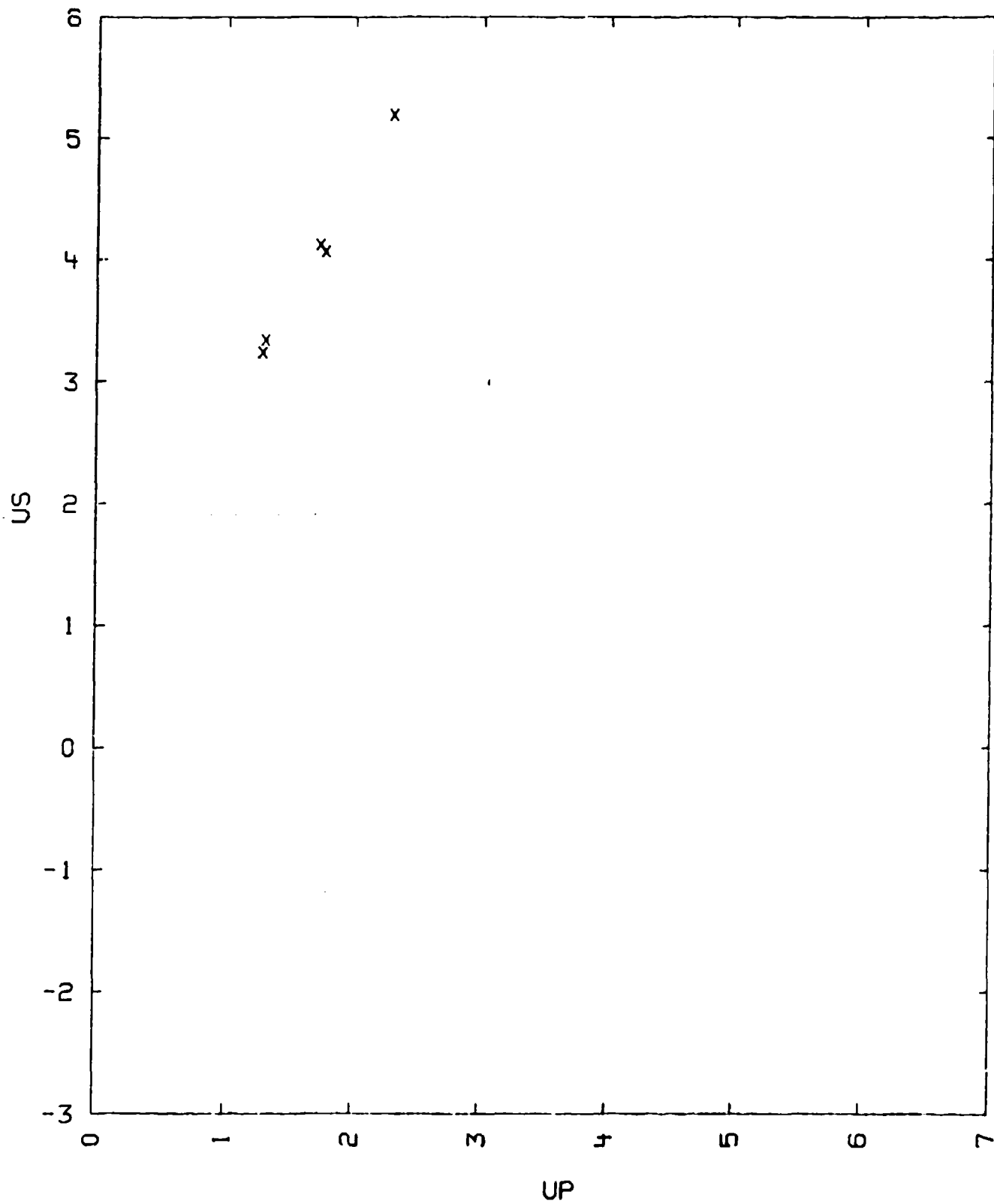
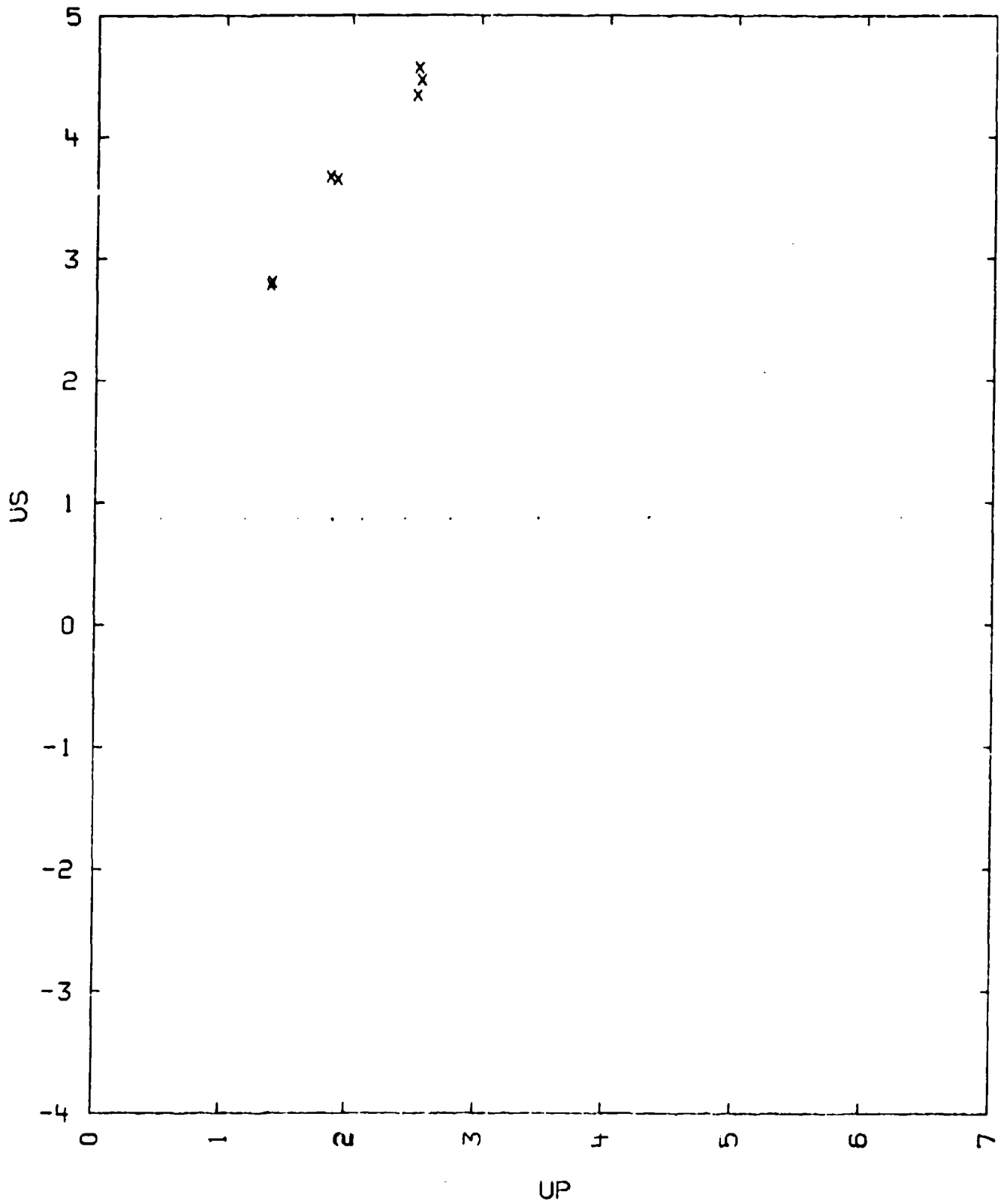


TABLE II

POLYRUBBER  
23-18-2-1 ?



29-24-1 ?  
PUMICE, MONO CRATER

SI-02 75.7 VOLUME PERCENT  
AL2-O3 13.0 - -  
VA2-O 4.0 - -  
K2-O 4.5 - -  
H2-O+ 0.71 - -  
FE2-O3 0.626 - -  
FE-O 0.44 - -  
POROSITY (CALCULATED) 78 PERCENT

V01 = 0.3937 CC/G  
V0 = 0.1818 CC/G

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC. VELOCITIES ARE IN KM/SEC  
AND PRESSURE IN KILOBARS.

TABLE

| RH00 | US   | UP   | P   | V/V0  |
|------|------|------|-----|-------|
| 0.55 | 2.77 | 2.32 | 35  | 0.166 |
| -    | 3.45 | 2.96 | 56  | 0.144 |
| -    | 6.59 | 5.31 | 192 | 0.195 |
| -    | 7.81 | 6.19 | 266 | 0.208 |

US =

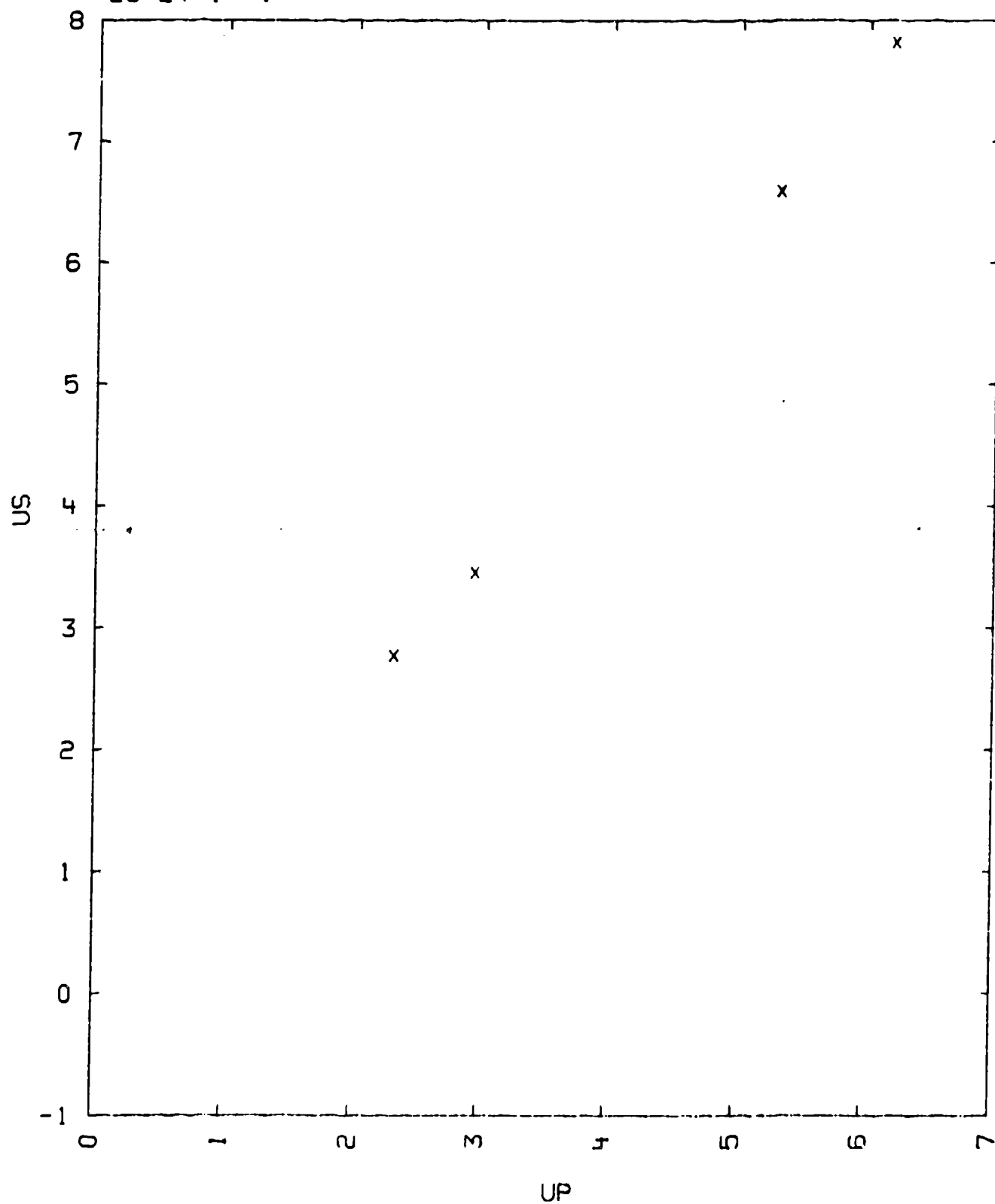
## COMMENTS:

- 1) SOURCE: JONES, A. H., ISBELL, W. M., SHIPMAN, F. N., PERKINS, R. D.,  
GREEN, S. J. AND MAIDEN, C. J.  
REPORT MSL-68-9; CONTRACT NASA 2-3927  
MATERIALS AND STRUCTURE LABORATORY  
GENERAL MOTORS TECHNICAL CENTER, MICHIGAN, USA 48090
- 2) EXPERIMENTAL TECHNIQUE A:  
DATA REDUCTION TECHNIQUE A: ASSUMING THE PARTICLE VELOCITY (UP) IS  
EQUAL TO ONE HALF OF THE PROJECTILE  
IMPACT VELOCITY.  
STANDARD MATERIAL USED WHERE OFHC COPPER AND FANSTEEL-77 ALLOY. THE  
COPPER STANDARD US-UP HUGONOT RELATIONSHIP IS  
GIVEN BY THE FOLLOWING EQUATION:  
$$US = 3.96 + 1.49 \cdot UP \text{ KM/SEC}$$
  
WHERE RH00 = 8.93 G/CC  
FOR THE FANSTEEL US-UP HUGONOT RELATIONSHIP SEE  
MATERIAL 53--39--36---2.
- 3) THESE PRESSURES WERE ACHIEVED BY USING A TWO-STAGE LIGHT GAS GUN.  
THE PROJECTILE IMPACT VELOCITY AND TILT WERE MEASURED BY FLASH  
X-RAYS. THE IMPACTOR VELOCITY MEASURING SYSTEM CONSISTED OF MEASURING  
THE INTERVAL TIME BETWEEN TWO SHORT DURATION FLASH X-RAYS LOCATED  
JUST AHEAD OF THE TARGET. THE IMPACT VELOCITY IS MEASURED ACCURATE  
TO 0.2 PERCENT.
- 4) THE MEASURED SHOCK VELOCITY (US) IS A AVERAGE VALUE THROUGH THE  
SPECIMEN. FOR THE SAMPLES OF THE SIZE USED IN THESE EXPERIMENTS

THERE MAY BE A NON-LINEAR SHOCK PROPAGATION DUE TO THE HIGH POROSITY WHICH WOULD PRODUCE IN ERROR IN THE US MEASUREMENTS.

TABLE I

PUMICE, MONO CRATER  
29-24-1 ?



24-1--23-18-2-1(7)---1  
QUARTZ PHENOLIC, FILAMENT WOUND

FIBERS:  
SI-02 99.5 PERCENT  
PHENOLIC

$V_0 = 0.536 \text{ CC/G.}$

THE TABLE LISTS DENSITY IN G/CC., VELOCITY IN KM/SEC. AND PRESSURE IN KBAR.

TABLE

| RH00  | US    | UP    | P     | V/V0  |
|-------|-------|-------|-------|-------|
| 1.834 | 4.104 | 0.696 | 52.4  | 0.830 |
| 1.840 | 3.77  | 0.78  | 54.0  | 0.79  |
| 1.875 | 4.05  | 0.82  | 63.0  | 0.80  |
| 1.86  | 4.156 | 1.083 | 83.7  | 0.739 |
| 1.861 | 4.40  | 1.09  | 89.0  | 0.75  |
| 1.86  | 4.51  | 1.423 | 119.4 | 0.684 |
| 1.84  | 4.678 | 1.538 | 132.4 | 0.671 |
| 1.838 | 4.58  | 1.56  | 131.0 | 0.66  |
| 1.840 | 4.60  | 1.63  | 137.0 | 0.65  |
| 1.870 | 4.72  | 1.73  | 153.0 | 0.63  |
| 1.856 | 4.95  | 2.11  | 194.0 | 0.57  |
| 1.840 | 5.02  | 2.12  | 196.0 | 0.58  |
| 1.86  | 5.030 | 2.143 | 200.6 | 0.573 |
| 1.86  | 5.155 | 2.358 | 226.1 | 0.543 |
| 1.880 | 5.20  | 2.36  | 231.0 | 0.55  |
| 1.840 | 5.21  | 2.43  | 233.0 | 0.53  |

$US = 3.39 + 0.77 \cdot UP \text{ KM/SEC.}$

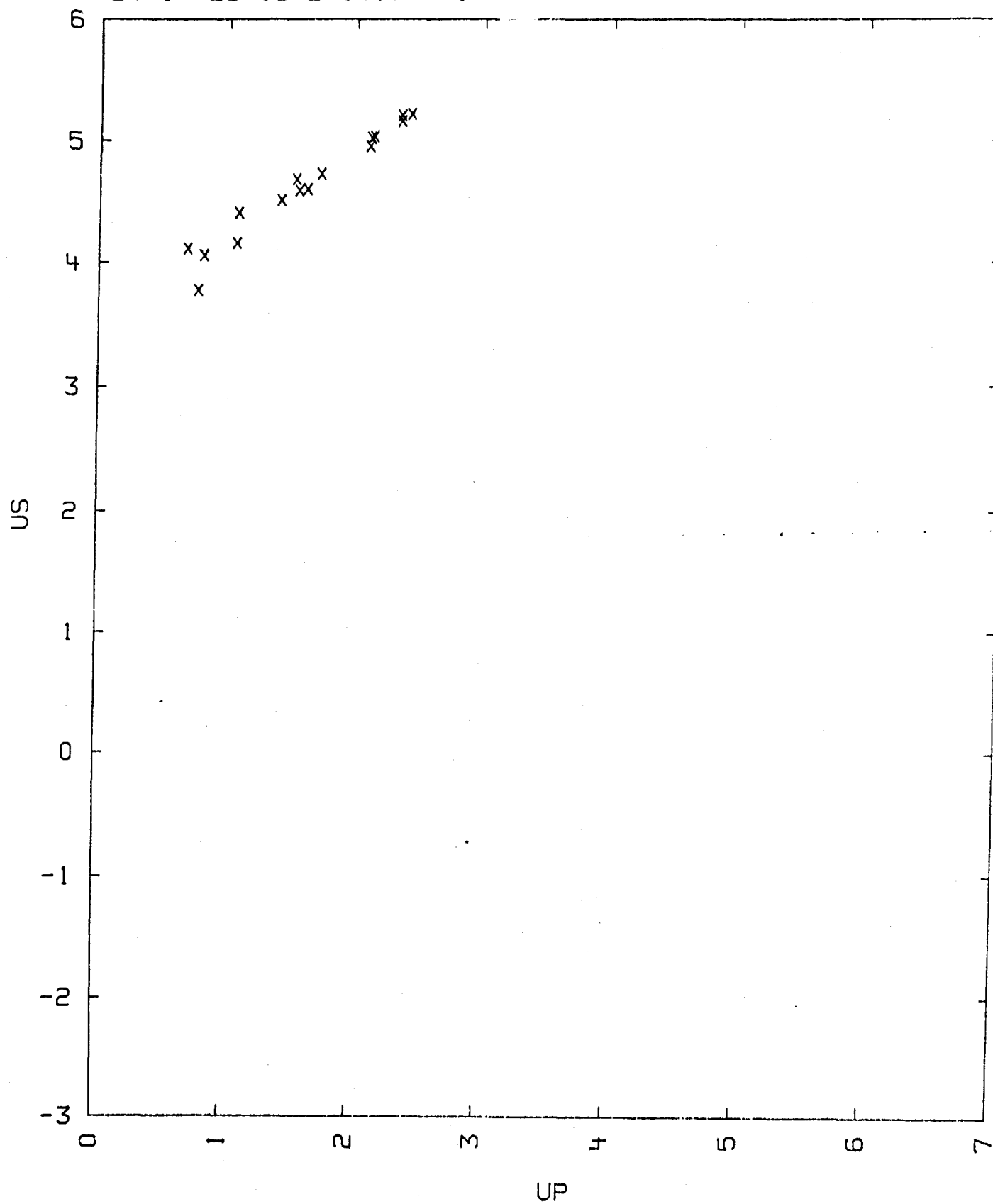
COMMENTS:

- 1) SOURCE: MAY, R. P. AND KINSEY  
SANDIA CORPORATION REPORT, SC-1M-67-642, SEPT. 1967  
SANDIA LABORATORY, ALBUQUERQUE, NEW MEXICO, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE A  
DATA REDUCTION TECHNIQUE B
- 3) 20 END QUARTZ ROVING  
AH-2 PHENOLIC RESIN 20 PERCENT BY WEIGHT  
FILAMENTS WOUND PARALLEL TO EACH OTHER AND BEING UNIDIRECTIONAL  
RESULT IN ANISOTROPIC PROPERTIES.

TABLE I

QUARTZ PHENOLIC, FILAMENT WOUND

24-1--23-18-2-1(?)---1





24-1---23-18-2-1(?)---2  
QUARTZ PHENOLIC

QUARTZ:  
PHENOLIC:

$V_0 = 0.556$

THE TABLE LISTS  $\rho_{H0}$  IN G/CC, VELOCITIES IN KM/SEC AND P IN KBARS.  
CU= COPPER, FS= FANSTEEL, WF= WEIGHTING FACTOR AND DIR= DIRECTION.  
PAR MEANS THAT THE QUARTZ FIBRES ARE PARALLEL AND PERP, THAT THEY ARE PERPENDICULAR TO THE PLANE OF THE SHOCK FRONT.

TABLE

| - - - - - SAMPLE - - - - - |             |        |       |       | - - IMPACTOR - - |     |       |    |
|----------------------------|-------------|--------|-------|-------|------------------|-----|-------|----|
| DIR                        | $\rho_{H0}$ | US     | UP    | P     | V/V <sub>0</sub> | MAT | U     | WF |
| PAR                        | 1.80        | 4.479  | 1.341 | 108.  | .7006            | CU  | 1.619 | 0  |
| PAR                        | 1.80        | 5.248  | 2.164 | 204.  | .5875            | CU  | 2.654 | 0  |
| PAR                        | 1.80        | 5.343  | 2.522 | 243.  | .5281            | CU  | 3.088 | 1  |
| PAR                        | 1.80        | 7.160  | 3.793 | 489.  | .4703            | CU  | 4.798 | 1  |
| PAR                        | 1.80        | 10.978 | 6.635 | 1311. | .3956            | FS  | 7.985 | 1  |
| PERP                       | 1.80        | 4.357  | 1.172 | 92.   | .7310            | CU  | 1.412 | 0  |
| PERP                       | 1.80        | 5.211  | 1.991 | 187.  | .6179            | CU  | 2.444 | 0  |
| PERP                       | 1.80        | 5.234  | 2.015 | 190.  | .6149            | CU  | 2.475 | 0  |
| PERP                       | 1.80        | 5.735  | 2.750 | 284.  | .5205            | CU  | 3.397 | 1  |
| PERP                       | 1.80        | 5.733  | 2.772 | 286.  | .5165            | CU  | 3.423 | 0  |
| PERP                       | 1.80        | 7.032  | 3.738 | 473.  | .4685            | CU  | 4.718 | 1  |

$US = 1.949 + 1.364 \cdot UP$  FOR UP ABOVE 2.3 KM/SEC  
 $SIG.US = 0.016$  KM/SEC.

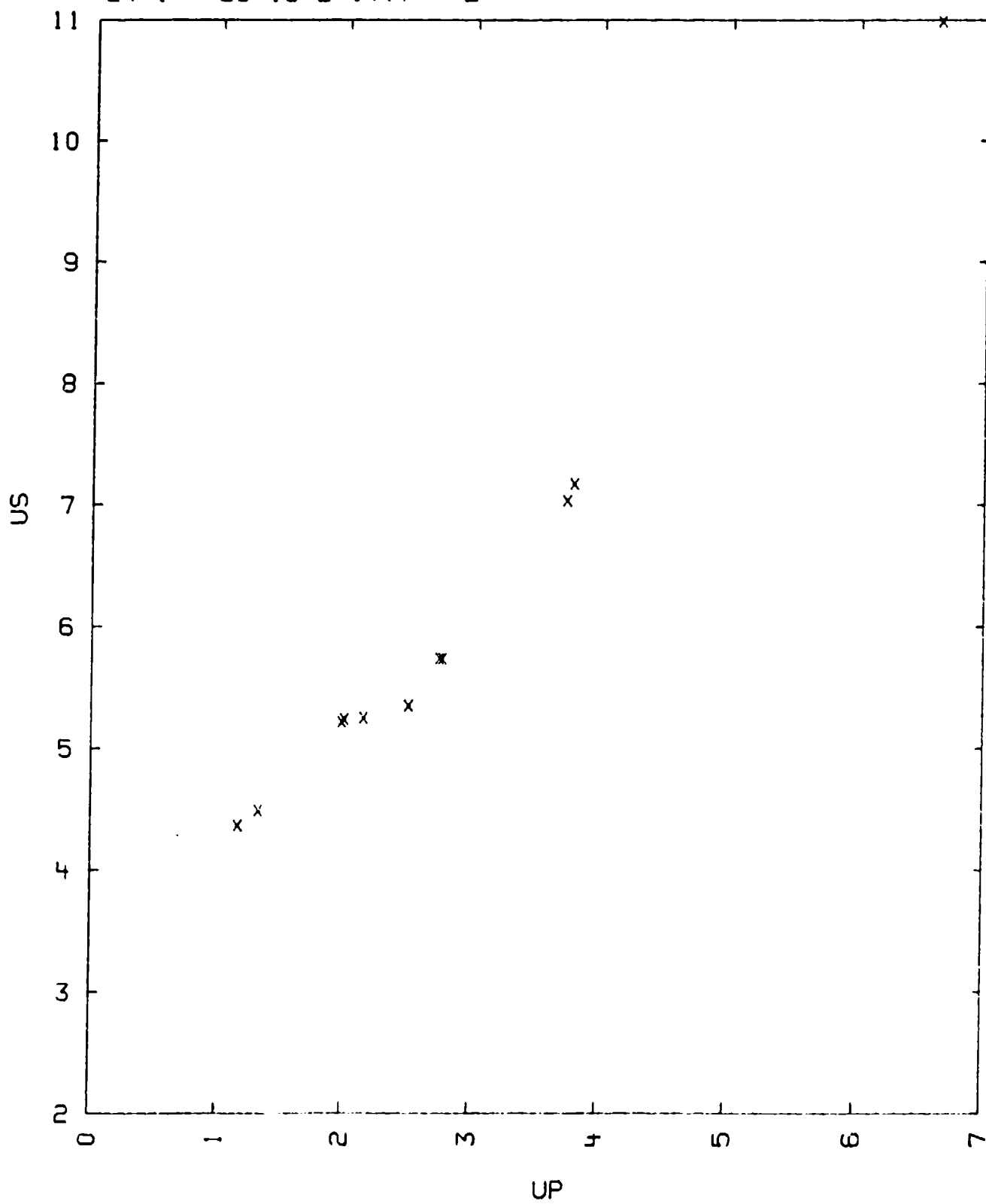
## COMMENTS:

- 1) SOURCE: ISBELL W.M., SHIPMAN F.H. AND JONES A.H.  
HUGONOT EQUATION OF STATE OF ELEVEN MATERIALS TO FIVE MBARS.  
MATERIALS SCIENCE LABORATORY REPORT: MSL-68-13
- 2) EXPERIMENTAL TECHNIQUE: A  
DATA REDUCTION METHOD: A
- 3) NOMINAL UNCERTAINTIES ARE:  $(SIG.US)/US = .005$  AND  $(SIG.U)/U = .005$   
THE UNCERTAINTY OF UP, P AND V/V<sub>0</sub> OF ENTRY 5 WERE 2, 2 AND 3 PERCENT RESPECTIVELY BECAUSE OF A SOMEWHAT HIGHER UNCERTAINTY IN THE PROJECTILE VELOCITY.

TABLE 1

QUARTZ PHENOLIC

24-1---23-18-2-1(?)---2



23-18-2-1 ?  
SELECTRON (POLYESTER)

$V_0 = 0.822 \text{ CC/G}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC. PRESSURE IN KILOBARS  
AND DENSITY IN G/CC.

TABLE

| -----SAMPLE----- |      |      |      |        | -----STANDARD----- |       |
|------------------|------|------|------|--------|--------------------|-------|
| RHOO             | US   | UP   | P    | V/V0   | MATERIAL US(ST)    |       |
| 1.219            | 4.23 | 1.14 | 59.  | 0.7305 | 2024 AL            | 6.33  |
| 1.215            | 4.28 | 1.26 | 66.  | 0.7056 | 2024 AL            | 6.44  |
| 1.215            | 4.61 | 1.34 | 75.  | 0.7093 | 2024 AL            | 6.53  |
| 1.215            | 5.02 | 1.64 | 100. | 0.6733 | 2024 AL            | 6.82  |
| 1.219            | 5.60 | 2.18 | 149. | 0.6107 | 2024 AL            | 7.34  |
| 1.216            | 6.68 | 3.08 | 250. | 0.5389 | 2024 AL            | 8.24  |
| 1.215            | 8.16 | 3.94 | 391. | 0.5172 | 2024 AL            | 9.16  |
| 1.215            | 9.45 | 5.09 | 594. | 0.4614 | 2024 AL            | 10.35 |

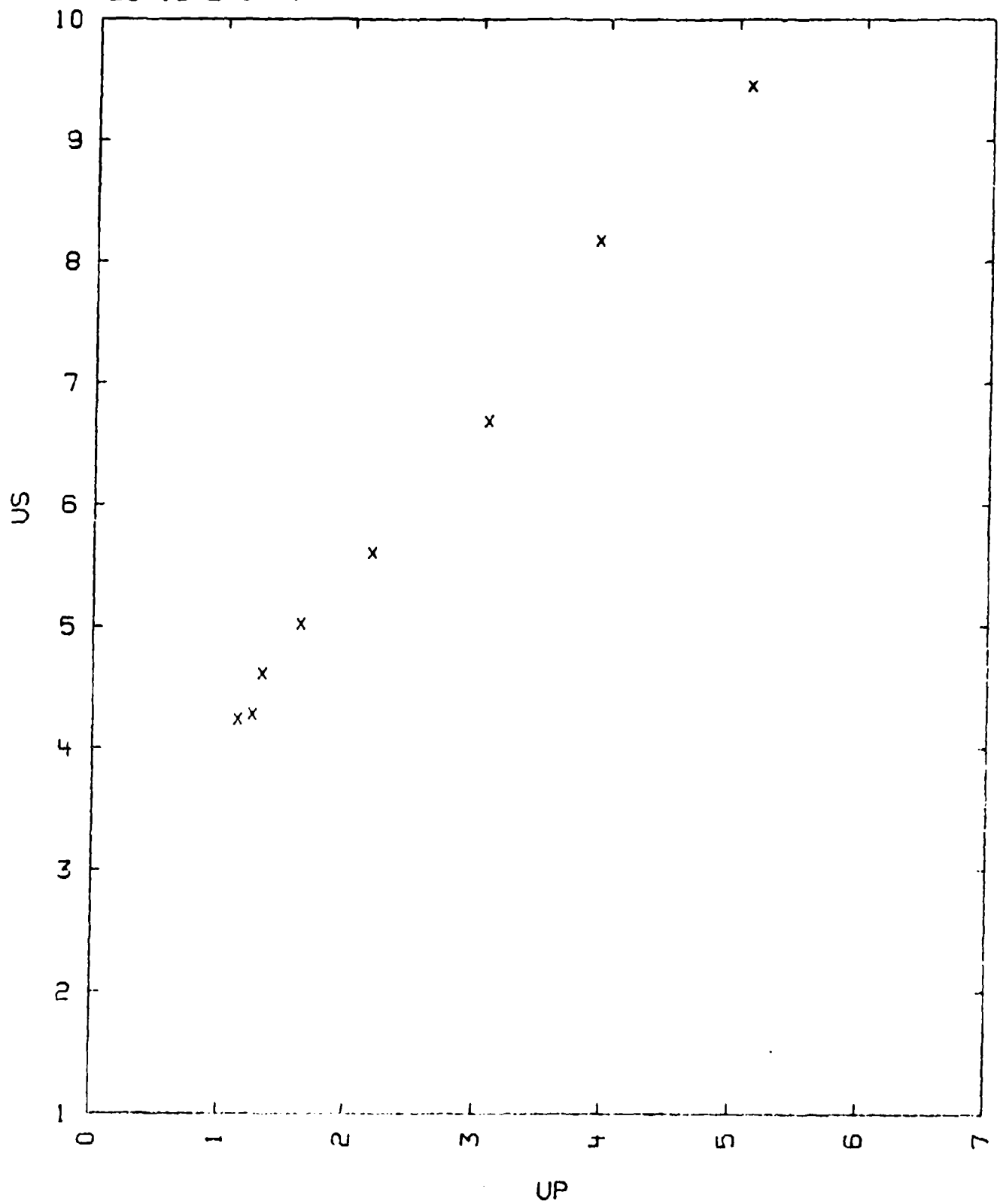
$US = 2.722 + 1.333 \cdot UP \text{ KM/SEC}$   
 $SIGMA \text{ US} = 0.128 \text{ KM/SEC}$

## COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,  
AND CARTER, W.J.  
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,  
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC  
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: S  
DATA REDUCTION TECHNIQUE: B
- 3) SELECTRON IS A TRADE NAME FOR A LINE OF PITTSBURGH PLATE GLASS  
POLYMERS - THIS SAMPLE IS ONE OF ITS POLYESTER RESINS

TABLE 1

SELECTRON (POLYESTER)  
23-18-2-1 ?



EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 10:09:41U 06/15

34 FRAMES PLOTTED

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 10:09:41U 06/15

1

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 10:09:41U 06/15