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Robert Kuklinski

NOTICE

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1 Navy Case No. 76638

2
3 METHOD AND APPARATUS FOR
4 SEPARATING PARTICULATE MATTER FROM A FLUID

5
6 STATEMENT OF GOVERNMENT INTEREST

7 The invention described herein may be manufactured and used
8 by or for the Government of the United States of America for
9 governmental purposes without the payment of any royalties
10 thereon or therefore.

11
12 CROSS-REFERENCE TO RELATED PATENT APPLICATIONS

13 The instant application is related to U.S. Patent
14 Application entitled "Method and Apparatus for Separating
15 Particulate Matter from a Flowing Fluid" (Navy Case No. 76591),
16 filed on the same date by the same inventors.

17
18 BACKGROUND OF THE INVENTION

19 (1) Field of the Invention

20 This invention relates to displacement of particulate matter
21 suspended within a fluid and more particularly to a method and
22 apparatus for ultrasonically and selectively displacing
23 particulate matter suspended in a fluid to provide a filtered
24 fluid.

1 (2) Description of the Prior Art

2 Fluid sources often comprise a fluid reservoir containing a
3 fluid with entrained or suspended particulate matter and a port
4 for drawing fluid from the reservoir. Such ports are generally
5 found in a defined surface structure in reservoirs of quiescent
6 water, such as at the bottom of a lake or pond or at the bottom
7 of a tank. The fluid in such reservoirs often contain
8 suspensions of organic and inorganic particulate matter.
9 Frequently, however, the fluid entering or drawn into the port
10 must be free of such particulate matter. Consequently various
11 methods and apparatus for separating particulate matter from
12 fluids are well known.

13 For example, in some applications, ports which draw fluid
14 from a reservoir of water frequently include a screen or mesh
15 filter over their openings to inhibit particulate matter from
16 entering the port with the water. However, mesh filters
17 generally cause a pressure drop across the port. For example, a
18 static system relies on the pressure of the fluid in the
19 reservoir to urge fluid into the conduit; and in a dynamic system
20 a pump forces fluid into the conduit through the port and the
21 filter. In either system, the pressure drop will increase over
22 time as the filter removes particulate matter. In a static
23 system increases in pressure drop reduces flow rates; in dynamic
24 systems either the flow rate reduces or pumping power must
25 increase until the flow rate through the filter becomes a long
26 time factor. At some point it is even possible for particulate

1 matter to transfer through the filter thereby degrading the
2 quality of the water emerging from the filter. Consequently, it
3 becomes necessary to clean the filter periodically; and in many
4 applications such maintenance is difficult to perform.

5 It has also been proposed to use ultrasonic or acoustic
6 energy as a medium for separating particulate matter from liquid
7 filters. For example:

8 United States Letters Patent No. 4,055,491 to Porath-Furedi
9 discloses a method and apparatus for removing microscopic
10 particles from a liquid medium by using ultrasonic waves
11 generated in the fluid medium. A generator propagates ultrasonic
12 waves of over 1 MHz in a horizontal direction through the medium
13 to cause flocculation of the particles at spaced points. Baffle
14 plates, disposed below the level of propagation of the wave
15 provide high resistance to horizontal propagation therethrough of
16 the ultrasonic waves and low resistance to vertical settling of
17 the flocculated particles. Periodic energization of the
18 generator is used to flocculate the particles; de-energization
19 permits the settling of the flocculated particles to the baffle
20 plates for removal from the fluid.

21 United States Letters Patent No. 4,346,011 to Brownstein
22 discloses a clarifying apparatus and process for separating
23 particulate matter from a fluid within a chamber. A transducer
24 induces a continuous particulate removing action from a filtering
25 screen separating the chambers receiving the liquid such that the
26 fluid in the second chamber is free of particulate matter and the

1 ultrasonic energy agglomerates the particulate matter trapped by
2 the screen to maintain the screen in a clean condition.

3 United States Letters Patent No. 4,398,925 to Trinh et al.
4 discloses a method for removing bubbles from a liquid bath, such
5 as molten glass to be used for optical elements. Larger bubbles
6 are first removed by applying acoustic energy of a frequency
7 suited to the container of the liquid. The selected acoustic
8 energy resonance drives the bubbles toward a pressure well for
9 coalescence with other bubbles to enhance removal from the
10 liquid. Smaller bubbles are then removed by applying an acoustic
11 energy of a resonant frequency suitable for small bubbles to
12 oscillate and thereby stir the liquid to facilitate the break up
13 and absorption of such bubbles within the liquid.

14 United States Letters Patent No. 4,759,775 to Peterson et
15 al. discloses a method and apparatus for controlling the movement
16 of particles having different physical properties when one of the
17 materials is a fluid. First and second acoustic waves propagate
18 through a vessel containing the materials with the frequency of
19 the waves being different so that the two acoustic waves are
20 superimposed upon each other. The super position of the two
21 waves creates a beat frequency wave with pressure gradients
22 dividing the vessel into regions of maximum and minimum pressure.
23 The regions of pressure move through space at a group velocity.
24 The movement of the gradients and regions act upon the materials
25 so as to move one of the materials toward a pre-determined
26 location in the vessel so that by selective appropriate frequency

1 differences one of the materials can be controllably moved to a
2 selected aggregating location within the vessel.

3 United States Letters Patent No. 4,877,516 to Schram
4 discloses a method for manipulating particulate matter by
5 generating an acoustic standing wave with nodal planes of varying
6 energy density in a fluid medium. Particles in the fluid medium
7 responsive to the acoustic energy of the standing wave accumulate
8 at these nodal planes so that in conjunction with the fluid
9 viscous force and field forces acting in the direction of the
10 nodal planes, movement of particles held at these planes can be
11 controlled. The attenuation of the acoustic beams producing the
12 standing wave do not affect the action of this method due to the
13 imbalance of the acoustic forces that tend to be perpendicular to
14 the movement of the particles in the nodal wave direction.

15 United States Letters Patent No. 5,225,089 to Benes et al.
16 discloses a method and apparatus for separating dispersed
17 particles in a medium by generating an ultrasonic standing wave.
18 Specifically a composite resonator is disposed in a vessel
19 containing the medium. The resonator generates a characteristic
20 frequency wave with an amplitude slightly smaller than the upper
21 threshold amplitude so that the pressure forces on the dispersed
22 particles are equivalent to longitudinal holding forces on the
23 particles. Thus the particulates tend to congregate at nodes and
24 antinodes of the standing wave.

25 Prior art efforts therefore have generally been directed;
26 either to mechanical filters that impede both the flow of the

1 particulate matter and the fluid or to ultrasonic apparatus and
2 methods that tend to be limited to relatively small confined
3 fluid bodies. None of this apparatus, however, provides a
4 relatively simple and efficient method and apparatus for
5 filtering particulate matter from a fluid drawn from a large body
6 of the fluid through a port by displacing the particulate matter
7 from the fluid entering the port. There is no disclosure of
8 self-cleaning methods and apparatus for filtering particulate
9 matter from the portion of the fluid drawn into a port from a
10 large body of such fluid. Moreover, there is no disclosure of
11 any method and apparatus for filtering water flowing from a large
12 reservoir into an inlet port without an associated pressure drop.

13 14 SUMMARY OF THE INVENTION

15 An object of this invention is to provide a method and
16 apparatus for ultrasonically filtering particulate matter
17 suspended within a fluid.

18 Another object of this invention is to separate particles
19 suspended in a fluid from a selected portion of the fluid.

20 Yet another object of this invention is to provide a method
21 and apparatus for acoustically separating particles suspended in
22 a fluid from a portion of the fluid entering a port from a
23 reservoir whereby fluid passing through the port is substantially
24 free of such particulate matter.

25 Still another object of this invention is to provide a
26 method and apparatus that separates particulate matter from a

1 fluid without any need for a physical filter with its attendant
2 clogging problems and maintenance requirements.

3 Yet still another object of this invention is to provide a
4 method and apparatus for filtering particulate matter from a
5 fluid without introducing a pressure drop.

6 A further object of this invention is to provide a method
7 and apparatus for removing particulate matter from a fluid
8 entering an inlet port from a large reservoir containing
9 particulate matter suspended in the fluid.

10 Yet a further object of this invention to provide a method
11 and apparatus for delivering a flow of relatively clear water
12 ultrasonically filtered of particulate matter to a cooling water
13 inlet system.

14 According to this invention a method and apparatus for
15 filtering particulate matter from fluid entering a port from a
16 reservoir comprises generating first and second ultrasonic waves
17 and superposing the first and second ultrasonic waves to define a
18 composite wave in the reservoir adjacent the port in a region
19 through which the fluid enters the port. The defined composite
20 wave urges particulate matter entrained in the fluid passing
21 through the region away from the port so fluid entering the port
22 from the reservoir is substantially free of such particulate
23 matter.

24 BRIEF DESCRIPTION OF THE DRAWINGS

25 The appended claims particularly point out and distinctly
26 claim the subject matter of this invention. The various objects,

1 advantages and novel features of this invention will be more
2 fully apparent from a reading of the following detailed
3 description in conjunction with the accompanying drawings in
4 which like reference numerals refer to like parts, and in which:

5 FIG. 1 diagrammatically illustrates a prior art filtration
6 system;

7 FIG. 2 diagrammatically illustrates a prior art filtration
8 system similar to FIG. 1;

9 FIG. 3 diagrammatically illustrates a side view in elevation
10 and partial section of an embodiment of this invention;

11 FIG. 4 is a view taken along the section line 4-4 of FIG. 3;

12 FIG. 5 is a view similar to FIG. 4 of an alternate
13 embodiment of this invention;

14 FIG. 6 is a graphical depiction of a composite wave pattern
15 formed by the embodiment of FIG. 3;

16 FIG. 7 is a graphical depiction taken along lines 7-7 in
17 FIG. 6; and

18 FIGS. 8 through 11 are diagrammatic views of alternative
19 embodiments of this invention.

20
21 DESCRIPTION OF THE PREFERRED EMBODIMENT

22 As background for an understanding of this invention, FIG. 1
23 illustrates a prior art system for filtering a fluid entering a
24 conduit 101 from a body or reservoir of the fluid 102. The fluid
25 passing through a port 103 at the extreme end of the conduit 101

1 is graphically depicted as moving along streams of flow,
2 represented by stream lines 105 within the fluid body 102.
3 Particulate matter 106 suspended in the fluid body 102 also tends
4 to move with that portion 107 of the fluid 102 flowing into the
5 conduit 101 through port 103. A mesh filter or grate 108
6 overlying the port 103 arrests the transit of the particulate
7 matter 106 having a nominal diameter greater than that of the
8 gauge of the filter 108 at the port 103.

9 FIG. 2 depicts a system with relative movement between an
10 object 110 with a port 111 and a fluid 112, such as water intake
11 in flowing river or in the hull of a moving ship. In this case,
12 stream lines 113 in the fluid initially parallel the object
13 surface and then divert toward the port 111. A mesh filter 114
14 in this instance also suffers from the same problems as the
15 filter 108 in FIG. 1. That is, the filter 114 can clog with
16 particulate matter so as to require periodic cleaning. Moreover,
17 the filter 114 even when clean, still causes the pressure drop,
18 albeit less than when partially clogged.

19 Referring now to FIG. 3, apparatus 10 constructed in
20 accordance with this invention filters particulate matter from a
21 relatively large body or reservoir of fluid 11, such as water.
22 In this embodiment a portion of the fluid 11 flows into a port 12
23 connected to a pump 13 through conduit 14. An ultrasonic
24 generator 15 produces an ultrasonic wave pattern that travels
25 along a path 16 to an acoustic reflector 17 disposed in the fluid
26 body 11 and spaced from the port 12. The reflector 17 in this

1 embodiment acts as a second ultrasonic wave generator and
2 reflects the ultrasonic wave pattern transversely along path 16
3 to produce a second ultrasonic wave pattern that travels in the
4 opposite direction 18. The ultrasonic wave patterns superpose in
5 a region 19 of the fluid 11.

6 The counter travelling wave patterns moving along the paths
7 16 and 18 superpose to define a composite wave pattern in the
8 region 19 that has nodes 20 and antinodes 21 corresponding to
9 maximum and minimum pressure gradients within the region 19.
10 These pressure gradients urge particulate matter in the fluid 11
11 passing through the region 19 to accumulate along the nodes 20 or
12 antinodes 21. Composite wave patterns formed by using the
13 apparatus 10 tend to urge particulate matter having a radius less
14 than half spacing of the adjacent ones of the nodes 20 and
15 antinodes 21 ($\frac{1}{2}$ the wave length of the composite ultrasonic wave
16 pattern) toward the nodes 20 and antinodes 21. If the frequency
17 differential is essentially zero, the composite wave pattern will
18 be a standing wave as the reflector 17 does not change the
19 frequency of the reflected sound 18, a standing wave will be
20 created. If, however, there is a relatively small frequency
21 difference (i.e., less than 750hz), the composite wave will be
22 pseudo-standing wave with nodes 20 and antinodes 21 that move at
23 a velocity $V_w \propto (f_1 - f_2)$, where f_1 and f_2 represent the two
24 frequencies. Particulate matter accumulating at the nodes 20 and
25 antinodes 21 will thus tend to move with such nodes 20 or
26 antinodes 21 toward a receiving surface 22 away from the port 12

1 where the velocity of the fluid, and thus particles borne in the
2 fluid, toward the port is negligible.

3 Thus the ultrasonic wave patterns traveling along the paths
4 16 and 18 when produced to have substantially the same frequency
5 produce a composite wave pattern exhibiting standing wave
6 characteristics. That is, when the frequencies of the ultrasonic
7 waves are substantially the same as used herein the composite
8 wave is either a standing wave or a pseudo-standing wave. For
9 the purposes of this application the frequencies which are
10 substantially the same although exhibiting relatively small
11 differences in frequencies, shall be referenced as "differential"
12 frequencies. In this embodiment, a differential frequency
13 between the ultrasonic wave patterns traveling in the direction
14 16 and 18 can be readily accomplished for example, by cycling the
15 generator apparatus 15 through a frequency range or by changing
16 the relative positions of the reflector and the source.

17 Alternatively appropriate positioning of the generating
18 apparatus can orient the nodes 20 and antinodes 21 substantially
19 parallel with the directions 16 and 18. With this construction,
20 accumulated particulate matter moves downwardly along the nodes
21 20 and antinodes 21 by the flowing fluid 11 through the region
22 19.

23 When this invention operates, fluid 11 at the inlet port 12
24 is substantially free of particulate matter. More specifically,
25 either or both the orientation and the velocity of the nodes 20
26 and antinodes 21 in the composite wave pattern can be selected so

1 particulate matter moves away from the port 12 and thereby
2 reduces clogging. Further displacement of particulate matter can
3 be achieved by a water jet 22A or other means that physically
4 displaces accumulated particulate matter from the receiving
5 surface 22 to a position even more distant from the inlet port
6 12.

7 Referring now to FIGS. 3 and 4, the generating apparatus 15
8 is included beneath an acoustically transparent cover 23 within
9 an annular chamber 24 surrounding the port 12. Frequency sources
10 25 energize amplifiers 26 to drive each of the transducers 27
11 thereby to produce the ultrasonic wave patterns that travel along
12 the path 16. The transducers 27 are supported in the chamber 24
13 which includes a suitable medium 28 such as oil, acoustic foam or
14 other medium for transmitting the generated ultrasonic wave
15 pattern 16 to the acoustically transparent cover 23. An acoustic
16 lens 32 is positioned on the face of each transducer 27 to match
17 the contour of cover 23. The transducers 27 are oriented within
18 the chamber 24 to direct the generated wave pattern 16 toward the
19 acoustic reflector 17. The acoustic reflector 17 is supported
20 above and spaced from the port 12 by a frame support 29 with a
21 conical reflective surface 30 for receiving the generated
22 ultrasonic wave pattern along the path 16 and inverting its path
23 to generate the second ultrasonic wave pattern along the path 18.
24 Obviously, the inventive device can be modified to accommodate
25 different port geometries.

1 It is preferred to cycle the frequency of the first
2 ultrasonic wave pattern generator upwardly through a range (e.g.,
3 0.8 MHz to 1.2 MHz) and then revert to the low end of the range
4 in order to vary the frequency with apparatus of minimum cost and
5 complexity. A control apparatus 31, such as a micro-processor,
6 connects to frequency sources 25. Those skilled in the art will
7 appreciate that for a short time the velocity of nodes 20 and
8 antinodes 21 will reverse as each cycle begins. However, the
9 relative speed of the composite wave pattern and width of the
10 region 19 can be selected so that particulate matter will not
11 cyclically leak through the region 19. It will also be apparent
12 that if frequency variation is used, the transducers 27 can be
13 connected to a single amplifier 26 and frequency source 25.

14 FIG. 5 discloses another embodiment of this invention that
15 includes a single annular transducer 33 that can be positioned in
16 the chamber 24 beneath the acoustically transparent surface 23
17 (shown in FIG. 3). In this instance the single transducer 33
18 produces a wave pattern that is reflected by the reflector 17
19 (see FIG. 3) in substantially the same manner, as described above
20 with respect to the transducers 27 of the embodiment of FIG. 3 to
21 produce the composite wave in the region 19 (see FIG. 3).

1 FIGS. 6 and 7 graphically depict a composite wave pattern
2 formed by the superposing ultrasonic wave patterns with the nodes
3 20 and antinodes 21 in the region 19. The orientation of the
4 nodes 20 and antinodes 21 according to this embodiment of the
5 invention is a function of an angle α , the angle of intersection

1 defined by the intersection of the wave patterns 16 and 18. In
2 FIG. 3 $\alpha=180^\circ$ so the nodes and antinodes extend perpendicularly
3 to the directions 16 and 18 of the generated wave patterns. The
4 planar orientation of the nodes and antinodes can vary between
5 45° relative to the generated waves (i.e., 90° intersection of
6 the waves) and 90° (0° and 180° intersections).

7 The velocity V_w of the nodes and antinodes is a function of
8 the frequency shift between the two wave patterns from the
9 transducers operating at frequency f_1 and f_2 . That is, the
10 velocity is equal to the spacing of the fringes times the
11 frequency shift:

$$12 \quad V_w = \frac{\lambda}{2\sin\alpha} (f_1 - f_2) \quad (1)$$

13 where term " λ " is the wavelength at the nominal frequency.

14 Thus, if the frequency sources 25 in FIG. 3 cycle through a
15 frequency range to achieve a frequency difference between the
16 first and second ultrasonic wave patterns, the velocity V_w during
17 the cycle would be positive provided $f_1 > f_2$. Upon reaching a
18 prescribed frequency level the frequency sources 25 would revert
19 to a preset lower frequency and begin the cycle again. As
20 previously indicated, this causes a momentary reversal of
21 velocity of the composite wave pattern and an instantaneously
22 standing wave pattern. For example, if the average frequency
23 differential within the region 19 during a cycle is approximately
24 287Hz and the ultrasonic wave patterns have a nominal wave length

1 of 4800 microns, the average spacing between the nodes 20 and
2 antinodes 21 would be approximately 2400 microns and the average
3 velocity V_w would be approximately 7 ft/sec or 2.1 m/sec. Thus,
4 those skilled in the art will appreciate that an appropriate
5 selection of differential frequencies and wavelength for the
6 ultrasonic generated wave patterns and cycle rate will enable the
7 system to filter substantially all particulate matter in the
8 fluid so that the fluid reaching the port would be generally free
9 of any particulate matter.

10 FIG. 8 depicts another embodiment of the instant invention
11 is shown where the reflector 17 of FIG. 3 has been replaced with
12 a second ultrasonic wave generator 40 substantially identical to
13 the first ultrasonic wave generator 15. Frequency sources 35 and
14 amplifiers 36 cause transducers 37 to produce an ultrasonic wave
15 pattern of a different frequency than that produced by the first
16 ultrasonic generator 15. Thus, provided the frequency of the
17 first ultrasonic wave pattern is greater than the second, the
18 composite wave patterns will have nodes 20 and antinodes 21
19 traveling at the indicated velocity V_w in the region 19.

20 FIG. 9 depicts another embodiment of an ultrasonic filter 50
21 apparatus. This apparatus includes an annular transducer
22 arrangement 51 that directs ultrasonic waves toward a port 12
23 extending above an object's surface 22. A structure 52 supports
24 the annular ultrasonic wave generator apparatus with a transducer
25 47 arranged above the port 12 so that the composite wave forms in
26 a region 53 above the port 12. Transducer 47 is driven by an

1 amplifier 46 and a wave generator 45. The conduit 13 and port 12
2 are preferably formed of an ultrasonic transparent material so
3 that the region 53 can be formed proximate, and even extend into
4 the conduit 13.

5 The composite wave in this embodiment moves at a velocity V_w
6 that is opposite in direction to that produced with the
7 embodiment of FIG. 3. The velocity V_w in FIG. 9 has a generally
8 upward direction to transport particulate matter away from the
9 port 12 albeit away from the surface 22, and into the region of
10 the fluid body remote from the port 12. The velocity V_w in the
11 upward direction occurs when the frequency sources 45 produce a
12 higher differential frequency signal than the frequency sources
13 26. It will be apparent that the orientation of the nodes 20 and
14 antinodes 21 are, as previously described, a function of the
15 angle α .

16 In this embodiment a cylindrical member 56 of a sound
17 absorbing material is supported by the structure 52. This member
18 56 limits interference from the intersection of the ultrasonic
19 wave patterns generated by the transducers 23 and 52 which could
20 otherwise limit the effectiveness of the particulate matter to
21 travel along such interface and thereby pass through the port 12
22 and into the conduit 17.

23 Ultrasonic filter apparatus 60 in FIG. 10 is similar to the
24 apparatus of FIG. 9 and includes first and second ultrasonic wave
25 generators 15 and 51 within the chamber 24. Concentric
26 transducers 27 and 27A are positioned about the base of an

1 extending conduit 12. The structure 52 supports an annular
2 reflector 61 above the transducers 27 and 27A to create a
3 composite wave pattern in the region 53 above and in the conduit
4 12. The transducers 27 and 27A preferably are driven at
5 differential frequencies, as previously described, so that the
6 velocity V_w of the nodes and antinodes of the composite waves
7 urges particulate matter entering the region 53 to a region of
8 the reservoir 11 remote from the fluid entering the port.

9 In another embodiment shown in FIG. 11, a plurality of sets
10 of first and second ultrasonic wave generators 15 and 51, 15' and
11 51', and 15" and 51", are arranged in a concentric fashion about
12 the port 12 to generate these sets of first and second wave
13 patterns 16 and 18, 16' and 18', and 16" and 18". Each set of
14 wave patterns are preferably generated with different nominal
15 frequencies so that each set is optimized to filter particulate
16 matter of different size ranges. As with the embodiment of FIG.
17 8, it is preferred that the first wave patterns in each of the
18 sets of wave patterns have a frequency greater than the second
19 corresponding wave pattern in regions 19, 19' and 19" so that the
20 nodes 20, 20' and 20" and the antinodes 21, 21' and 21" move at
21 velocities V_w , V_w' and V_w'' , respectively. Consequently,
22 particulate matter in various size ranges (e.g., approximately
23 from 2 to 100 microns, 100 to 400 microns, and 400 to 1000
24 microns, respectively) can be accumulated along the nodes and
25 antinodes in respective ones of the regions 19, 19' and 19". The
26 moving nodes and antinodes transport this matter to a region of

1 the fluid 11 remote from the fluid entering the port. Thus, the
2 fluid entering the port 12 is substantially free of particulate
3 matter.

4 In each of the foregoing embodiments the frequencies and
5 energy determine the sizes of particles that will be filtered.
6 The optimum frequency, F_1 for filtering a given particle for the
7 pseudo-standing ultrasonic plane wave is given by:

$$8 \quad F_{1X} = \Pi R^2 (kR) \rho v_0^2 \cdot f \left(\frac{\rho_b}{\rho}, \frac{c_b}{c} \right) \quad (2)$$

$$9 \quad f \left(\frac{\rho_b}{\rho}, \frac{c_b}{c} \right) = \left[\frac{\rho_b + \frac{2}{3}(\rho_b - \rho)}{2\rho_b + \rho} \frac{1}{3} \cdot \frac{c^2 \rho}{c_b^2 \rho_b} \right] \quad (3)$$

10 where: R is the radius of the particle
11 K is the wave spacing of the composite wave
12 (K = 2π over λ)
13 V_0 is the fluid's velocity amplitude which is a
14 function of the energy of the composite wave
15 ρ is the density of the fluid
16 ρ_b is the density of the particle
17 C is the speed of sound in the fluid
18 C_b is the speed of sound in the particle

1 Thus, according to equation (2), the greater the difference in
2 the densities and the speed of sound in the particle and the
3 fluid, the easier it will be to move a particle of a given size.

4 It will be understood now that apparatus constructed in
5 accordance with this invention improves the flow of filtered
6 fluid through a port. There are no pressure drops across the
7 port, as are encountered with systems using mesh filters.
8 Relatively large amounts of the filtered fluid can be drawn from
9 an essentially infinite body or reservoir of the unfiltered
10 fluid. Adjustment of the frequency and wavelengths of the
11 generated ultrasonic wave patterns enables users to selectively
12 control the size of the particulate matter filtered and the rate
13 at which the particulate matter is displaced from the fluid
14 passing through the region in which the acoustic energy acts on
15 the fluid.

16 This invention has been disclosed as a general purpose
17 filtering apparatus for filtering particulate matter suspended in
18 fluid entering a port from a large body of such fluid. The
19 apparatus includes first and second ultrasonic wave pattern
20 generators that produce superposing ultrasonic wave patterns in a
21 region through which fluid flows as it enters a port. The second
22 ultrasonic generator can comprise a reflector for redirecting the
23 first ultrasonic wave pattern to form the second ultrasonic wave
24 pattern. The wave patterns are of substantially the same
25 frequencies which are preferably differential frequencies, as
26 defined herein, so the nodes and antinodes of the composite wave

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2
3 METHOD AND APPARATUS FOR
4 SEPARATION OF PARTICULATE MATTER FROM A FLUID

5
6 ABSTRACT OF THE DISCLOSURE

7 A method and apparatus for filtering particulate matter
8 entrained in a fluid entering a port from a reservoir. First and
9 second ultrasonic wave generators produce ultrasonic waves to
10 define a composite wave pattern. The patterns produce nodes and
11 antinodes in a region through which fluid entering a port passes.
12 The particulate matter in the portion of the fluid passing
13 through the region accumulates along the nodes and antinodes.
14 The accumulating particulate matter is thereby separated and is
15 displaced from the fluid entering the port.

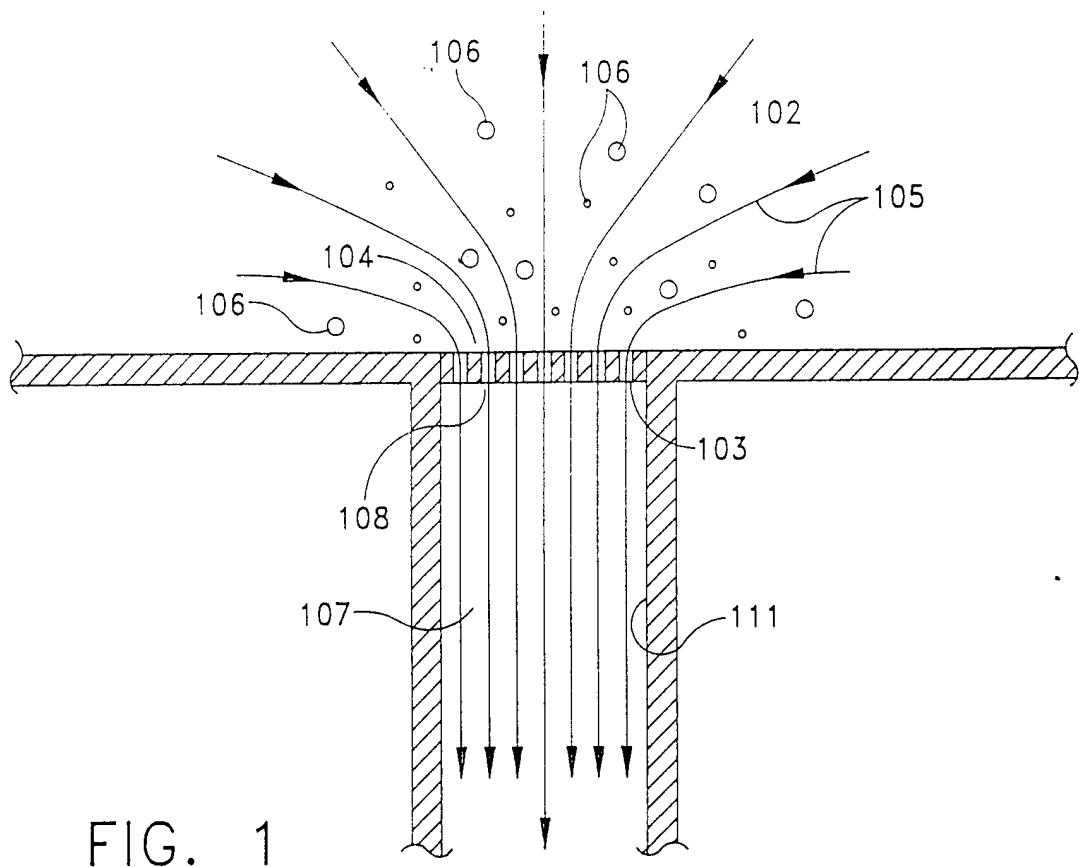


FIG. 1
(PRIOR ART)

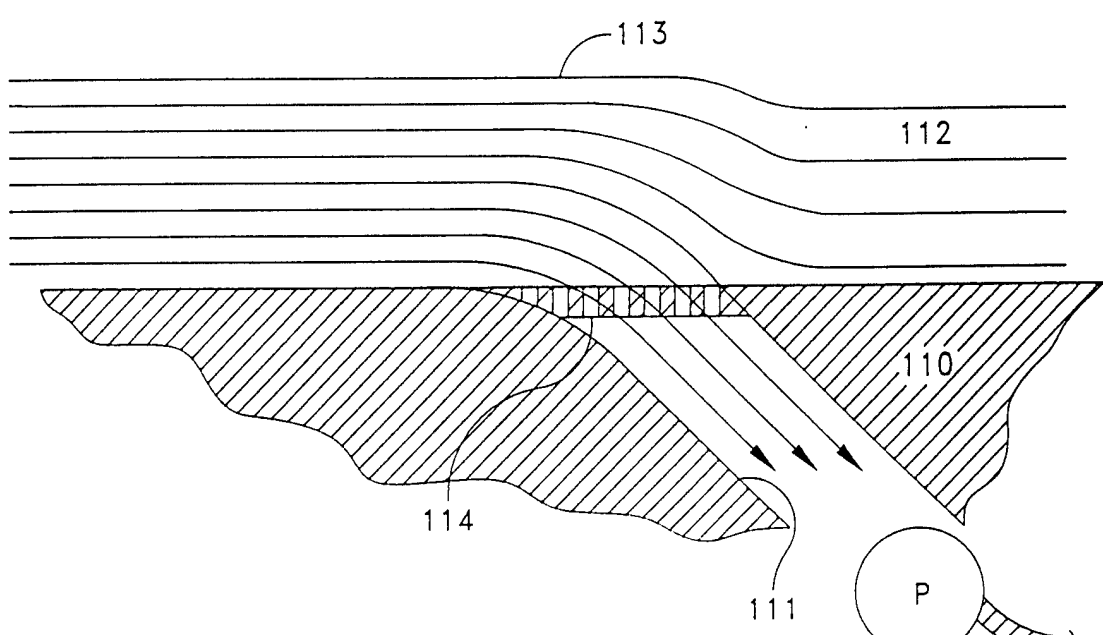


FIG. 2
(PRIOR ART)

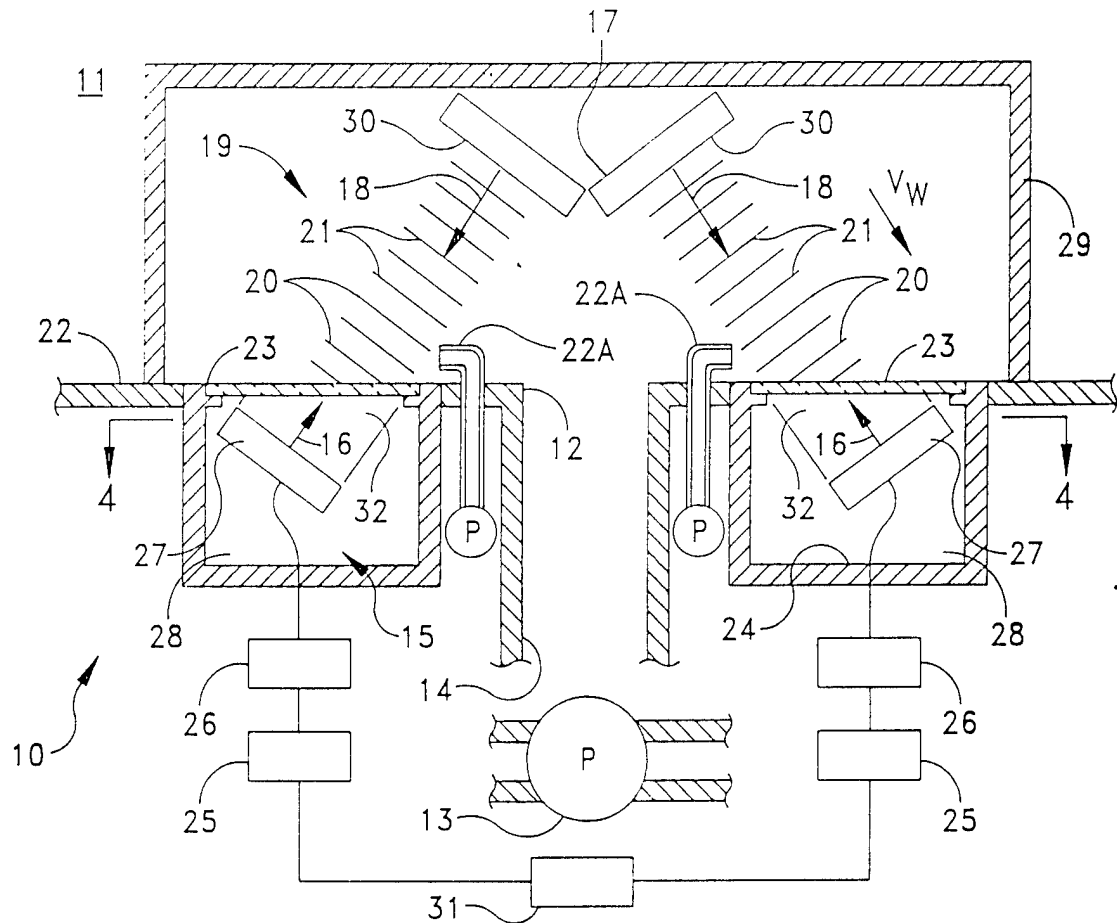


FIG. 3

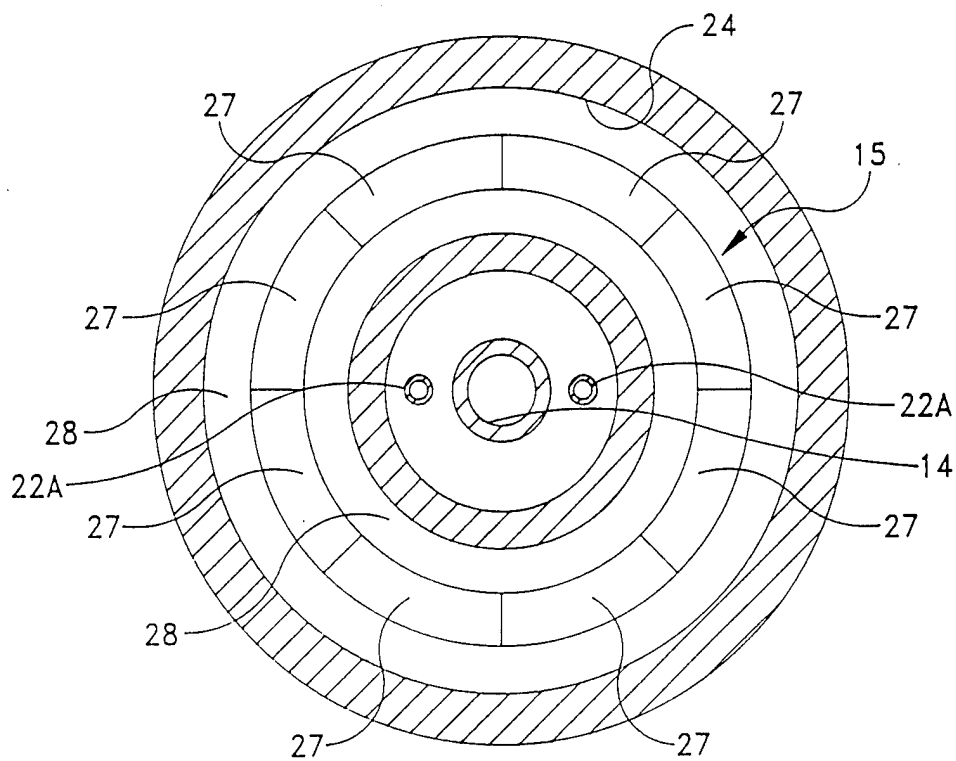


FIG. 4

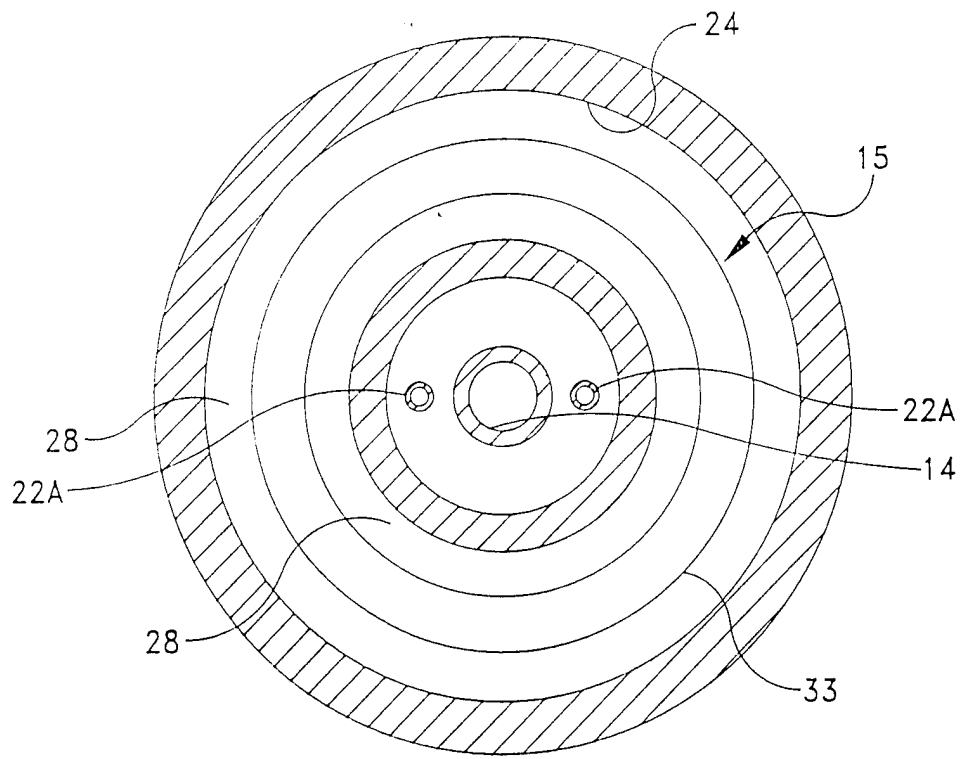


FIG. 5

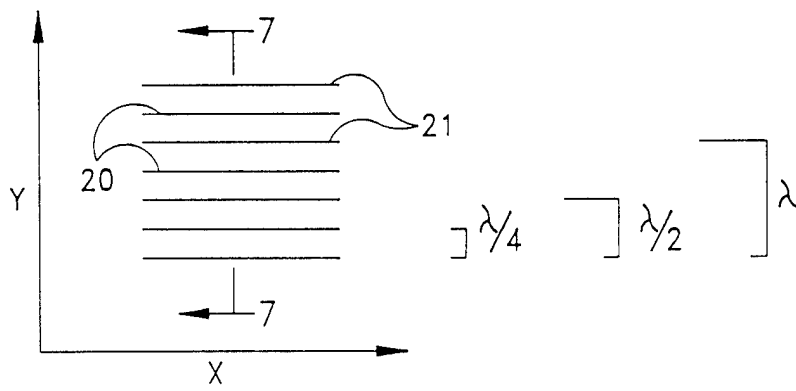


FIG. 6

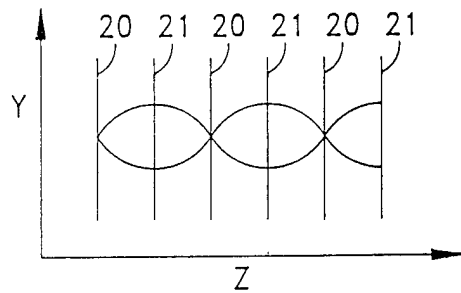


FIG. 7

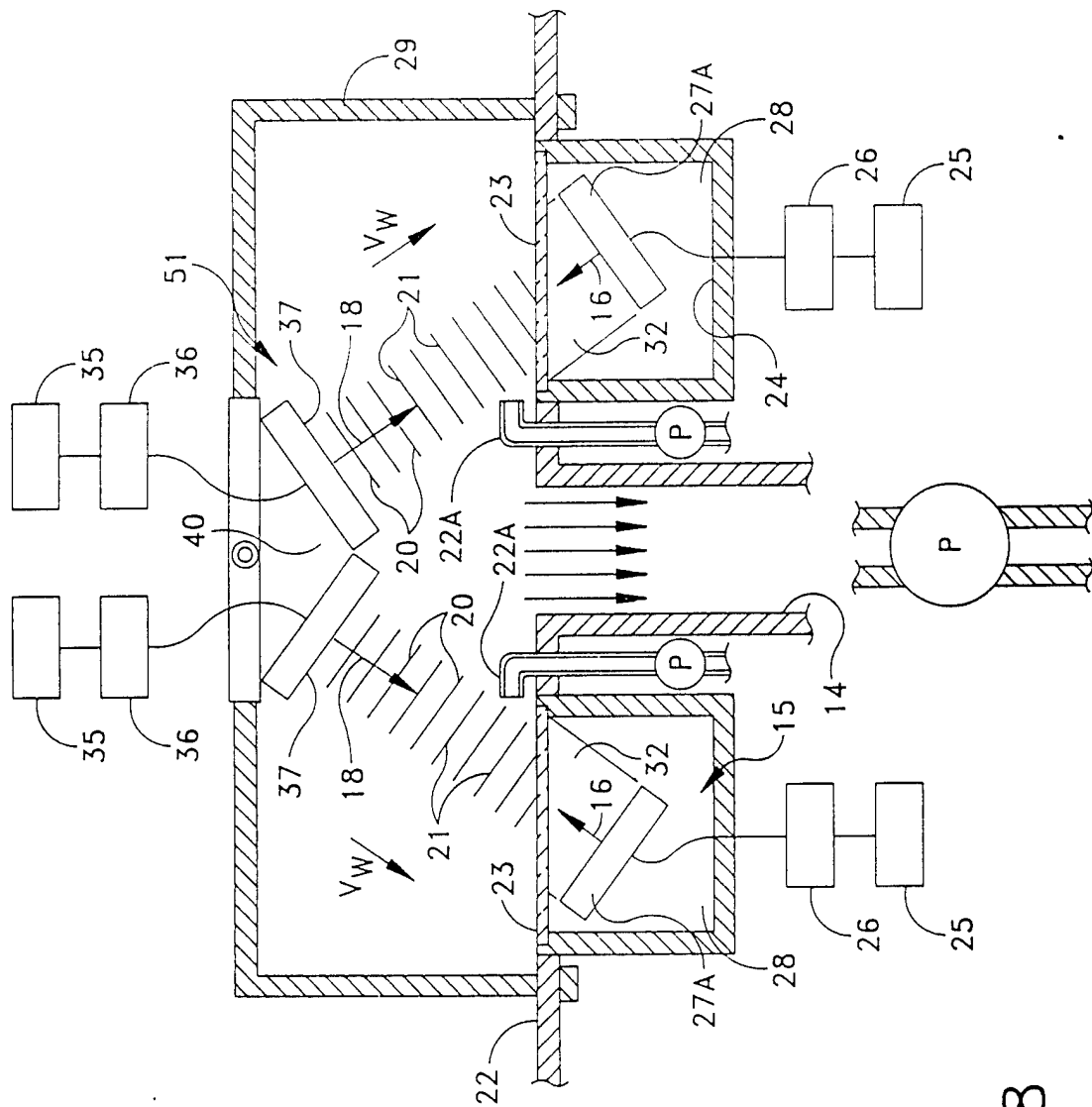


FIG. 8

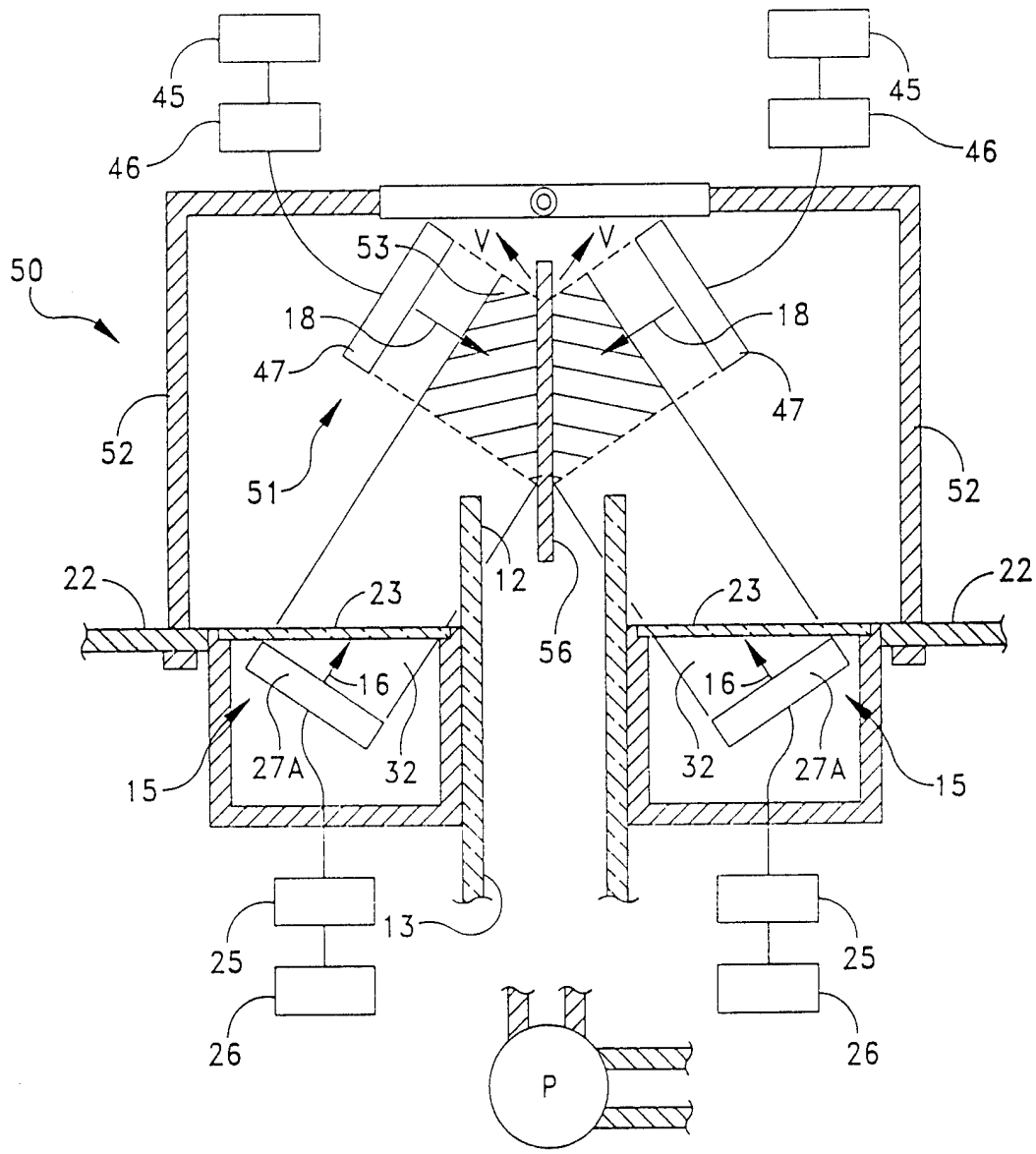


FIG. 9

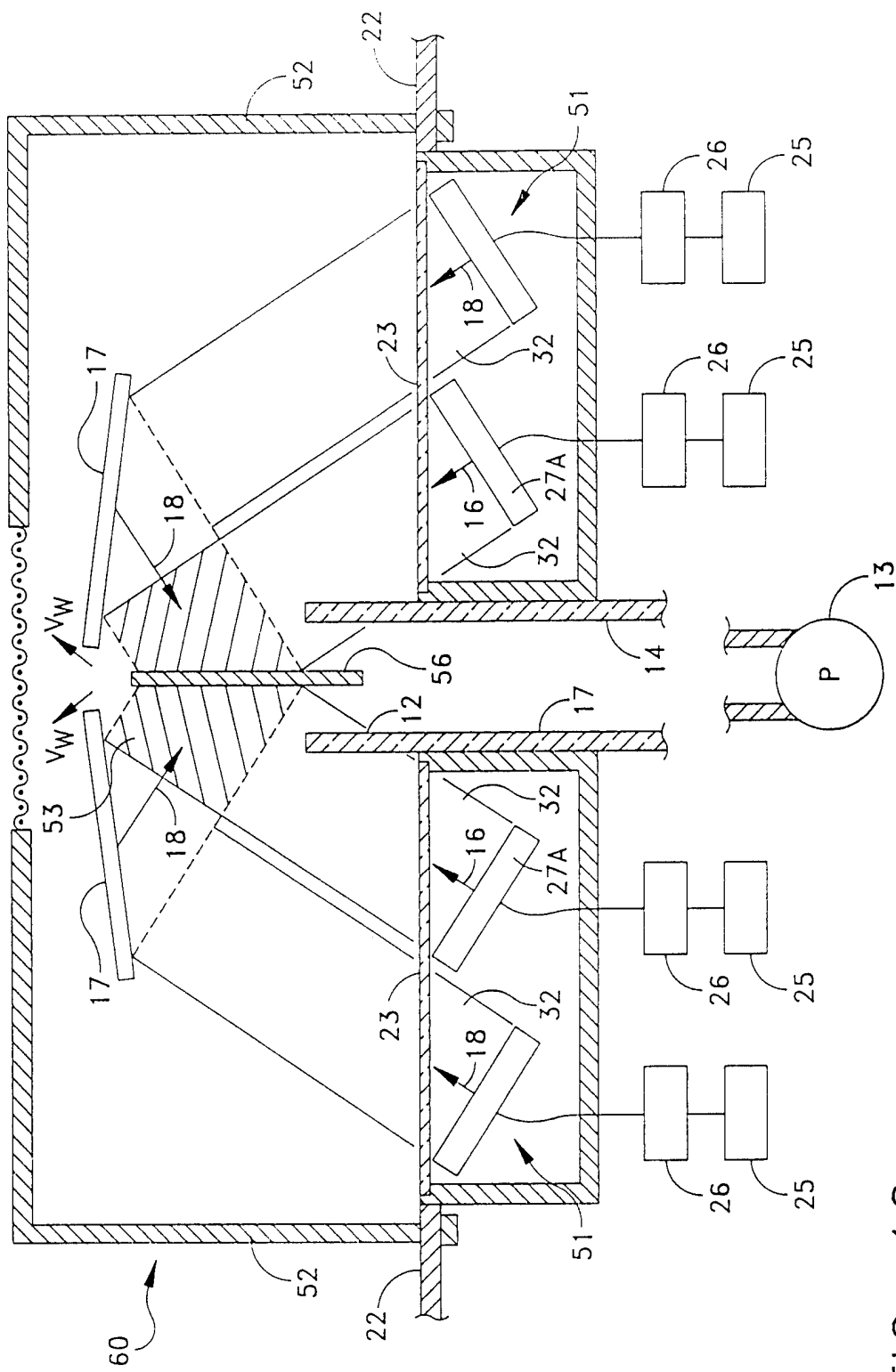


FIG. 10

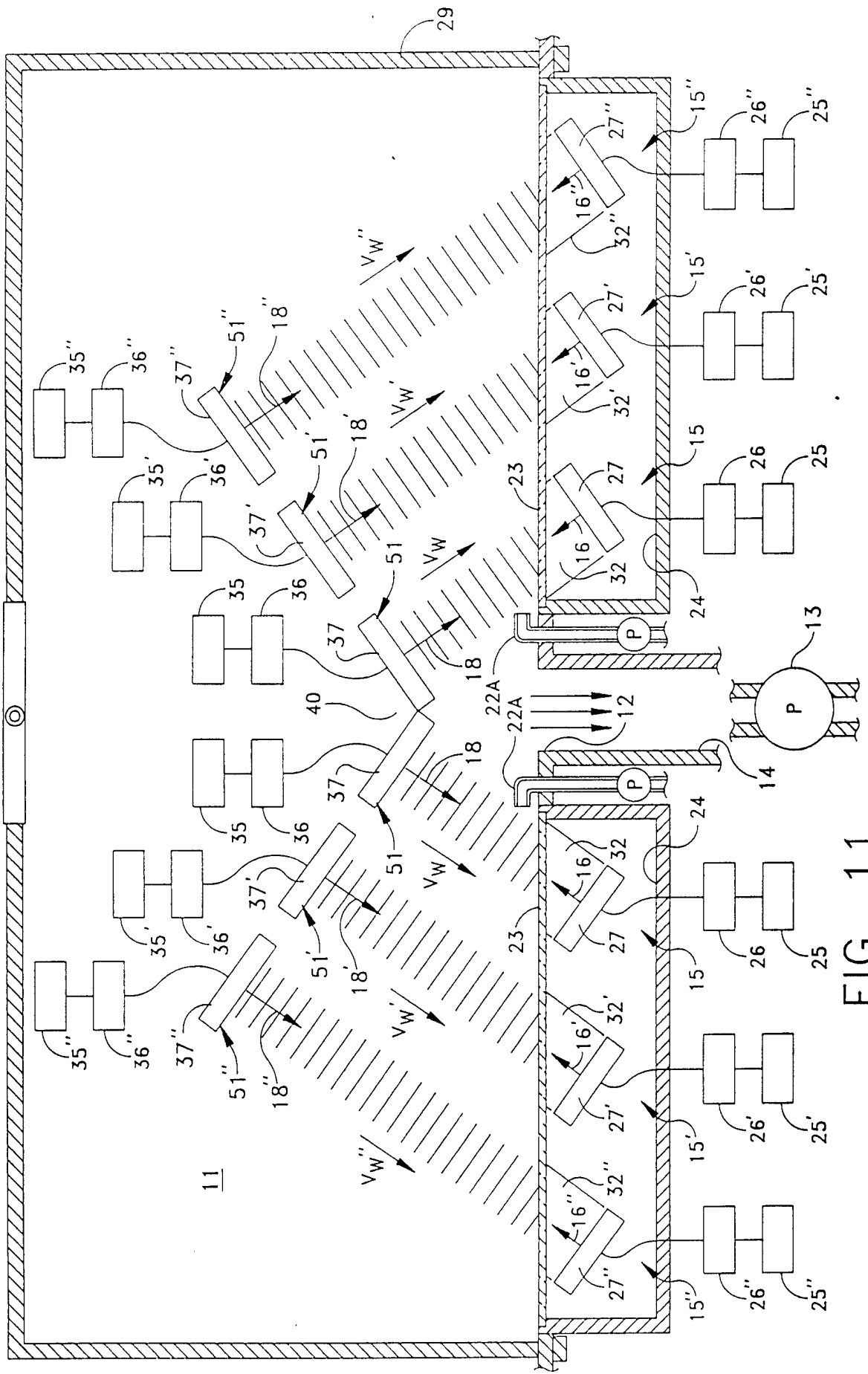


FIG. 11