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1 Attorney Docket No. 79064

2  
3 OPTIMAL FSTOP/RESOLUTION APPARATUS AND METHOD  
4 FOR SPECIFIED DEPTH-OF-FIELD

5  
6 STATEMENT OF GOVERNMENT INTEREST

7 The invention described herein may be manufactured and used  
8 by or for the Government of the United States of America for  
9 governmental purposes without the payment of any royalties  
10 thereon or therefore.

11  
12 BACKGROUND OF THE INVENTION

13 (1) Field of the Invention

14 The present invention relates generally to determining a  
15 camera's optimal  $f_{\text{stop}}$ , and more particularly to a method and  
16 apparatus for computing the  $f_{\text{stop}}$  that provides optimal resolution  
17 for a specified depth-of-field.

18 (2) Description of the Prior Art

19 It is well known that a camera's  $f_{\text{stop}}$  controls the depth-of-  
20 field in a photographic image. The depth-of-field is the region  
21 in which objects remain focused, and objects outside the depth-  
22 of-field are not focused. For a given depth-of-field, another  
23 measure of image quality is the resolution, or image sharpness,  
24 within that depth-of-field. The depth-of-field resolution is

1 determined by film properties (grain size), lens properties  
2 (focal length and aperture), light properties (wavelength), and  
3 depth-of-field size.

4 Because depth-of-field and resolution are each affected by a  
5 camera's  $f_{\text{stop}}$ , photographers often compromise depth-of-field for  
6 increased resolution, or vice-versa. U.S. Patent No. 4,785,323  
7 details a method of selecting an aperture/shutter combination  
8 with an optimum depth-of-field to blur ratio, but maximum  
9 resolution throughout the depth-of-field is not considered.  
10 Alternately, U.S. Patent No. 4,792,823 describes a manual depth-  
11 of-field preview device in which an optimum depth-of-field is  
12 user-determined by previewing images. Again, optimum settings  
13 are not computed or considered. U.S. Patent Nos. 5,049,916 and  
14 5,130,739 optimize photographic exposure through extra system  
15 speed, but sacrifice depth-of-field for shutter speed to minimize  
16 blur from system and object motion. These patents do not address  
17 picture sharpness or depth-of-field control. U.S. Patent No.  
18 5,532,782 provides calculations for an  $f_{\text{stop}}$  that ensure focus for  
19 multiple objects at various distances; however, maximum sharpness  
20 or resolution is not addressed.

21 There is currently no method or apparatus for computing the  
22 maximum resolution or image sharpness within a predefined depth-  
23 of-field. What is needed is a method and apparatus that allow a



1 available. When the approximate field technique is utilized, the  
2 camera must be adjusted to the discrete  $f_{\text{stop}}$  closest to, but not  
3 exceeding, the computed  $f_{\text{stop}}$ .

4  
5 BRIEF DESCRIPTION OF THE DRAWINGS

6 A more complete understanding of the invention and many of  
7 the attendant advantages thereto will be readily appreciated as  
8 the same becomes better understood by reference to the following  
9 detailed description when considered in conjunction with the  
10 accompanying drawings, wherein like reference numerals refer to  
11 like parts and wherein:

12 FIG. 1 is a basic camera lens diagram to explain the  
13 notation;

14 FIG. 2 is a plot of spot size/resolution versus  $f_{\text{stop}}$  for  
15 grain size;

16 FIG. 3 is a plot of spot size/resolution versus  $f_{\text{stop}}$  for  
17 diffraction using a fixed wavelength of light;

18 FIG. 4 is a plot of spot size/resolution versus  $f_{\text{stop}}$  for a  
19 fixed depth-of-field;

20 FIG. 5 is a plot of spot size/resolution versus  $f_{\text{stop}}$  for a  
21 specified short-range photography scenario;

22 FIG. 6 is a plot of spot size/resolution versus  $f_{\text{stop}}$  for a  
23 specified mid-range photography scenario;



1           As FIG. 1 shows, a point **30** on the object plane translates  
2 to a point **32** on the image plane. As objects move away from the  
3 object plane **16**, the focus of the image of those objects  
4 deteriorates; however, objects close to the object plane **16** may  
5 still provide focused images, and this is known as the depth-of-  
6 field effect. Objects within the depth-of-field, but not on the  
7 object plane **16**, project to a spot or disk on the image plane **22**.

8           If  $D_f$  **34** is the depth-of-field in front of the object, then a  
9 point **36** at a distance  $D_f$  **34** in front of the object plane **16**  
10 projects to a point **36i** in image space such that the image plane  
11 **22** contains a spot or disk of diameter  $h_i$  **38**. Similarly, if  $D_r$   
12 **40** is the depth-of-field to the rear of the object, then a point  
13 **42** at a distance  $D_r$  **40** to the rear of the object plane **16** also  
14 projects to a point **42i** in the image space such that the image  
15 plane **22** contains a spot or disk of diameter  $h_i$  **38**. For objects  
16 within the total depth-of-field,  $D_f + D_r$  **44**, the resolution limit  
17 at the image plane **22** is therefore  $h_i$  **38**, otherwise known as the  
18 spot size, or resolution.

19           A point in object space **12** is therefore in focus if its  
20 image on the image plane **22** is less than  $h_i$  **38** in diameter, and a  
21 point in object space **12** is in perfect focus if its image on the  
22 image plane **22** is also a point. It then follows that two points  
23 in object space are resolvable if their image plane images are  
24 disjoint.

1           Image resolution is affected by several factors including  
2 film grain size, diffraction, and depth-of-field. Film grain  
3 size does not depend upon camera settings and is independent of  
4  $f_{\text{stop}}$  that controls the camera aperture. Additionally, film grain  
5 size remains constant regardless of depth-of-field, object  
6 distance, or lens focal length.

7           Referring now to FIG. 2, there is shown a plot of spot size  
8 in the image plane versus  $f_{\text{stop}}$  as a function of grain size. As  
9 FIG. 2 indicates, the relationship between spot size or  
10 resolution, and  $f_{\text{stop}}$ , is constant for all  $f_{\text{stop}}$  values.

11           A camera aperture restricts light waves to cause  
12 interference known as diffraction, and diffraction limits image  
13 resolution. The resolution effects from diffraction depend on  
14 the light wavelength, aperture diameter (i.e.,  $f_{\text{stop}}$ ), and  
15 distance between the film and the lens. E. Hecht, *Optics*, 2<sup>nd</sup>  
16 Edition, provides a well known relationship between diffraction  
17 spot size and the circular aperture opening:

$$18 \quad \text{Diffraction spot diameter} \quad = 2.44 * i * \lambda / A \quad (2)$$

$$19 \quad = \lambda * \{ (o * f) / (o - f) \} * (f_{\text{stop}} / f) \quad (3)$$

20           where:

21            $\lambda$  is the wavelength of light (angstroms);

22           A is the aperture diameter (meters); and

23            $f_{\text{stop}} = f / A$ .

1 Referring now to FIG. 3, there is shown the basic linear  
2 relationship between spot size and  $f_{\text{stop}}$  for a constant light  
3 wavelength,  $\lambda$ , where  $o$  and  $f$  are held constant. As FIG. 3  
4 indicates, for a constant wavelength, resolution from diffraction  
5 decreases (spot size increases) as  $f_{\text{stop}}$  increases.

6 Image resolution is also limited by the fact that all  
7 objects cannot be located in the object plane. As stated  
8 previously, objects within the depth-of-field and located on the  
9 lens axis, project onto the image plane as a disk with diameter  
10  $h_i$  given by the well known equation:

$$11 \quad h_i = (f/f_{\text{stop}}) * (f/(o-f)) * (d/(o-d)) \quad (4)$$

12 where:

13  $d$  is depth-of-field (in front of object) (meters).

14 The resolution due to depth-of-field therefore depends upon  $f_{\text{stop}}$ ,  
15 focal length, object distance, and distance from the object plane  
16 (depth-of-field). Referring now to FIG. 4, there is shown a plot  
17 of spot size or resolution versus  $f_{\text{stop}}$  for a constant depth-of-  
18 field, with  $f$  and  $o$  held constant, indicating a hyperbolic shape.

19 As  $f_{\text{stop}}$  increases, depth-of-field changes cause resolution to  
20 increase (spot size decreases).

21 Referring now to FIG. 5, there is shown a plot of film grain  
22 size, diffraction, and depth-of-field on the same plot of  
23 resolution versus  $f_{\text{stop}}$ . Because the three effects are always  
24 present, plotting on the same graph allows insight into the

1 dominating effect. To produce the graphs in FIG. 5, light  
2 wavelength was set to 5500 angstroms as a compromise between the  
3 4000 angstrom and 7000 angstrom values in the visible spectrum.  
4 For FIG. 5, close distance, or short-range photography was  
5 considered, and accordingly, object distance was set at 1 meter,  
6 focal length to 28 millimeters, depth-of-field to 0.1 meter, and  
7 film grain size to 4 micrometers.

8 Conventional  $f_{\text{stop}}$  computations suggest the  $f_{\text{stop}}$   
9 corresponding to the intersection of the depth-of-field and grain  
10 size curves **60**. As FIG. 5 indicates, the  $f_{\text{stop}}$  at the  
11 intersection of the depth-of-field and grain size curves **60**  
12 corresponds to an  $f_{\text{stop}}$  where diffraction **62**, not depth-of-field  
13 or grain size, limits the resolution or spot size. Selecting the  
14  $f_{\text{stop}}$  at the intersection of the depth-of-field and grain size  
15 curves **60** therefore ignores the dominating and limiting  
16 diffraction effect **62** on resolution at that  $f_{\text{stop}}$ .

17 The invention presented herein is to use the  $f_{\text{stop}}$  providing  
18 maximum resolution, or equivalently, the  $f_{\text{stop}}$  that minimizes the  
19 maximum of the three spot sizes. FIG. 5 shows that depth-of-  
20 field limits the resolution for  $f_{\text{stop}}$  values less than 8.5 **64, 66**,  
21 while diffraction limits the resolution for  $f_{\text{stop}}$  values greater  
22 than 8.5 **64, 66**. Because depth-of-field resolution decreases as  
23  $f_{\text{stop}}$  increases, while diffraction resolution increases as  $f_{\text{stop}}$   
24 increases, the minimum spot size, or optimum resolution, occurs

1 at the intersection **64** of the depth-of-field and diffraction  
2 curves. When this intersection **64** is above the film grain line  
3 as in this short-range scenario, film grain does not limit  
4 resolution more than diffraction or depth-of-field. The  $f_{\text{stop}}$   
5 providing optimal resolution in the short-range scenario is  
6 therefore that  $f_{\text{stop}}$  corresponding to the intersection of the  
7 depth-of-field and diffraction curves **64**. As FIG. 5 shows, the  
8 invention's  $f_{\text{stop}}$  **66** is nearly one-third the conventional method  
9  $f_{\text{stop}}$  **68**, with the invention producing a smaller spot size **70**  
10 (i.e., increased resolution) of nearly one-third the conventional  
11 method  $f_{\text{stop}}$  spot size **72**.

12 Referring now to FIG. 6, there is shown a plot of the three  
13 resolution factors for mid-range photography. The FIG. 6 curves  
14 used an object distance set to 100 meters, focal length to 50  
15 millimeters, depth-of-field to 40 meters, film grain size to 4  
16 micrometers, and light wavelength to 5500 angstroms. As FIG. 6  
17 indicates, just as in FIG. 5, for all  $f_{\text{stop}}$  values, either  
18 diffraction or depth-of-field limits the resolution, with the  
19 intersection of the depth-of-field and diffraction curves  
20 occurring above the film grain size curve. Since film grain size  
21 is not the limiting resolution factor in the mid-range scenario,  
22 the  $f_{\text{stop}}$  providing maximum resolution remains the intersection of  
23 the diffraction and depth-of-field curves **80**. Once again, the  
24  $f_{\text{stop}}$  generated by the conventional technique, at the intersection

1 of the depth-of-field and grain size curves **82**, exists in a  
2 region where diffraction limits the resolution. Using the  
3 invention to determine  $f_{stop}$  as the intersection of the depth-of-  
4 field and diffraction curves **80**, the optimal  $f_{stop}$  **84** providing  
5 maximum resolution is obtained. An  $f_{stop}$  less than the optimal  
6  $f_{stop}$  **84** is limited by depth-of-field to produce larger spot sizes  
7 than the optimal spot size **86**; and an  $f_{stop}$  greater than the  
8 optimal  $f_{stop}$  **84** is limited by diffraction to produce larger spot  
9 sizes than the optimal spot size **86**.

10 Referring now to FIG. 7, there is shown a plot of the three  
11 resolution factors for long-range photography. FIG. 7 curves  
12 used an object distance of 1000 meters, focal length set to 200  
13 millimeters, depth-of-field set to 100 meters, film grain size of  
14 4 micrometers, and light wavelength set to 5500 angstroms. As  
15 FIG. 7 indicates, the depth-of-field and diffraction curves  
16 intersect **100** below the film grain size. The invention indicates  
17 through FIG. 7 that when the depth-of-field and diffraction  
18 curves intersect **100** below the film grain size, any  $f_{stop}$  value in  
19 the region where the depth-of-field and diffraction curves are  
20 below the film grain curve, provides the maximum resolution as  
21 limited by the film grain size. As the diffraction curve crosses  
22 the film grain curve, the diffraction effect limits the  
23 resolution. The  $f_{stop}$  computed by the invention **102** therefore  
24 provides equal resolution to the  $f_{stop}$  provided by the

1 conventional computation **104** in this long-range photography case;  
2 however, the invention provides insight into a range of  $f_{stop}$   
3 values that achieve this optimal resolution. For this long-range  
4 photography scenario, all  $f_{stop}$  in the region where the  
5 diffraction spot size is less than the film grain spot size  
6 provide a resolution equal to the film grain spot size **106**;  
7 otherwise, diffraction limits the resolution. The  $f_{stop}$  providing  
8 maximum resolution is therefore an  $f_{stop}$  in the range in which the  
9 film grain size remains the dominating effect.

10 FIGS. 5, 6, and 7 illustrate the invention that stipulates  
11 for a predetermined depth-of-field, the optimal  $f_{stop}$  is the  
12 intersection of the diffraction and depth-of-field curves. If  
13 this intersection is greater than the film grain spot size, the  
14 intersection provides the optimal resolution; alternately, if the  
15 intersection is less than the film grain spot size, the invention  
16 provides a range of suitable  $f_{stop}$  values that provide maximum  
17 resolution, however that resolution is provided by the film grain  
18 spot size.

19 The intersection of the depth-of-field and diffraction  
20 curves requires solving equations (3) and (4) simultaneously for  
21  $f_{stop}$ , assuming  $f \ll o$  and  $d \ll o$ , setting  $\lambda = 4000$  angstroms, and  
22 specifying  $f$  in millimeters, thereby resulting in the following  
23 computation for the optimal  $f_{stop}$ :

$$24 \quad \text{optimal } f_{stop} = f * \text{sqrt}(d) / o \quad (5)$$

1                   where:

2                     $f$  is in millimeters;

3                     $o$  is in meters; and,

4                     $d$  is in meters.

5       Since  $\lambda$  ranges between 4000 and 7000 angstroms, and equation (5)  
6       was derived using  $\lambda=4000$  angstroms, equation (5) provides an  
7       upper bound on the optimal  $f_{\text{stop}}$ .

8               When the optimal expression for  $f_{\text{stop}}$  from equation (5) is  
9       substituted into equation (4), and the same assumptions are made  
10       that  $f \ll o$ ,  $d \ll o$ ,  $\lambda=4000$  angstroms, and specifying  $f$  in  
11       millimeters, the following expression for optimal resolution  
12       results:

13               optimal resolution =  $f \cdot \sqrt{d} / o$  microns                   (6)

14                   where:

15                     $f$  is in millimeters;

16                     $o$  is in meters; and,

17                     $d$  is in meters.

18               Equations (5) and (6) indicate that the optimal  $f_{\text{stop}}$  and  
19       optimal resolution expressions are computationally identical.  
20       The photographer must merely compute the expression  $f \cdot \sqrt{d} / o$   
21       and interpret the result as being the optimal  $f_{\text{stop}}$  or the optimal  
22       resolution in microns. If the resolution is smaller than the  
23       film grain resolution, the film grain limits the image  
24       resolution; otherwise, diffraction and depth-of-field effects

1 limit the resolution and the invention provides the optimal  
2 resolution  $f_{stop}$  for the given depth-of-field.

3 Because  $f_{stop}$  settings are discrete rather than continuous,  
4 photographic equipment may not contain the exact  $f_{stop}$  provided by  
5 equation (5). Since equation (5) assumes  $\lambda=4000$  angstroms and  
6  $d \ll o$ , equation (5) provides an upper bound for the optimal  $f_{stop}$ ;  
7 therefore, in setting photographic equipment for the optimal  $f_{stop}$   
8 computed by equation (5), the  $f_{stop}$  closest to the computed  $f_{stop}$ ,  
9 but not exceeding the computed  $f_{stop}$ , should be chosen.

10 Although equations (5) and (6) are accurate, reliable, and  
11 easily computed expressions for the optimal  $f_{stop}$  and optimal  
12 resolution in microns, the expressions were derived using the  
13 approximations that  $f \ll o$ ,  $d \ll o$ ,  $\lambda=4000$  angstroms, and  $f$  units of  
14 millimeters. Expressions (5) and (6) are therefore referred to  
15 as the "field technique" or approximate method, as the  
16 computations may be simply computed. For more exact  
17 computations, the optimal  $f_{stop}$  follows, derived by solving  
18 equations (3) and (4) simultaneously for  $f_{stop}$ :

$$19 \quad \text{exact optimal } f_{stop} = f \cdot \sqrt{d / (2.44 \cdot \lambda \cdot o \cdot (o - d))} \quad (7)$$

20 where:

21  $\lambda$  is in meters;

22  $f$  is in meters;

23  $o$  is in meters; and,

24  $d$  is in meters.

1 For photographers desiring an exact computation of the optimal  
2  $f_{\text{stop}}$  or resolution in microns, the computation described by  
3 equation (7) may be used. Because equation (7) is more complex  
4 than equations (5) or (6), it is anticipated that a computer or  
5 calculator could be programmed or utilized in solving equation  
6 (7). The computer or calculator may be integrated with the  
7 camera, or a separate device. The same devices and  
8 configurations may be utilized for the field technique; however,  
9 the field technique's relative simplicity increases the  
10 likelihood that a the optimal  $f_{\text{stop}}$  can be computed without any  
11 extraneous device.

12 Referring now to FIG. 8, there is shown a procedure **110** for  
13 determining the optimum  $f_{\text{stop}}$  and resolution. The general  
14 photographic procedure **112** is not altered until the  $f_{\text{stop}}$   
15 determination is required. The general photographic procedure  
16 includes choosing a film speed **112a**, selecting a lens focal  
17 length **112b**, choosing a shutter speed **112c**, focusing the object  
18 **112d**, and obtaining values for focal length, object distance, and  
19 depth-of-field **112e**. The invention presented herein is then  
20 inserted into the general photographic procedure to provide the  
21 optimal  $f_{\text{stop}}$  for the desired depth-of-field. The photographer  
22 must first determine whether the exact or approximate  $f_{\text{stop}}$  will  
23 be computed **114**. If the approximate or field technique is being  
24 implemented, the approximate  $f_{\text{stop}}$  established by equation (5) is

1        computed **116**, and the camera is adjusted using the  $f_{\text{stop}}$  closest  
2        to, but not exceeding, the  $f_{\text{stop}}$  provided by equation (5) **118**.  
3        This  $f_{\text{stop}}$  value is equivalent to the resolution in microns.  
4        Alternately, if the exact method is desired, the exact  $f_{\text{stop}}$  is  
5        computed using equation (7) **120**, and the camera is adjusted to  
6        the closest discrete  $f_{\text{stop}}$  **122**. Once the camera is adjusted for  
7        the computed  $f_{\text{stop}}$ , at **118** or **122**, the shutter release may be  
8        depressed **124**.

9                The advantage of the present invention over the prior art is  
10        that the invention provides a method and apparatus to determine  
11        an  $f_{\text{stop}}$  to provide optimal resolution for a specified depth-of-  
12        field. Within the method provided, an estimate and an exact  
13        procedure are identified depending upon the computational  
14        resources available.

15                What has thus been described is a method and apparatus to  
16        determine the  $f_{\text{stop}}$  that provides optimal image resolution for a  
17        predetermined depth-of-field. An approximate and exact method  
18        and apparatus are provided to determine the optimal resolution  
19         $f_{\text{stop}}$ . The optimal resolution  $f_{\text{stop}}$  is a function of the lens  
20        focal length, depth-of-field in front of the object, wavelength  
21        of light, and distance of the object to the lens center. Once  
22        the optimal resolution  $f_{\text{stop}}$  is determined, the camera is adjusted  
23        to the closest discrete  $f_{\text{stop}}$  available. When the approximate

1 field technique is utilized, the camera must be adjusted to the  
2 discrete  $f_{\text{stop}}$  closest to, but not exceeding, the computed  $f_{\text{stop}}$ .

3 Although the present invention has been described relative  
4 to a specific embodiment thereof, it is not so limited.

5 Obviously many modifications and variations of the present

6 invention may become apparent in light of the above teachings.

7 For example, the computations may be performed with or without

8 the assistance of electronics; and such electronics may or may

9 not be integrated to the camera for automatic adjustment. The

10 desired depth-of-field in front of the object may be approximated

11 or measured using a range finder, etc. Although the wavelength

12 of light range specified the visible spectrum, other spectra

13 (e.g., infrared) are also valid in the optimal  $f_{\text{stop}}$  computations.

14 Many additional changes in the details, materials, steps and

15 arrangement of parts, herein described and illustrated to explain

16 the nature of the invention, may be made by those skilled in the

17 art within the principle and scope of the invention. It is

18 therefore understood that

19 the invention may be practiced otherwise than as

20 specifically described.

1 Attorney Docket No. 79064

2

3 OPTIMAL FSTOP/RESOLUTION APPARATUS AND METHOD

4 FOR SPECIFIED DEPTH-OF-FIELD

5

6 ABSTRACT OF THE DISCLOSURE

7 A method and apparatus to determine the  $f_{\text{stop}}$  that provides  
8 optimal image resolution for a predetermined depth-of-field. An  
9 approximate and exact method and apparatus are provided to  
10 determine the optimal resolution  $f_{\text{stop}}$ . The optimal resolution  
11  $f_{\text{stop}}$  is a function of the lens focal length, depth-of-field in  
12 front of the object, wavelength of light, and distance of the  
13 object to the lens center. Once the optimal resolution  $f_{\text{stop}}$  is  
14 determined, the camera is adjusted to the closest discrete  $f_{\text{stop}}$   
15 available. When the approximate field technique is utilized, the  
16 camera must be adjusted to the discrete  $f_{\text{stop}}$  closest to, but not  
17 exceeding, the computed  $f_{\text{stop}}$ .

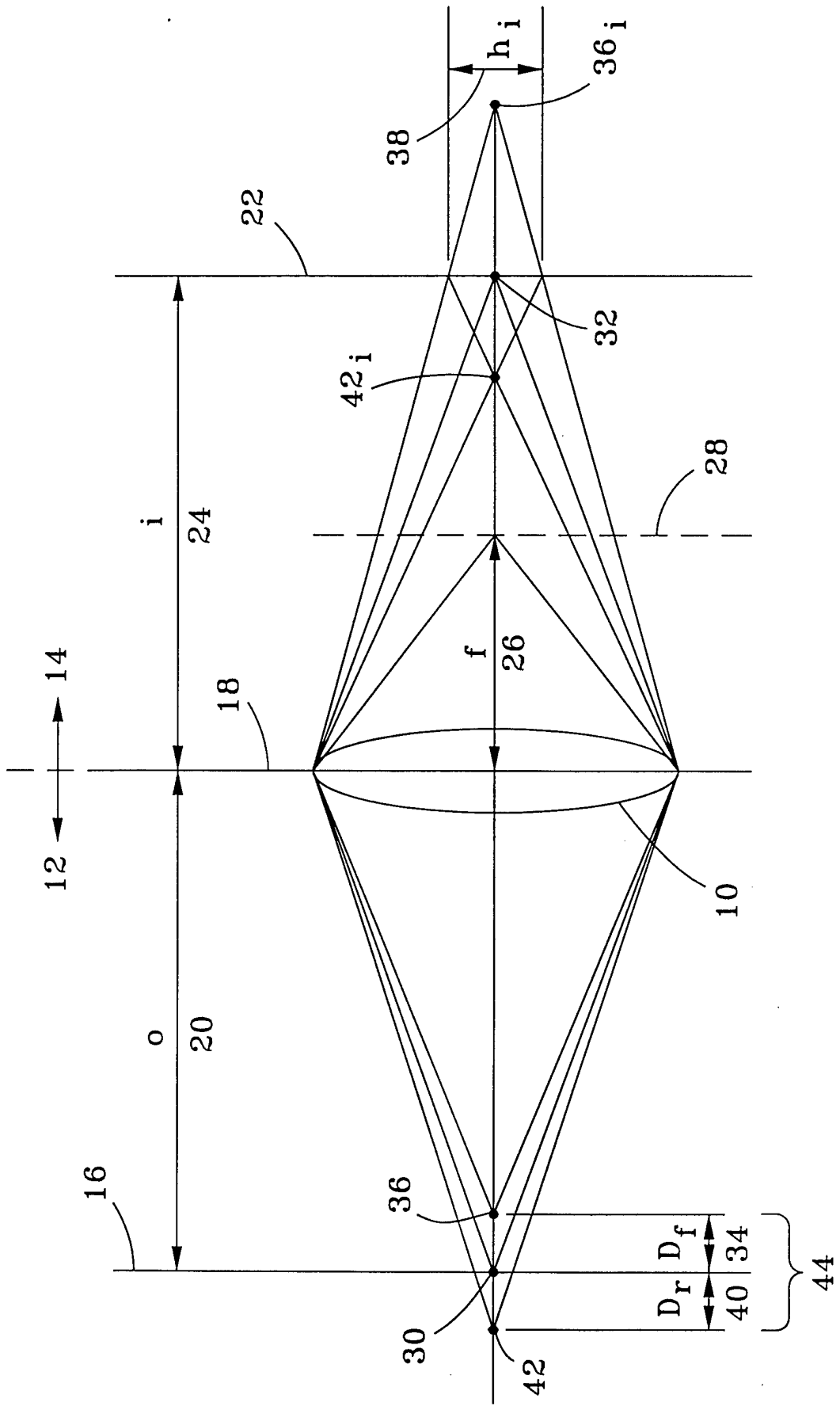


FIG. 1

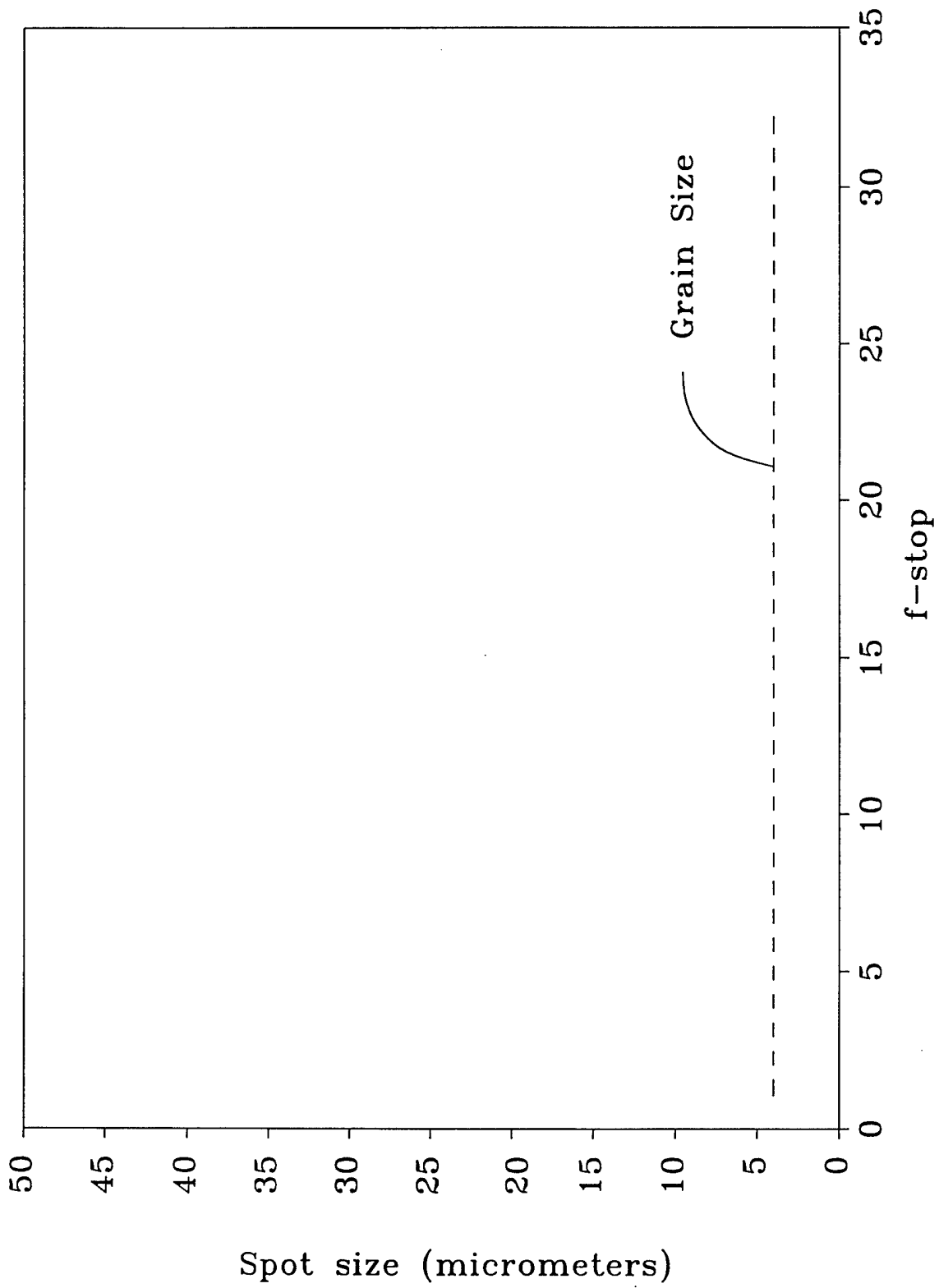


FIG. 2

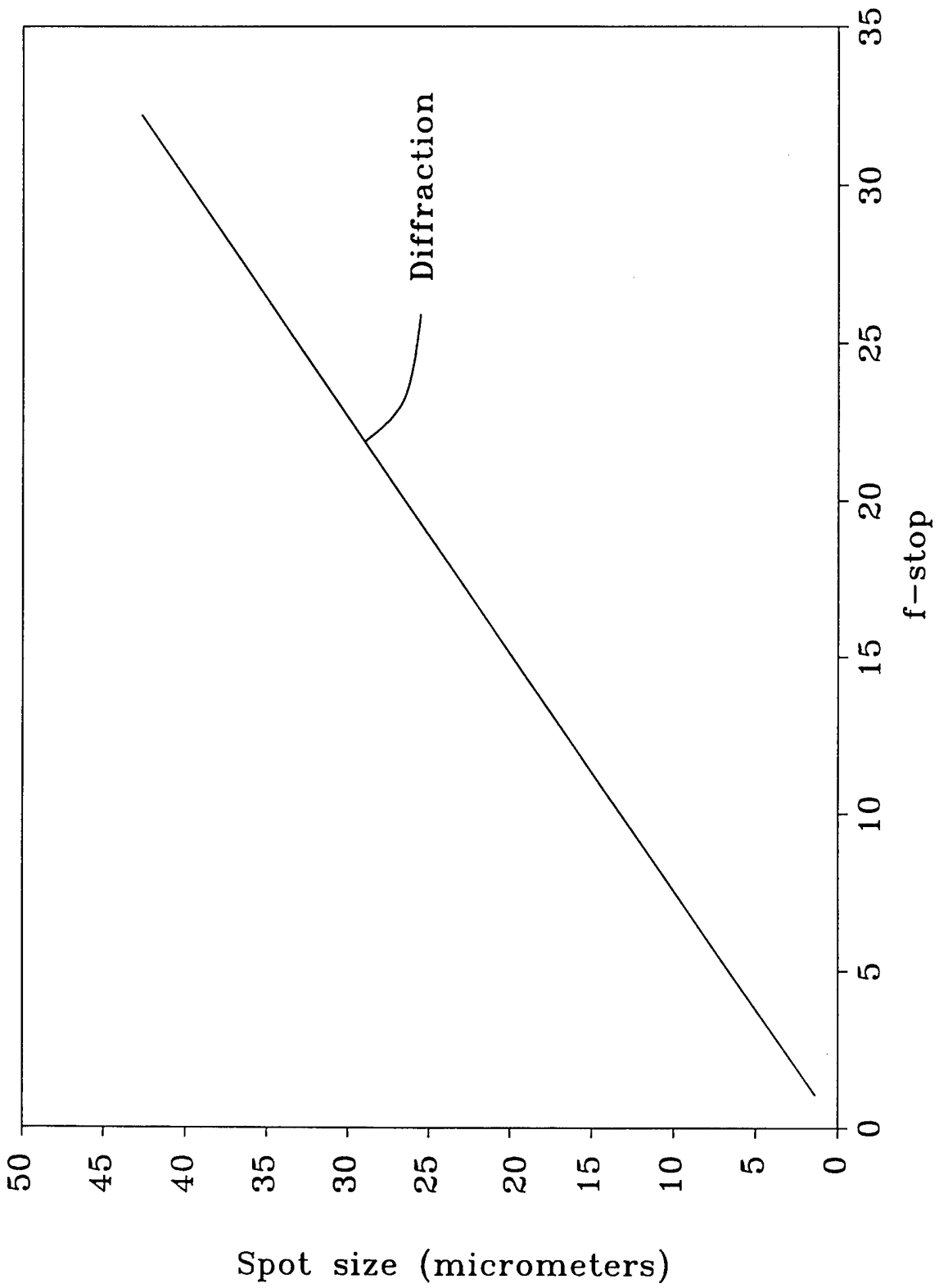


FIG. 3

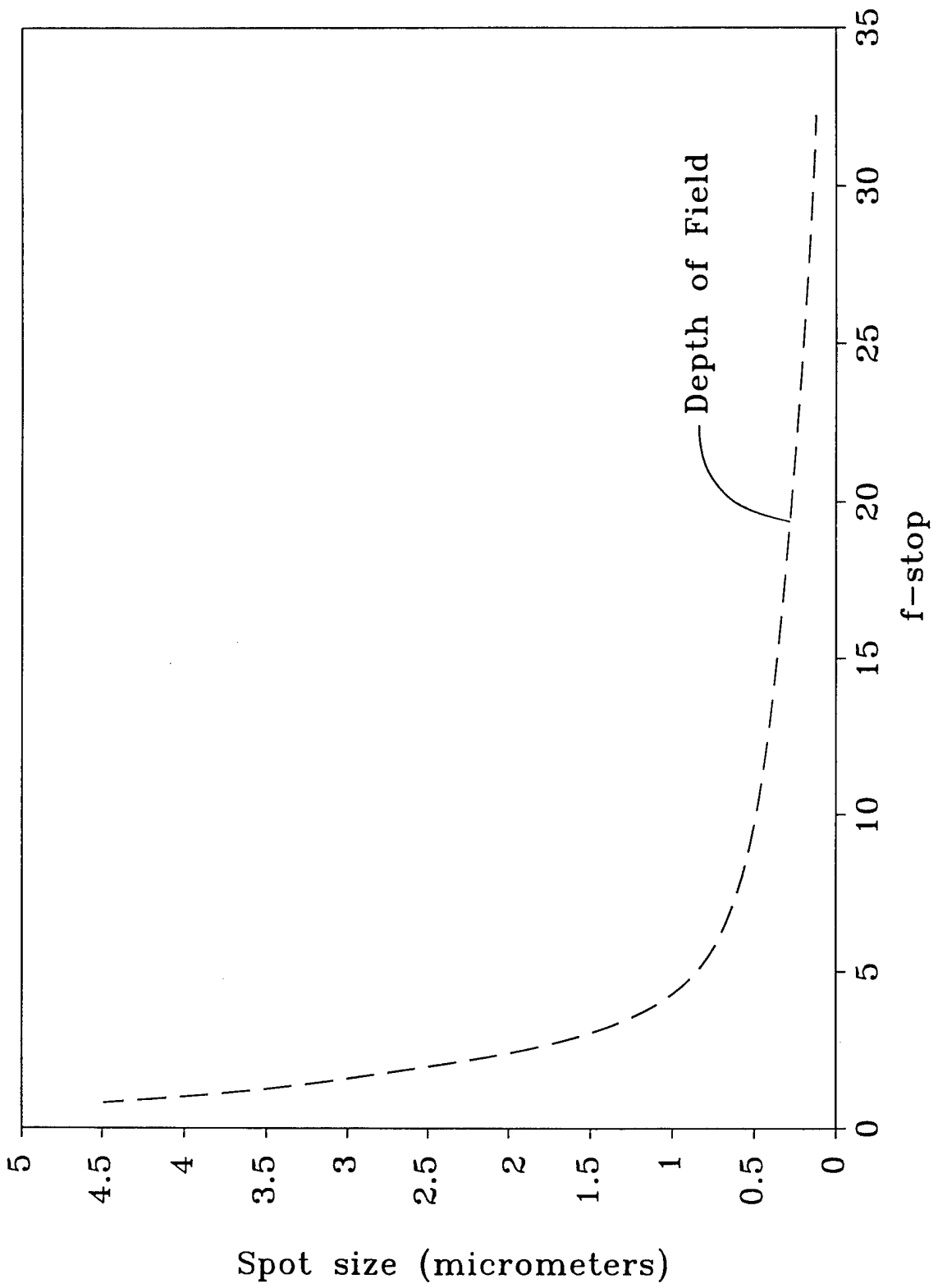


FIG. 4

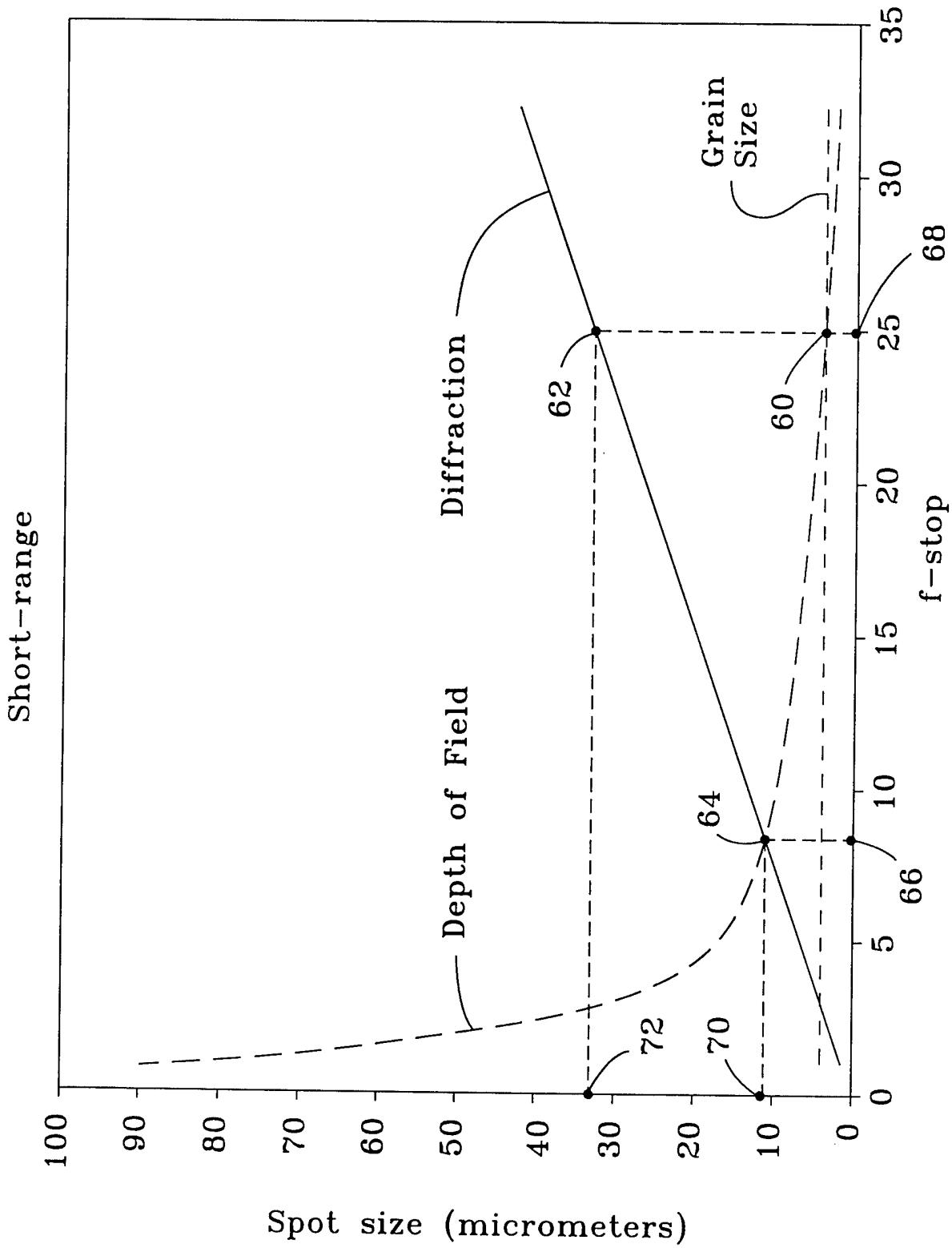


FIG. 5

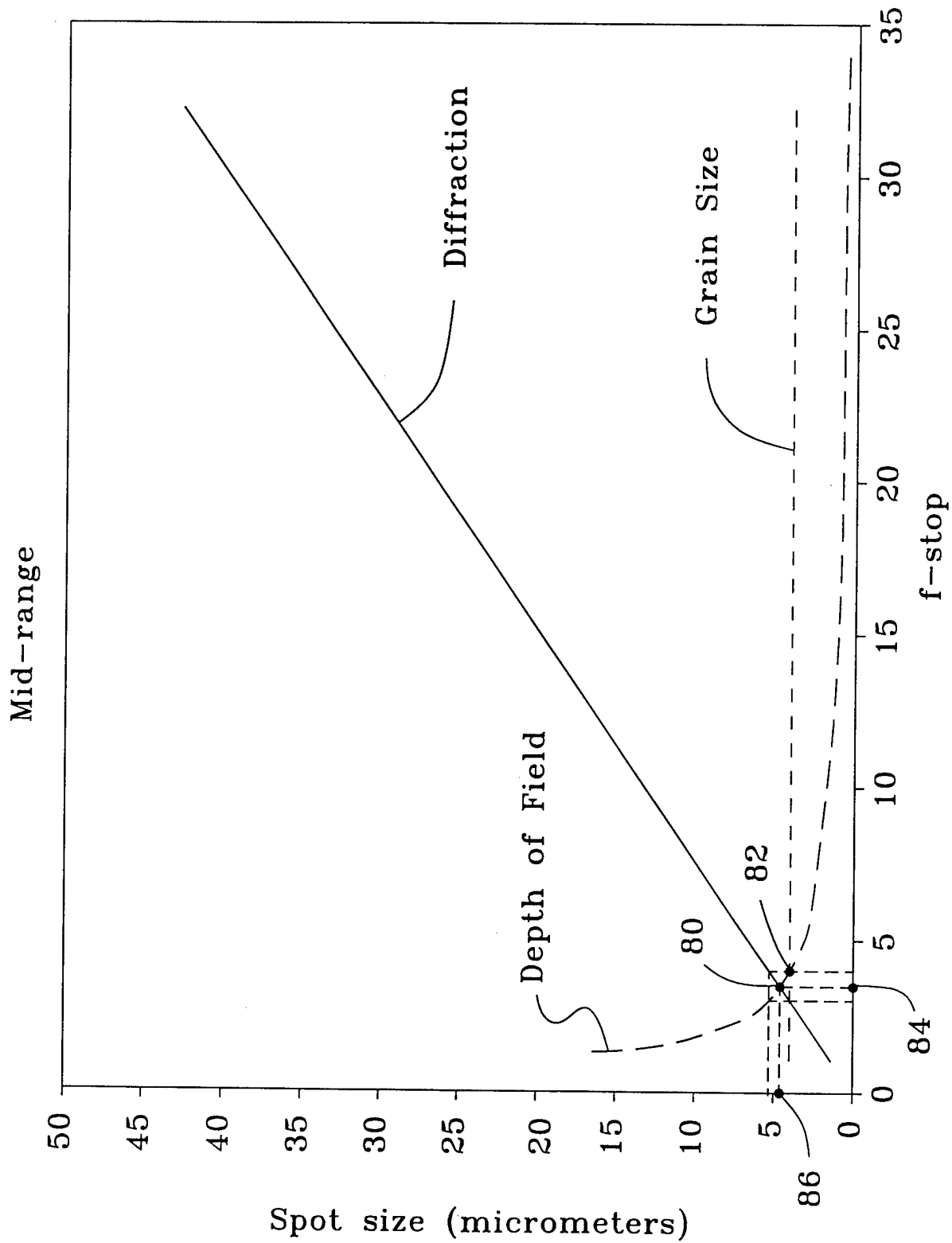


FIG. 6

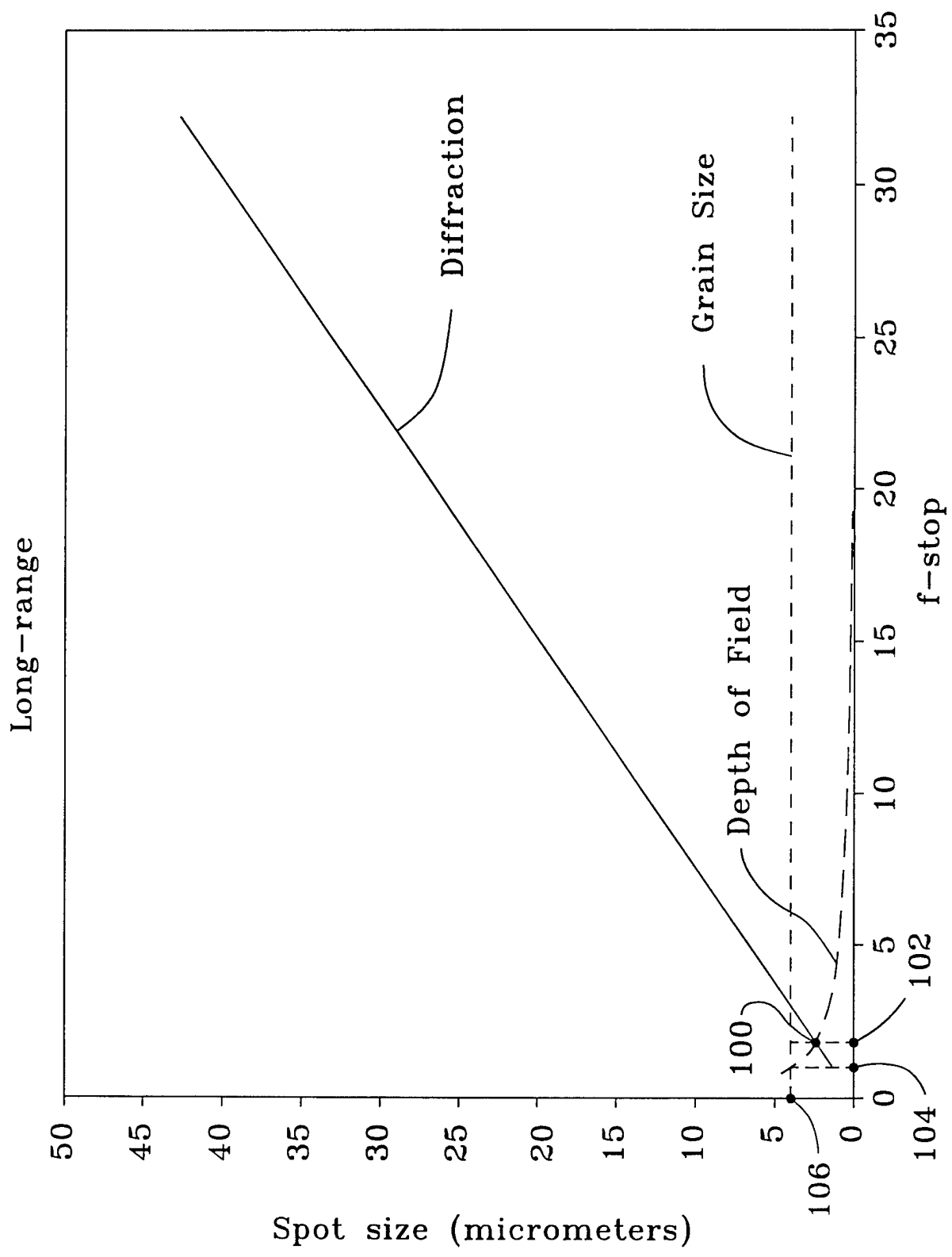


FIG. 7

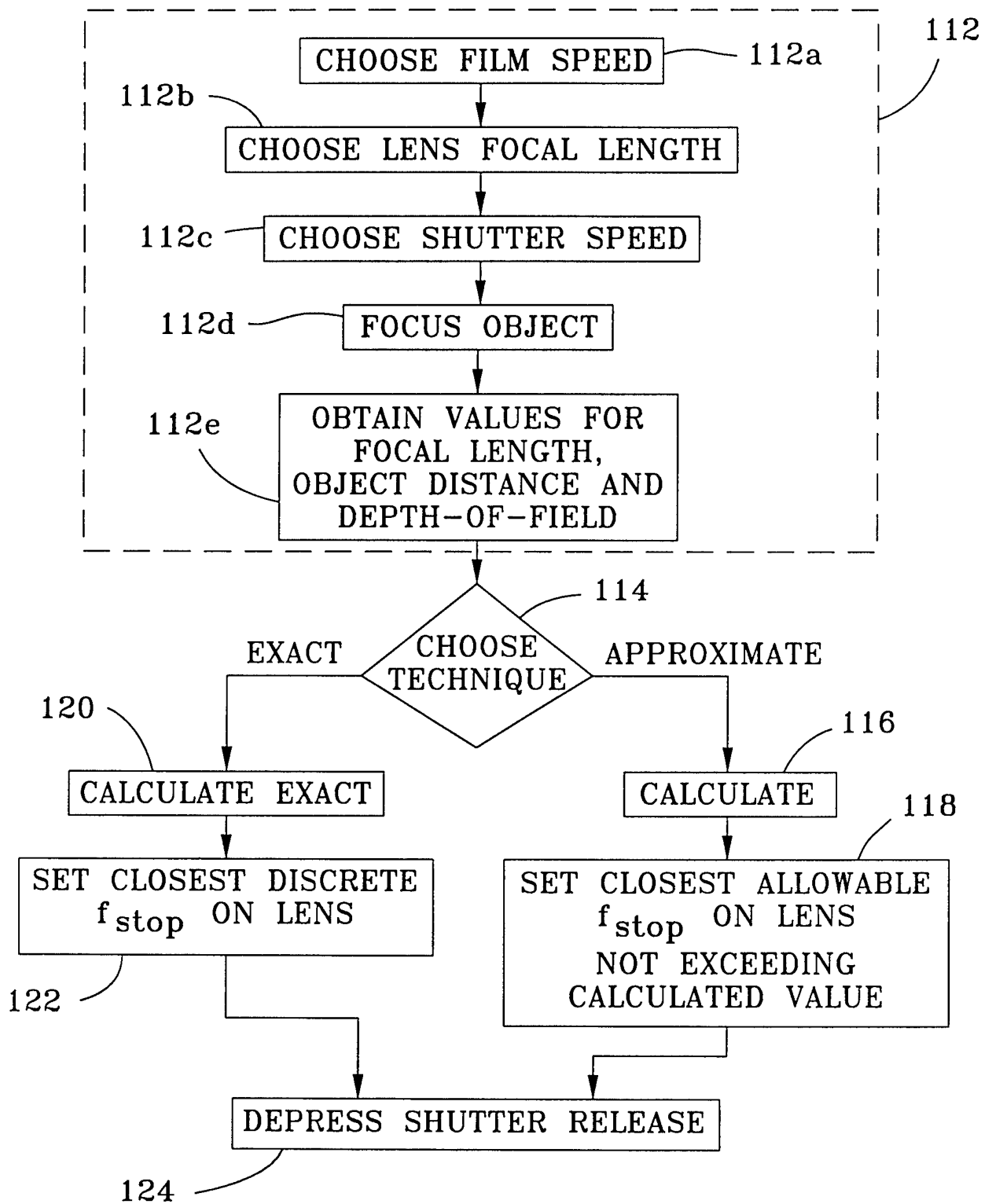


FIG. 8