

Serial Number 09/548,387
Filing Date 11 April 2000
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METHOD AND APPARATUS FOR DETERMINING LINEAR

AND ANGULAR VELOCITY OF A MOVING BODY

STATEMENT OF GOVERNMENT INTEREST

7 The invention described herein may be manufactured and used
8 by or for the Government of the United States of America for
9 governmental purposes without the payment of any royalties
10 thereon or therefor.

BACKGROUND OF THE INVENTION

(1) Field Of The Invention

The present invention generally relates to a method and
system for determining the velocity of a moving body, and more
particularly to a method and system for determining the linear
and angular velocity of a moving body using the Barkhausen
effect.

(2) Description of the Prior Art

Magnetic sensors are commonly used in determining the
velocity of moving bodies. Some of the conventional sensors
typically used today are Hall Effect sensors, fluxgate sensors,
magneto-resistive sensors, magnetostrictive sensors,

1 magnetoinductive sensors and SQUID sensors. However, these
2 devices have several disadvantages. For example, the SQUID
3 sensor can only operate properly at superconductive temperatures.
4 The flip coil magnetometer utilizes moving parts thereby creating
5 problems associated with component malfunction and replacement.
6 Hall Effect sensors, fluxgate sensors, magneto-resistive sensors,
7 magnetostrictive sensors, magnetoinductive sensors all require an
8 external bias or bridge-type circuit for proper operation. What
9 is needed is a sensor that is a passive device and which can
10 operate at room temperature. A further desired feature is that
11 it must be simple in construction in order to reduce the costs
12 related to manufacturing, maintenance and repair.

13

14 SUMMARY OF THE INVENTION

15 Therefore, it is an object of the present invention to
16 provide a system and method for measuring the velocity of a
17 moving body that does not exhibit or present the problems and
18 disadvantages of conventional sensors.

19 It is another object of the present invention to provide a
20 passive system for measuring the velocity of a moving body.

21 It is a further object of the present invention to provide a
22 system for measuring the velocity of a moving body that can
23 operate at room temperature.

1 It is yet another object of the present invention to provide
2 a system for measuring the velocity of a moving body that is
3 relatively less complex in design and construction than
4 conventional systems.

5 Other objects and advantages of the present invention will
6 be apparent to one of ordinary skill in the art in light of the
7 ensuing description of the present invention.

8 The present invention is directed to a method and system for
9 determining the rotational (or angular) or linear velocity of a
10 moving body. The system utilizes a Barkhausen Effect magnetic
11 field sensor. In one embodiment, the Barkhausen Effect magnetic
12 field sensor comprises a coil wound about a silicon-steel core.
13 In one embodiment, the coil comprises a predetermined number of
14 turns of magnet wire. A permanent magnet is attached to the body
15 whose motion is to be monitored in order to determine its
16 velocity. As the body moves, the permanent magnet realigns
17 small, atomic size magnetic domains in the silicon-steel core
18 and, as a result of Faradays law, e.m.f. (electromotive force)
19 impulses (also known as "inductive kicks") are produced in the
20 coil. As the velocity of the body increases, a plurality of
21 e.m.f. impulses are created which define a distinct signal. This
22 analog voltage is filtered, amplified and then converted into a
23 digital signal. The digital signal is then fed into other signal

1 processing circuitry that processes the signal to determine the
2 velocity of the moving body.

3

4 BRIEF DESCRIPTION OF THE DRAWINGS

5 The features of the invention are believed to be novel and
6 the elements characteristic of the invention are set forth with
7 particularity in the appended claims. The figures are for
8 illustration purposes only and are not drawn to scale. The
9 invention itself, however, both as to organization and method of
10 operation, may best be understood by reference to the detailed
11 description which follows taken in conjunction with the
12 accompanying drawings in which like reference numerals refer to
13 like parts and in which:

14 FIG. 1 is a block diagram illustrating the system of the
15 present invention and a moving body, the velocity of which is
16 being measured by the aforementioned system;

17 FIG. 2 is a diagram of a Barkhausen Effect Passive Magnetic
18 Field Sensor utilized in the system shown in FIG. 1; and

19 FIG. 3 is a block diagram illustrating a feed back system
20 that utilizes the system of the present invention.

21

1 DESCRIPTION OF THE PREFERRED EMBODIMENT

2 The present invention provides a new and improved system and
3 method for accurately determining the rotational (angular) or
4 linear velocity of a moving body. Referring to FIG. 1, there is
5 shown a moving body that is indicated by the numeral 10. Moving
6 body 10 can be a moving gear, moving machinery components,
7 turbines, etc. In accordance with the present invention, magnet
8 12 is attached to moving body 10. In a preferred embodiment,
9 magnet 12 is a permanent magnet. The purpose of magnet 12 will
10 be discussed in the ensuing description.

11 Referring to FIG. 1, there is shown system 14 of the present
12 invention. System 14 generally comprises magnetic field sensor
13 16, filter 18, amplifier 20, analog-to-digital converter (ADC) 22
14 and signal processing circuitry 24.

15 Referring to FIG. 2, in accordance with the present
16 invention, magnetic field sensor 16 is configured as a Barkhausen
17 Effect passive magnetic field sensor. Sensor 16 comprises core
18 26 and a coil 28 that is wound about core 26. In one embodiment,
19 the coil 28 comprises a plurality of turns of conductor or wire
20 28a. It is highly preferable that core 26 be fabricated from
21 ferro-magnetic material. In a preferred embodiment, wire 28a is
22 preferably fabricated from tin-coated copper or other well known
23 conductors that exhibit a relatively low resistance per unit of

1 length such as copper, silver or gold. In a preferred
2 embodiment, wire 28a is sized between 24 AWG and 28 AWG,
3 inclusive, and is coated with a substance such as lacquer or
4 varnish. Such a wire configuration is known in the art as
5 "magnet wire". The use of magnet wire, with its thin wall of
6 insulation, reduces the size of coil 28 or size of the volume of
7 sensor 16. In a preferred embodiment, the plurality of turns is
8 between about 2500 and 3500 turns, inclusive.

9 Referring to FIG. 2, core 26 may be fabricated from a
10 variety of magnetic materials. For example, in one embodiment,
11 core 26 is fabricated from silicon-steel. Other materials can
12 also be used, such as magnesium-zinc ferrite, nickel-zinc
13 ferrite, silicon iron, etc. In a preferred embodiment, magnetic
14 core 26 has a DC permeability (relative) between about 100 and
15 1000, inclusive.

16 Referring to FIGS. 1 and 2, as body 10 and magnet 12 move
17 with respect to sensor 16, a time-varying magnetic field is
18 created between magnet 12 and core 26. This magnetic field
19 produces a statistical realignment of the magnetic domains in
20 core 26. Ferromagnetic materials exhibit jumps in magnetization
21 in the presence of an applied magnetic field of increasing
22 strength. This phenomenon is commonly known as the Barkhausen
23 effect. The effect is a result of the motion of domain wall

1 boundaries of the material in response to a fluctuating field.
2 The pattern of jumps gives important information about the
3 material microstructure that is used to characterize photo-
4 optical devices and recording media. Each realignment produces
5 an inductive voltage kick, the sum total of which induces a time-
6 varying voltage (e.m.f.) in wire 28a. This induced voltage is
7 the result of the relationship between induced voltage and time-
8 varying magnetic flux linkage defined by Faraday's Law which may
9 be expressed as the following formula:

$$v = N (d\phi/dt)$$

11 wherein v is the induced voltage, ϕ is the magnetic flux that
12 links the coil, t is time, and N is the number of turns in the
13 coil 28 (i.e., the number of turns of wire 28a around core 26).
14 Thus, the magnitude of the generated flux is related to the
15 permeability of the magnetic material from which core 26 is
16 fabricated, and the magnitude of the induced voltage v is
17 directly proportional to the product of the number of turns N and
18 the change in flux for a particular time interval. Thus, as
19 permeability increases, so will flux linkage and induced voltage.

20 One important feature and advantage of sensor 16 is that it
21 is passive and does not require an external bias (power supply
22 voltage) or a bridge circuit to operate. Another feature and

1 advantage of sensor 16 is that it operates at room temperature.
2 Thus, no special environment is required for proper operation of
3 sensor 16.

4 Referring to FIGS. 1 and 2, ends 29a and 29b of wire 28a are
5 used as inputs to filter 18. Filter 18 filters out extraneous
6 noise signals. In one embodiment, filter 18 comprises a passive
7 noise filter. In another embodiment, filter 18 is configured as
8 a DSP (Digital Signal Processing) filter. In a preferred
9 embodiment, the signal-to-noise (S/N) ratio of filter 18 is at
10 least about 13dB (decibel). The output of filter 18 is then fed
11 into amplifier 20. In a preferred embodiment, amplifier 20 is a
12 low-noise amplifier. Preferably, amplifier 20 has a noise figure
13 between about 6dB and 10dB, inclusive. Preferably, amplifier 20
14 has a 3dB bandwidth between about 100Hz and 10kHz, inclusive.
15 Amplifier 20 may be realized in any one of a variety of
16 configurations, e.g. integrated circuits, discrete components,
17 etc.

18 Referring to FIG. 1, the output of amplifier 20 is fed into
19 ADC 22. The signal fed into ADC 22 is sampled at a predetermined
20 sampling rate. The sampled signal is converted into a multi-bit
21 digital signal that represents the sampled amplitude. In one
22 embodiment, the sampling rate is between about 50kHz and 100kHz,
23 inclusive. The digital signals outputted by ADC 22 are fed into

1 signal processor 24. Signal processor 24 effects real-time
2 manipulation of the digital signals outputted from ADC 22. Such
3 manipulation includes the application of various signal
4 processing algorithms such as FFTs (Fast Fourier Transforms),
5 DFTs (Discrete Fourier Transforms) and algorithms that perform
6 various other operations on the signal data, e.g. interpolation,
7 averaging, etc. Specifically, signal processor 24 uses
8 particular information from the digital signals outputted from
9 ADC 22 such as (i) the magnitude of the signals, (ii) the
10 frequency of signals having particular magnitudes, and (iii) the
11 repetition of certain signal patterns, in order to determine the
12 velocity of moving body 10 and whether the velocity is rotational
13 (angular) or linear. Additionally, system 14 may be calibrated
14 using known rotational or linear velocities. In one embodiment,
15 circuitry 24 includes a memory storage device, such as a random
16 access memory (RAM), to store signal information and the results
17 of all mathematical calculations.

18 Referring to FIG. 3, in one embodiment, the output of signal
19 processor 24 is fed into display device 30. Display device 30
20 can be a computer screen, oscilloscope, video monitor, cathode-
21 ray-tube, liquid-crystal-display, etc. Additional driver or
22 buffer circuitry, well known in the art, may be needed to couple
23 the output of signal processor 24 to the input of display device

1 30 to prevent signal degradation. As shown in FIG. 3, system 10
2 can also be used to effect a feedback system. In such a feedback
3 system, the output of signal processor 24 is fed into correction
4 circuitry 32 which compares the current velocity of the moving
5 body to a preset, predetermined or desired velocity. Correction
6 circuitry 32 outputs error signal 34 that is fed into control
7 circuitry 36. In response to error signal 34, control circuitry
8 36 increases, decreases or maintains the velocity of moving body
9 10.

10 Thus, the system of the present invention achieves the
11 objects set forth above. Specifically, the system of the present
12 invention:

- 13 a) utilizes a sensor that is passive and does not require
14 biasing or bridge circuitry for operation;
- 15 b) utilizes a sensor that can properly operate at room
16 temperature;
- 17 c) provides accurate and consistent measurements;
- 18 d) can be implemented with a variety of hardware and software
19 systems and components; and
- 20 e) can be implemented at a relatively low cost.

21 While the present invention has been particularly described,
22 in conjunction with a specific preferred embodiment, it is

1 evident that many alternatives, modifications and variations will
2 be apparent to those skilled in the art in light of the foregoing
3 description.

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1 Attorney Docket No. 78765

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METHOD AND APPARATUS FOR DETERMINING LINEAR

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AND ANGULAR VELOCITY OF A MOVING BODY

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ABSTRACT OF THE DISCLOSURE

7 An apparatus and method for determining linear and angular
8 velocity of a moving body. A magnet is attached or fixed to the
9 body, the velocity of which is to be determined. The apparatus
10 comprises a sensor comprising a core of magnetic material and a
11 coil wound about the core. The movement of the body and magnet
12 relative to the core effects a time-varying magnetic field
13 between the magnet and the core thereby producing Barkhausen
14 effect time-varying voltage signals in the coil. The apparatus
15 further comprises a system for detecting and processing the time-
16 varying voltage signals so as to effect a transformation of the
17 signals into data defining the velocity of the moving body.

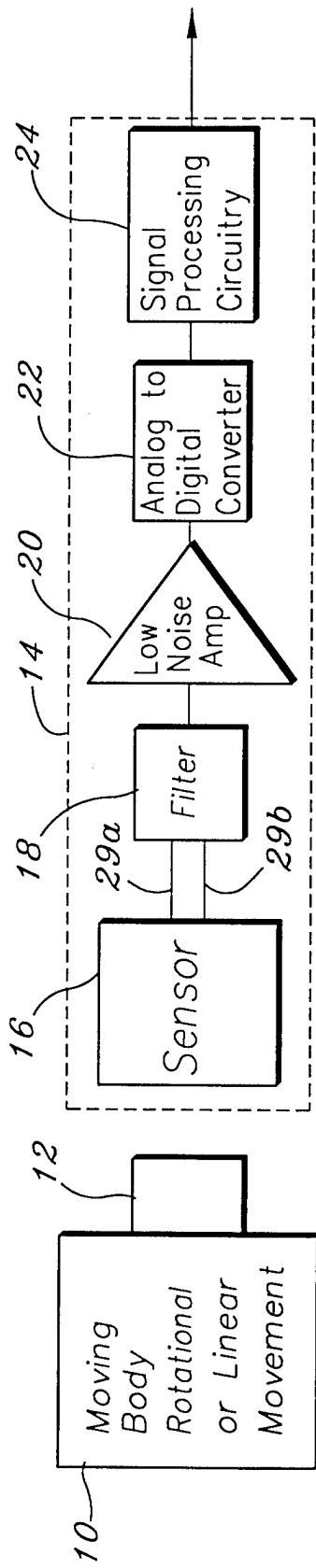


Fig. 1

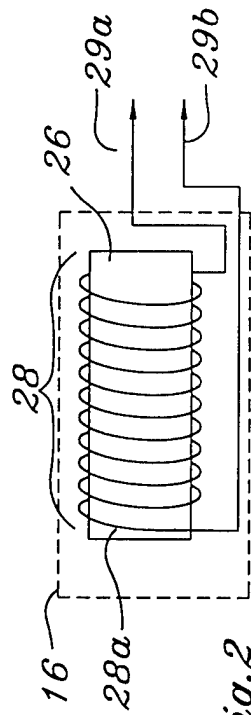


Fig. 2

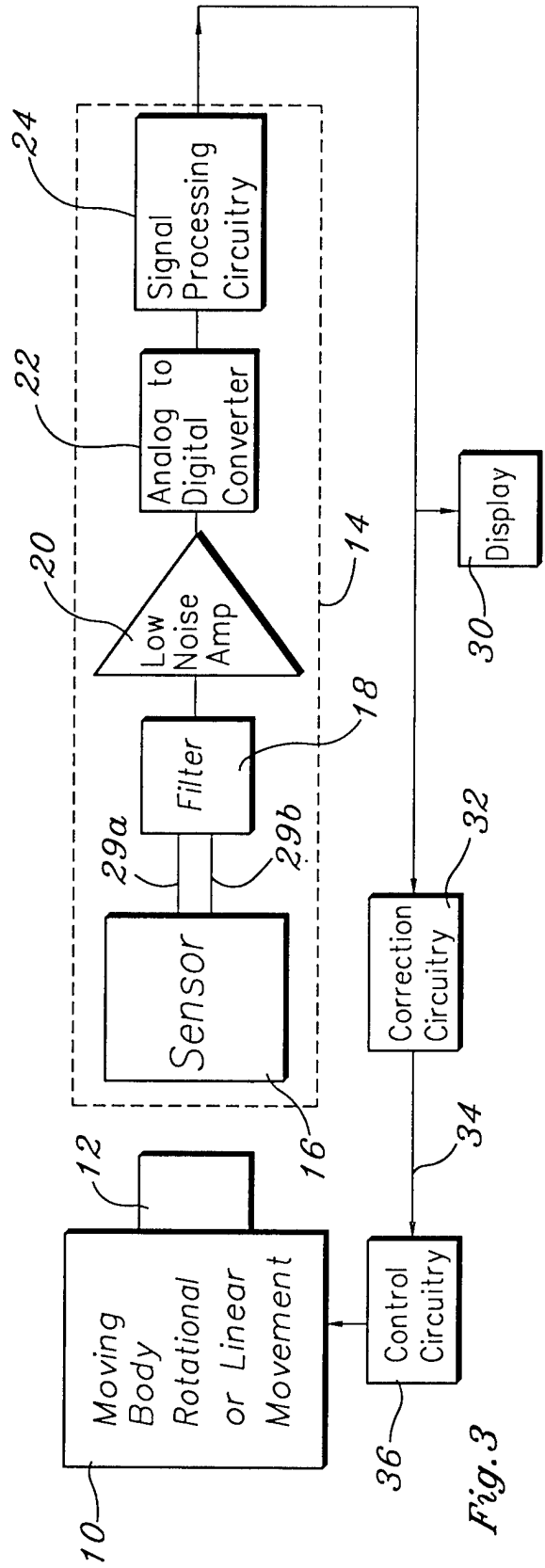


Fig. 3