

FIBER OPTIC PITCH OR ROLL SENSOR

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT (1) GREGORY H. AMES, citizen of the United States of America, employee of the United States Government, a resident of Wakefield, County of Washington, State of Rhode Island, have invented certain new and useful improvements entitled as set forth above of which the following is a specification.

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PATENT TRADEMARK OFFICE

1 Attorney Docket No. 78381

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3 FIBER OPTIC PITCH OR ROLL SENSOR

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5 STATEMENT OF GOVERNMENT INTEREST

6 The invention described herein may be manufactured and used
7 by or for the Government of the United States of America for
8 governmental purposes without the payment of royalties thereon
9 or therefore.

10

11 CROSS REFERENCE TO OTHER PATENTS

12 This patent application is co-pending with two related
13 patent applications entitled MULTIPLEXED FIBER LASER SENSOR
14 SYSTEM (Attorney Docket No. 78371) and FIBER OPTIC CURVATURE
15 SENSOR FOR TOWED HYDROPHONE ARRAYS (Attorney Docket No. 78333),
16 by the same inventors as this application.

17

18 BACKGROUND OF THE INVENTION

19 (1) Field of the Invention

20 This invention relates to a device for sensing the local
21 gravitational field so as to provide a roll or pitch sensor.
22 The device of the present invention, in combination with other
23 sensors, may be used to determine the shape of a towed
24 hydrophone array.

1 (2) Description of the Prior Art

2 Sensors which employ optical fibers to measure physical
3 motion of a structure are known in the prior art. For example,
4 U.S. Patent Nos. 4,788,868 to Wilk; 4,654,520 to Griffiths; and
5 4,812,645 to Griffiths illustrate structural monitoring systems
6 using fiber optics. U.S. Patent No. 4,806,012 to Meltz et al.
7 illustrates a distributed, spatially resolving optical fiber
8 strain gauge in which the core of the optical fiber is written
9 with periodic grating patterns effective for transmitting and
10 reflecting light injected into the core. Spectral shifts in the
11 transmitted and reflected light indicate the intensity of the
12 strain or temperature variations at positions of the grating
13 corresponding to the associated wavelengths of injected light.
14 U.S. Patent No. 5,012, 679 to Haefner illustrates an optical
15 sensor which uses a beam waveguide embedded in a force or
16 pressure transmitting material, in particular an elastomer. To
17 be used as a force measuring sensor, the beam waveguide is
18 mounted on an elastic deformable body and embedded in a material
19 that does not undergo creep under the influence of a force.
20 None of these sensors have utility as a roll or pitch sensor.

21 Some towed hydrophone arrays require precise determination
22 of their shape in the water. This has been done in the past
23 with gimballed heading sensors. These devices are quite
24 expensive. It is desirable to reduce cost in the towed array.

1 Fiber optic hydrophone systems are under development and it is
2 desirable to provide shape sensing that is compatible and that
3 reduces the cost of the shape sensing.

4 An alternative way to determine array shape is by curvature
5 sensors and either roll or twist sensors. Roll sensors have the
6 advantage of sensing an absolute parameter at each point
7 measured.

8 SUMMARY OF THE INVENTION

9 Accordingly, it is an object of the present invention to
10 provide a fiber optic sensing device which may be used as a
11 fiber optic roll sensor or as a fiber optic pitch sensor.

12 It is yet another object of the present invention to
13 provide a fiber optic sensing device which may be used as a
14 fiber optic roll sensor or as a fiber optic pitch sensor in a
15 towed array.

16 It is a further object of the present invention to provide
17 a sensing device as above which is simple and relatively
18 inexpensive.

19 The foregoing objects are attained by the sensing device of
20 the present invention.

21 In accordance with the present invention, a sensing device
22 is provided which may be used as a roll sensor and/or as a pitch
23 sensor. The sensing device broadly comprises at least one
24 optical fiber supported in a structure, a movable mass supported

1 within the structure, and means for detecting changes in tension
2 in the at least one optical fiber due to movement of the movable
3 mass. The only deformable structure in the sensing device of
4 the present invention is the optical fiber(s), thereby
5 maximizing sensitivity.

6 Other details of the sensing device of the present
7 invention, as well as other objects and advantages attendant
8 thereto, are set forth in the following detailed description and
9 the accompanying drawings wherein like reference numerals depict
10 like elements.

11
12 BRIEF DESCRIPTION OF THE DRAWINGS

13 FIG. 1 is a sectional view of a sensing device in
14 accordance with the present invention;

15 FIG. 2 is a sectional view of the sensing device of the
16 present invention taken along lines 2 - 2 in FIG. 1;

17 FIG. 3 shows an alternative embodiment of the sensing
18 device of the present invention; and

19 FIG. 4 shows yet another alternative embodiment of the
20 sensing device of the present invention.

21
22 BRIEF DESCRIPTION OF THE PREFERRED EMBODIMENT(S)

23 A first embodiment of the sensing device of the present
24 invention is shown in FIGS. 1 and 2. As shown therein, the

1 sensing device 10 has a plurality of optical fibers 12 strung
2 under tension inside a cage 14.

3 The side wall 17 of the cage 14 has a plurality of notches
4 15. The notches 15 serve two purposes. First, they keep the
5 optical fibers 12 radially distributed in an even manner around
6 a mass 16. Second, the notches 15 provide a space so that the
7 optical fibers 12 are not crushed between the cage 14 and the
8 mass 16 during shock events. Instead, the outside surface 40 of
9 the mass 16 contacts the inside surface 41 of the cage 14,
10 limiting the travel without crushing any of the optical fibers
11 12.

12 While FIG. 2 shows the notches 15 in the side wall of the
13 cage 14, they could alternatively be located in the mass 16,
14 instead of the cage, as shown in FIG. 3.

15 As can be seen from FIGS. 1 and 2, the mass 16 is suspended
16 within a portion 19 of the cage 14 by the surrounding optical
17 fibers 12. The mass 16 is initially in contact with all of the
18 optical fibers 12. This places each of the optical fibers 12 in
19 a prestrained state. If the device 10 is disposed vertically,
20 all of the optical fibers 12 have the same prestrain. When the
21 device 10 is disposed horizontally and rolls, the relationship
22 of the optical fibers 12 and the mass 16 to the axis of the
23 gravitational field changes. The optical fiber or fibers 12 on
24 the bottom bear more weight and are strained greater than their

1 initial prestrain. The optical fiber or fibers 12 on the top
2 bear no weight and actually are strained less than their initial
3 prestrain as the mass 16 moves off axis downward.

4 As can be seen from the foregoing description, as the
5 device 10 rolls or pitches, the weight of the mass 16 will be
6 directly borne by different combinations of the optical fibers
7 12. This leads to a different tension in each of the fibers 12.

8 A fiber optic Bragg grating 18 is written into the core of
9 each optical fiber 12. The changing tension in each optical
10 fiber 12 results in a wavelength shift of the reflectivity peak
11 of the Bragg grating 18. Such a wavelength shift may then be
12 measured by a variety of means already disclosed in the
13 technical literature. For example, the measuring means may
14 utilize a broadband light source such as an Erbium doped
15 spontaneous emission source to illuminate the grating 18. The
16 reflection is analyzed with a spectrum analyzer to determine the
17 reflection peak wavelength. In another type of measuring means,
18 a scanning single wavelength laser is used. The reflection
19 versus the scan time is analyzed to determine the reflection peak
20 wavelength. The difference in wavelength shift determines the
21 difference in tension. The difference in tension between the
22 optical fibers 12 allows direct calculation of the local
23 direction of the gravitational field relative to the optical
24 fibers 12 and the cage 14.

1 The gap 20 between the sides of the suspended mass 16 and
2 the cage 14 is small so that the cage 14 limits the motion of
3 the mass 16 in shock or high acceleration and limits the maximum
4 tension seen by any optical fiber 12. The exact dimension of
5 the gap 20 depends on the mass of the mass 16, the diameters of
6 the optical fibers 12, and the number of optical fibers 12. The
7 gap 20 must be large enough to accommodate the movement of the
8 mass 16 away from the center as the device 10 rolls with some
9 room to spare.

10 Because the gratings 18 reflect at a distinct wavelength,
11 multiple sensors may be placed on the same optical fiber 12 with
12 gratings 18 placed at different wavelengths. A plurality of
13 gratings 18 comprising a single sensing device may be placed on
14 separate optical fibers.

15 Referring now to FIG. 4, while it is preferred to use a
16 plurality of optical fibers 12 in the sensor 10, it is possible
17 to replace the plurality of optical fibers 12 by a single
18 optical fiber 12' having a serpentine configuration in which
19 each of the legs 30, 32, and 34 of the optical fiber 12' has a
20 grating 18 incorporated therein.

21 In yet another alternative embodiment, the optic Bragg
22 gratings 18 may be replaced by fiber optic Bragg grating laser
23 sensors such as those described in U.S. Patent No. 5,513,913.
24 These are built into the optical fibers of the sensing device

1 10. Changes in the tension in each optical fiber 12 changes the
2 wavelength of the light emitted by each laser.

3 The device of the present invention offers several new and
4 distinct advantages. First, the sensing device 10 comprises a
5 means for fiber optic sensing of roll or pitch. Further, the
6 sensing device 10 of the present invention is simple and
7 potentially inexpensive. Still further, the sensing device 10
8 may be multiplexed with many other such sensors on a single
9 optical fiber.

10 It should be noted that the sensing device of the present
11 invention may use a wide number of optical fibers 12. It is
12 preferred that at least three optical fibers 12 are used in the
13 sensing device.

14 It should also be noted the shape of the mass 16 may vary
15 from that shown in the drawings. In such a situation, the
16 optical fibers 12 may just enclose the mass 16 as shown or may
17 be affixed to the mass 16.

18 The sensing device 10 of the present invention may be
19 oriented into a towed array in different ways to function as
20 either a roll or pitch sensor. Since the only deformable
21 structures in the sensing device 10 are the optical fibers 12,
22 sensitivity of the sensing device is maximized.

23 The sensing device 10 of the present invention may be used
24 in other applications requiring a roll or pitch sensor such as a

1 navigational system for an aircraft, a marine vessel, and the
2 like.

3 It is apparent that there has been provided in accordance
4 with the present invention a fiber optic motion sensor which
5 fully satisfies the objects, means, and advantages set forth
6 hereinbefore. While the present invention has been described in
7 the context of specific embodiments thereof, other alternatives,
8 modifications, and variations will become apparent to those
9 skilled in the art having read the foregoing description.

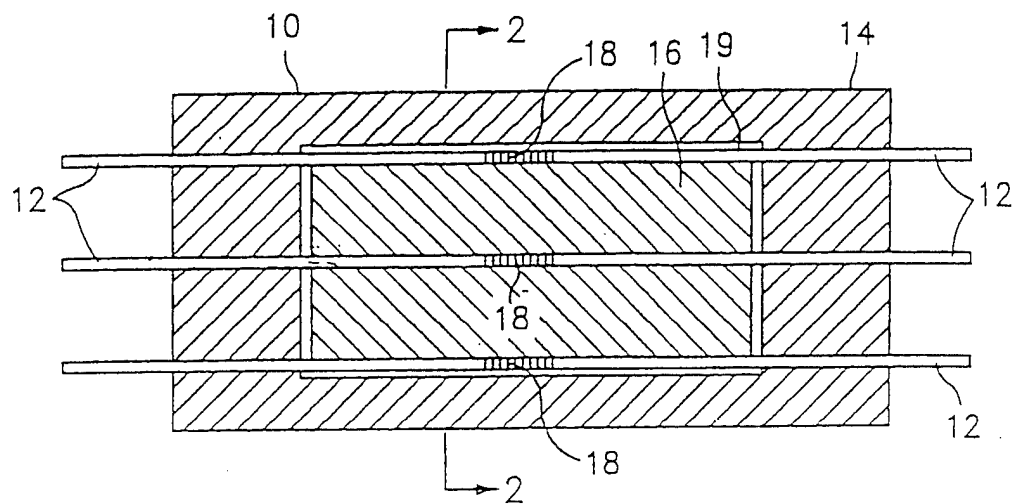


FIG. 1

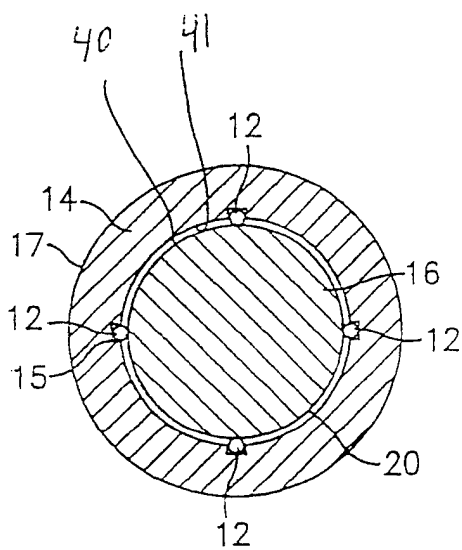


FIG. 2

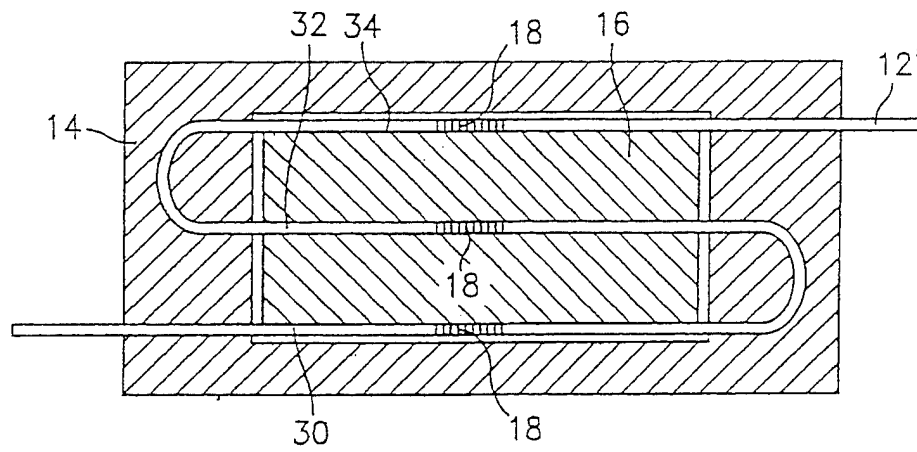


FIG. 3

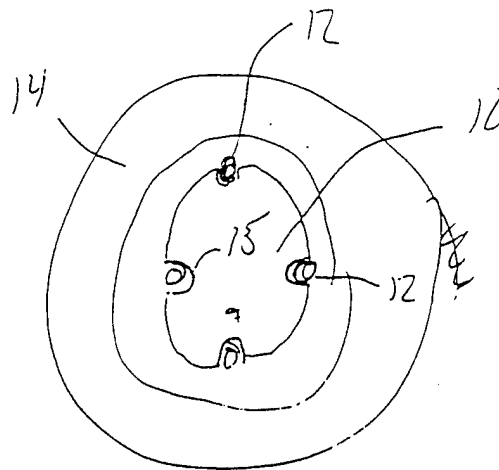


FIG. 4

1 Attorney Docket No. 78381

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3 FIBER OPTIC PITCH OR ROLL SENSOR

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5 ABSTRACT OF THE DISCLOSURE

6 The present invention relates to a fiber optic sensing
7 device having utility as a roll sensor and/or a pitch sensor.
8 The sensing device comprises at least one optical fiber
9 supported in a structure, a movable mass supported within the
10 structure, and at least one detector for detecting changes in
11 tension in the at least one optical fiber due to movement of the
12 movable mass. In the sensor of the present invention, the
13 optical fiber(s) are the only deformable structures, thus
14 maximizing sensitivity.



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