Attorney Docket No. 78333

15 Oct 2001

FIBER OPTIC CURVATURE SENSOR FOR TOWED HYDROPHONE ARRAYS

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT (1) GREGORY H. AMES, and (2) ANTONIO L. DEUS III, citizens of the United States of America, employees of the United States Government, and residents of (1) Wakefield, County of Washington, State of Rhode Island, (2) Saunderstown, County of Washington, State of Rhode Island, have invented certain new and useful improvements entitled as set forth above of which the following is a specification.

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IN REPLY REFER TO.

Attorney Docket No. 78333
Date: 18 March 2002

The below identified patent application is available for licensing. Requests for information should be addressed to:

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Serial Number	09/983,048
Filing Date	15 October 2001
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STATEMENT OF GOVERNMENT INTEREST

The invention described herein may be manufactured and used by or for the Government of the United States of America for governmental purposes without the payment of royalties thereon or therefore.

CROSS REFERENCE TO OTHER PATENT APPLICATIONS

This patent application is co-pending with two related patent applications entitled FIBER OPTIC PITCH OR ROLL SENSOR (Attorney Docket No. 78381) and MULTIPLEXED FIBER LASER SENSOR SYSTEM (Attorney Docket No. 78371), by the same inventors as this application.

BACKGROUND OF THE INVENTION

(1) Field of the Invention

The invention relates to a device and method for sensing the curvature of a towed array. The device of the present invention, in combination with other sensors, may be used to determine the shape of a towed hydrophone array.

(2) Description of the Prior Art

Optical fibers have been used in a variety of sensors. For example, U.S. Patent Nos. 4,654,520; 4,812,645; and 4,927,232, all to Griffiths, illustrate structural monitoring systems which have an optical fiber securely and continuously fastened to a structure such as a pipeline, offshore platform, bridge, building, or a dam or to a natural object. A light signal is passed into one end of the optical fiber. Any physical movement of the structure, or sectional movements along the optical fiber path, such as deflection, bending, displacement, or fracture of the structure affects the optical fiber. As a consequence, detectable changes occur in the electro-optical signature or in the light signal transmission.

U.S. Patent No. 5,321,257 to Danisch illustrates a fiber optic bending and positioning sensor which is composed of a fiber optic or light wave guide for attachment to the member which is to be bent or displaced. Light is injected at one end and detected at the other end. Bending of the fiber results in light loss through a surface strip or band, along one side of the fiber, this loss being detected. The loss of light detection is used to produce indication of bending or displacement. Two or more light guides can be oriented to give indication of the direction of bending or displacement.

One of the deficiencies of these systems however is that the optical fiber(s) used in the sensor is/are attached directly to the structure whose behavior is being observed.

Some towed hydrophone arrays require precise determination of their shape in the water. This has been done in the past with gimbaled heading sensors. Such sensors are quite expensive. They are unsuitable in today's environment where one needs to reduce cost in a towed array. It is also desirable in modern towed arrays to provide shape sensing that is compatible with optical hydrophones and that is relatively inexpensive to perform.

An alternative way to determine array shape is by curvature sensors and either roll or twist sensors. It has been proposed to use fiber optic sensors to sense curvature. Such sensors embed optical fibers containing Bragg gratings in the hose wall of the towed array. The Bragg gratings sense the strain in the hose wall when the array is bent and the differential strain from the outside to the inside of the bend permits calculation of the curvature. However, the strain seen in the hose wall as the array passes over small diameter handling sheaves can exceed the survival strain of an optical fiber. It has been suggested to reduce the strain seen by winding at a pitch angle, but that approach is awkward. It has also been suggested to reduce strain by minimizing the distance each fiber is placed from the centerline of the array. The disadvantage of all these mounting schemes is that while limiting the maximum strain seen, these schemes also limit the strain sensitivity achievable. One may define a total dynamic range of curvature from the maximum curvature of the handling system sheaves to the minimum curvature associated with the ultimate array position accuracy desired. This range may be 50 dB. Meanwhile, the sensor system actually only has to operate in towing conditions where the range of curvatures seen may be less than 30 dB.

Thus, there remains a need for a system which senses the curvature of a towed array as well as the shape of the towed array.

SUMMARY OF THE INVENTION

Accordingly, it is an object of the present invention to provide a sensor system which senses the curvature of a towed hydrophone array.

It is a further object of the present invention to provide a sensor system as above which can in combination with other sensors may be used to determine the shape of a towed hydrophone array.

It is yet a further object of the present invention to provide a sensor system as above which achieves high strain sensitivity while limiting the maximum strain seen by the optical fiber(s) therein so that only the operational dynamic range is required of the optical fiber(s).

The foregoing objects are attained by the curvature sensor of the present invention.

In accordance with the present invention, a curvature sensor is provided. The curvature sensor broadly comprises a bend member which bends as the array into which it is incorporated bends, at least one optical fiber within the bend member, and at least one detection device embedded within the at least one optical fiber to detect a change in strain in the at least one optical fiber.

A system for detecting the curvature in a towed hydrophone array comprises at least two of said curvature sensors positioned along the length of the array.

A system for also detecting the shape of the towed array includes a roll sensor positioned adjacent each of the curvature sensors.

Other details of the fiber optic curvature sensor of the present invention and the systems into which it can be incorporated, as well as other objects and advantages attendant thereto, are set forth in the following detailed description and the accompanying drawings wherein like reference numerals depict like elements.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic representation of a system for sensing the curvature of a towed array and the shape of the towed array;

FIG. 2 is a sectional view showing a first embodiment of a curvature sensor in accordance with the present invention;

FIG. 3 is a sectional view showing a second embodiment of a curvature sensor in accordance with the present invention;

FIG. 4 is a perspective view of a third embodiment of a curvature sensor in accordance with the present invention; and

FIG. 5 is a sectional view of a fourth embodiment of a curvature sensor in accordance with the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENT(S)

Referring now to the drawings, FIG. 1 illustrates a system 10 for sensing the curvature and shape of a towed array. Instead of a continuous optical fiber embedded into the hose wall of the array, the system 10 has a plurality of single point curvature sensors 12 placed at various locations along the length of the towed hydrophone array 14. As depicted in FIG. 1, the curvature sensors 12 may be placed quite far apart because of the long transverse wavelengths of the tow cables under tow. As a result, the system 10 requires fewer curvature sensors 12. The system 10 further has a plurality of roll sensors 16 with each roll sensor 16 being in close proximity to each curvature sensor 12 so that the direction of curvature relative to the surrounding environment may be determined. Because the curvature sensors 12 are single point sensors, the optical fiber(s) 18 that lead to and from each curvature sensor 12 may be separated from the structure of the towed hydrophone array 14 so that the optical fiber(s) 18 do not see excessive strain as the towed hydrophone array 14 is bent over small diameter handling sheaves. The curvature sensors 12 of the present invention are shorter than the minimum rigid length requirement associated with the towed hydrophone array 14 and the handling system (not shown).

The roll sensors 16 used in the system 10 may comprise any suitable roll sensor known in the art. However, in a preferred embodiment, each roll sensor 16 comprises the motion sensor shown in copending U.S. Patent Application Serial No. , filed , entitled FIBER OPTIC PITCH OR ROLL SENSOR which is incorporated by reference herein. Together with the curvature sensors 12, the roll sensors 16 may be used in a known manner to determine the shape of the towed hydrophone array 14.

Figure 2 illustrates a first embodiment of a curvature sensor 12 in accordance with the present invention. The curvature sensor 12 in this embodiment has a plurality of optical fibers 18, preferably three or four optical fibers 18, embedded in a bend rod 20. Each of the optical fibers 18 runs longitudinally down the length of the bend rod 20. The optical fibers 18 are radially distributed around the perimeter of the bend rod 20. The diameter of the bend rod 20 and the diameter of the optical fiber centers are determined by the strain sensing requirements.

The separation of the optical fibers 18 acts as a lever arm multiplying the strain differences seen by the optical fibers 18. When the bend rod 20 is bent, the optical fiber 18 on the inside of the bend experiences compression, while the optical fiber 18 on the outside of the bend experiences stretching. The magnitude and sign of the strain difference between the two optical fibers 18 gives the magnitude and sign of the curvature of the array 14 at the point where the curvature sensor 12 is placed.

The strain in each optical fiber 18 is preferably sensed by embedding or incorporating a detection device 22 within each of the optical fibers 18 in the bend rod 20. The detection device may be an optical fiber Bragg grating written into the core of the optical fiber 18. The changing strain in the optical fiber 18 results in a wavelength shift of the reflectivity peak of the Bragg grating 18. Such a wavelength shift may then be measured by any of a number of conventional means known in the art. The difference in wavelength shift determines the difference in the strain in a particular optical fiber 18. By comparing the outputs of the Bragg gratings embedded in the optical fibers, one can determine the curvature of the array at the location of the curvature sensor 12.

In lieu of incorporating an optical fiber Bragg grating into each optical fiber 18, an optical fiber Bragg grating laser, such as that shown in U.S. Patent Nos. 4,761,073 and 5,513,913, which are hereby incorporated by reference, may be embedded into each optical fiber 18. Changes in the strain in a respective optical fiber 18 causes changes in the wavelength of the light emitted by the optical fiber Bragg grating laser, which changes can be measured by a number of means well known in the art. By comparing the light emitted by the lasers incorporated into the optical fibers 18, one can determine the curvature of the array 14 where the curvature sensor 12 is located.

The bend rod 20 is less than the maximum rigid length for the array 14 and its handling system (not shown). The ends 24 and 26 of the bend rod 20 may be coupled by any of a variety of means known in the art to the array structure so that the bending of the array 14 results in the bending of the bend rod 20. For example, rigid pieces 28 may be used to couple the ends 24 and 26 of the bend rod 20 to the hose wall 30 of the array 14.

The bend rod 20 is preferably placed within a mount assembly 32 which may be mounted in the array 14 by any of a number of mounting techniques with the specific mounting technique being determined by the construction of the array 14. For example, the array 14 may have internal stringers 34 and the mount assembly 32 may be mounted on the stringers 34. The inner diameter of the mount assembly 32 preferably is greater than but close to the outer diameter of the bend rod 20. The gap 36 between the outer surface 37 of the bend rod 20 and the inner surface 39 of the mount assembly 32 is selected so that, at a certain maximum curvature, the bending of the bend rod 20 is limited by the mount assembly 32 and so that the optical fibers 18 and the detection devices 22 within the bend rod 20 experience no further strain at smaller bend diameters. This maximum operational curvature is set so that each of the curvature sensors 12 will sense across the entire range of curvatures encountered during actual towing, but the maximum operational curvature is much less than the curvature seen in the handling system. This limitation allows the optical fibers 18 in the bend rod 20 to be placed further apart and still survive, leading to greater strain sensitivity for the system. This limitation also limits how far in wavelength the detection devices 22, such as the gratings or lasers, shift.

If desired, in an alternative embodiment of the present invention, a number of different detection devices 22 can be placed on each optical fiber 18. The detection devices 22 placed on each optical fiber 18 can be operated at different wavelengths if desired. With a smaller wavelength shift range, these wavelengths can be spaced more closely, allowing more detection devices per optical fiber.

Referring now to FIG. 3, a curvature sensor 12 is shown that replaces the plurality of optical fibers 18 positioned within the bend rod 20 with a single optical fiber 18'. As can be seen in this figure, the optical fiber 18' has a serpentine configuration with legs 40, 42, and 44. Incorporated into each of the legs 40, 42, and 44 is a detection device 22. As before the detection device 22 in each leg 40, 42, and 44 can be an optical fiber Bragg grating or an optical fiber Bragg grating laser. As the array 14 is bent, the leg closest to the bend will experience compression while the leg farthest from the bend will experience an increased strain. Again, by measuring the changes in wavelengths in the detection devices 22, one can determine the change in curvature of the array 14. One of the advantages to this embodiment is that by including a plurality of detection devices 22 in a single optical fiber 18, less splices are required to connect the curvature sensor 12 into a system.

FIG. 4 illustrates a modified mounting assembly 46 for a curvature sensor 12. The mounting assembly 46 is a cylindrical structure 47 designed to leave the center 48 of the array 14 free. The cylindrical structure 47 has an off axis slot 49. As can be seen from this figure, the bend rod 20 with the optical fibers 18 is positioned off axis in the slot 49. This leaves the center 48 free for some other use. This mounting assembly 46 configuration does however reduce the distance that can be achieved between the optical fibers 18 in the bend rod 20.

Referring now to FIG. 5, an embodiment of a curvature sensor 12 is shown which replaces the bend rod 20 by a hollow bend cylinder 50 with embedded optical fibers 18 having embedded detecting devices 22. As before the detection devices 22 may be an optical fiber Bragg grating or an optical fiber Bragg grating laser. In this embodiment, the mount assembly 52 is located on the inside of the cylinder 50. The outer diameter of the mount assembly 52 is designed to be tight fitting to the inner diameter of the bend cylinder 50 so that the maximum bend of the optical fibers 18 is limited. This embodiment allows the optical fibers 18 with the detection devices 22 embedded therein to be placed further apart, thus giving greater curvature sensitivity in the same array diameter.

As can be seen from the foregoing discussion, the present invention provides a means for fiber optic sensing of the curvature of a towed array. The sensing means is simple and relatively inexpensive. If desired, the curvature sensor of the present invention may be multiplexed with many other such sensors on a single optical fiber.

The dynamic range of the curvature sensors 12 of the present invention is limited so that it just meets the requirements of the system. This allows the curvature sensor 12 to be designed for maximum sensitivity without risk to the fiber during small diameter bending in the handling system. This also allows different wavelength channels to be spaced more closely, leading to more curvature sensors on each optical fiber.

While the curvature sensors of the present invention have been described as having one, three or four optical fibers, it should be recognized that more than four fibers can be used in each sensor if desired.

It is apparent that there has been provided in accordance with the present invention a fiber optic curvature sensor for towed hydrophone arrays which fully satisfies the objects, means and advantages set forth hereinbefore. While the present invention has been described in the context of specific embodiments thereof, other alternatives, modifications, and variations will become apparent to those skilled in the art having read the foregoing description. Therefore, it is intended to embrace those alternatives, modifications, and variations that fall within the broad scope of the appended claims.

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ABSTRACT OF THE DISCLOSURE

The present invention relates to a system for sensing the curvature of a towed hydrophone array and a curvature sensor used in the system. The system has at least two curvature sensors positioned along the length of the array. Each of the curvature sensors comprises a bend member which bends as the array bends, at least one optical fiber within the bend member, and at least one detection device embedded within the at least one optical fiber to detect a change in the strain in the at least one optical fiber.

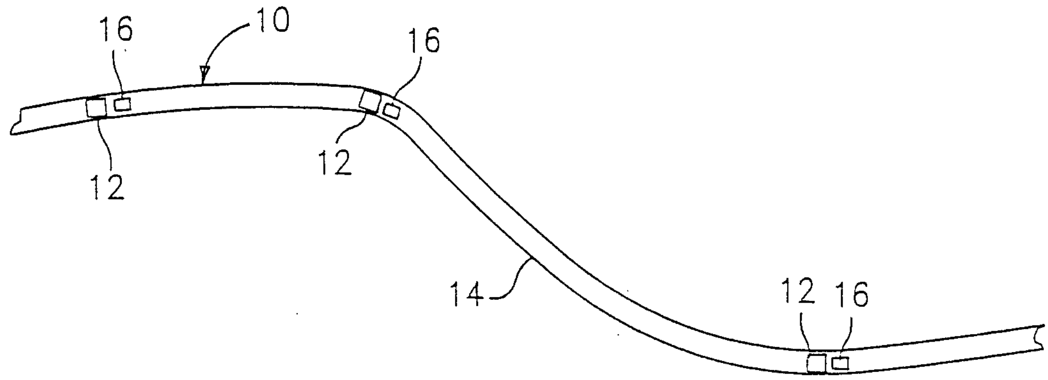
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FIG. 1

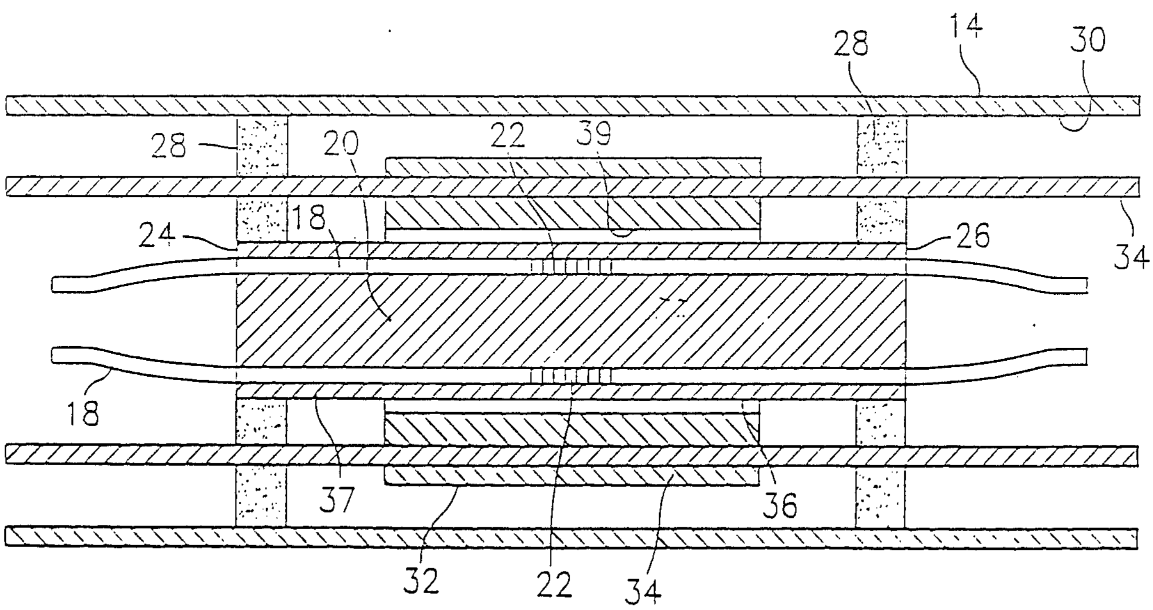
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FIG. 2

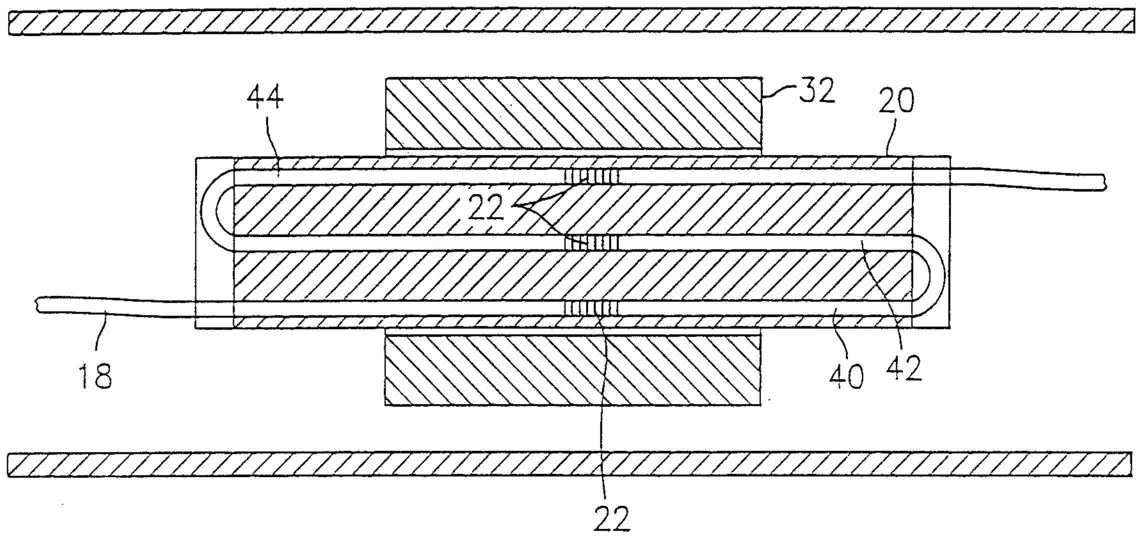

FIG. 3

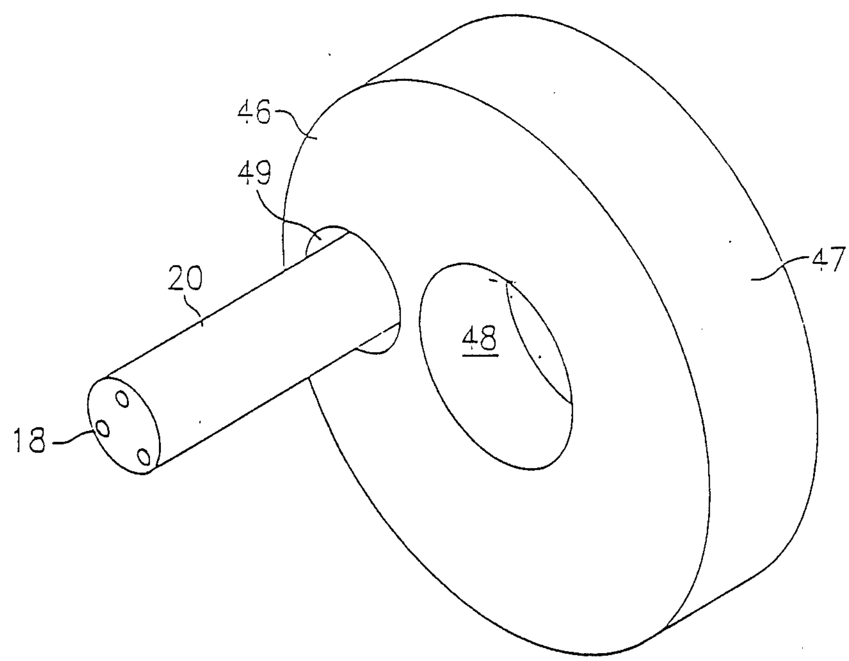

FIG. 4

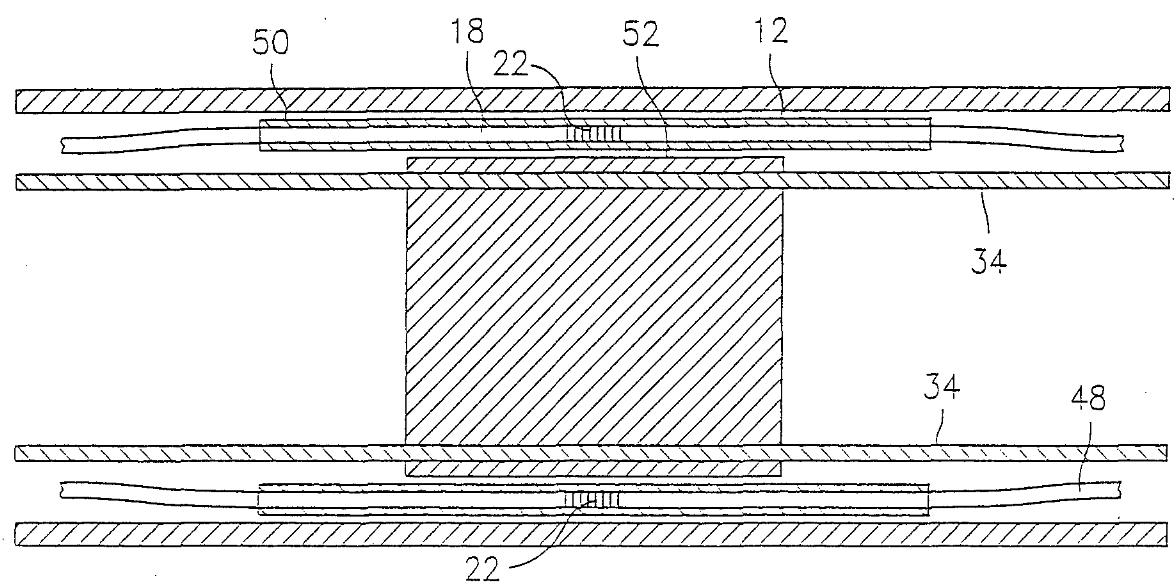

FIG. 5